WIND-TUNNEL STUDY OF MILLION DOLLAR PIER, ATLANTIC CITY

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LIST OF SYMBOLS

Symbol	Definition
U	Local mean velocity
D	Characteristic dimension (building height, width, etc.)
ν, ρ	Kinematic viscosity and density of approach flow
$\frac{UD}{\nu}$	Reynolds number
E	Mean voltage
A, B, n	Constants
U_{rms}	Root-mean-square of fluctuating velocity
E_{rms}	Root-mean-square of fluctuating voltage
U_∞	Reference mean velocity outside the boundary layer
X, Y	Horizontal coordinates
Z	Height above surface
δ	Height of boundary layer
T_u	Turbulence intensity $\frac{U_{rms}}{U_\infty}$ or $\frac{U_{rms}}{U}$
$C_{p_{mean}}$	Mean pressure coefficient, $\frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{rms}}$	Root-mean-square pressure coefficient, $\frac{\left((p-p_\infty)-(p-p_\infty)_{mean}\right)_{rms}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{max}}$	Peak maximum pressure coefficient, $\frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$
$C_{p_{min}}$	Peak minimum pressure coefficient, $\frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$
$(\ )_{min}$	Minimum value during data record
$(\ )_{max}$	Maximum value during data record

Symbol	Definition
p	Fluctuating pressure at a pressure tap on the structure
p_∞	Static pressure in the wind tunnel above the model
F_x, F_y	Forces in X, Y direction
A_R	Reference Area
CF_X	Force coefficient, X direction, $\dfrac{F_x}{A_R\ 0.5\rho\ U_\infty^2}$
CF_Y	Force coefficient, Y direction, $\dfrac{F_y}{A_R\ 0.5\rho\ U_\infty^2}$

1. INTRODUCTION

1.1 General

A significant characteristic of modern building design is lighter cladding and more flexible frames. These features produce an increased vulnerability of glass and cladding to wind damage and result in larger deflections of the building frame. In addition, increased use of pedestrian plazas at the base of the buildings has brought about a need to consider the effects of wind and gustiness in the design of these areas.

The building geometry itself may increase or decrease wind loading on the structure. Wind forces may be modified by nearby structures which can produce beneficial shielding or adverse increases in loading. Overestimating loads results in uneconomical design; underestimating may result in cladding or window failures. Tall structures have historically produced unpleasant wind and turbulence conditions at their bases. The intensity and frequency of objectionable winds in pedestrian areas is influenced both by the structure shape and by the shape and position of adjacent structures.

Techniques have been developed for wind tunnel modeling of proposed structures which allow the prediction of wind pressures on cladding and windows, overall structural loading, and also wind velocities and gusts in pedestrian areas adjacent to the building. Information on sidewalk-level gustiness allows plaza areas to be protected by design changes before the structure is constructed. Accurate knowledge of the intensity and distribution of the pressures on the structure permits adequate but economical selection of cladding strength to meet selected maximum design winds and overall wind loads for the design of the frame for flexural control.

Modeling of the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in references (1), (2), and (3). In general, the requirements are that the model and prototype be geometrically similar, that the approach mean velocity at the building site have a vertical profile shape similar to the full-scale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal.

These criteria are satisfied by constructing a scale model of the structure and its surroundings and performing the wind tests in a wind tunnel specifically designed to model atmospheric boundary-layer flows. Reynolds number similarity requires that the quantity UD/ν be similar for model and prototype. Since ν, the kinematic viscosity of air, is identical for both, Reynolds numbers cannot be made precisely equal with reasonable wind velocities. To accomplish this the air velocity in the wind tunnel would have to be as large as the model scale factor times the prototype wind velocity, a velocity which would introduce unacceptable compressibility effects. However, for sufficiently high Reynolds numbers ($>2\times10^4$) the pressure coefficient at any location on the structure will be essentially constant for a large range of Reynolds numbers. Typical values encountered are 10^7-10^8 for the full-scale and 10^5-10^6 for the wind-tunnel model. In this range acceptable flow similarity is achieved without precise Reynolds number equality.

1.2 The Wind-Tunnel Test

The wind-engineering study is performed on a building or building group modeled at scales ranging from 1:150 to 1:400. The building model

is constructed of clear plastic fastened together with screws. The structure is modeled in detail to provide accurate flow patterns in the wind passing over the building surfaces. The building under test is often located in a surrounding where nearby buildings or terrain may provide beneficial shielding or adverse wind loading. To achieve similarity in wind effects the area surrounding the test building is also modeled. A flow visualization study is first made (smoke is used to make the air currents visible) to define overall flow patterns and identify regions where local flow features might cause difficulties in building curtain-wall design or produce pedestrian discomfort.

The test model, equipped with pressure taps (200 to 600 or more), is exposed to an appropriately modeled atmospheric wind in the wind tunnel and the fluctuating pressure at each tap measured electronically. The model, and the modeled area, are rotated 10 or 15 degrees and another set of data recorded for each pressure tap. Normally, 24 or 36 sets of data (360 degrees of turning) are taken; however, when flow visualization or recorded data indicate high pressure regions of small azimuthal extent, data is obtained in smaller azimuthal steps.

Data are recorded, analyzed and processed by an on-line computerized data-acquisition system. Pressure coefficients of several types are calculated by the computer for each reading on each piezometer tap and are printed in tabular form as computer readout. Using wind data applicable to the building site, representative wind velocities are selected for combination with measured pressures on the building model. Integration of test data with wind data results in prediction of peak local wind pressures for design of glass or cladding and may include overall forces and moments on the structure (by floor if desired) for design of

the structural frame. Pressure contours are drawn on the developed building surfaces showing the intensity and distribution of peak wind loads on the building. These results may be used to divide the building into zones where lighter or heavier cladding or glass may be desirable.

Based on the visualization (smoke) tests and on a knowledge of heavy pedestrian use areas, a dozen or more locations may be chosen at the base of the building where wind velocities can be measured to determine the relative comfort or discomfort of pedestrians in plaza areas, near building entrances, near building corners, or on sidewalks. Usually a reference pedestrian position is also tested to determine whether the wind environment in the building area is better or worse than the environment a block or so away in an undisturbed area.

The following pages discuss in greater detail the procedures followed and the equipment and data collecting and processing methods used. In addition, the data presentation format is explained and the implications of the data are discussed.

2. EXPERIMENTAL CONFIGURATION

2.1 Wind Tunnel

Wind-engineering studies are performed in the Fluid Dynamics and Diffusion Laboratory at Colorado State University (Figure 1). Three large wind tunnels are available for wind loading studies depending on the detailed requirements of the study. The wind tunnel used for this investigation is shown in Figure 2. All tunnels have a flexible roof adjustable in height to maintain a zero pressure gradient along the test section. The mean velocity can be adjusted continuously in each tunnel to the maximum velocity available.

2.2 Model

In order to obtain an accurate assessment of local pressures using piezometer taps, models are constructed to the largest scale that does not produce significant blockage in the wind-tunnel test section. The models are constructed of 1/2 in. thick Lucite plastic and fastened together with metal screws. Significant variations in the building surface, such as mullions, are machined into the plastic surface. Piezometer taps (1/16 in. diameter) are drilled normal to the exterior vertical surfaces in rows at several or more elevations between the bottom and top of the building. Similarly, taps are placed in the roof and on any sloping, protruding, or otherwise distinctive features of the building that might need investigation.

Pressure tap locations are chosen so that the entire surface of the building can be investigated for pressure loading and at the same time permit critical examination of areas where experience has shown that maximum wind effects may be expected to occur. Locations of the pressure taps for this study are shown in Figure 3. Dimensions are

given both for full-scale building (in ft) and for model (in in.). The pressure tap numbers are shown adjacent to the taps.

The pressure tests are sometimes made in two stages. In the first stage measurements are made on the initial distribution of pressure taps. If it becomes apparent from the data that the loading on the building is being influenced by some unsuspected geometry of the building or adjacent structures, additional pressure taps are installed in the critical areas. The locations of the taps are selected so that the maximum loading can be detected and the area over which this loading is acting can be defined. Any added taps are also shown in Figure 3.

A circular area 750 to 2000 ft in radius depending on model scale and characteristics of the surrounding buildings and terrain is modeled in detail. Structures within the modeled region are made from styrofoam and cut to the individual building geometries. They are mounted on the turntable in their proper locations. Significant terrain features are included as needed. The model is mounted on a turntable (Figure 2) near the downwind end of the test section. Any buildings or terrain features which do not fit on the turntable are placed on removable pieces which are placed upwind of the turntable for appropriate wind directions. A plan view of the building and its surroundings is shown in Figure 4. The turntable is calibrated to indicate azimuthal orientation to 0.1 degree.

The region upstream from the modeled area is covered with a randomized roughness constructed using various sized cubes placed on the floor of the wind tunnel. Different roughness sizes may be used for different wind directions. Spires are installed at the test-section entrance to provide a thicker boundary layer than would otherwise be

available. The thicker boundary layer permits a somewhat larger scale model than would otherwise be possible. The spires are approximately triangularly shaped pieces of 1/2 in. thick plywood 6 in. wide at the base and 1 in. wide at the top, extending from the floor to the top of the test section. They are placed so that the broad side intercepts the flow. A barrier approximately 8 in. high is placed on the test-section floor downstream of the spires to aid in development of the boundary-layer flow.

The distribution of the roughness cubes and the spires in the roughened area was designed to provide a boundary-layer thickness of approximately 4 ft, a velocity profile power-law exponent similar to that expected to occur in the region approaching the modeled area for each wind direction (a number of wind directions may have the same approach roughness). A photograph of the completed model in the wind tunnel is shown in Figure 5. The wind-tunnel ceiling is adjusted after placement of the model to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Making the air flow visible in the vicinity of the model is helpful (a) in understanding and interpreting mean and fluctuating pressures, (b) in defining zones of separated flow and reattachment and zones of vortex formation where pressure coefficients may be expected to be high and (c) in indicating areas where pedestrian discomfort may be a problem. Titanium tetrachloride smoke is released from sources on and near the model to make the flow lines visible to the eye and to make it possible to obtain motion picture records of the tests. Conclusions obtained from these smoke studies are discussed in Sections 4.1 and 5.1.

3.2 Pressures

Mean and fluctuating pressures are measured at each of the pressure taps on the model structure. Data are obtained for 24 or 36 wind directions, rotating the entire model assembly in a complete circle. Seventy-six pieces of 1/16 in. I.D. plastic tubing are used to connect 76 pressure ports at a time to an 80 tap pressure switch mounted inside the model. The switch was designed and fabricated in the Fluid Dynamics and Diffusion Laboratory to minimize the attenuation of pressure fluctuations across the switch. Each of the 76 measurement ports is directed in turn by the switch to one of four pressure transducers mounted close to the switch. The four pressure input taps not used for transmitting building surface pressures are connected to a common tube leading outside the wind tunnel. This arrangement provides both a means of performing in-place calibration of the transducers and, by connecting this tube to a pitot tube mounted inside the wind tunnel, a means of automatically monitoring the tunnel speed. The switch is operated by means of a shaft projecting through

the floor of the wind tunnel. A computer-controlled stepping motor steps the switch into each of the 20 required positions. The computer keeps track of switch position but a digital readout of position is provided at the wind tunnel.

The pressure transducers used are setra differential transducers (Model 237) with a 0.10 psid range. Reference pressures are obtained by connecting the reference sides of the four transducers, using plastic tubing, to the static side of a pitot-static tube mounted in the wind tunnel free stream above the model building. In this way the transducer measures the instantaneous difference between the local pressures on the surface of the building and the static pressure in the free stream above the model.

Output from the pressure transducers is fed to an on-line data acquisition system consisting of a Hewlett-Packard 21 MX computer, disk unit, card reader, printer, Digi-Data digital tape drive and a Preston Scientific analog-to-digital converter. The data are processed immediately into pressure coefficient form as described in Section 4.3 and stored for printout or further analysis.

All four transducers are recorded simultaneously for 16 seconds at a 250 sample per second rate. The results of an experiment to determine the length of record required to obtain stable mean and rms (root-mean-square) pressures and to determine the overall accuracy of the pressure data acquisition system is shown in Figure 6. A typical pressure port record was integrated for a number of different time periods to obtain the data shown. Examination of a large number of pressure taps showed that the overall accuracy for a 16 second period is, in pressure coefficient form, 0.03 for mean pressures, 0.1 for peak pressures, and 0.01 for rms pressures. Pressure coefficients are defined in Section 4.3.

3.3 Velocity

Mean velocity and turbulence intensity profiles are measured upstream of the model to determine that an approach boundary-layer flow appropriate to the site has been established. Tests are made at one wind velocity in the tunnel. This velocity is well above that required to produce Reynolds number similarity between the model and the prototype as discussed in Section 1.1.

In addition, mean velocity and turbulence intensity measurements are made 5 to 7 ft (prototype) above the surface at a dozen or more locations on and near the building for 16 wind directions. The measurement locations are shown on Figure 4. The surface measurements are indicative of the wind environment to which a pedestrian at the measurement location would be subjected. The locations are chosen to determine the degree of pedestrian comfort or discomfort at the building corners where relatively severe conditions frequently are found, near building entrances and on adjacent sidewalks where pedestrian traffic is heavy, and in open plaza areas. In most studies a reference pedestrian position, located about a block away, is also tested. These data are helpful in evaluating the degree of pedestrian comfort or discomfort in the proposed plaza area in terms of the undisturbed environment in the immediate vicinity.

Measurements are made with a single hot-wire anemometer mounted with its axis vertical. The instrumentation used is a Thermo Systems constant temperature anemometer (Model 1050) with a 0.001 in. diameter platinum film sensing element 0.020 in. long. Output is directed to the on-line data acquisition system for analysis.

Calibration of the hot-wire anemometer is performed by comparing output with the pitot-static tube in the wind tunnel. The calibration

data are fit to a variable exponent King's Law relationship of the form

$$E^2 = A + BU^n$$

where E is the hot-wire output voltage, U the velocity and A, B, and n are coefficients selected to fit the data. The above relationship was used to determine the mean velocity at measurement points using the measured mean voltage. The fluctuating velocity in the form U_{rms} (root-mean-square velocity) was obtained from

$$U_{rms} = \frac{2\ E\ E_{rms}}{B\ n\ U^{n-1}}$$

where E_{rms} is the root-mean-square voltage output from the anemometer. For interpretation all turbulence measurements for pedestrian winds were divided by the mean velocity outside the boundary-layer U_∞. Turbulence intensity in velocity profile measurements used the local mean velocity.

4. RESULTS

4.1 Flow Visualization

A film is included as part of this report showing the characteristics of flow about the structure using smoke to make the flow visible. A listing of the contents of the film is shown in Table 1. Several features can be noted from the visualization. As with all large structures, wind approaching the building is deflected down to the plaza level, up over the structure and around the sides. A description of the smoke test results emphasizing flow patterns of concern relative to possible high-wind load areas and pedestrian comfort is given in Section 5.1.

4.2 Velocity

Velocity and turbulence profiles are shown in Figure 7. Profiles were taken upstream from the model which are characteristic of the boundary layer approaching the model and sometimes at the building site with building removed. The boundary-layer thickness, δ, is shown in Figure 7. The corresponding prototype value of δ for this study is also shown in the figure. This value was established as a reasonable height for this study. The mean velocity profile approaching the modeled area has the form

$$\frac{U}{U_\infty} = \left(\frac{z}{\delta}\right)^n .$$

The exponent n for the approach flow established for this study is shown in Figure 7.

Profiles of longitudinal turbulence intensity in the flow approaching the modeled area are shown in Figure 7. The turbulence intensities are appropriate for the approach mean velocity profile selected. For the velocity profiles, turbulence intensity is defined

as the root-mean-square about the mean of the longitudinal velocity fluctuations divided by the local mean velocity U,

$$Tu = \frac{U_{rms}}{U} .$$

Velocity data obtained at each of the pedestrian measurement locations shown in Figure 4 are listed in Table 2 as mean velocity U/U_∞, turbulence intensity U_{rms}/U_∞, and largest effective gust

$$U_{pk} = \frac{U + 3U_{rms}}{U_\infty}$$

These data are plotted in polar form in Figure 8. Measurements were taken 5 to 7 ft above the ground surface. A site map is superimposed on the polar plots to aid in visualization of the effects of the nearby structures on the velocity and turbulence magnitudes. An analysis of these wind data is given in Section 5.2.

To enable a quantitative assessment of the wind environment, the wind-tunnel data were combined with wind frequency and direction information obtained at the local airport. Table 3 shows wind frequency by direction and magnitude obtained from summaries published by the National Weather Service. These data, usually obtained at an elevation of about 30-40 ft, were converted to velocities at the reference velocity height for the wind-tunnel measurements and combined with the wind-tunnel data to obtain cumulative probability distributions (percent time a given velocity is exceeded) for wind velocity at each measuring location. The percentage times were summed by wind direction to obtain a percent time exceeded at each measuring position independent of wind direction (but accounting for the fact that the wind blows from different directions with varying frequency). These results are plotted in Figure 9.

Interpretation of Figure 9 is aided by a description of the effects of wind of various magnitudes on people. The earliest quantitative description of wind effects was established by Sir Francis Beaufort in 1806 for use at sea and is still in use today. Several recent investigators have added to the knowledge of wind effects on pedestrians. These investigations along with suggested criteria for acceptance have been summarized by Penwarden and Wise (4) and Melbourne (5). The Beaufort scale (from ref. 4), based on mean velocity only, is reproduced as Table 4 including qualitative descriptions of wind effects. Table 4 suggests that mean wind speeds below 12 mph are of minor concern and that mean speeds above 24 mph are definitely inconvenient. Quantitative criteria for acceptance from reference 5 are superimposed as dashed lines on Figure 9. The peak gust curves shown in Figure 9 are the percent of time during which a short gust of the stated magnitude could occur (say about one of these gusts per hour). Implications of the data plotted in Figure 9 are presented in Section 5.2

Because some pedestrian wind measuring positions are purposely chosen at sites where the smoke tests showed large velocities of small spacial extent, the general wind environment about the structure may be less severe than one might infer from a strict analysis of Table 2 and Figure 9.

4.3 Pressures

For each of the pressure taps examined at each wind direction, the data record is analyzed to obtain four separate pressure coefficients. The first is the mean pressure coefficient

$$C_{p_{mean}} = \frac{(p-p_\infty)_{mean}}{0.5\ \rho\ U_\infty^2}$$

where the symbols are as defined in the List of Symbols. It represents the mean of the instantaneous pressure difference between the building pressure tap and the static pressure in the wind tunnel above the building model, nondimensionalized by the dynamic pressure

$$0.5\ \rho\ U_\infty^2$$

at the reference velocity position. This relationship produces a dimensionless coefficient which indicates that the mean pressure difference between building and ambient wind at a given point on the structure is some fraction less or some fraction greater than the undisturbed wind dynamic pressure near the upper edge of the boundary layer. Using the measured coefficient, prototype mean pressure values for any wind velocity may be calculated.

The magnitude of the fluctuating pressure is obtained by the rms pressure coefficient

$$C_{p_{rms}} = \frac{\left((p-p_\infty) - (p-p_\infty)_{mean}\right)_{rms}}{0.5\ \rho\ U_\infty^2}$$

in which the numerator is the root-mean-square of the instantaneous pressure difference about the mean .

If the pressure fluctuations followed a Gaussian probability distribution, no additional data would be required to predict the

frequency with which any given pressure level would be observed. However, the pressure fluctuations do not, in general, follow a Gaussian probability distribution so that additional information is required to show the extreme values of pressure expected. The peak maximum and peak minimum pressure coefficients are used to determine these values:

$$C_{p_{max}} = \frac{(p-p_\infty)_{max}}{0.5\ \rho\ U_\infty^2}$$

$$C_{p_{min}} = \frac{(p-p_\infty)_{min}}{0.5\ \rho\ U_\infty^2}$$

The values of $p-p_\infty$ which were digitized at 250 samples per second for 16 seconds, representing about one hour of time in the full-scale, are examined individually by the computer to obtain the most positive and most negative values during the 16-second period. These are converted to $C_{p_{max}}$ and $C_{p_{min}}$ by nondimensionalizing with the free stream dynamic pressure.

The four pressure coefficients are calculated by the on-line data acquisition system computer and tabulated along with the approach wind azimuth in degrees from true north. The list of coefficients is included as Appendix A. The pressure tap code numbers used in the appendix are explained in Figure 3.

To determine the largest peak loads acting at any point on the structure for cladding design purposes, the pressure coefficients for all wind directions were searched to obtain, at each pressure tap, the largest absolute value of peak pressure coefficient. Table 6 provides these pressure coefficients and associated wind directions. Included in Section 5.3 is an analysis of the coefficients of Table 6 including the maximum values obtained and where they occurred on the building.

The pressure coefficients of Table 6 can be converted to full-scale loads by multiplication by a suitable reference pressure selected for the field site. This reference pressure is represented in the equations for pressure coefficients by the $0.5\ \rho\ U_\infty^2$ denominator. This value is the dynamic pressure associated with an hourly mean wind at the reference velocity measurement position at the edge of the boundary layer. In general, the method of arriving at a design reference pressure for a particular site involves selection of a design wind velocity, translation of the velocity to an hourly mean wind at the reference velocity location and conversion to a reference pressure. Selection of the design velocity can be made from statistical analysis of extreme wind data or selected from wind maps contained in the proposed wind loading code ANSI A58.1 of the American National Standards Institute (6). The calculation of reference pressure for this study is shown in Table 5. The factor used in Table 5 to reduce gust winds to hourly mean winds is given in reference (7).

The reference pressure associated with the design hourly mean velocity at the reference velocity location can be used directly with the peak-pressure coefficients to obtain peak local design wind loads for cladding design. Local, instantaneous peak loads on the full-scale building suitable for cladding design were computed by multiplying the reference pressure of Table 5 by the peak coefficients of Table 6 and are listed as peak pressures in that table. The maximum psf load given at each tap location is the absolute value of the maximum value found in the tests, irrespective of its algebraic sign. For ease in visualizing the loads on the structure, contours of equal peak pressures for cladding load shown in Table 6 have been plotted on developed elevation

views of the structure, Figure 10. For control of water infiltration from outside to inside, the largest positive (inward-acting) pressure at each tap location is tabulated in Table 6.

For glass design pressures, a glass load factor is used to account for the different duration between measured peak pressures and the one minute loading commonly used in glass design charts. The design pressure used for glass is normally less than the peak pressures used for cladding design because of the static fatigue property of glass which can withstand higher pressures for short duration loads than for long duration loads. Recent research (8) indicates that the period of application of the peak pressures reported herein is about 5-10 seconds or less. If a glass design is based on these peak-pressure values, then a glass strength associated with this duration load should be used. Because glass design charts are normally based on some alternate load duration--usually one minute--then some reduction in peak loads should be made. An estimate of a load reduction factor can be obtained from an empirical relation of glass strength as a function of load duration. Current glass selection charts showing glass strength as a function of load duration (9) and older references (10) indicate the following load reduction factors:

	ref 9	ref 10
annealed float	0.80	0.81
heat strengthened	0.94	
tempered	0.97	0.98

Loadings appropriate for glass design can be computed by multiplying the peak-pressure loads of Table 6 by these load factors.

4.4 Forces and Moments

Force coefficients in the horizontal X and Y directions and moment coefficients about the X, Y, and Z axes with the origin at ground level at the base of the building with Z axis vertical may be computed for all wind directions tested by integration of mean pressures on the building. Overall forces and moments acting on the full-scale building due to wind loading which are useful in designing the structural framing of the proposed building may be obtained from use of these coefficients.

Force coefficients were computed for each floor for each wind direction using the equations shown below.

$$CF_X = \frac{F_X}{A_R \; 0.5 \; \rho \; U_\infty^2} \qquad CF_Y = \frac{F_Y}{A_R \; 0.5 \; \rho \; U_\infty^2}$$

Terms and symbols used in the equations are defined in the List of Symbols and the axes are defined for the building in Figure 3. Force coefficients CF_X and CF_Y were computed for the horizontal forces acting along the X and Y axes using the mean pressure coefficient at each pressure tap. A_R represents a constant reference area for nondimensionalization of the forces and moments.

The total forces acting on the full-scale building for each floor and wind direction were computed by multiplying the above coefficients by the appropriate full-scale reference area, by the reference pressure of Table 5, and by a gust load factor selected for an appropriate wind gust duration. The gust load factor, shown in Table 5, was selected to increase the loads from an hourly mean load to that of a gust whose duration would be sufficient for its effect to be fully felt by the structure. A table of gust load factors for various gust durations is

incorporated in Table 5 so that force and moment data of Table 7 may be adjusted to a different load duration if desired.

The forces obtained at each floor were used to obtain load, shear, and moment diagrams for the building for each wind direction. The shear diagram, in kips, was obtained by algebraic sum of all forces in each coordinate direction acting above the floor of interest. The load diagram, in psf, was obtained by dividing the shear values by their contributing areas (listed in Table 7). The moment diagram, in 1000 ft-kips, was obtained by integration of the shear values so that the moment due to forces acting above the floor level of interest was calculated. The sign of the moment was established by the right-hand rule about an X', Y' axis through the floor of interest. Moments about the Z axis were calculated by considering the displacement of forces in the X and Y directions from the Z axis shown in Figure 3.

5. DISCUSSION

5.1 Flow Visualization

Flow patterns identified with smoke showed that flow passed both over and under the Pier. No flow patterns were identified whose characteristics would indicate large local pressures. Smoke flow in pedestrian areas showed that deck areas exposed to onshore winds would experience somewhat higher wind velocities than nearby beach areas--primarily because the increased elevation of the decks provided exposure to higher velocity winds. Some acceleration of flow which could be due to the Pier geometry was observed in exposed areas, but small local accelerations were difficult to detect with smoke flow.

5.2 Pedestrian Winds

Figure 4 shows the 54 locations selected for investigation of pedestrian wind comfort. Locations 1 and 2 were selected as reference locations on the beach and Boardwalk which should be reasonably undisturbed by presence of the Million Dollar Pier. Table 2 and Figure 8 show that the largest values of mean velocity were measured at locations 14, 22, 32, 35 and 42 with values ranging from 77 to 83 percent of U_∞, the mean velocity at the boundary-layer height. The winds approaching the Pier over water at the elevations of these pedestrian locations were 60 to 65 percent of U_∞ so that some acceleration of wind was due to the Pier itself. For comparison, the largest mean velocities at reference locations 1 and 2 on the beach and Boardwalk were 48 and 51 percent respectively.

The largest values of fluctuating velocity, U_{rms}, were measured at locations 20, 32, 42 and 47 with values ranging from 22 to 28 percent of U_∞. For comparison, maximum values measured at reference locations 1

and 2 were 13 and 15 percent respectively. The largest values of peak gust, represented by the mean plus three rms as discussed in Section 4.2, were measured at locations 21, 22, 32, 35 and 47 with values ranging from 122 to 152 percent of U_∞. For comparison, the largest values measured at reference locations 1 and 2 were 87 and 90 percent of U_∞.

Velocity data of Table 2 integrated with local wind data tabulated in Table 3 are shown in Figure 9. Based on the data of this figure, the windiest locations will be 22 and 32 at the top of the staircases at the south end of the Pier which should be unacceptably windy 25 to 40 percent of the time for mean winds. Locations 3 and 34 should be unacceptably windy 10 percent or more of the time. These data should be interpreted in light of data at reference locations 1 and 2 which, according to Figure 9, are under the unacceptable bounds but above the walking comfort criteria. The beaches at Atlantic City are obviously used in a way that indicates an environment more acceptable than would be anticipated by location 1 in Figure 9; two possibilities exist. The most likely one is that a somewhat windy environment is expected by beach users effectively raising the level of the acceptability criteria lines on Figure 9. The second possibility, less likely, is that errors exist in the meteorological data record for Atlantic City published by the National Weather Service. In either case, a reasonable guide would be to use the reference location 1 curve in Figure 9 as a generally acceptable condition and to examine windier locations using that location as a guide. On that basis, the areas of most concern are locations 3, 22, and 32. Location 3 is of concern because it is substantially windier than location 1 and is in a high traffic area. Locations 22 and 32 are of concern because of their exposed location at the top of a staircase.

Locations 22 and 32 could be protected by enclosing the staircase or shielding the upper portions with a deflection device--a solid railing about 4 ft high might work. Location 3 represents a more difficult location to protect without major changes in the Pier geometry since it experiences winds from any particular direction only a little larger in magnitude than those at reference location 1.

Results of the pedestrian wind analysis showed that the Pier would have a substantial number of locations where winds would be rather high based on acceptability criteria published in the literature. Since the beach area away from the Pier also shows rather high winds, it is reasonable to use the adjacent beach area as a standard against which locations on the Pier can be measured and presuming the existing beach to be an acceptable environment. A substantial number of locations on the Pier decks will be windier than the beach area, in part because they are at a higher elevation where wind speeds are higher and in part because the Pier itself accelerates flow in local areas. Three locations are of particular concern because they are among the highest percentage of larger wind speeds and because they are either high-traffic areas or of safety concern--these areas are locations 3, 22 and 32 discussed above.

5.3 Pressures

Pressures were measured at 164 pressure taps located on one-half of the model. These data were applied by symmetry to the other half of the model resulting in effectively 328 locations on the entire Pier. Table 6 shows the largest peak pressure coefficients and corresponding loads measured on the building for each pressure tap location. Data identified as Configuration A in Table 6 and Appendix A represent data obtained at each tap location for 36 wind directions. Configuration B represents

data obtained at selected taps at 2-degree azimuthal increments near azimuths where large pressure peaks were observed in Configuration A to ensure that the largest peaks were obtained. The largest peak pressure coefficient measured on the building was -1.5 measured at taps 33 and 204. This coefficient value is not large for a building of this height. The peak pressure coefficient of -1.5 represents, using the 50-yr recurrence wind reference pressure of Table 5, peak cladding pressures of -59 psf. Figure 10 shows that peak pressures over most areas of the Million Dollar Pier were in the 20 to 40 psf range for the 50-yr recurrence wind.

Table 7 tabulates shear in the X and Y direction and moments about the Z axis as discussed in Section 4.4. Moments about the X and Y axis were not reported for this structure since these moments are sensitive to the distribution of deck pressures. An insufficient number of deck pressures were obtained to provide a useful estimate of X and Y moments.

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FIGURES

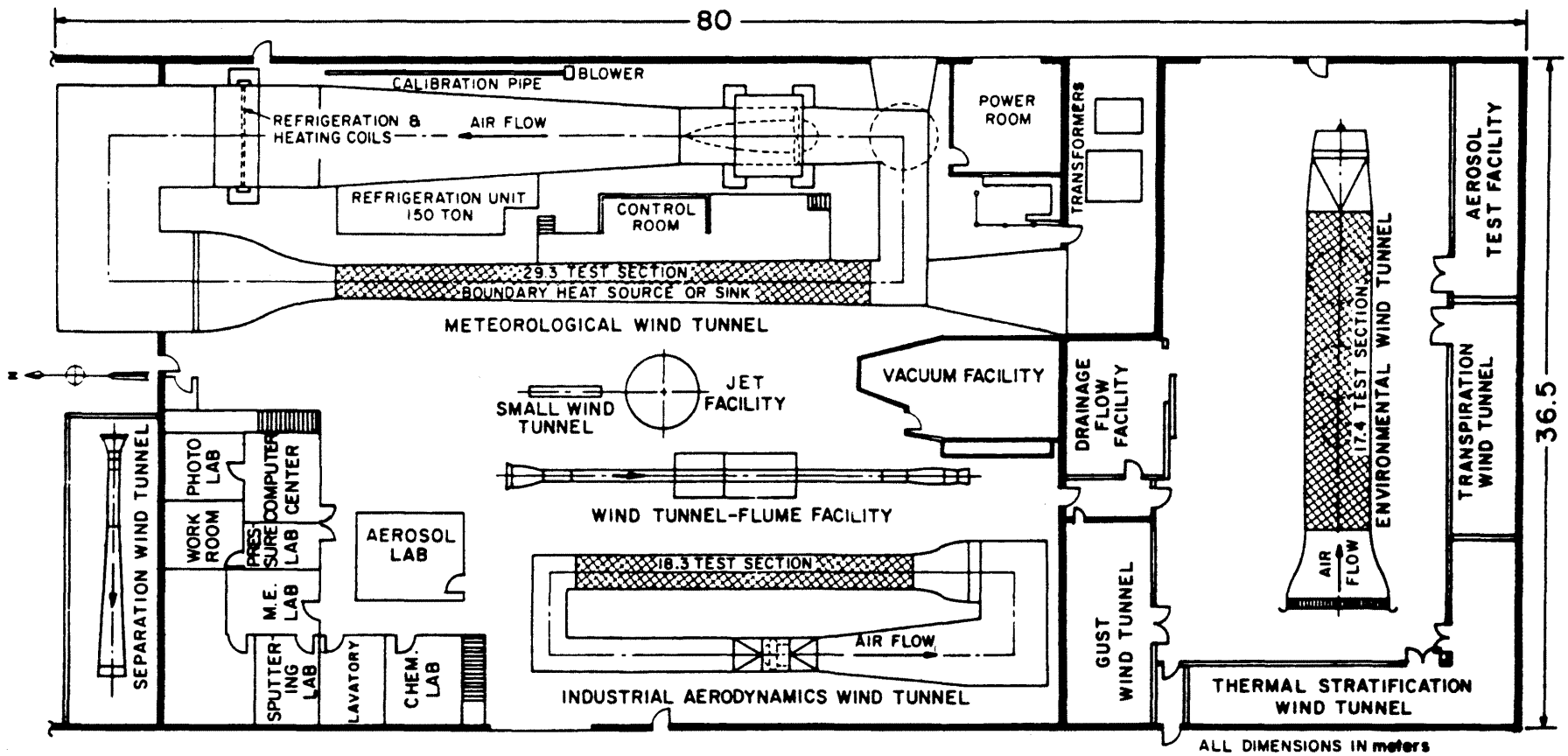
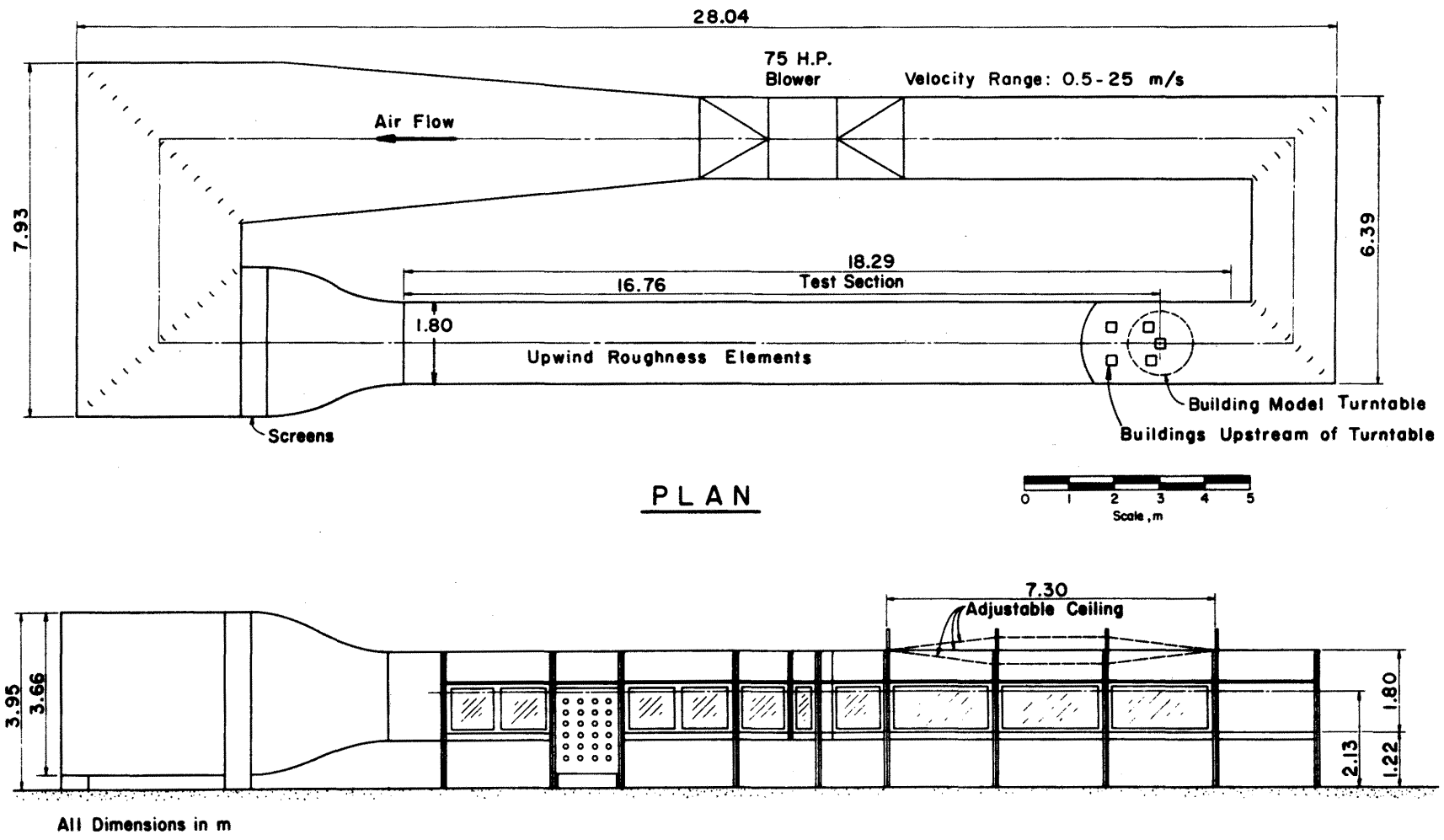


Figure 1. **FLUID DYNAMICS AND DIFFUSION LABORATORY COLORADO STATE UNIVERSITY**



INDUSTRIAL AERODYNAMICS WIND TUNNEL

Figure 2 - Wind Tunnel Configuration

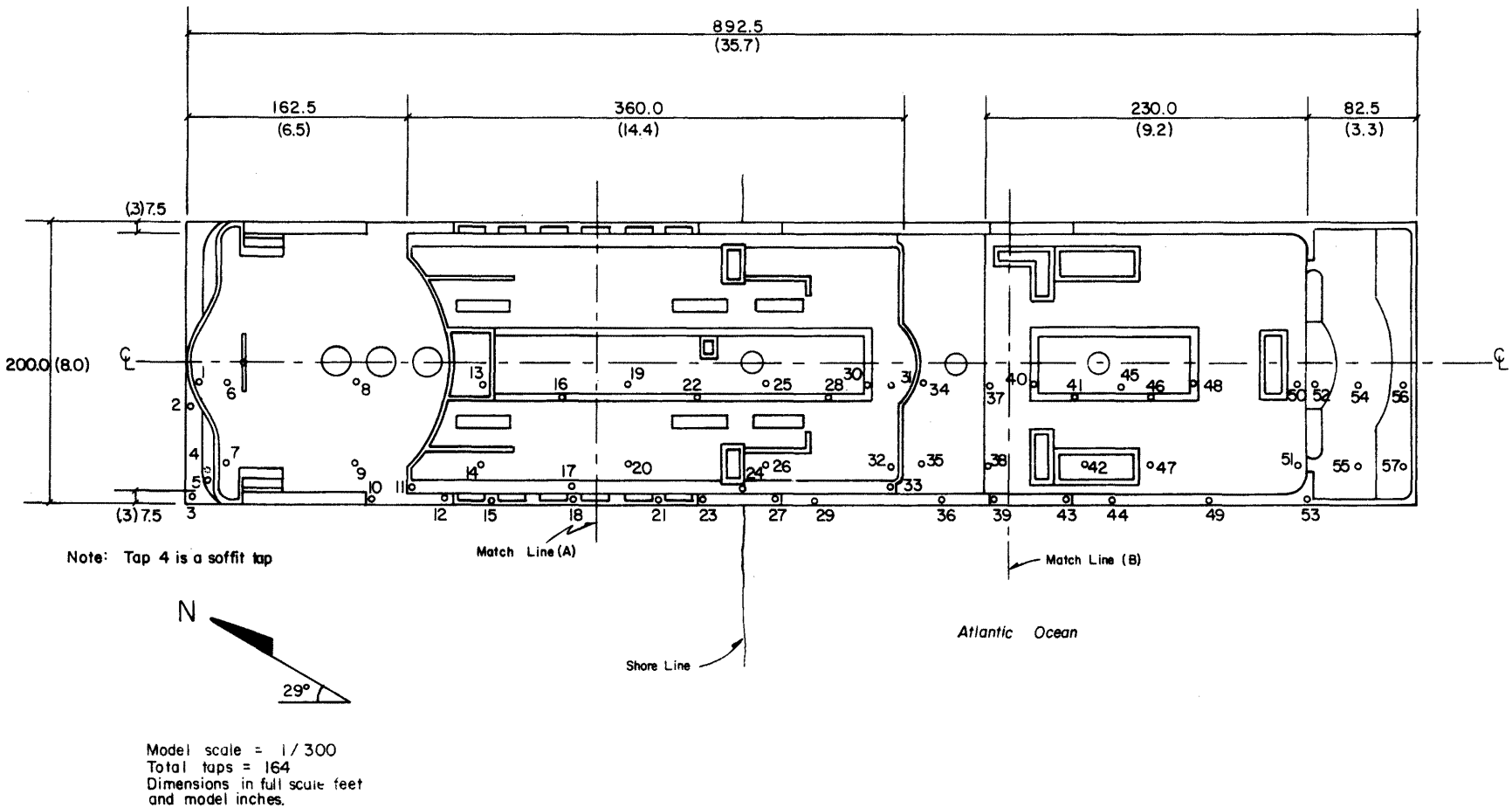


Figure 3a. Pressure Tap Locations

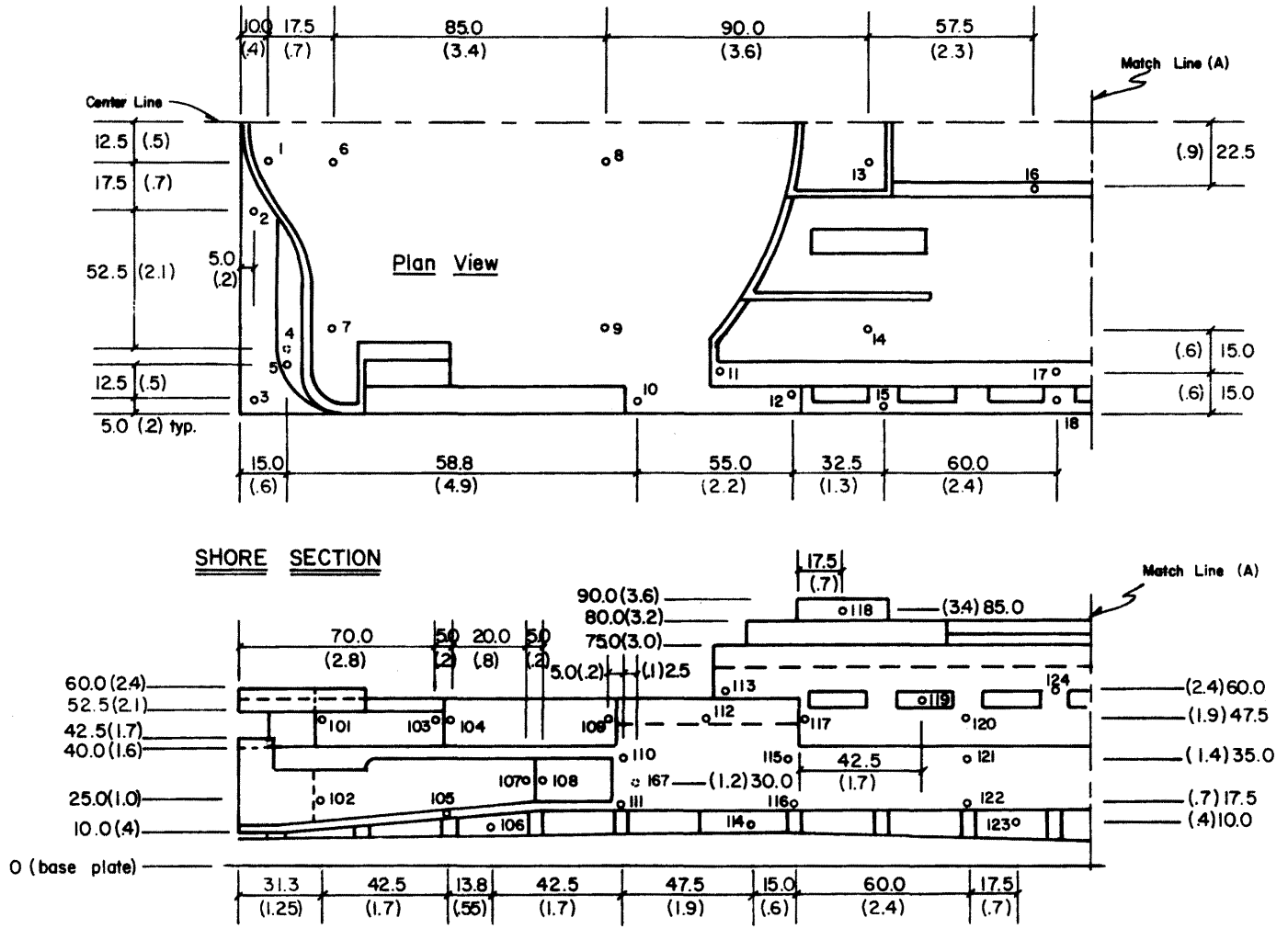


Figure 3b. Pressure Tap Locations

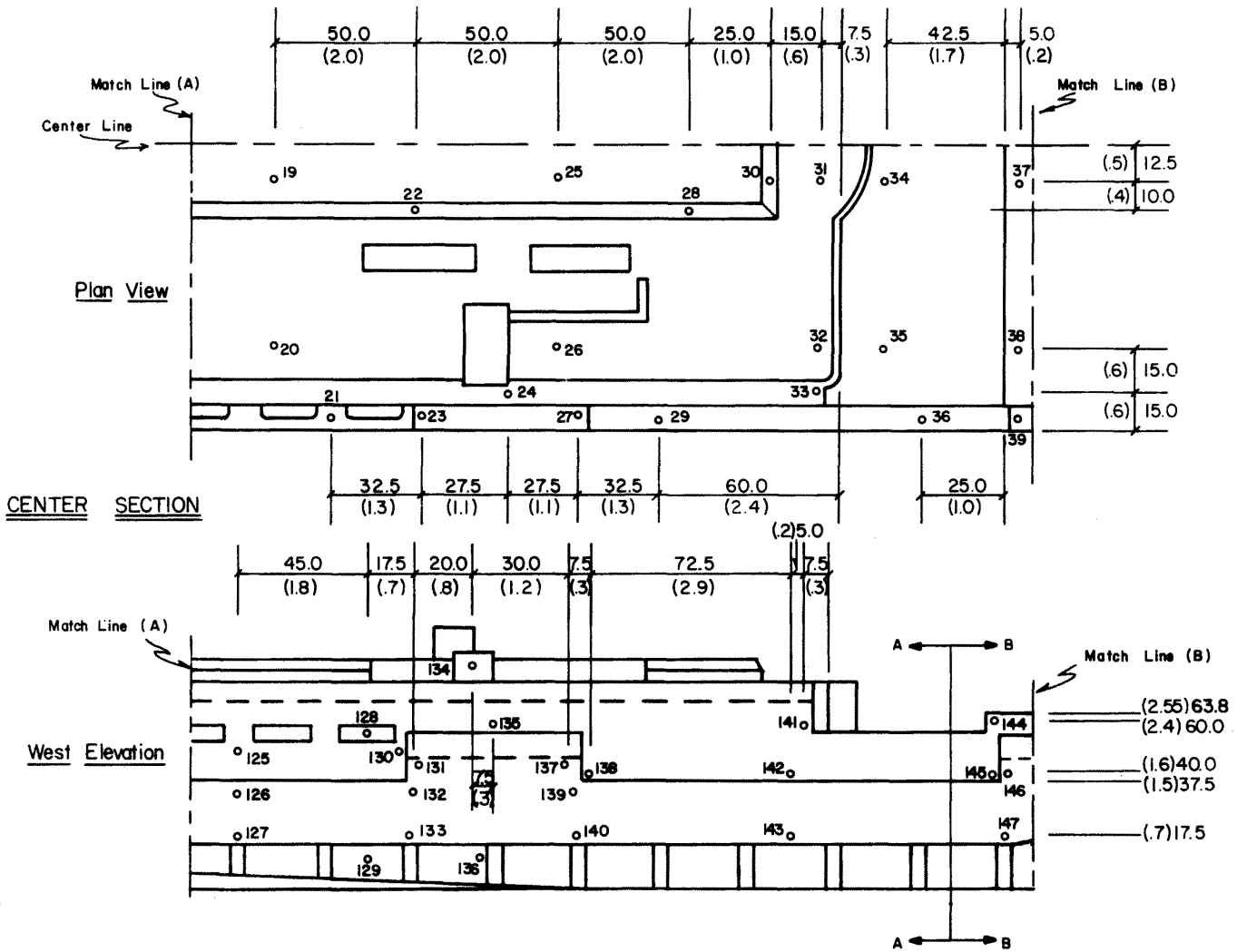


Figure 3c. Pressure Tap Locations

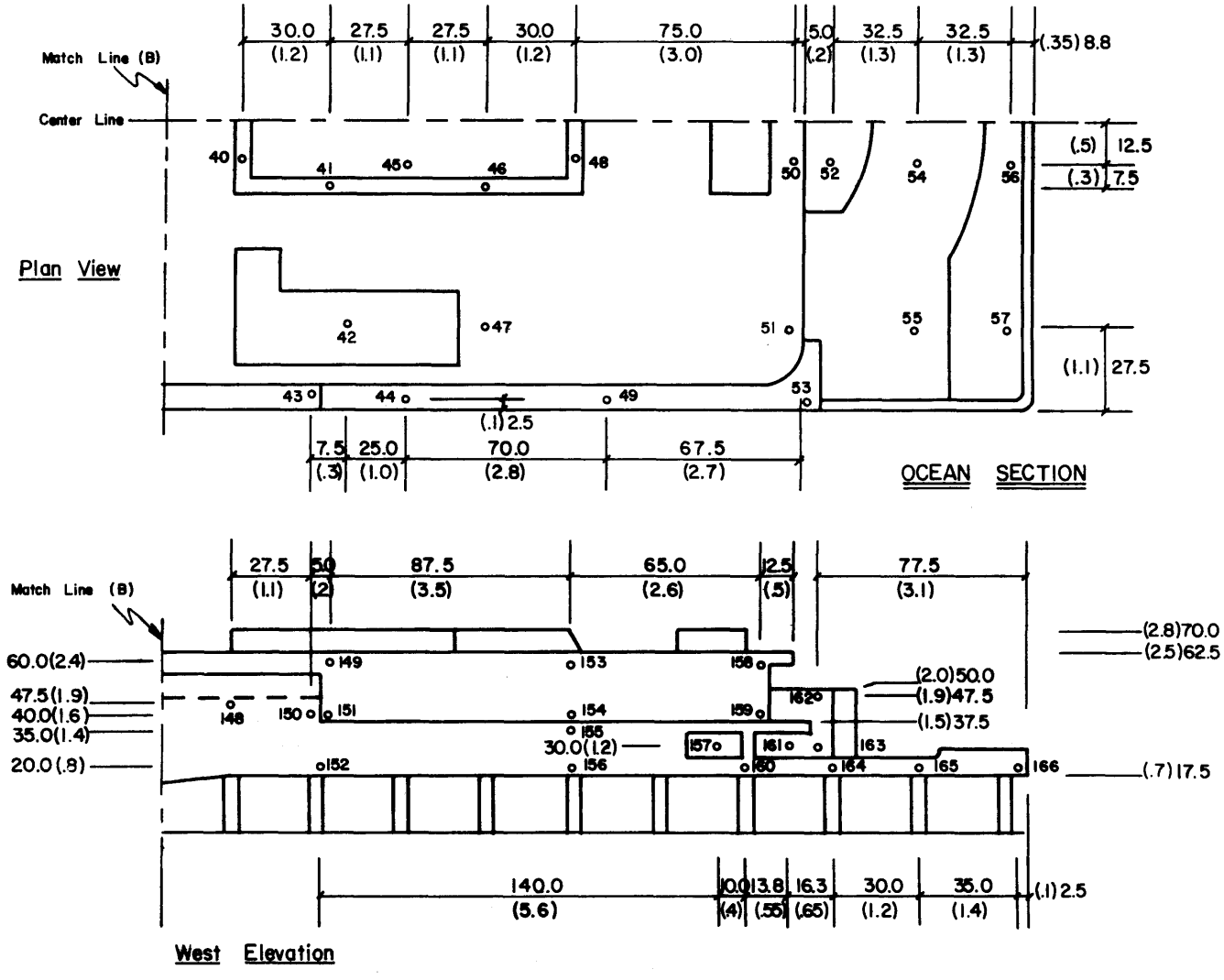


Figure 3d. Pressure Tap Locations

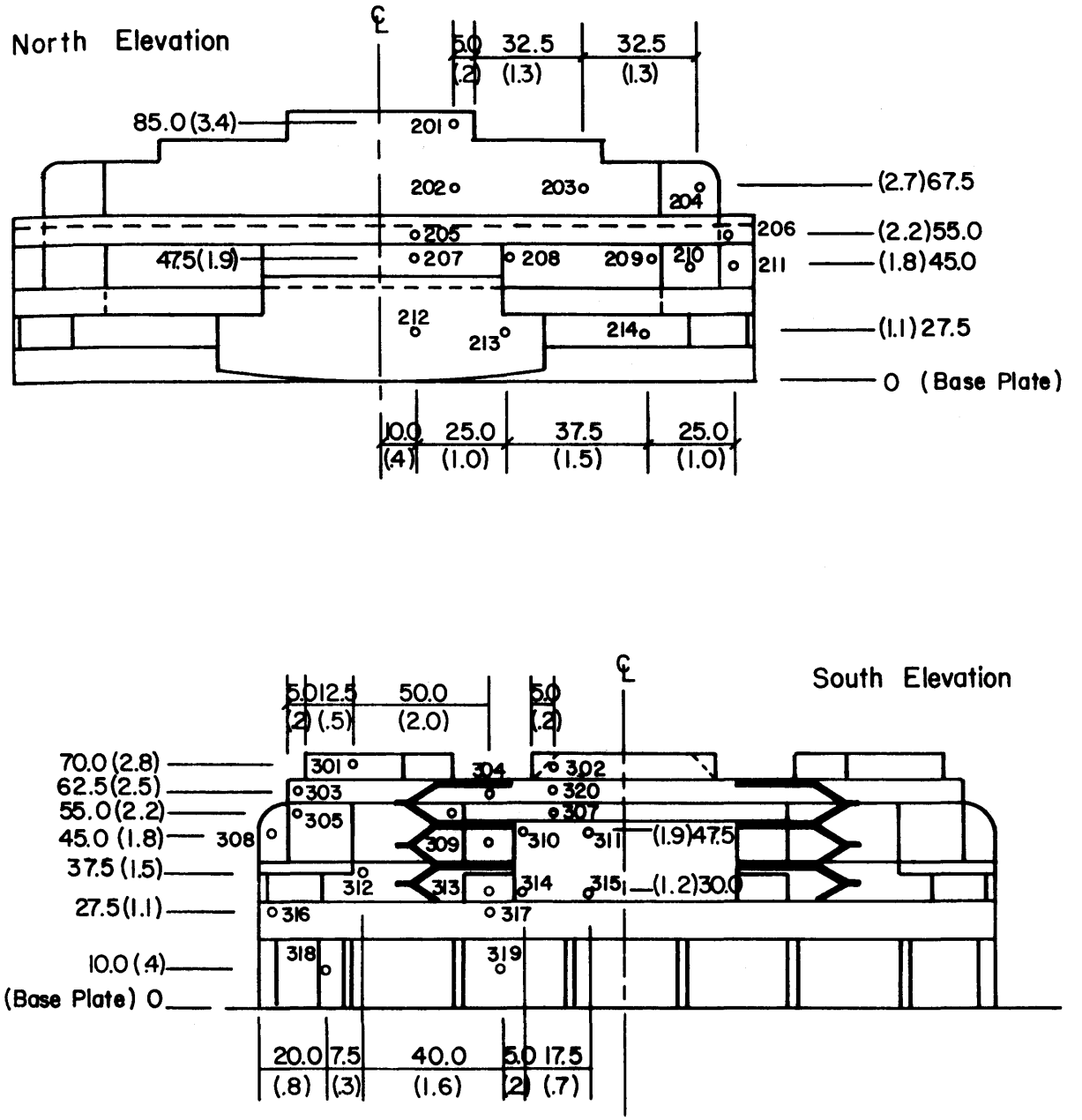
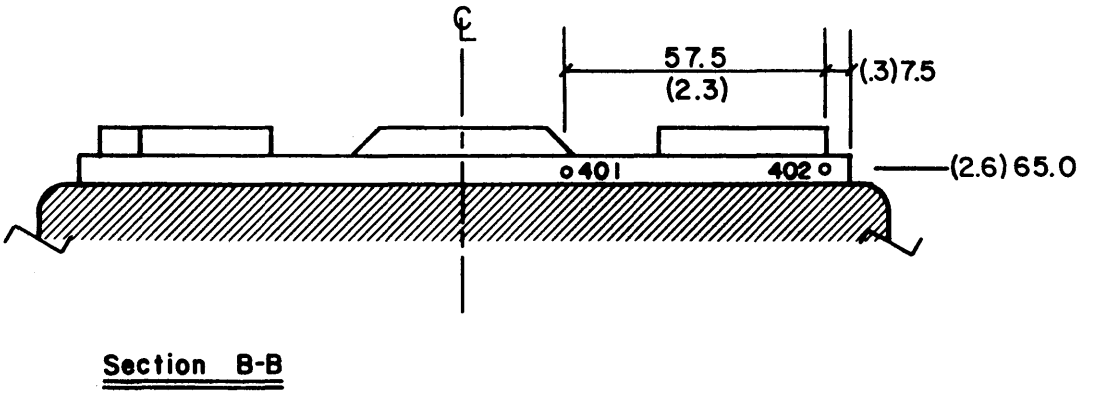
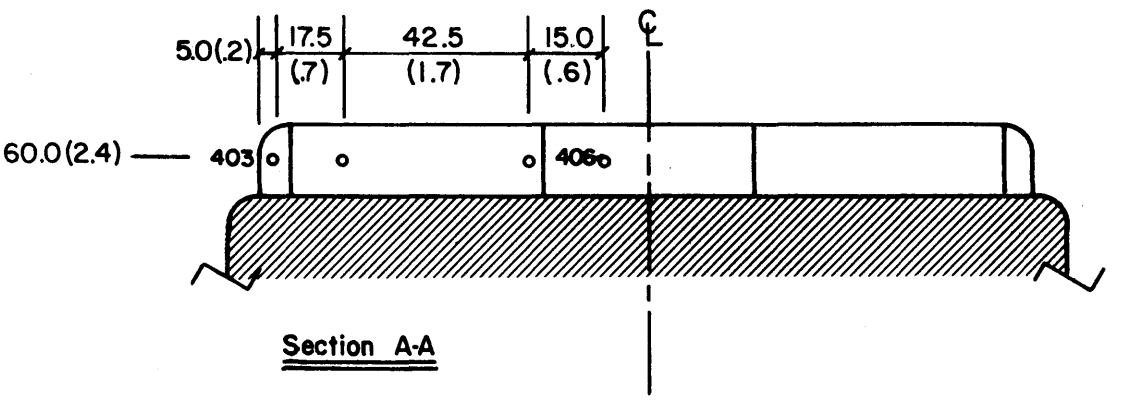


Figure 3e. Pressure Tap Locations



Section B-B



Section A-A

Figure 3f. Pressure Tap Locations

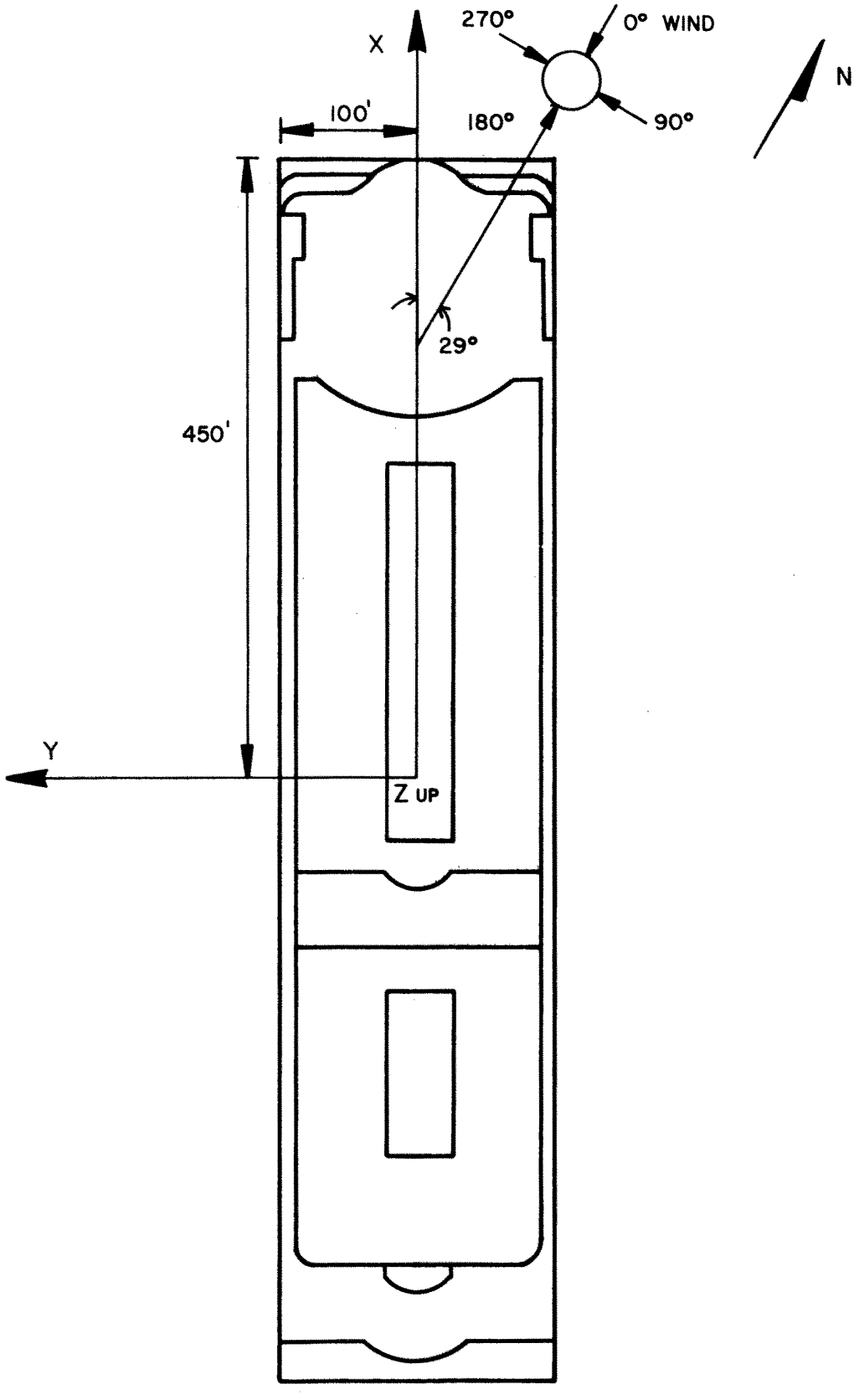


Figure 3g. Net Force Coordinate System

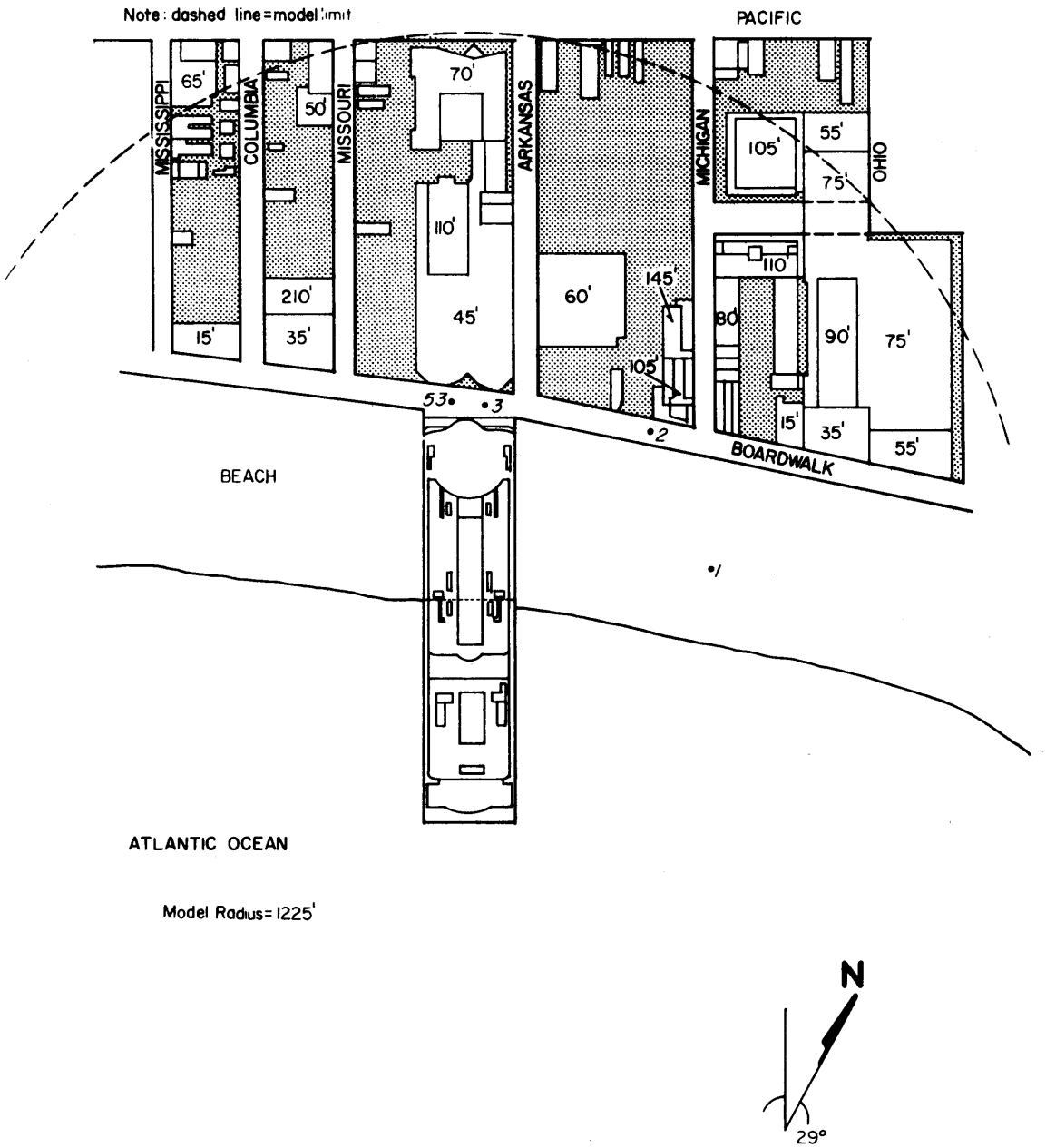


Figure 4a. Building Location and Pedestrian Wind Velocity Measuring Positions

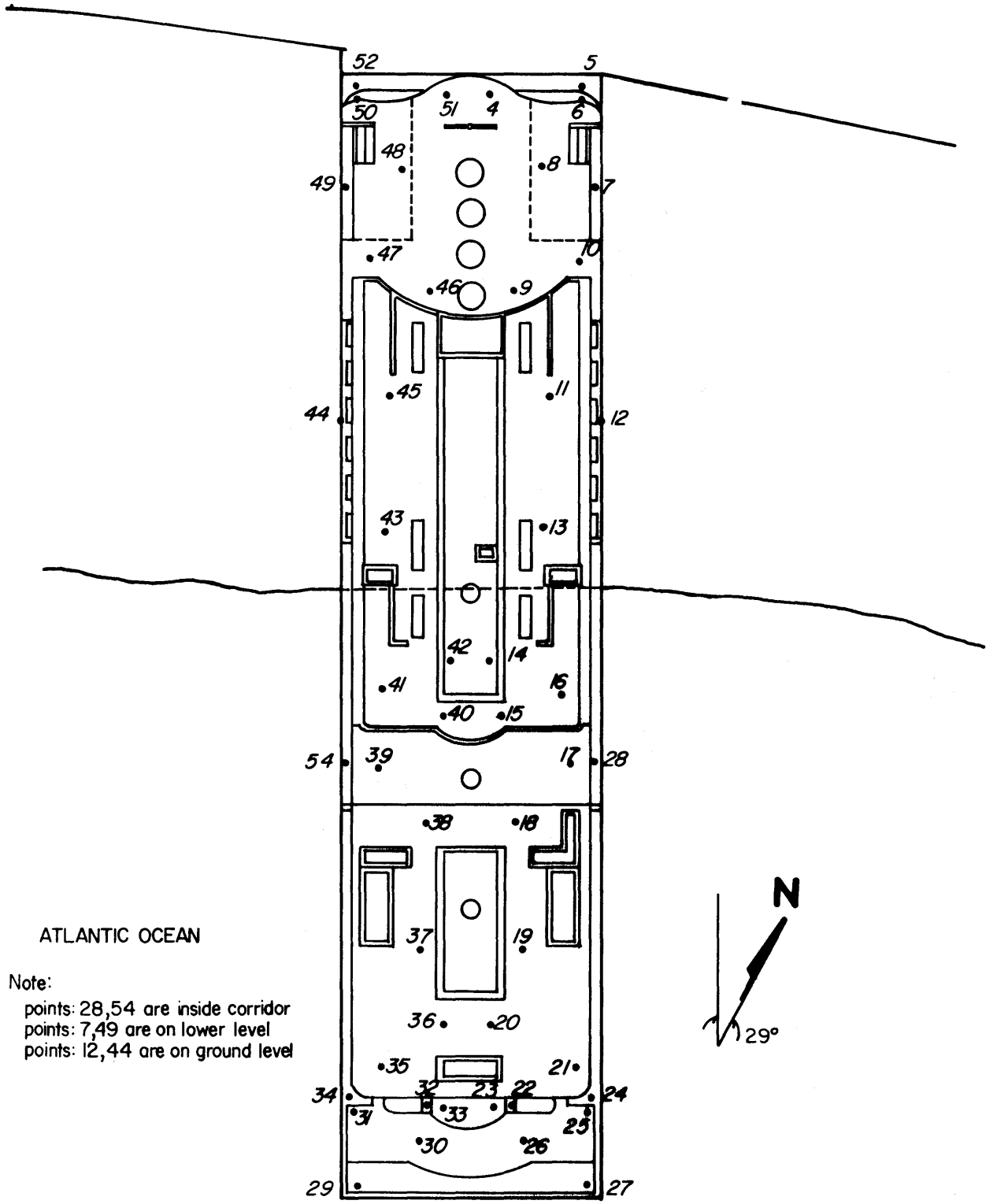


Figure 4b. Building Location and Pedestrian Wind Velocity Measuring Positions

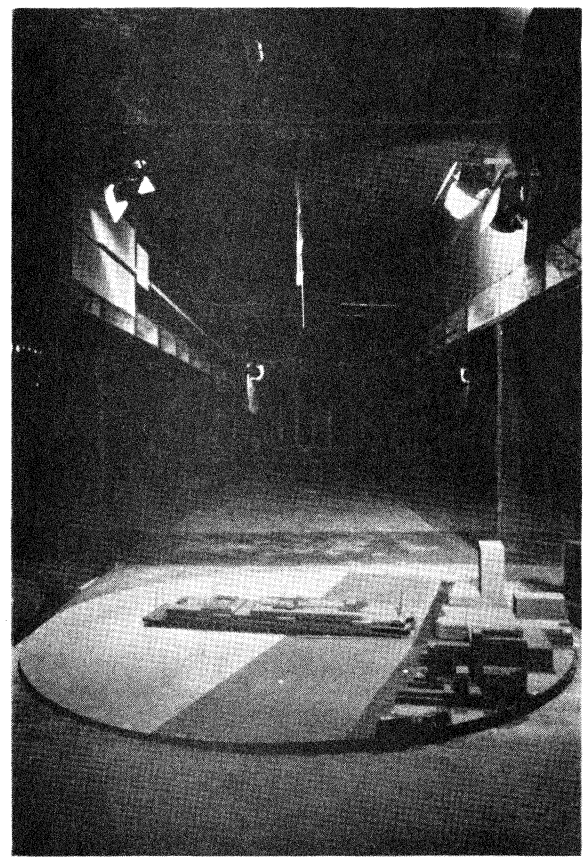


Figure 5. Completed Model in Wind Tunnel

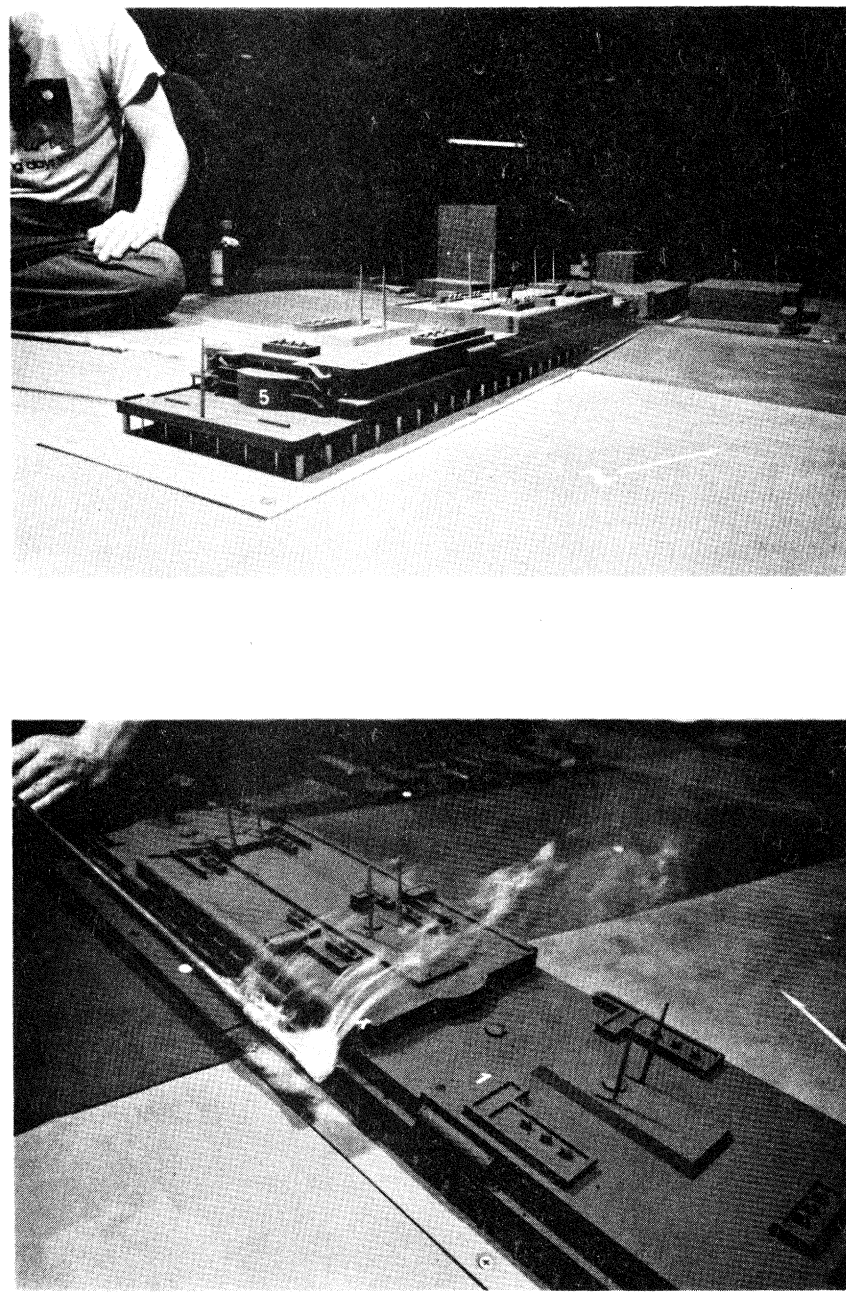


Figure 5. Completed Model in Wind Tunnel

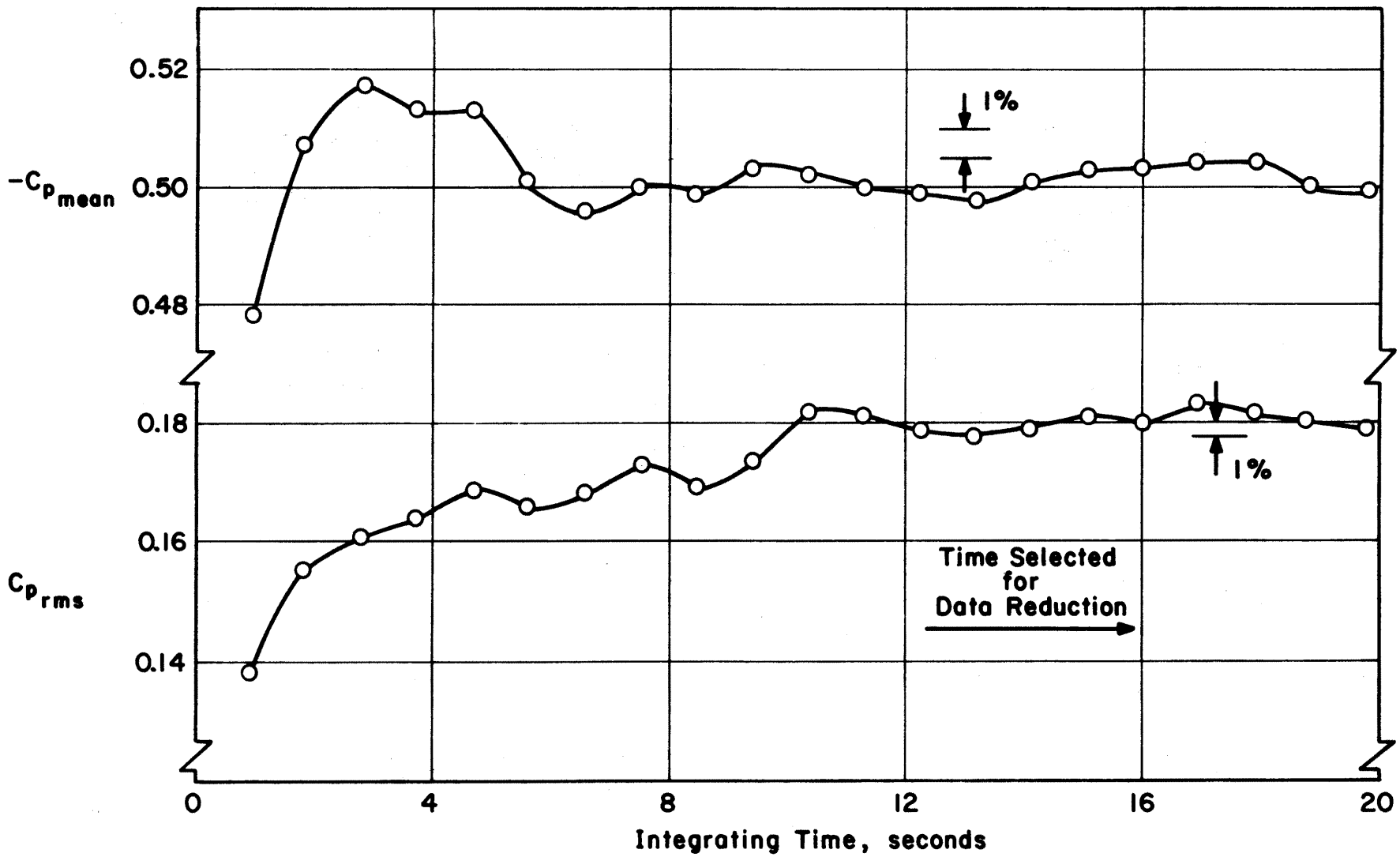


Figure 6- Data Sampling Time Verification

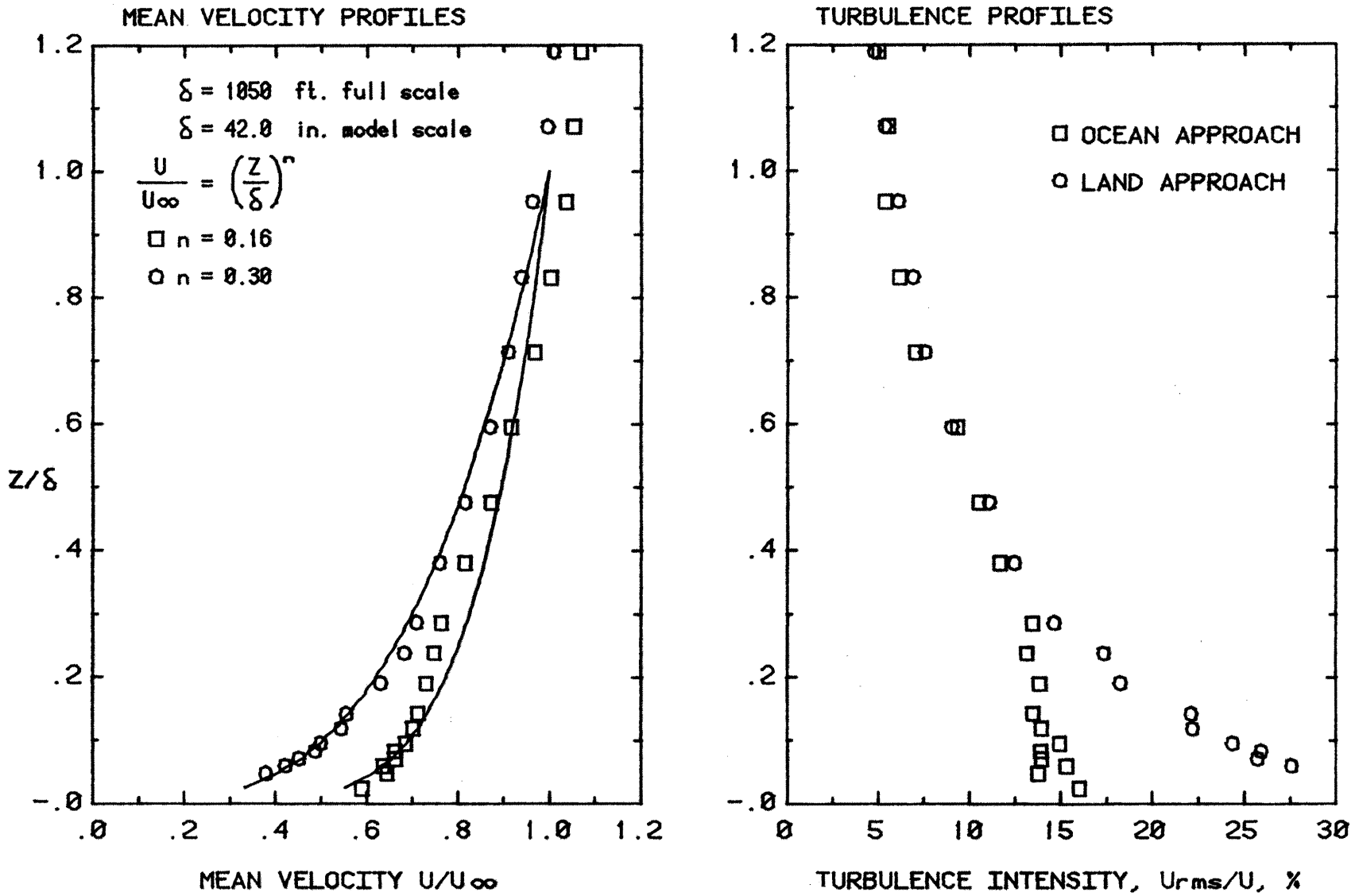
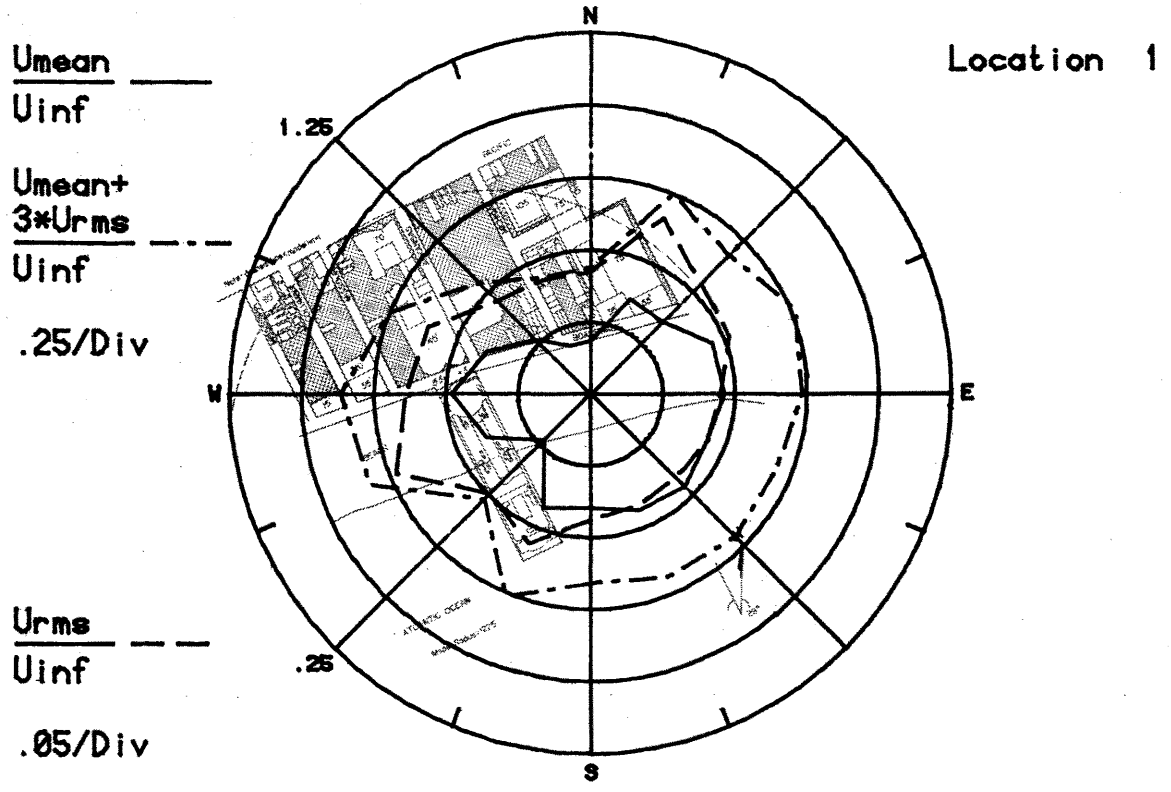


Figure 7. Mean Velocity and Turbulence Profiles Approaching the Model.



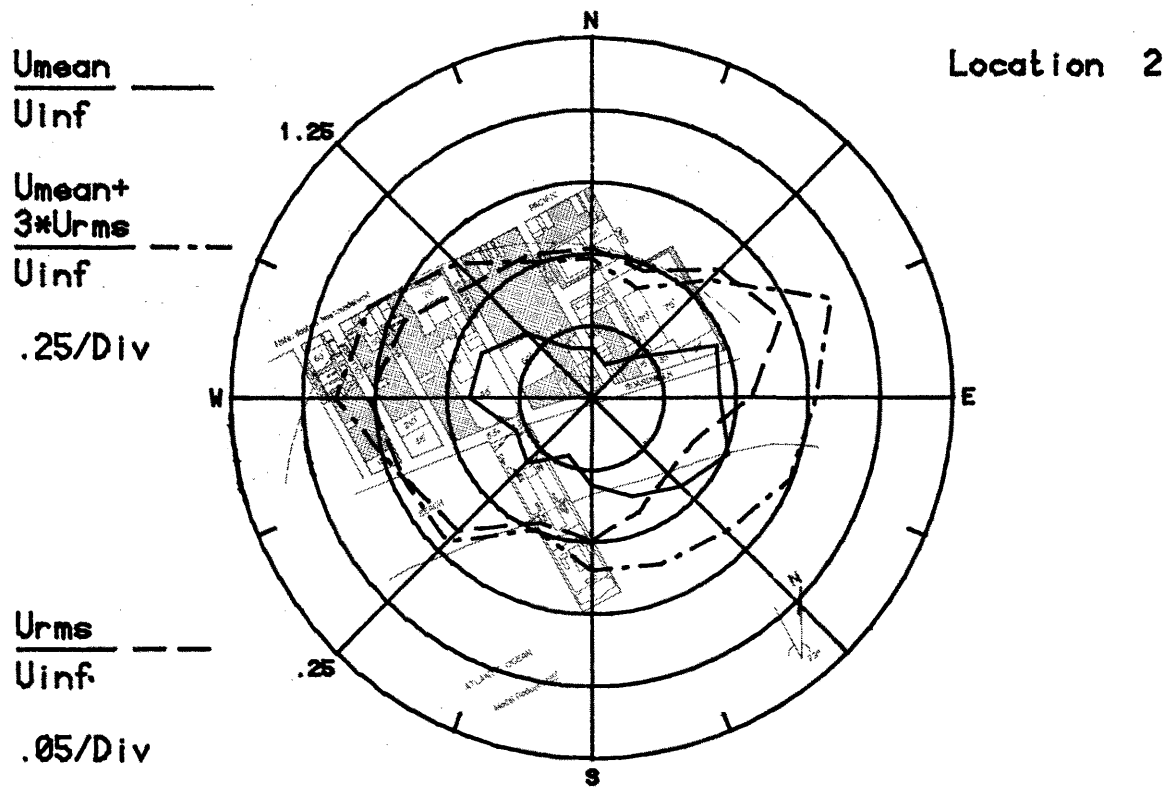


Figure 8a. Mean Velocities and Turbulence Intensities at Pedestrian Locations 1 and 2

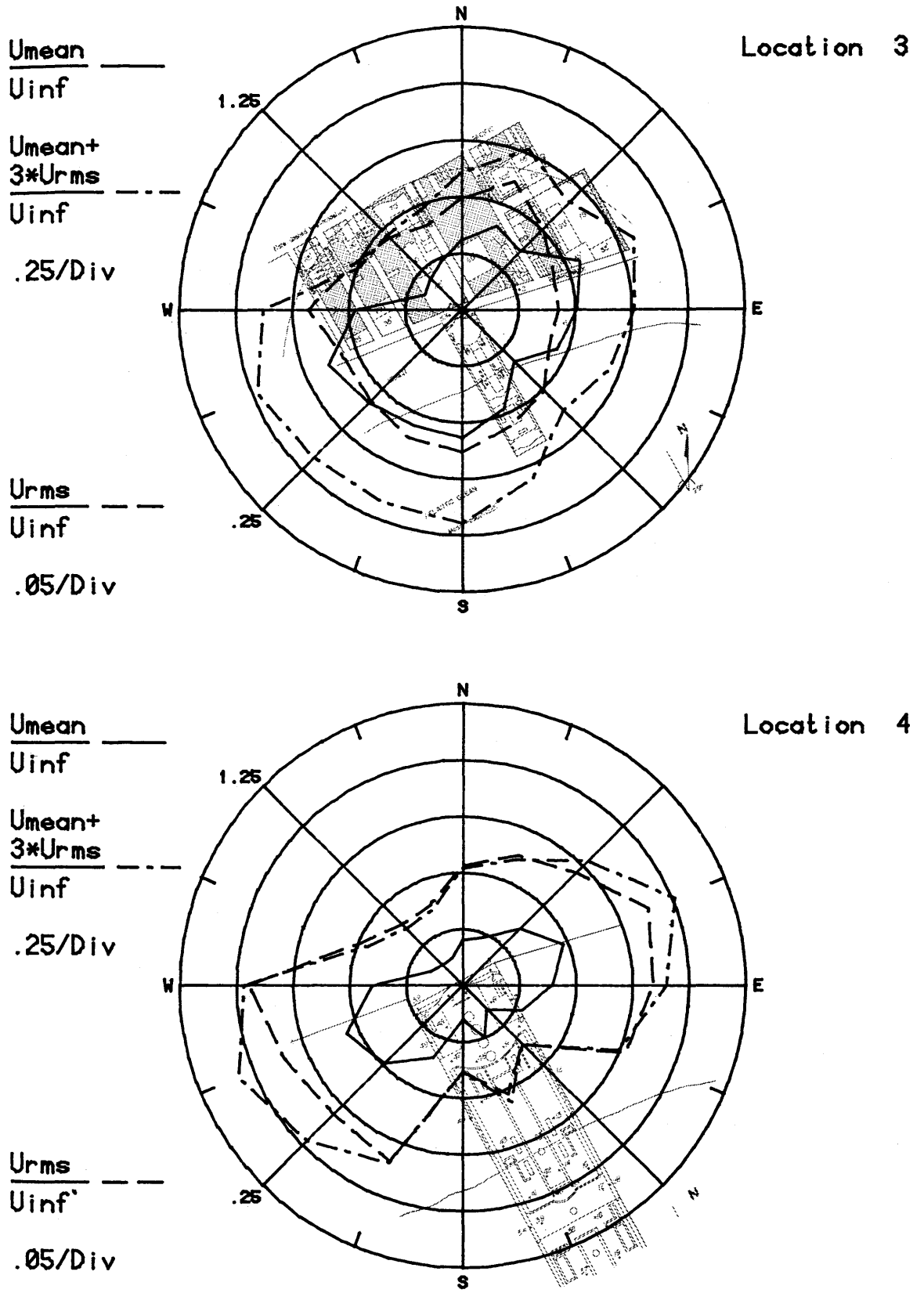


Figure 8b. Mean Velocities and Turbulence Intensities at Pedestrian Locations 3 and 4

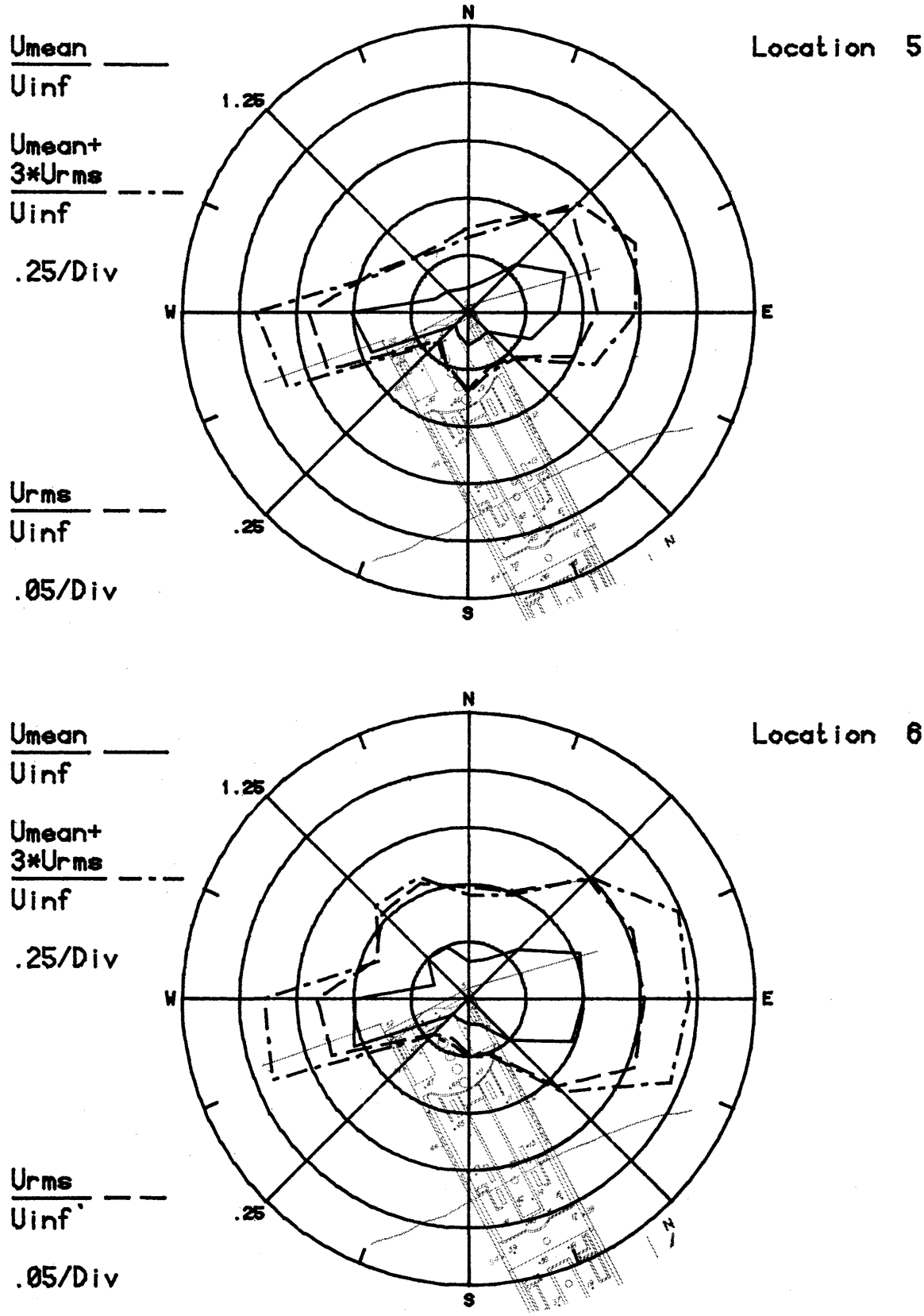


Figure 8c. Mean Velocities and Turbulence Intensities at Pedestrian Locations 5 and 6

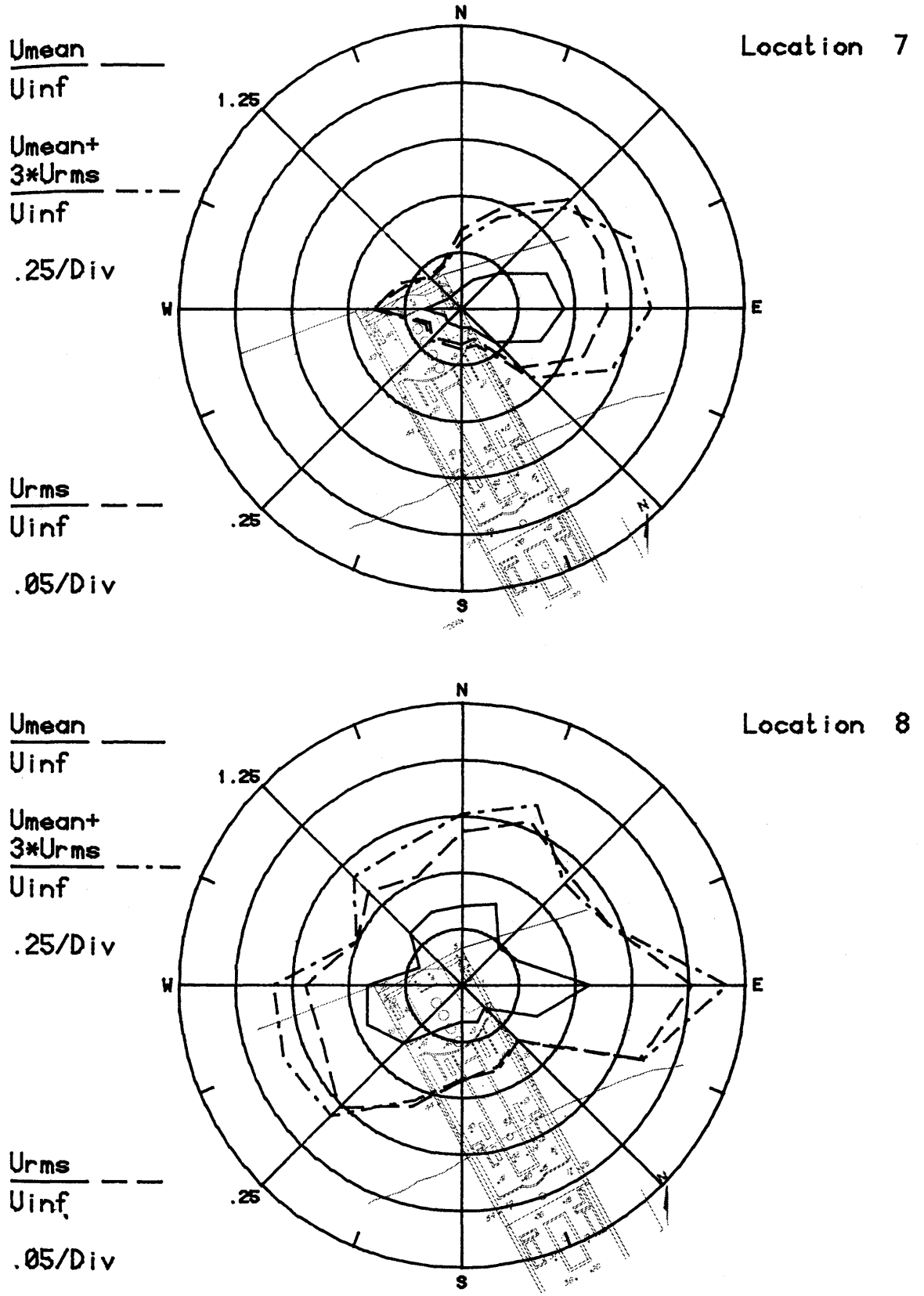


Figure 8d. Mean Velocities and Turbulence Intensities at Pedestrian Locations 7 and 8

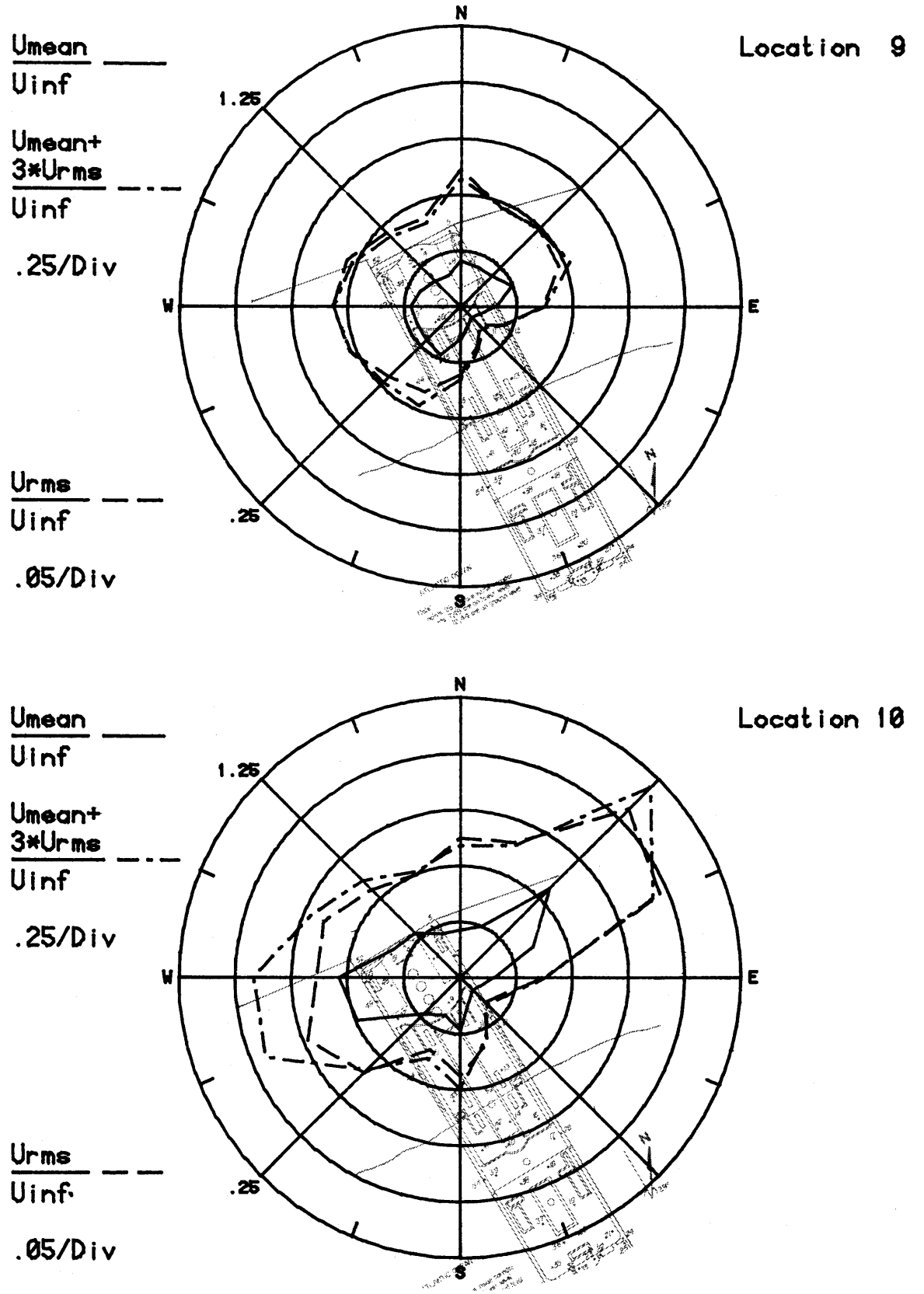


Figure 8e. Mean Velocities and Turbulence Intensities at Pedestrian Locations 9 and 10

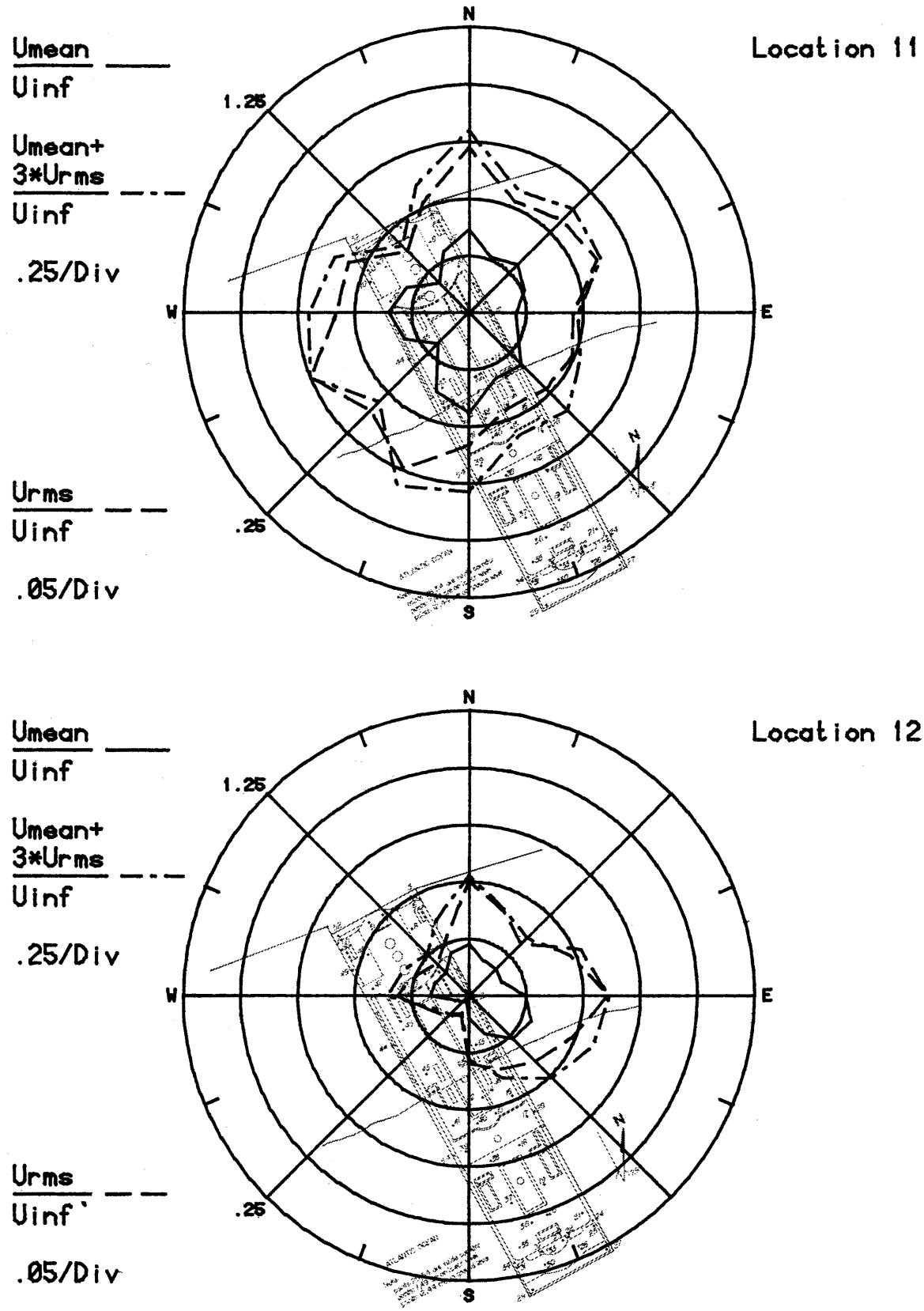
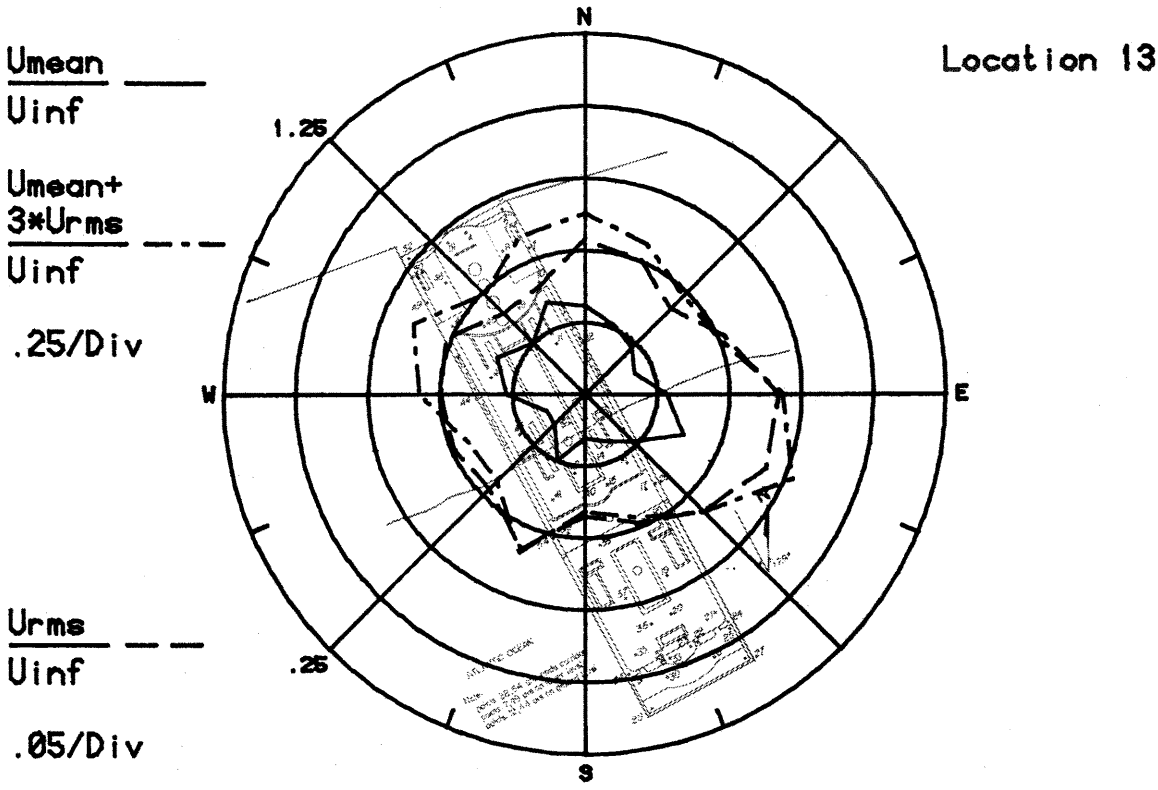
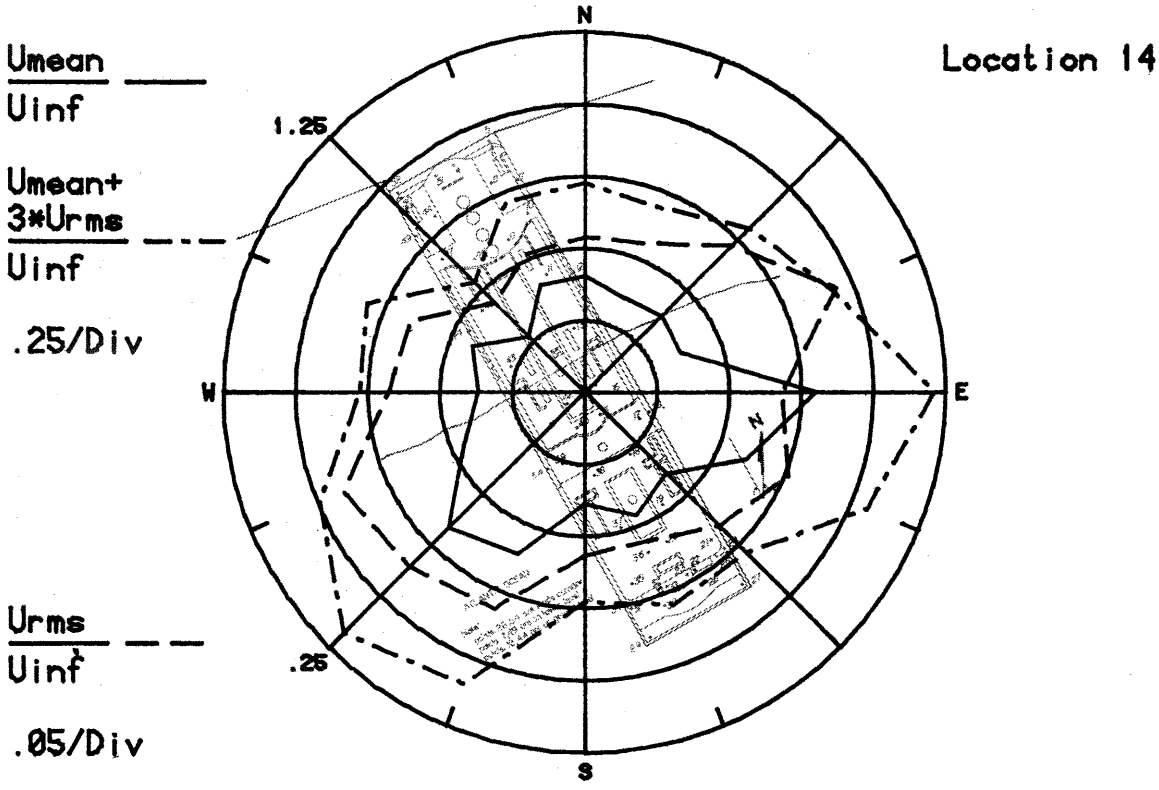


Figure 8f. Mean Velocities and Turbulence Intensities at Pedestrian Locations 11 and 12





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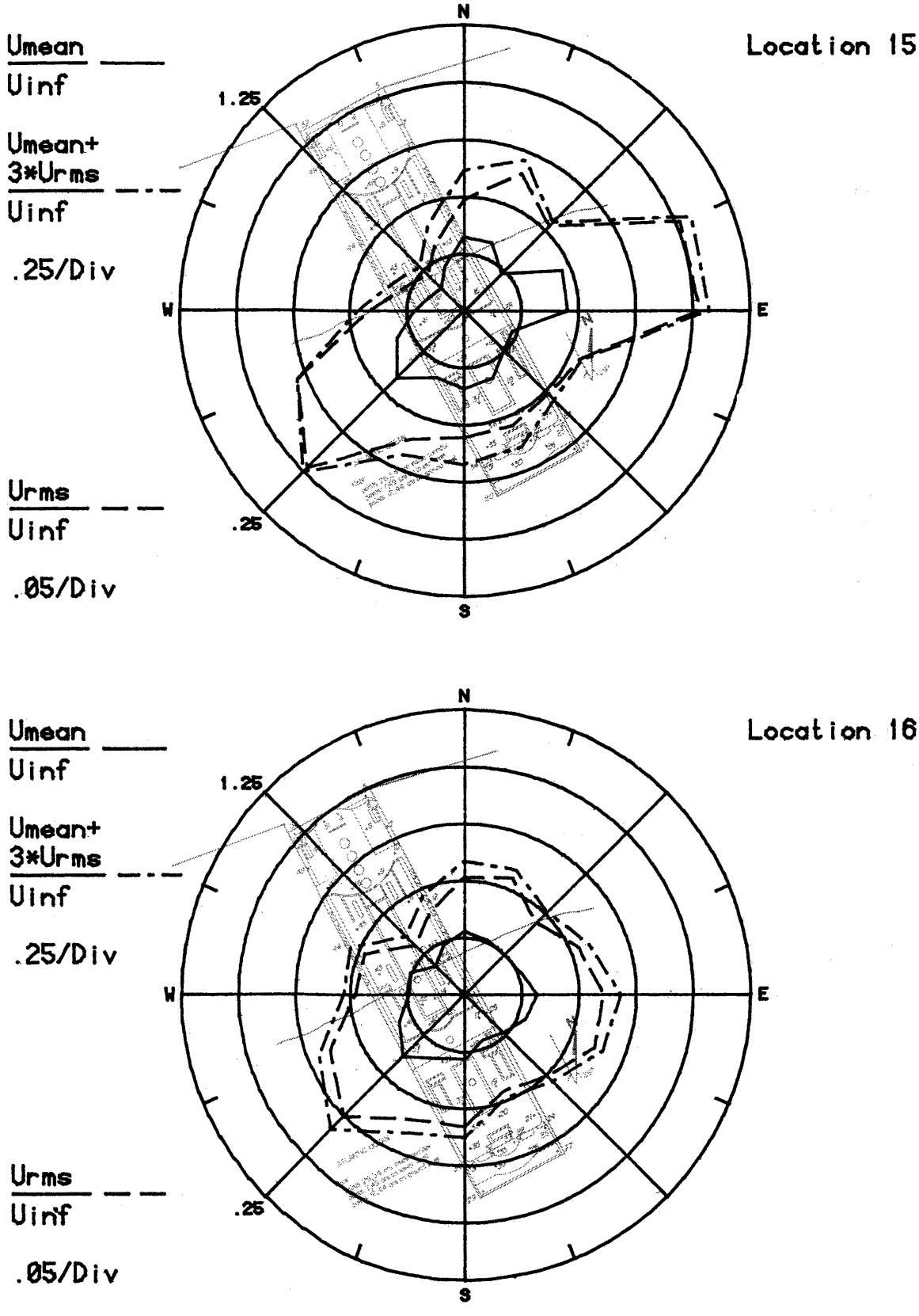

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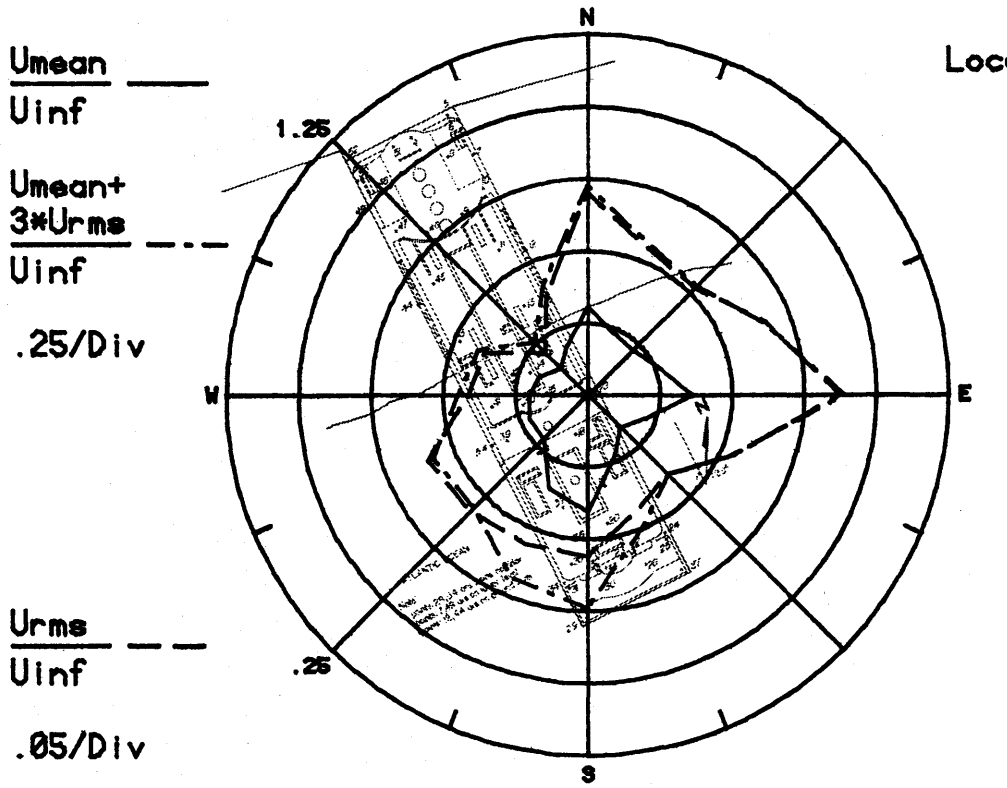


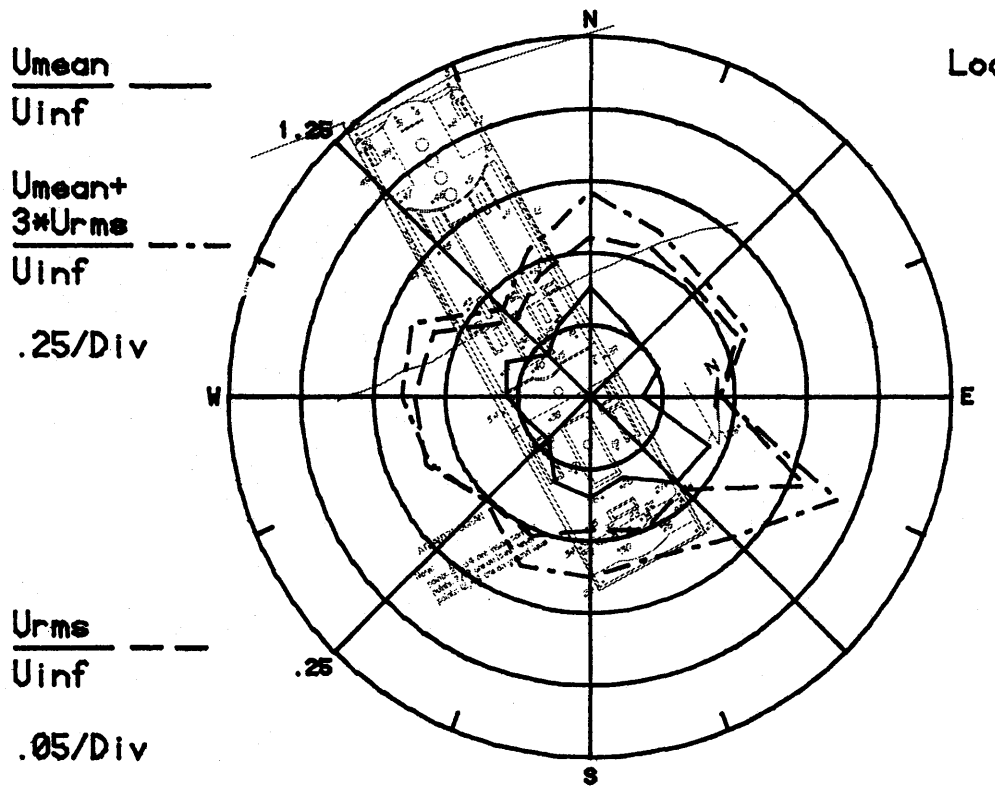


Figure 81. Mean Velocities and Turbulence Intensities at Pedestrian Locations 17 and 18

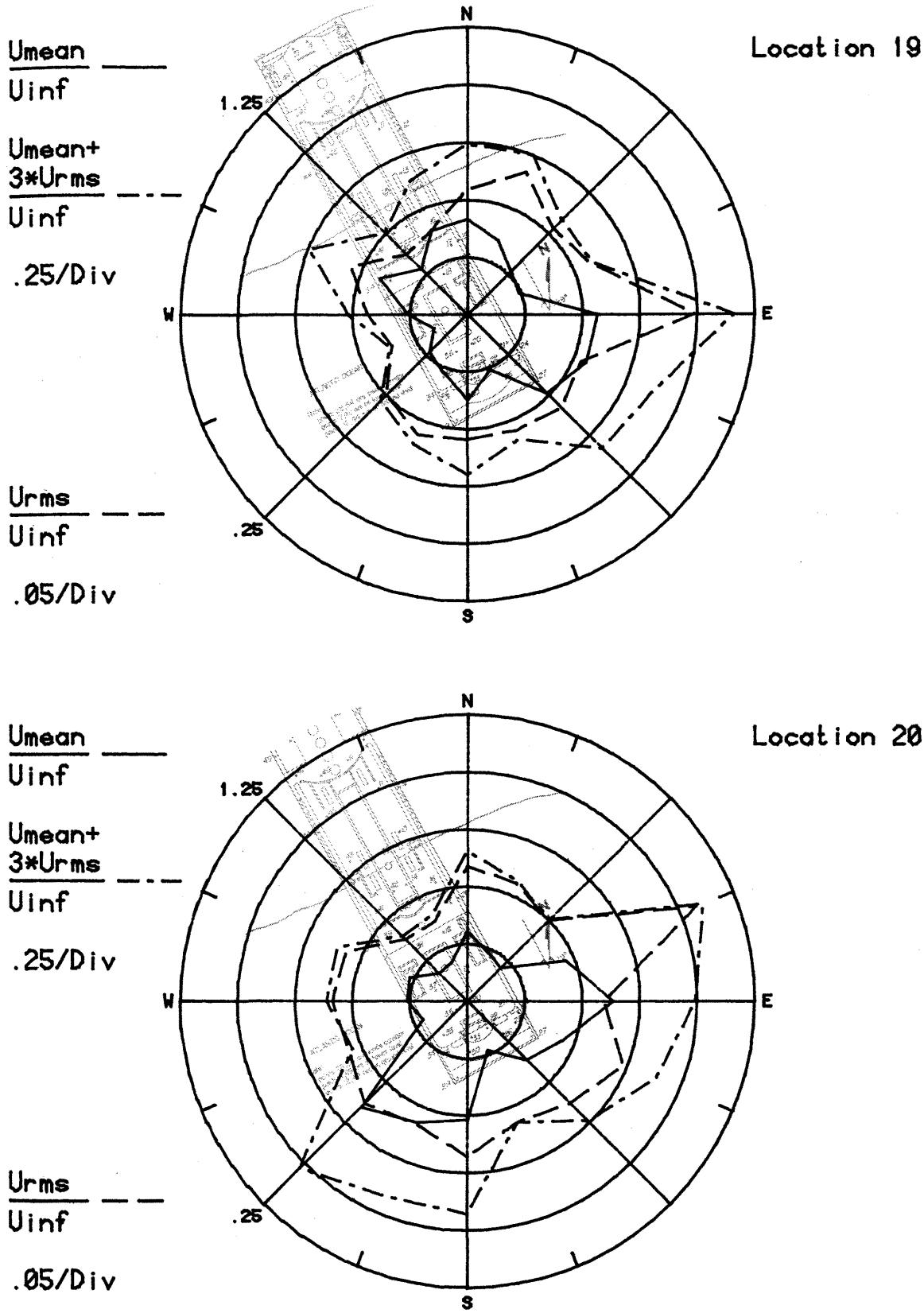
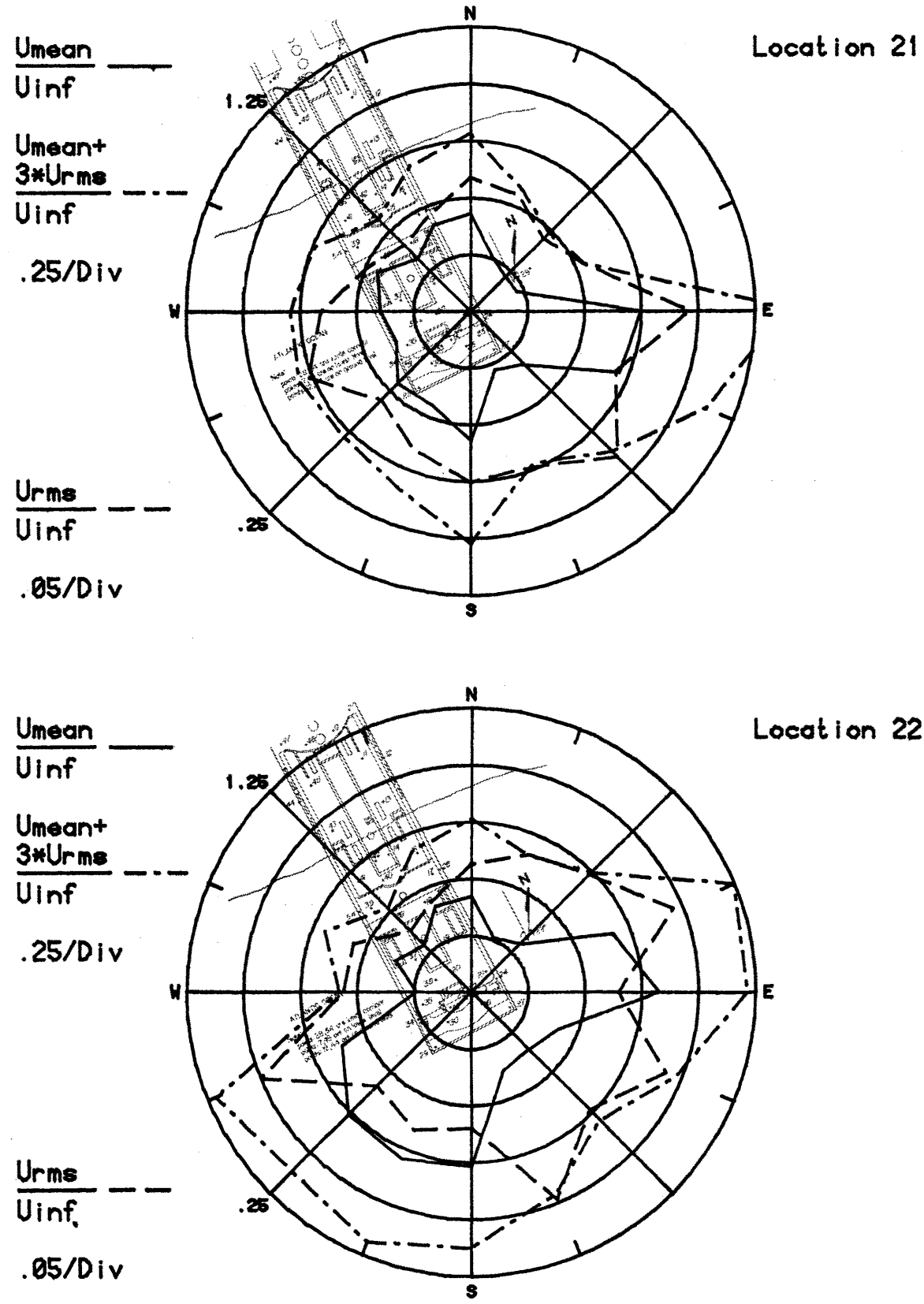


Figure 8j. Mean Velocities and Turbulence Intensities at Pedestrian Locations 19 and 20



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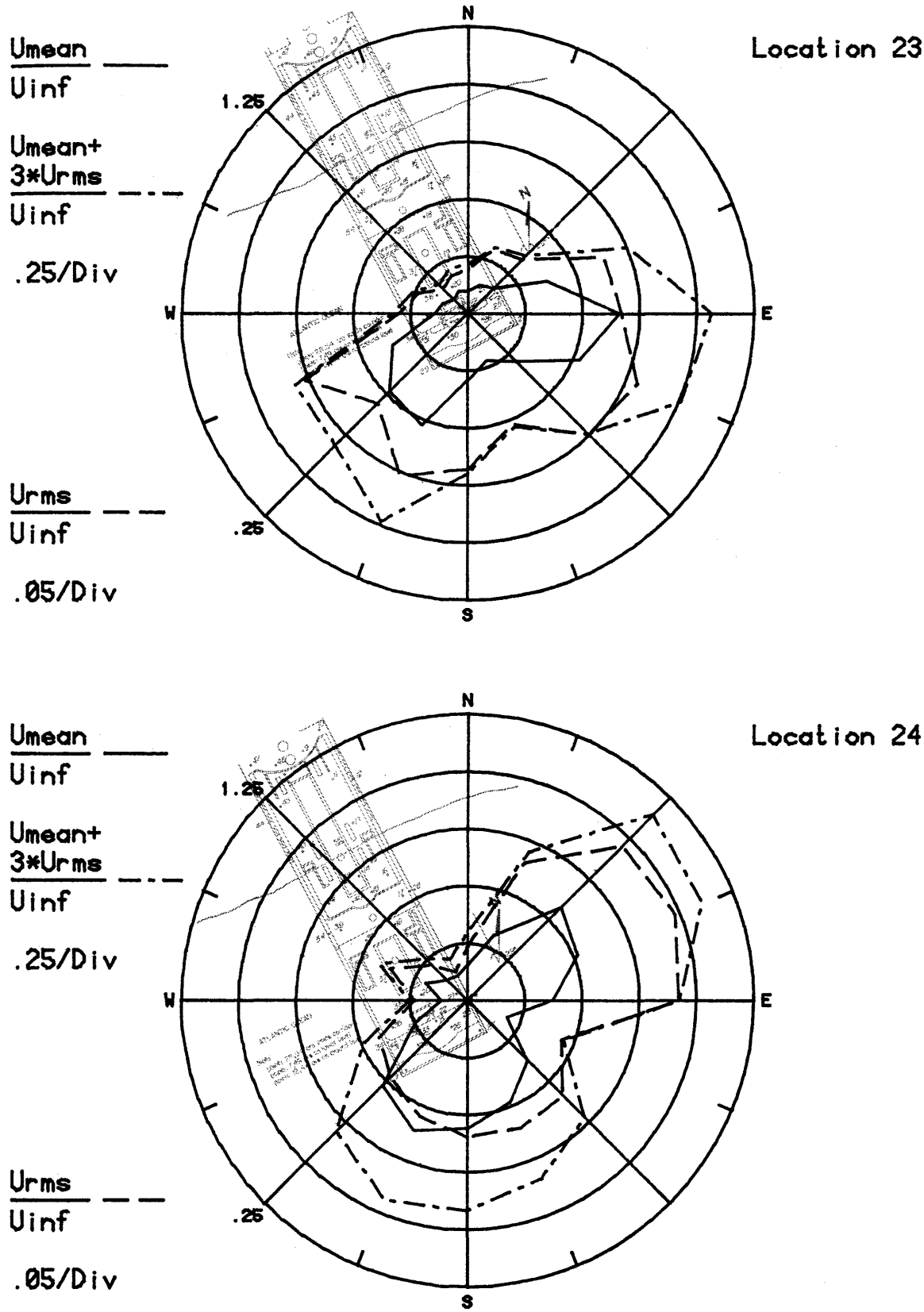

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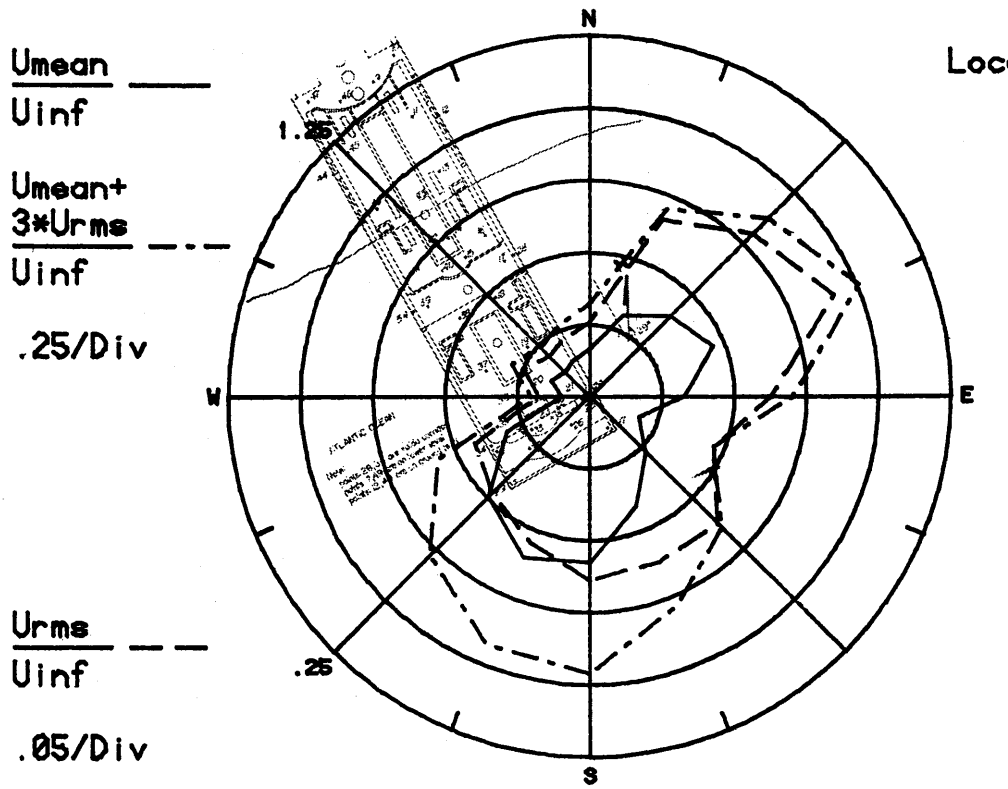


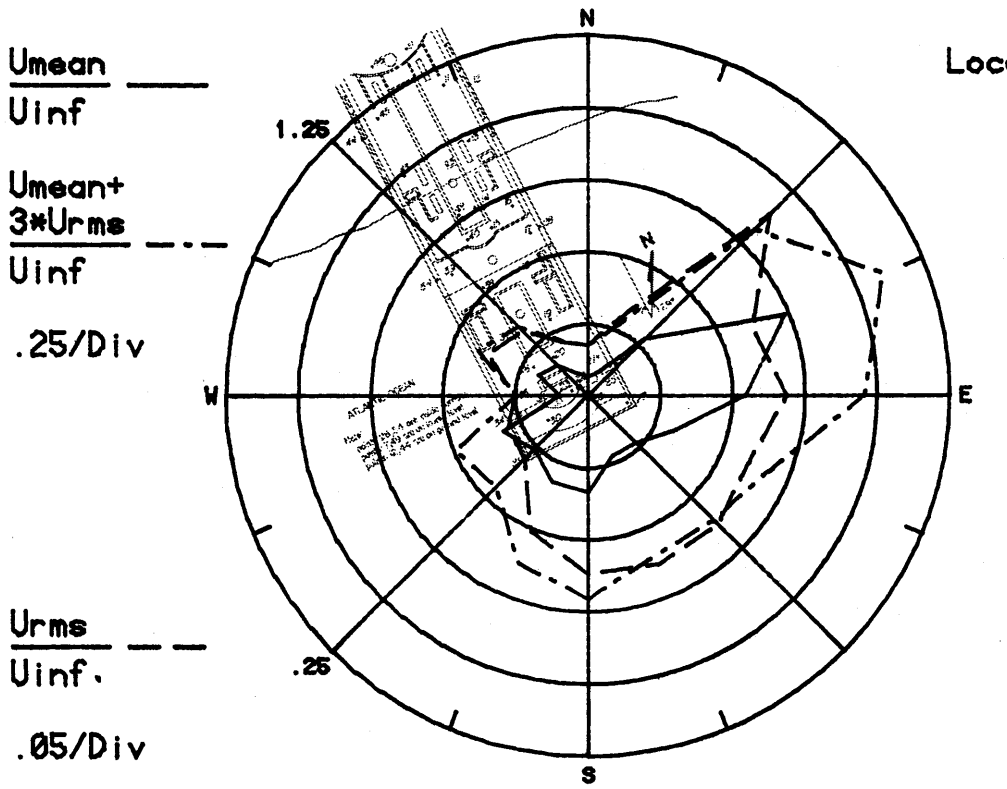
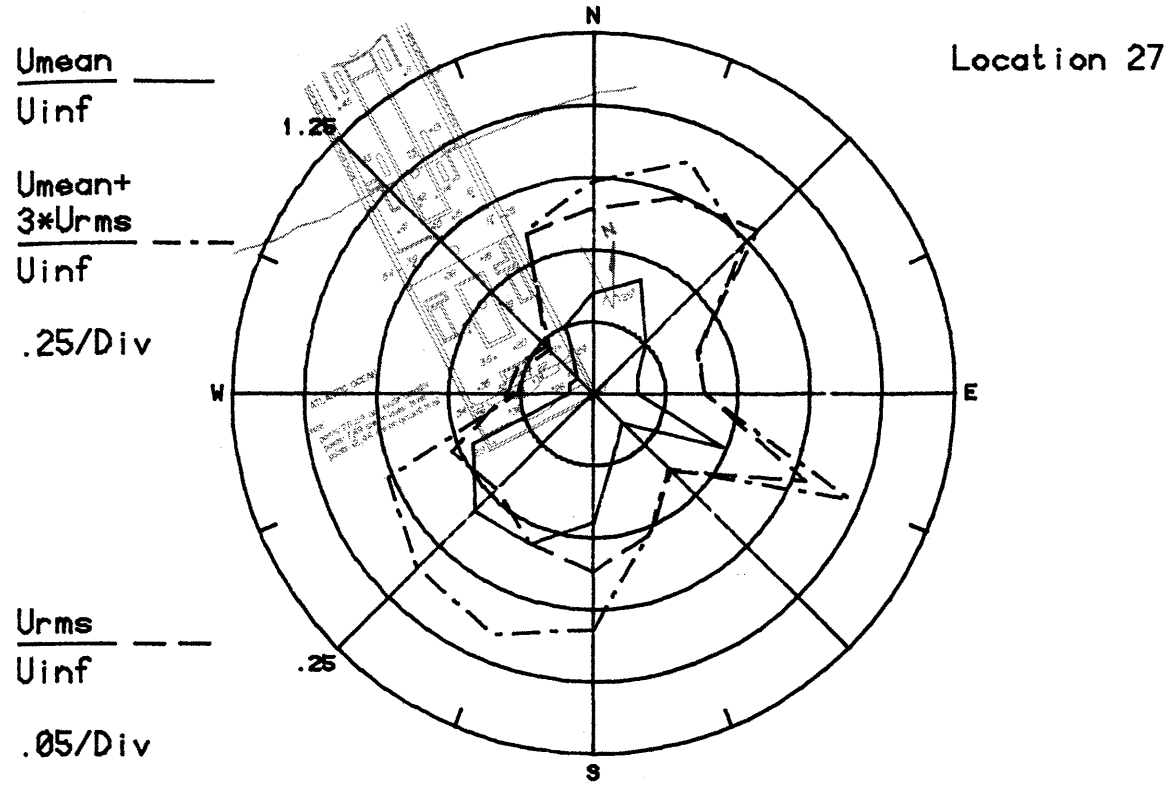


Figure 8m. Mean Velocities and Turbulence Intensities at Pedestrian Locations 25 and 26



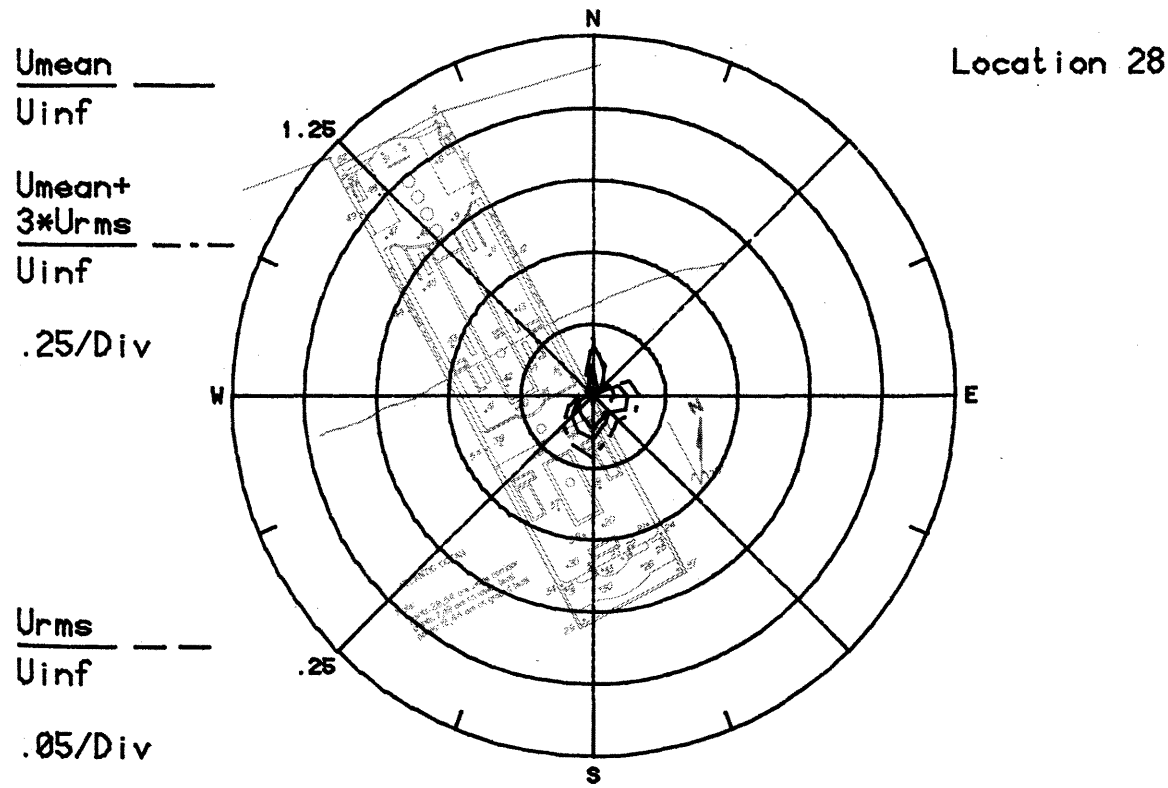
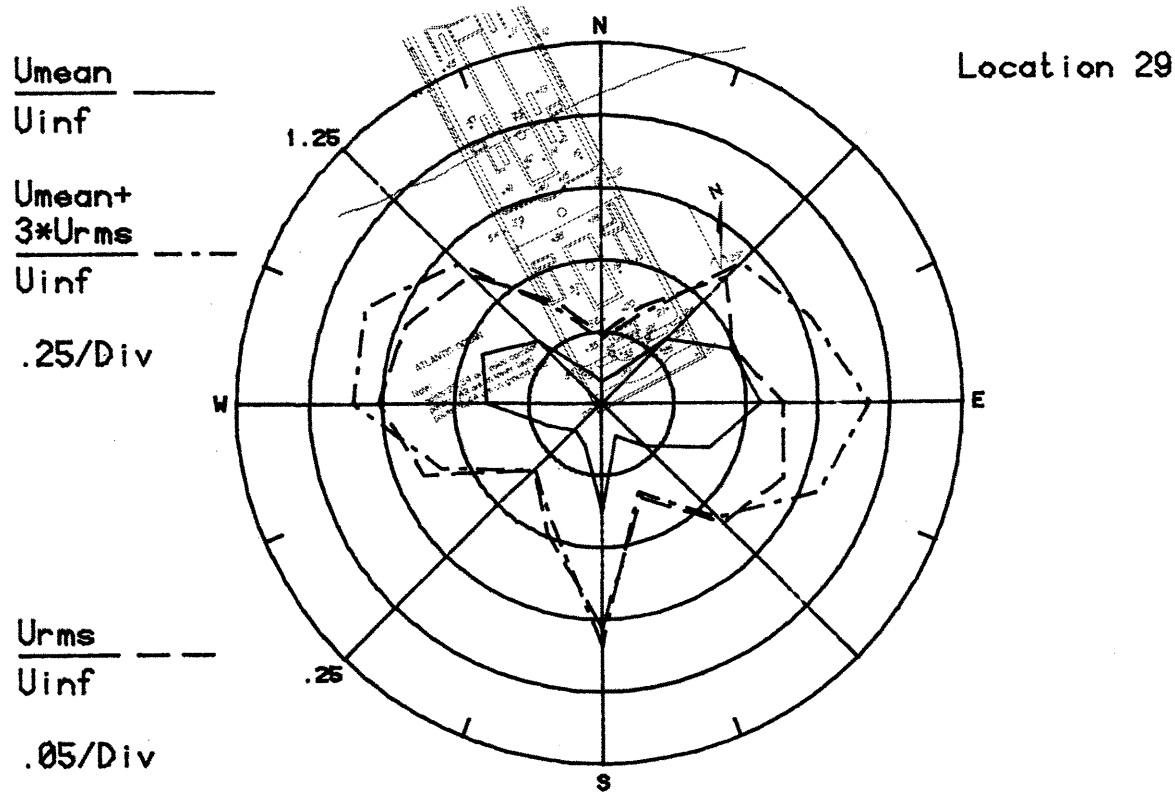


Figure 8n. Mean Velocities and Turbulence Intensities at Pedestrian Locations 27 and 28



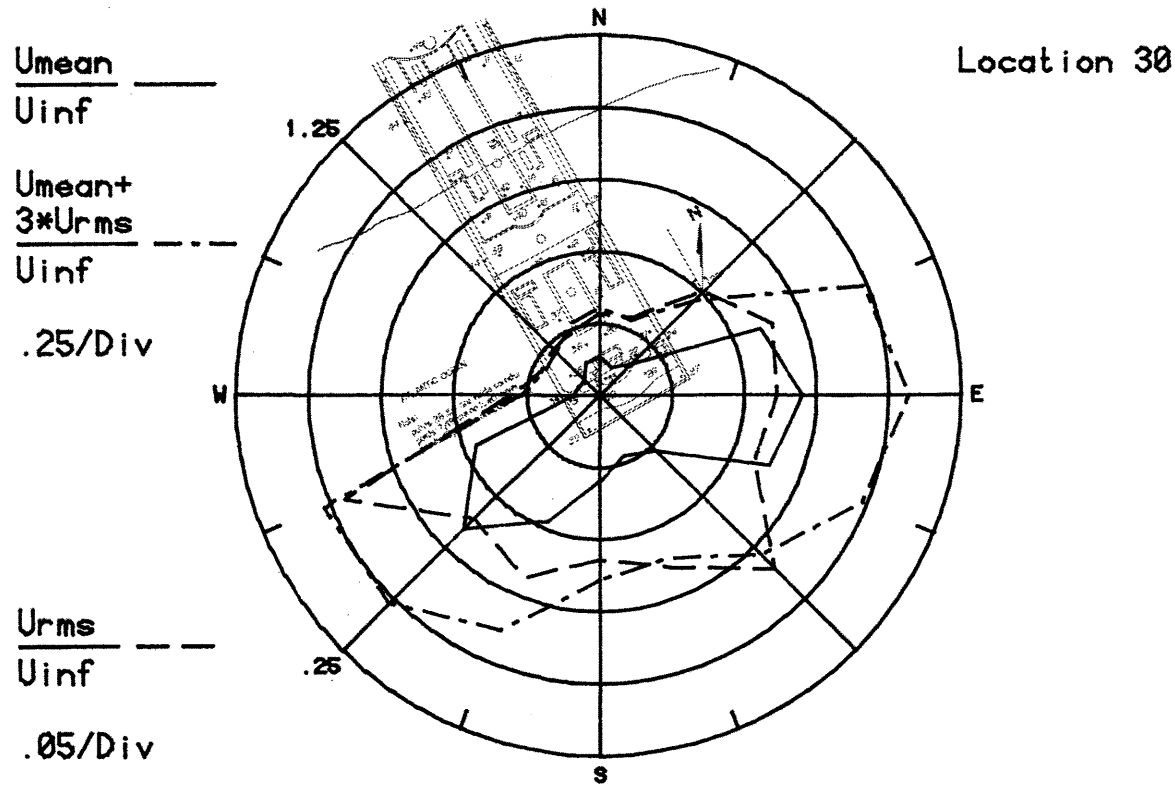
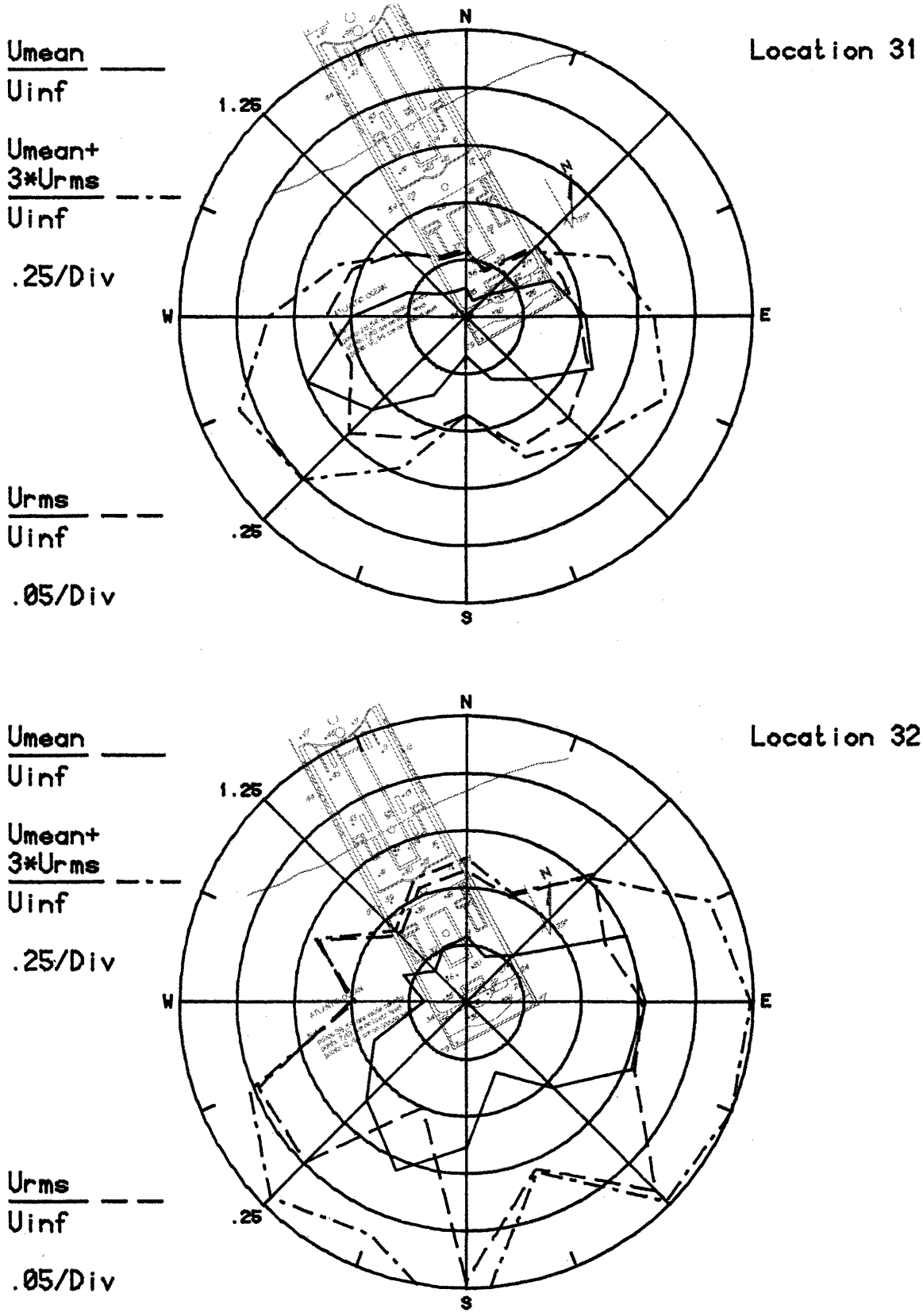


Figure 8o. Mean Velocities and Turbulence Intensities at Pedestrian Locations 29 and 30



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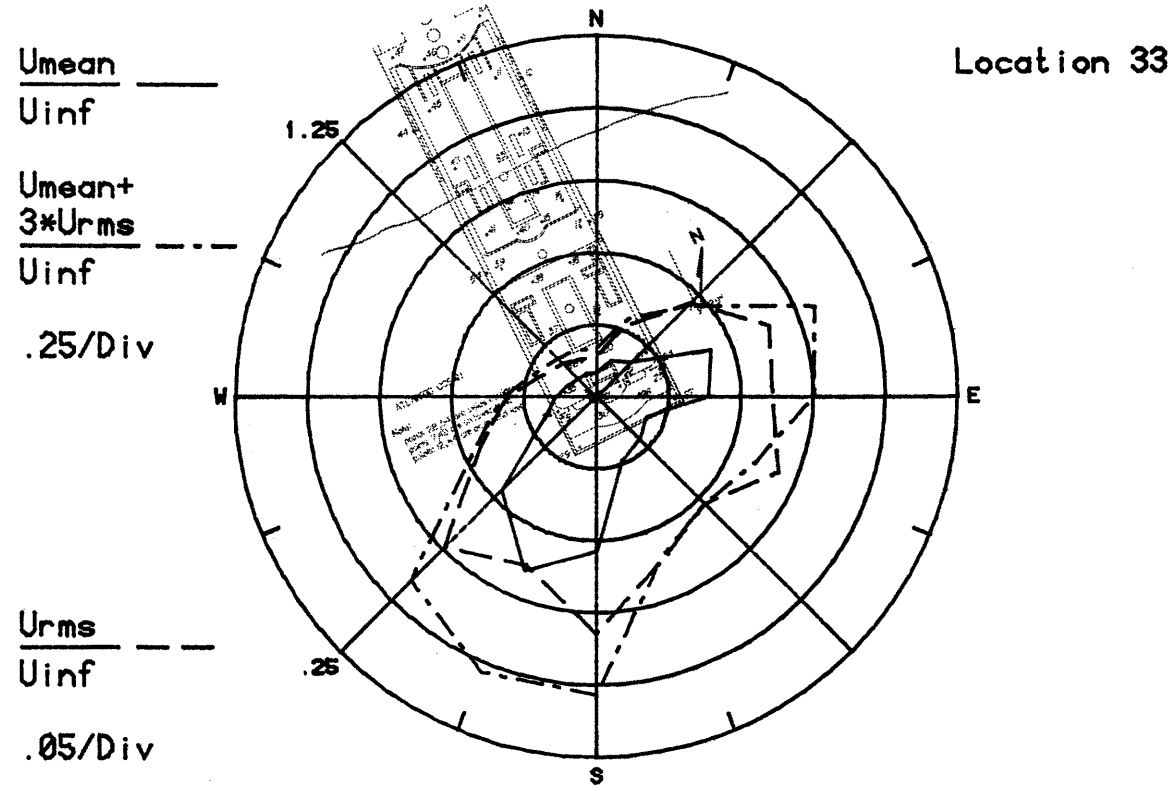


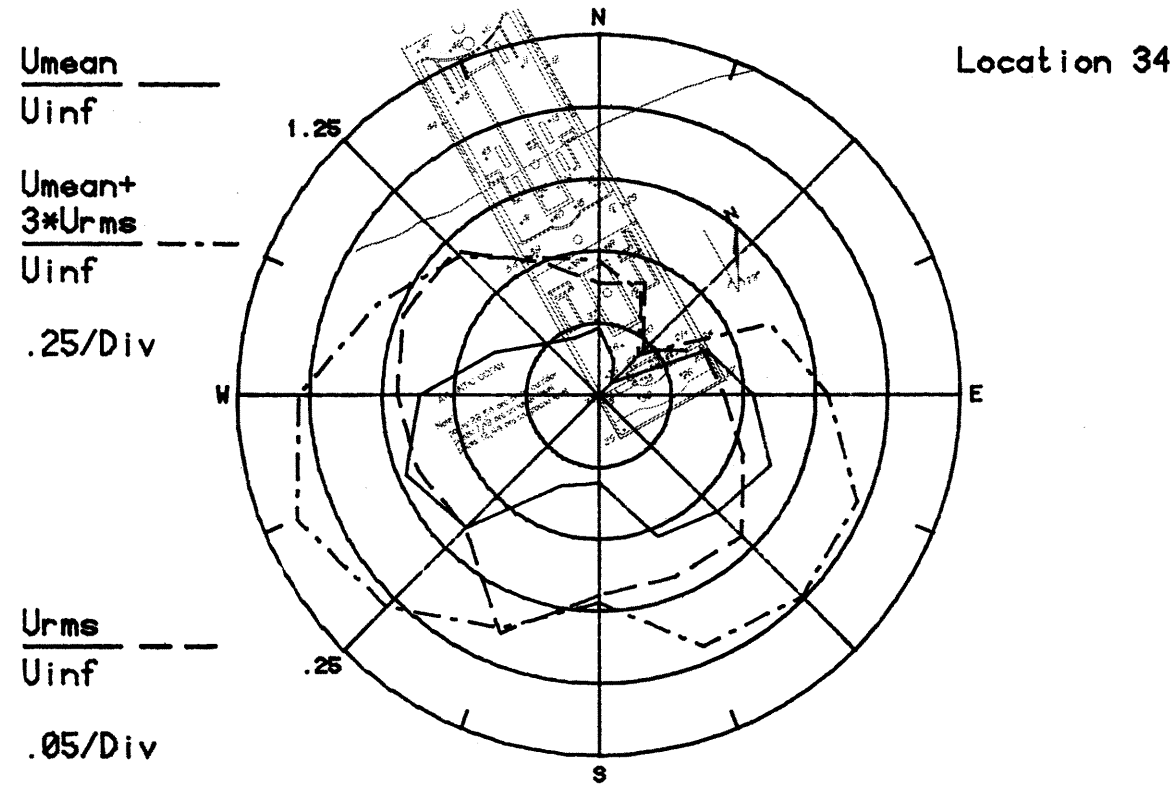


Figure 8q. Mean Velocities and Turbulence Intensities at Pedestrian Locations 33 and 34

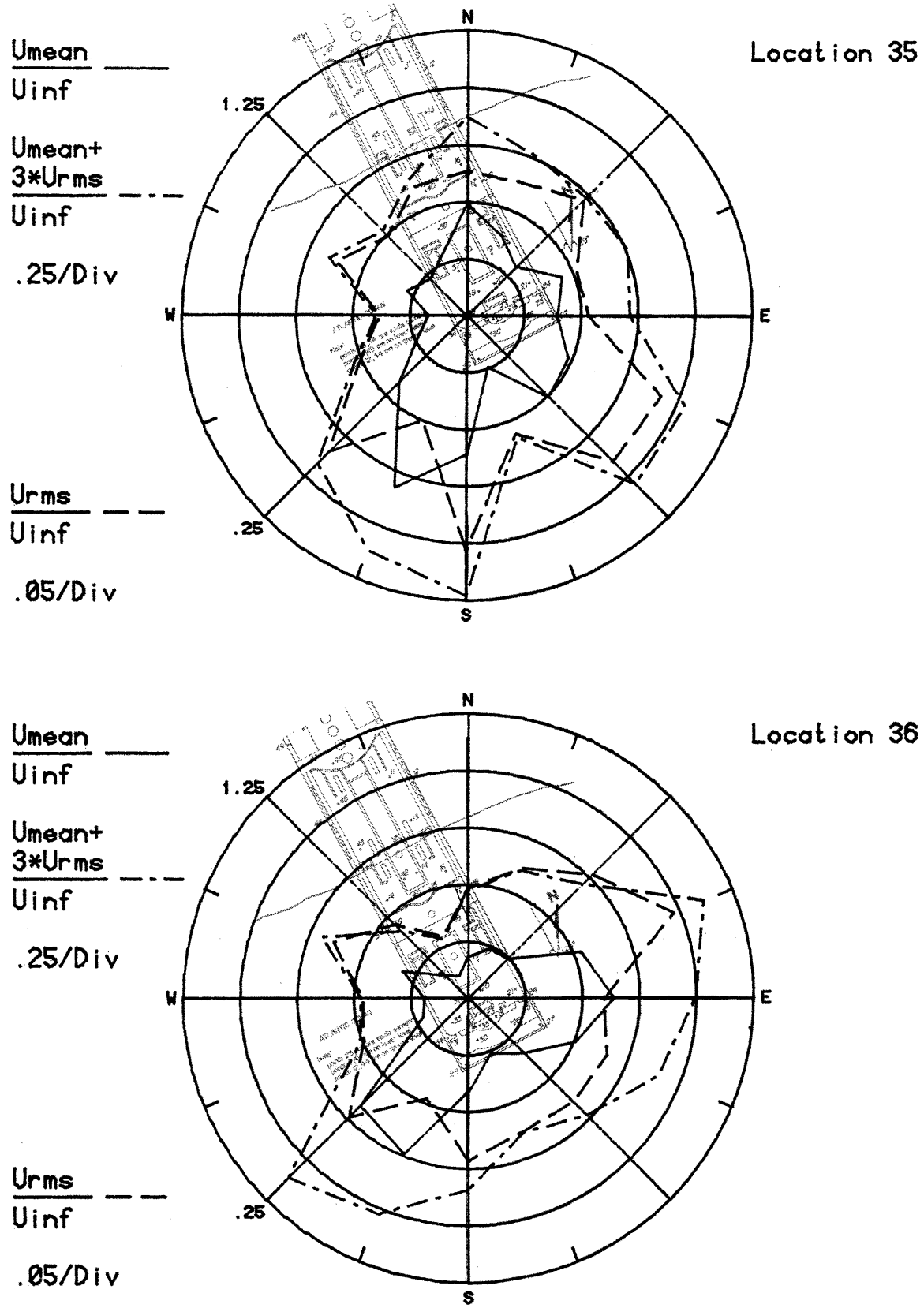


Figure 8r. Mean Velocities and Turbulence Intensities at Pedestrian Locations 35 and 36

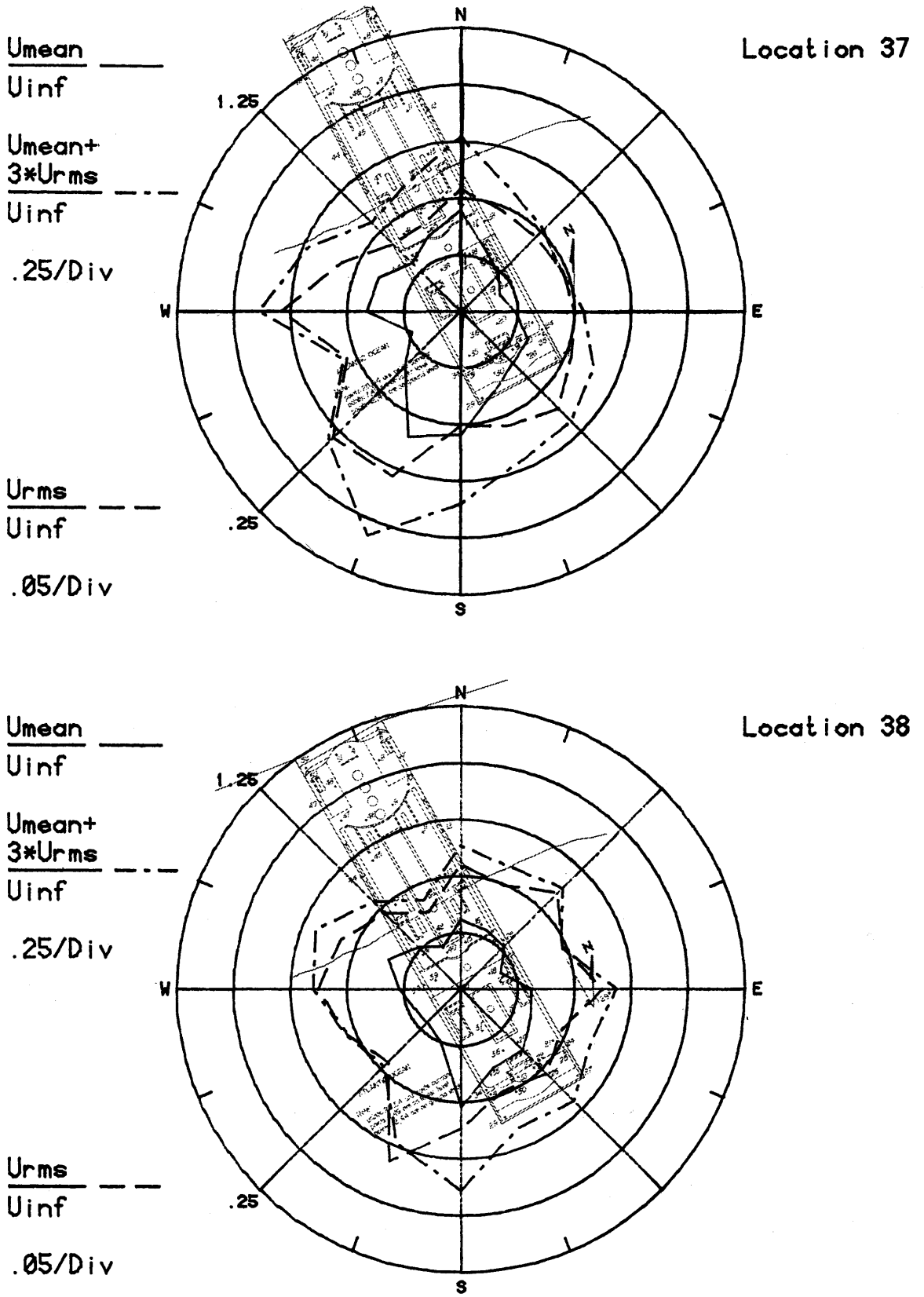


Figure 8s. Mean Velocities and Turbulence Intensities at Pedestrian Locations 37 and 38

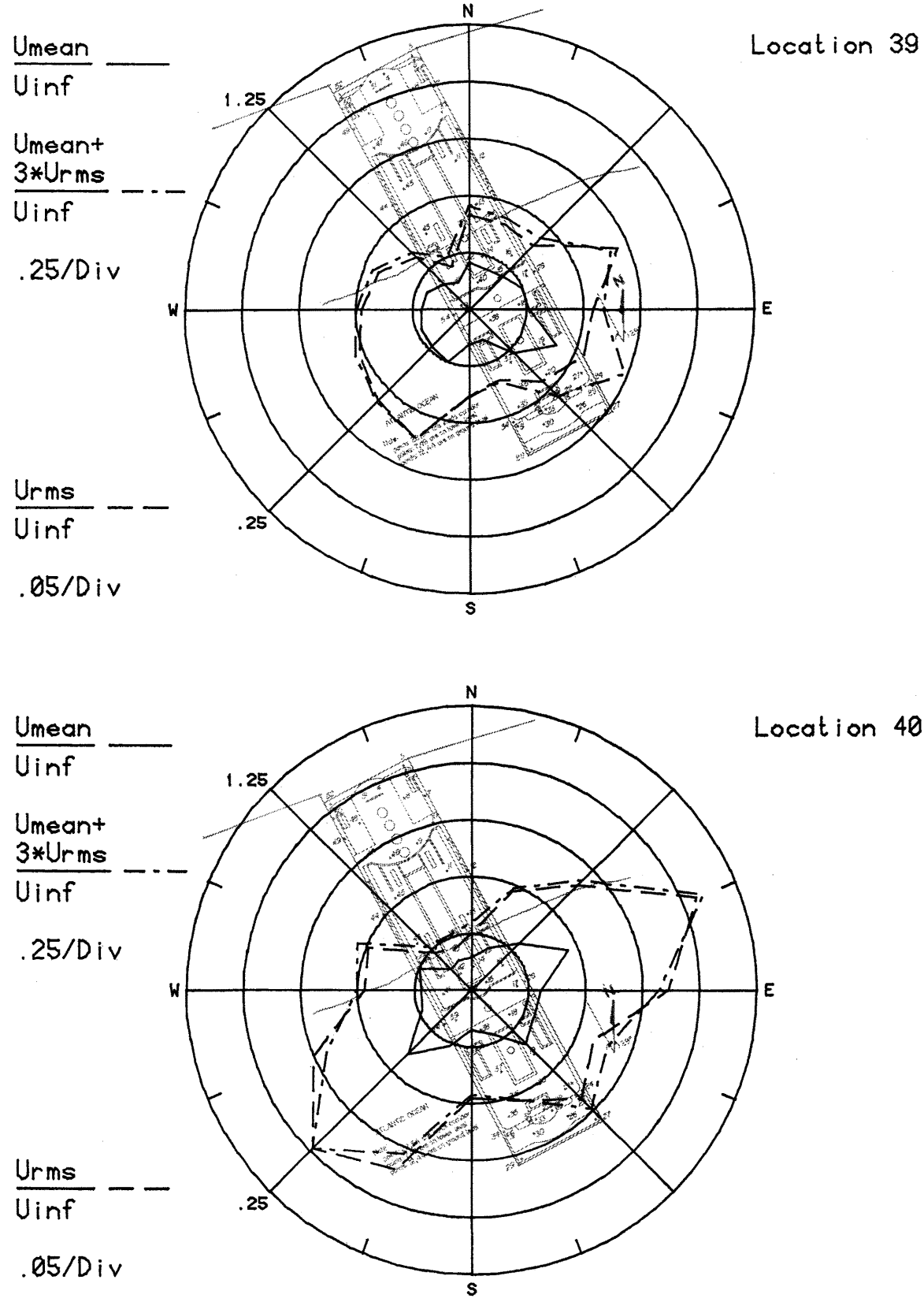
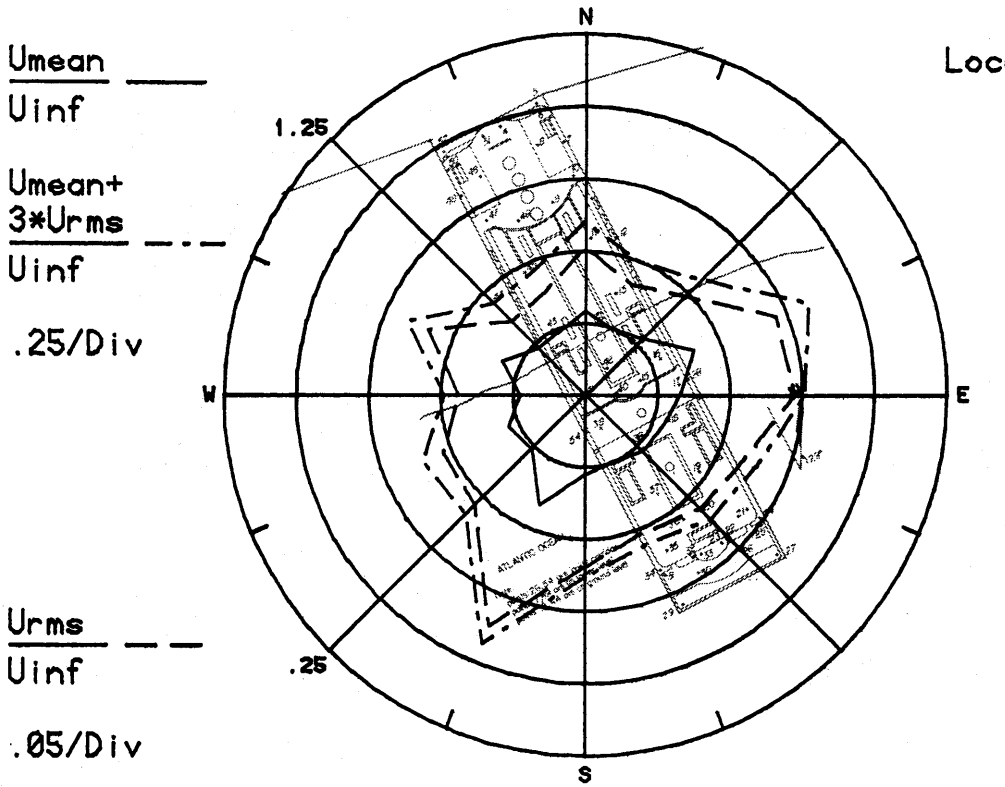


Figure 8t. Mean Velocities and Turbulence Intensities at Pedestrian Locations 39 and 40



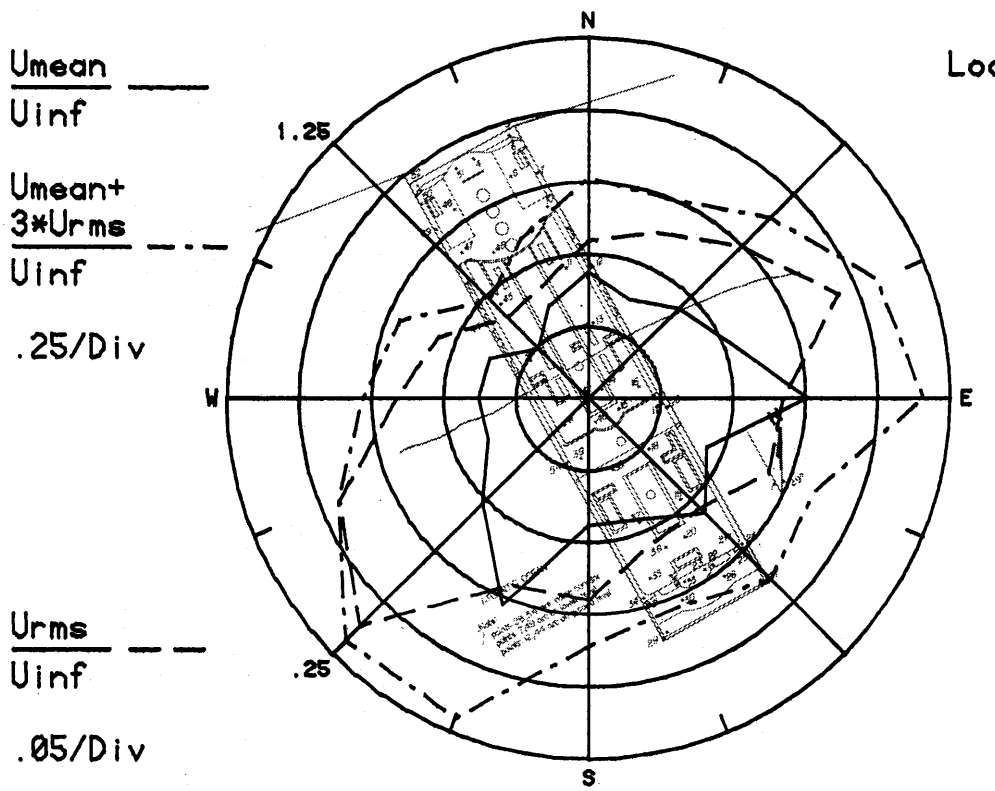


Figure 8u. Mean Velocities and Turbulence Intensities at Pedestrian Locations 41 and 42

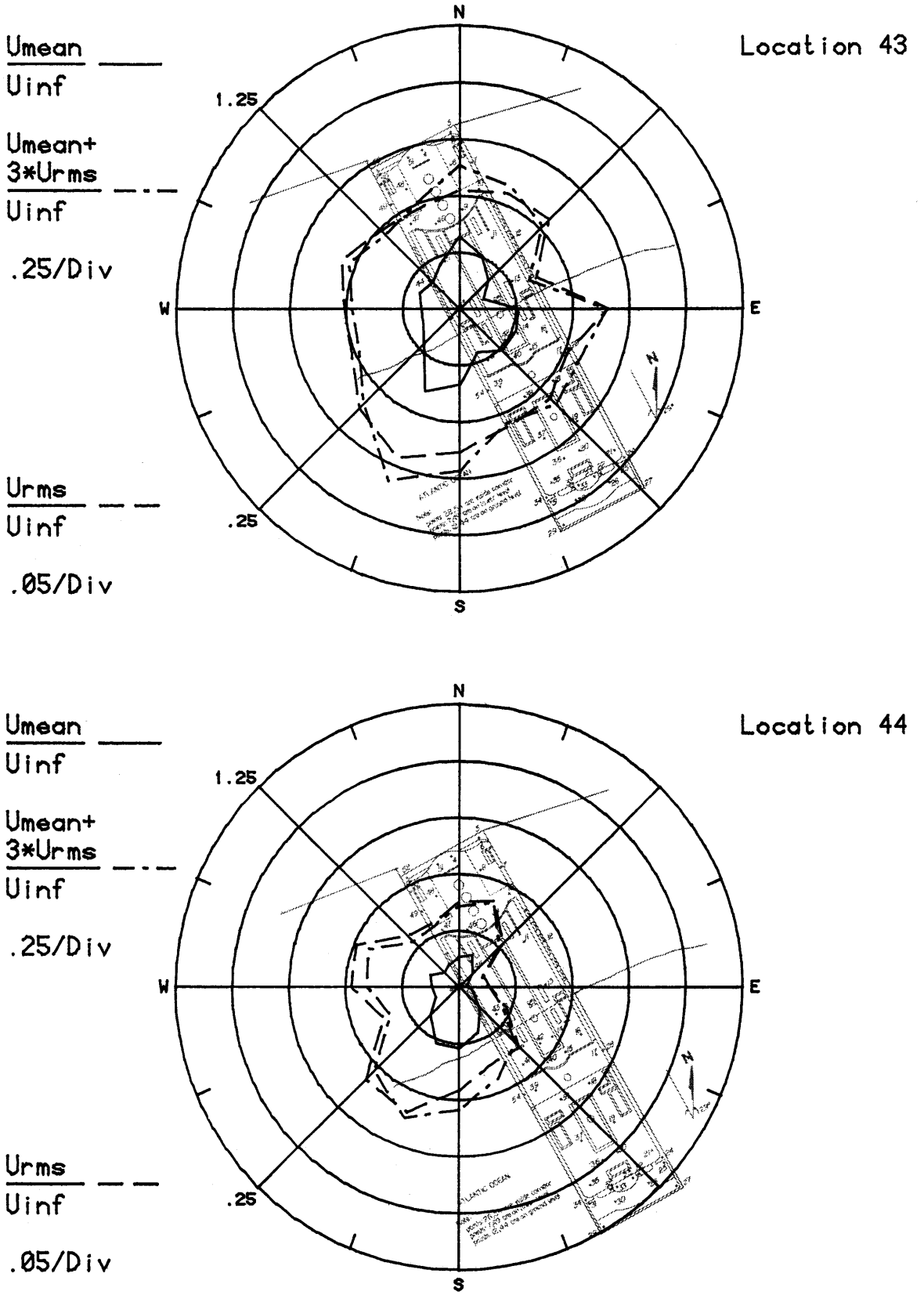


Figure 8v. Mean Velocities and Turbulence Intensities at Pedestrian Locations 43 and 44

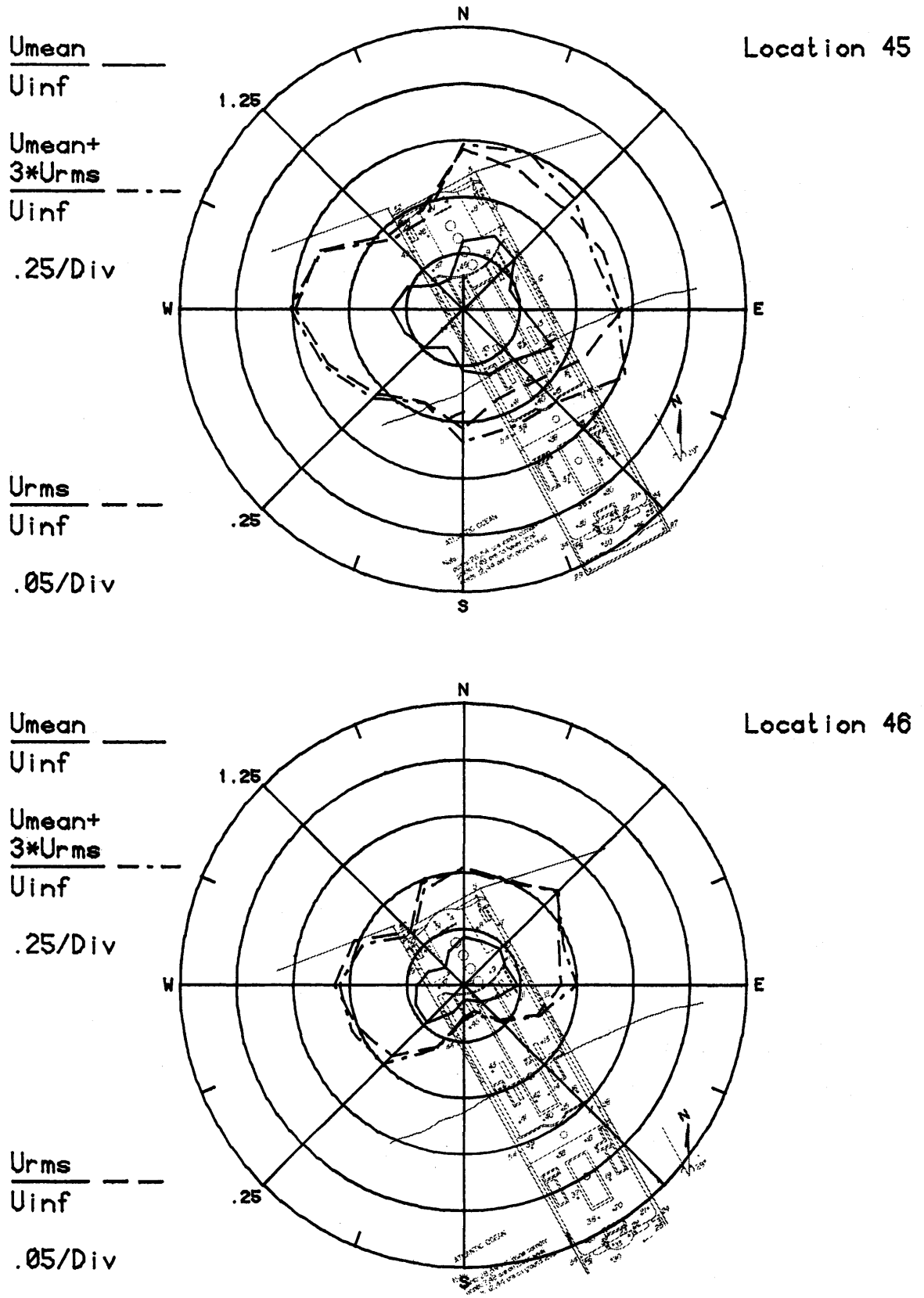
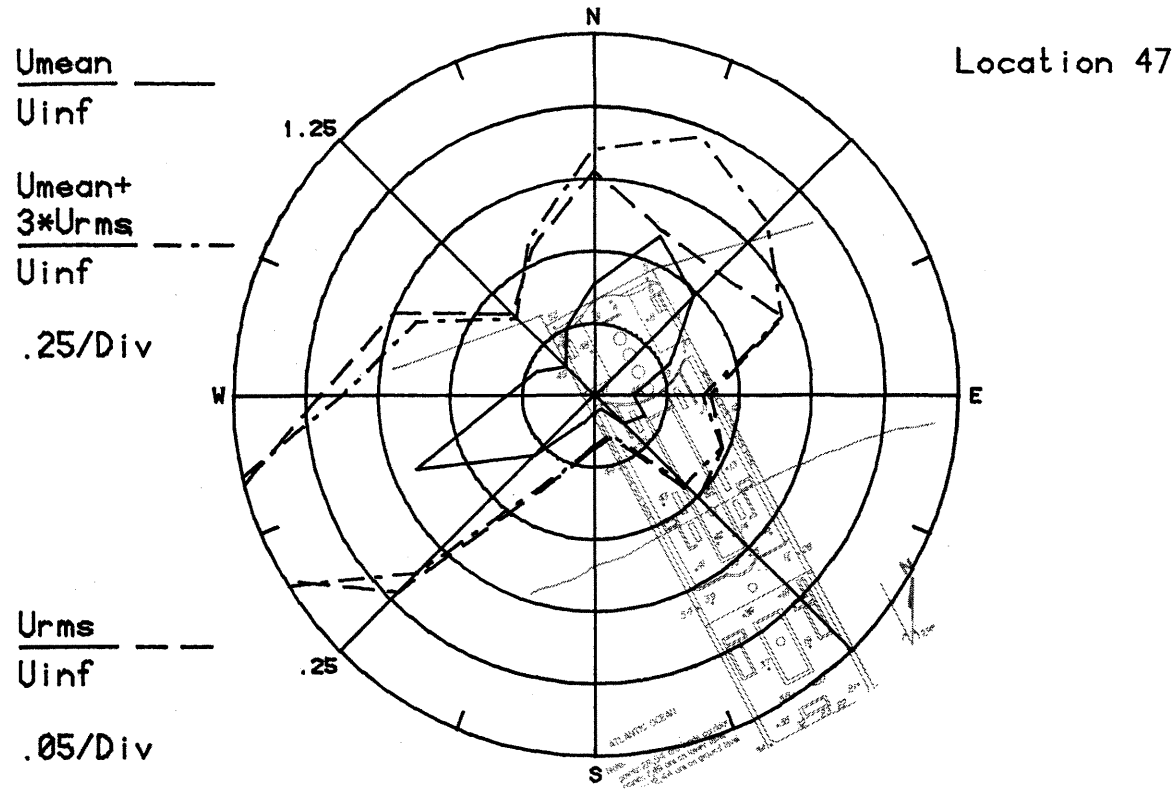


Figure 8w. Mean Velocities and Turbulence Intensities at Pedestrian Locations 45 and 46



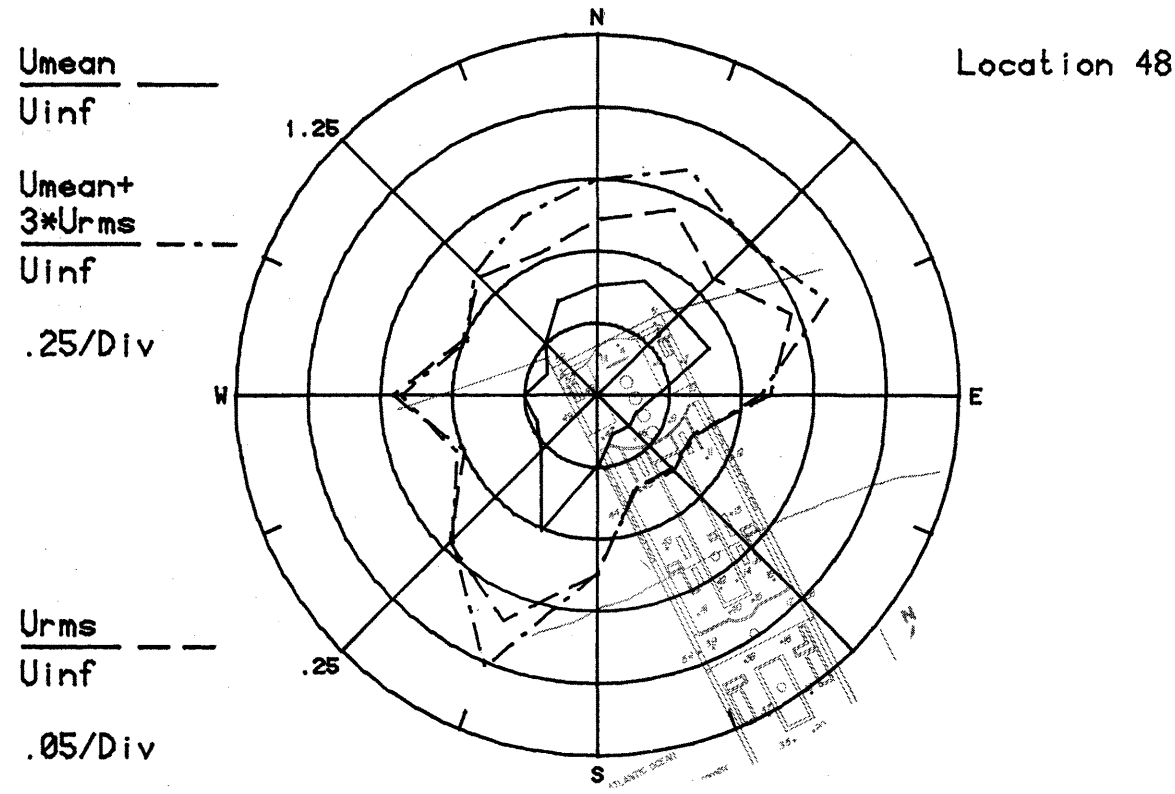


Figure 8x. Mean Velocities and Turbulence Intensities at Pedestrian Locations 47 and 48

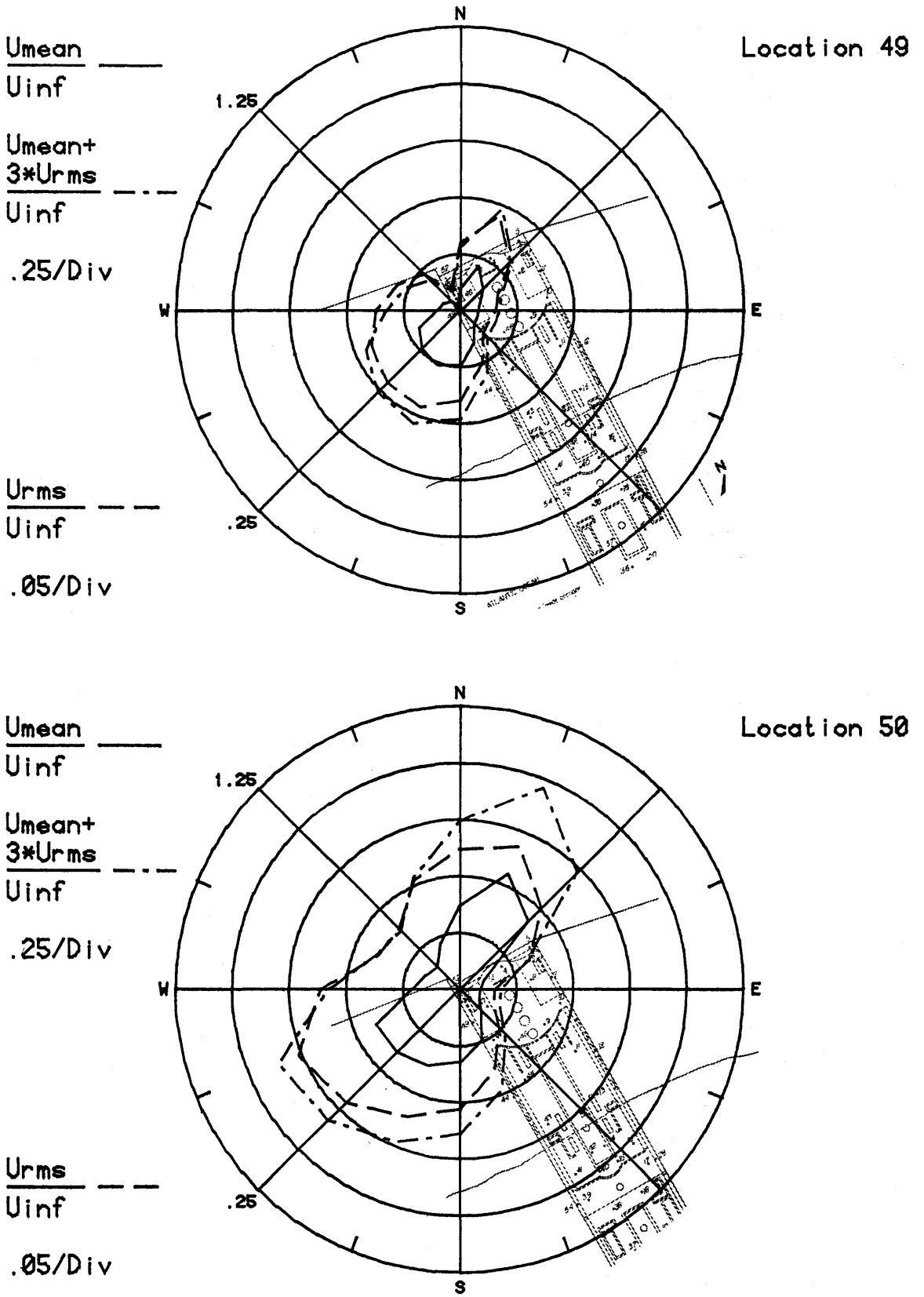


Figure 8y. Mean Velocities and Turbulence Intensities at Pedestrian Locations 49 and 50

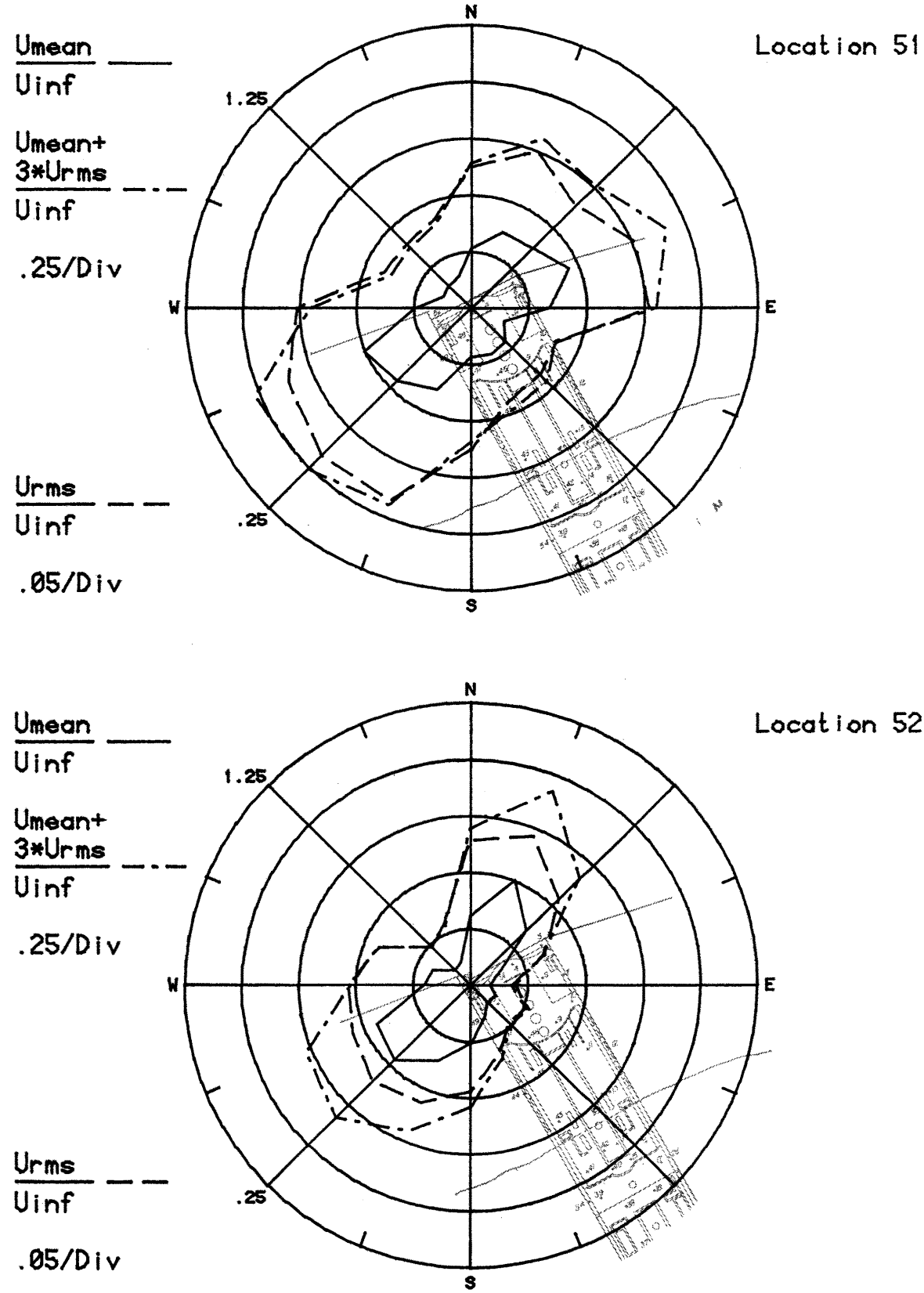


Figure 8z. Mean Velocities and Turbulence Intensities at Pedestrian Locations 51 and 52

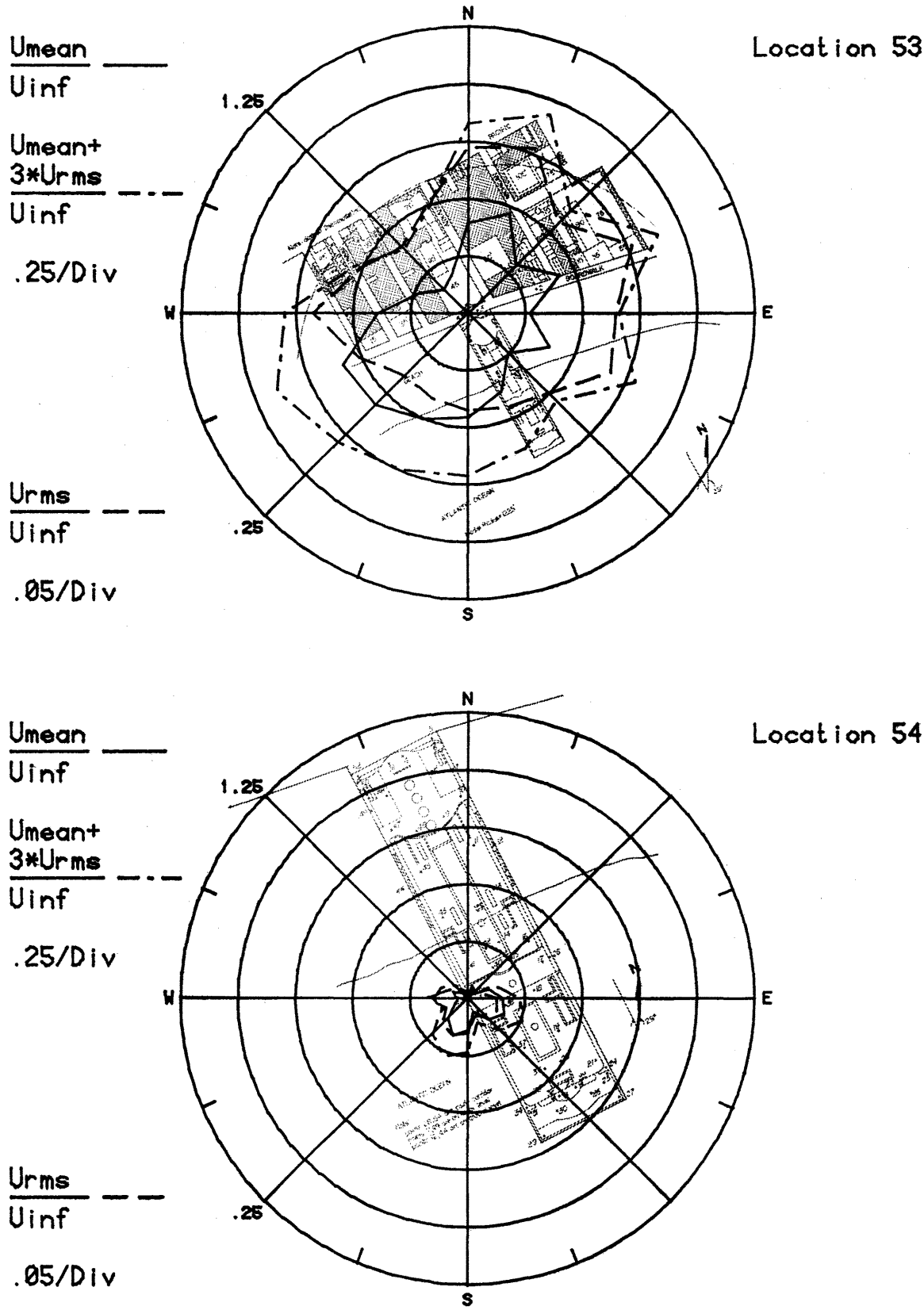


Figure 8#. Mean Velocities and Turbulence Intensities at Pedestrian Locations 53 and 54

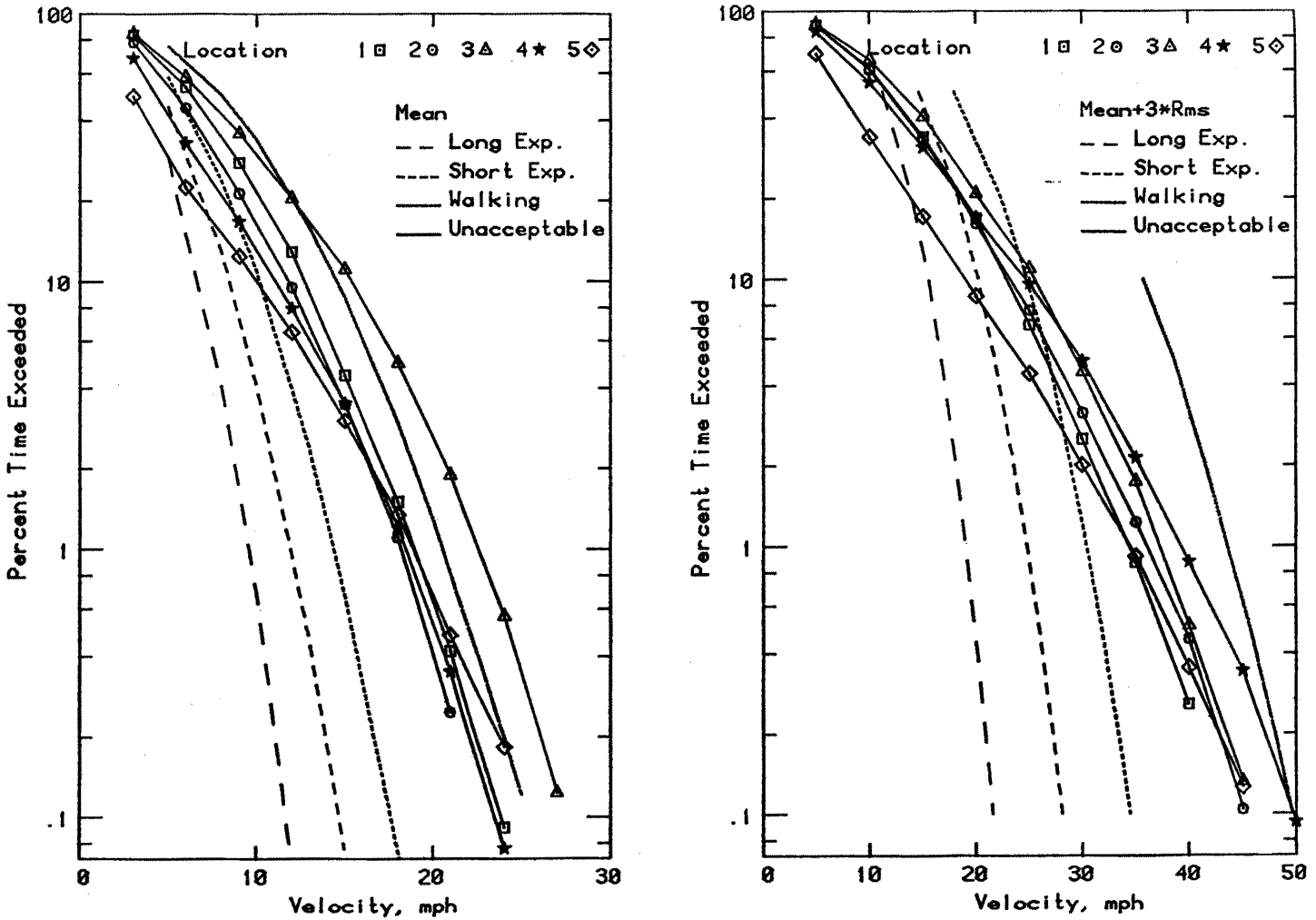


Figure 9a. Wind Velocity Probabilities for Pedestrian Locations

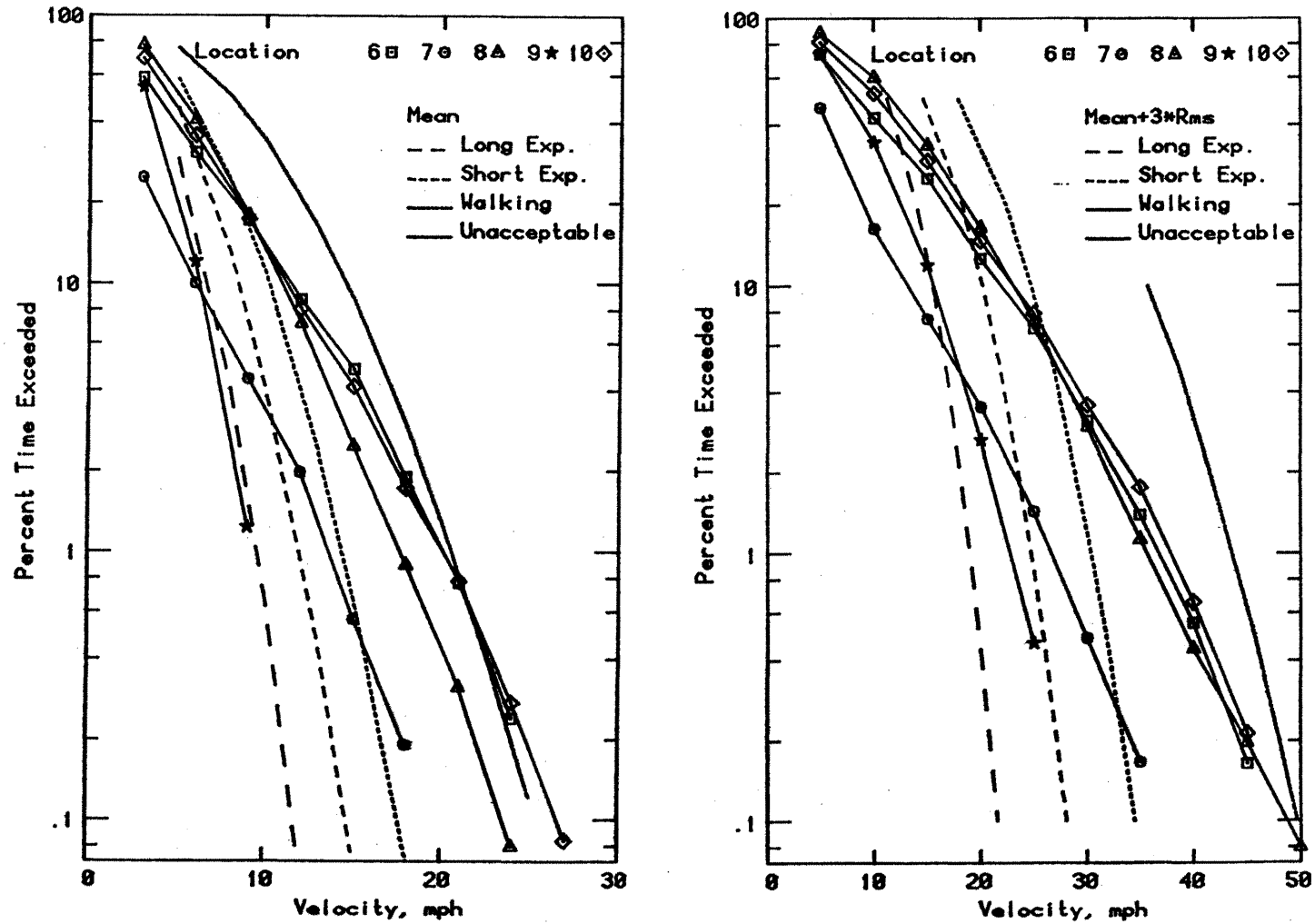


Figure 9b. Wind Velocity Probabilities for Pedestrian Locations

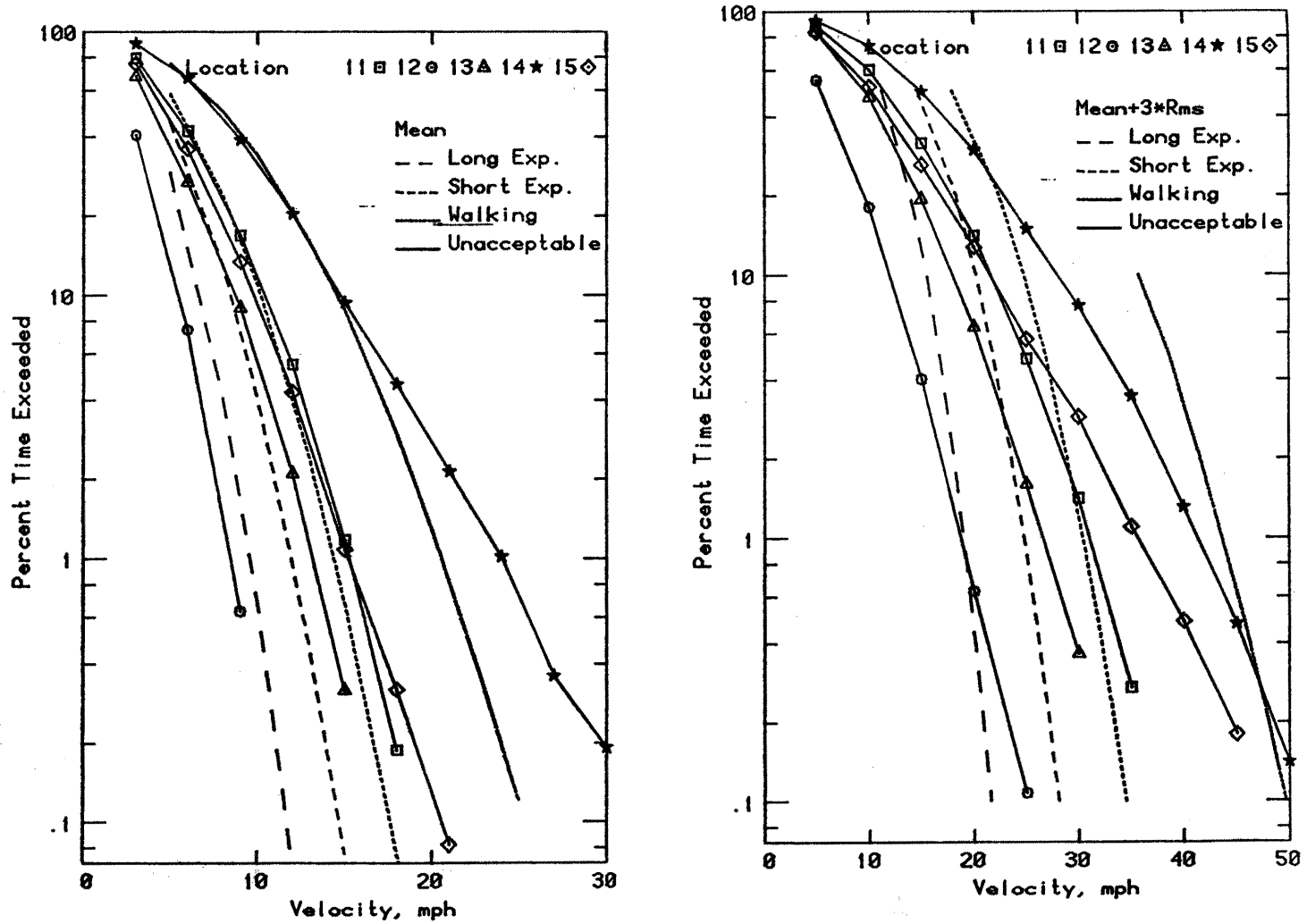


Figure 9c. Wind Velocity Probabilities
for Pedestrian Locations

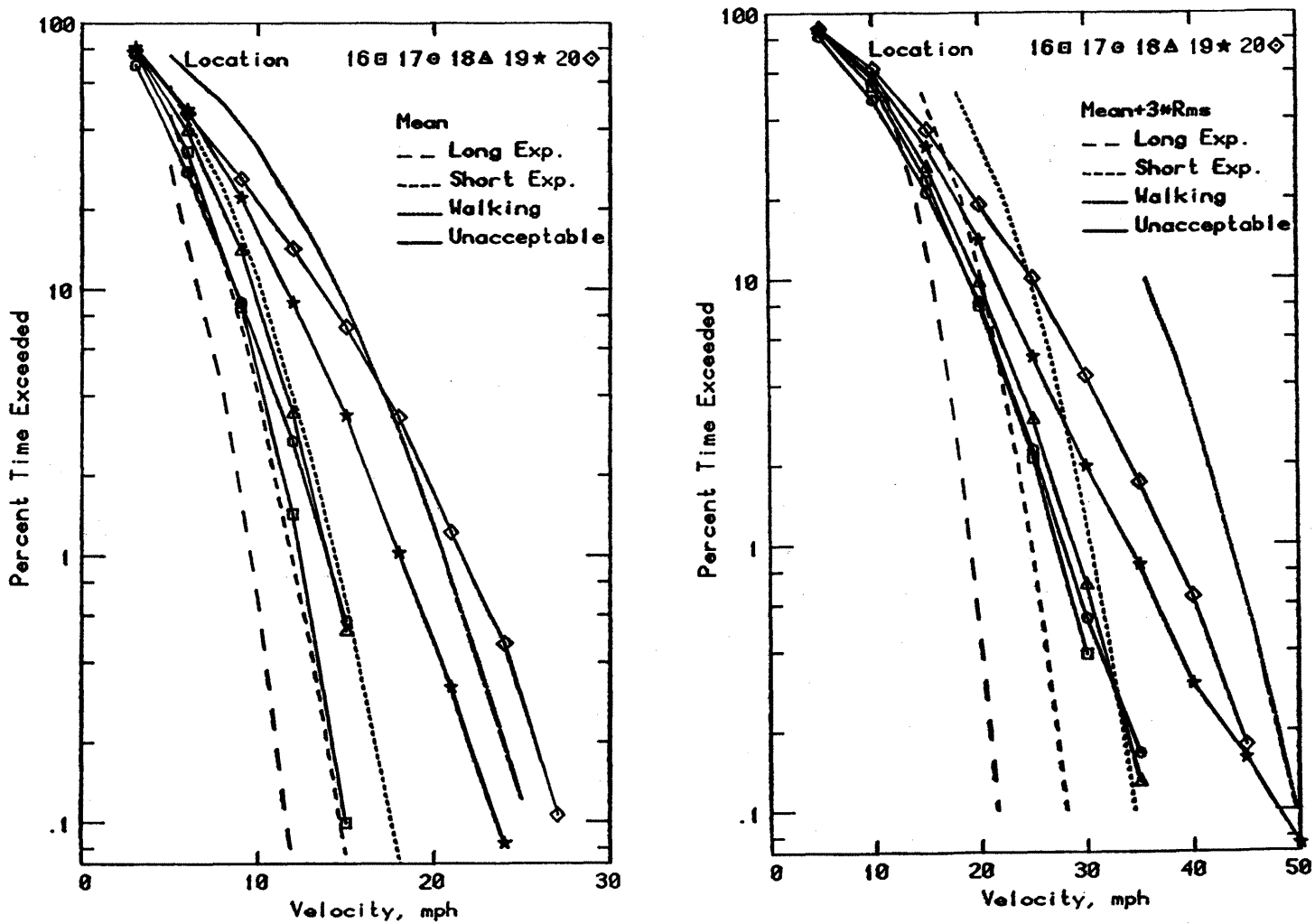


Figure 9d. Wind Velocity Probabilities for Pedestrian Locations

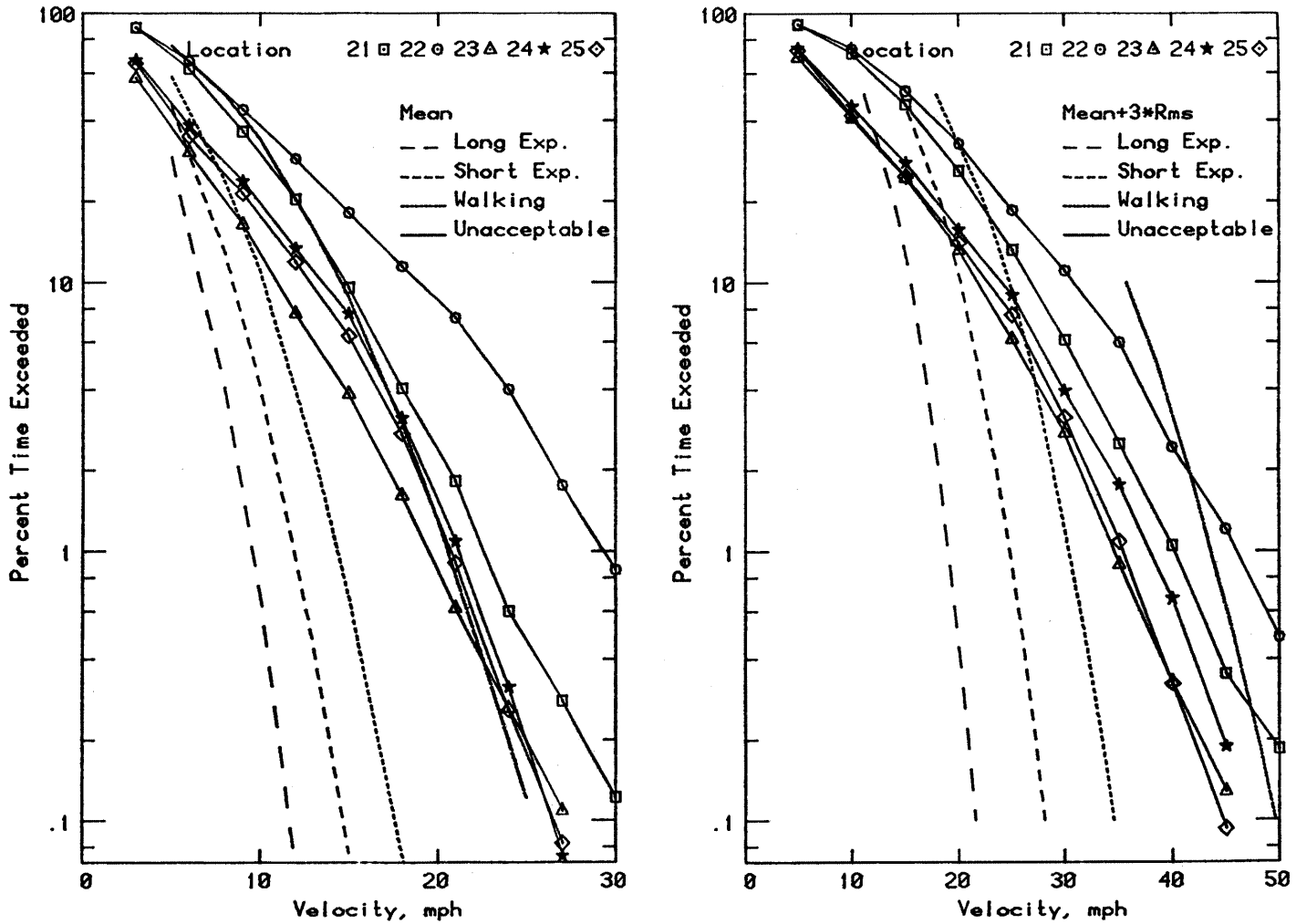


Figure 9e. Wind Velocity Probabilities
for Pedestrian Locations

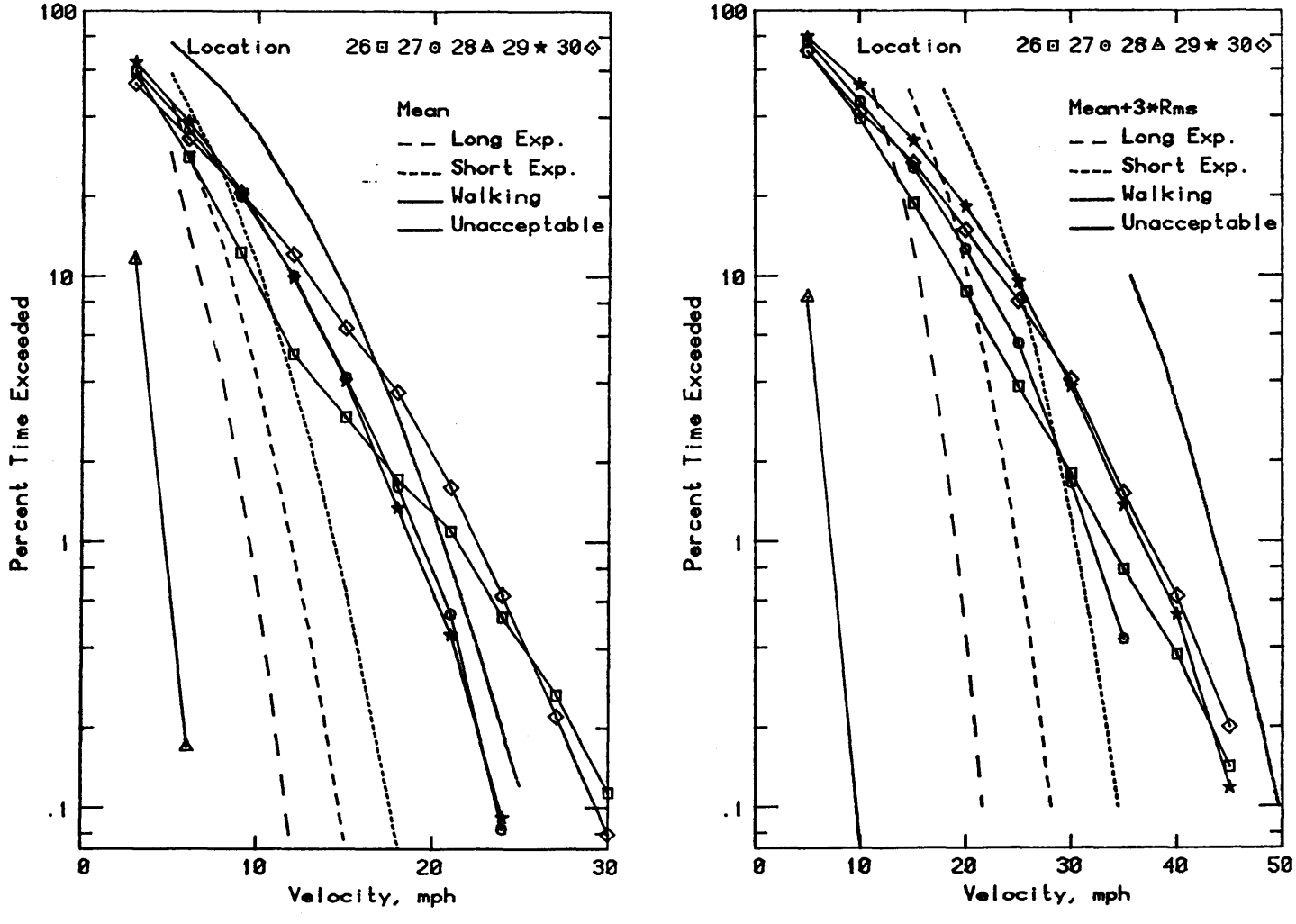


Figure 9f. Wind Velocity Probabilities
for Pedestrian Locations

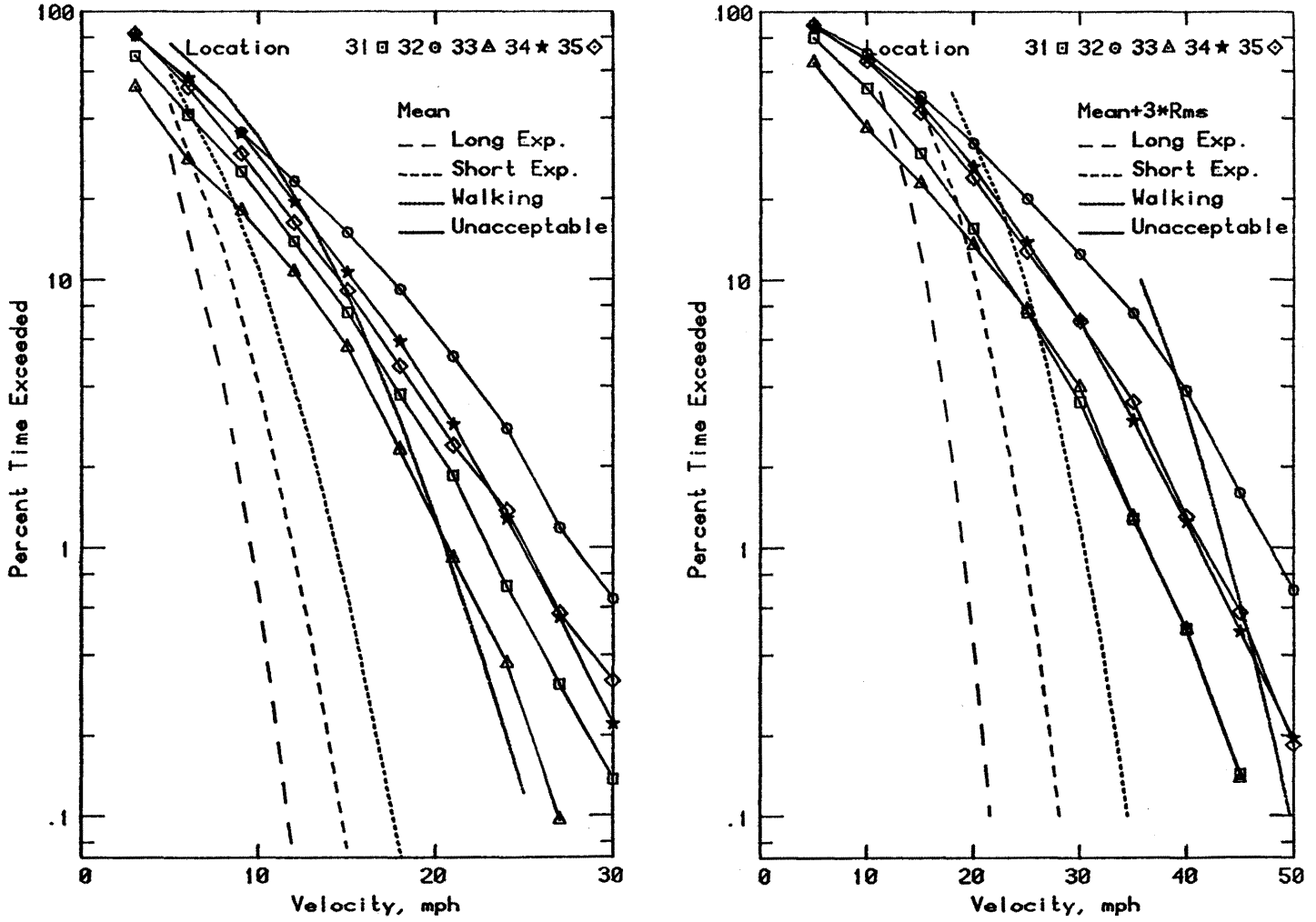


Figure 9g. Wind Velocity Probabilities for Pedestrian Locations

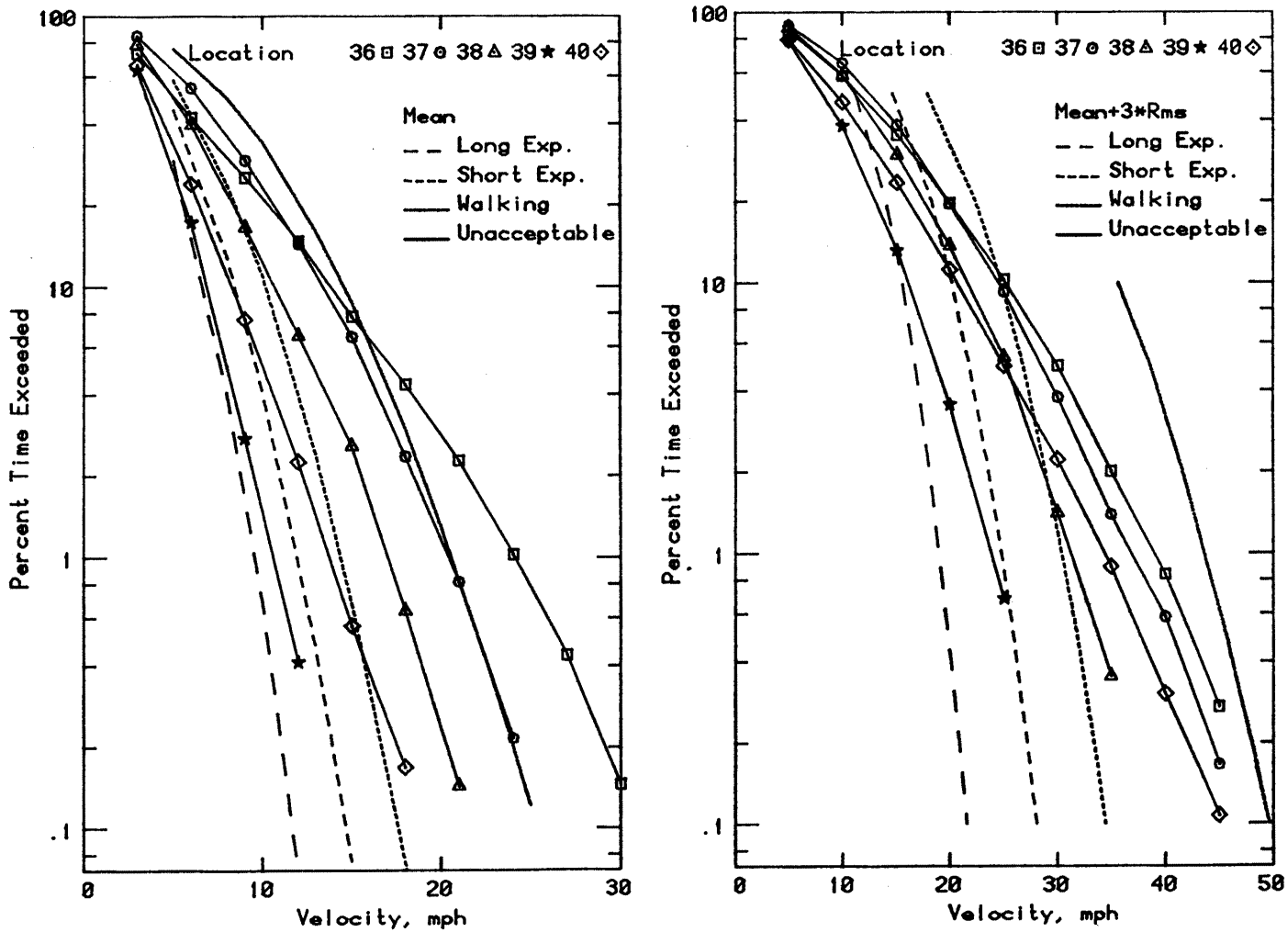


Figure 9h. Wind Velocity Probabilities
for Pedestrian Locations

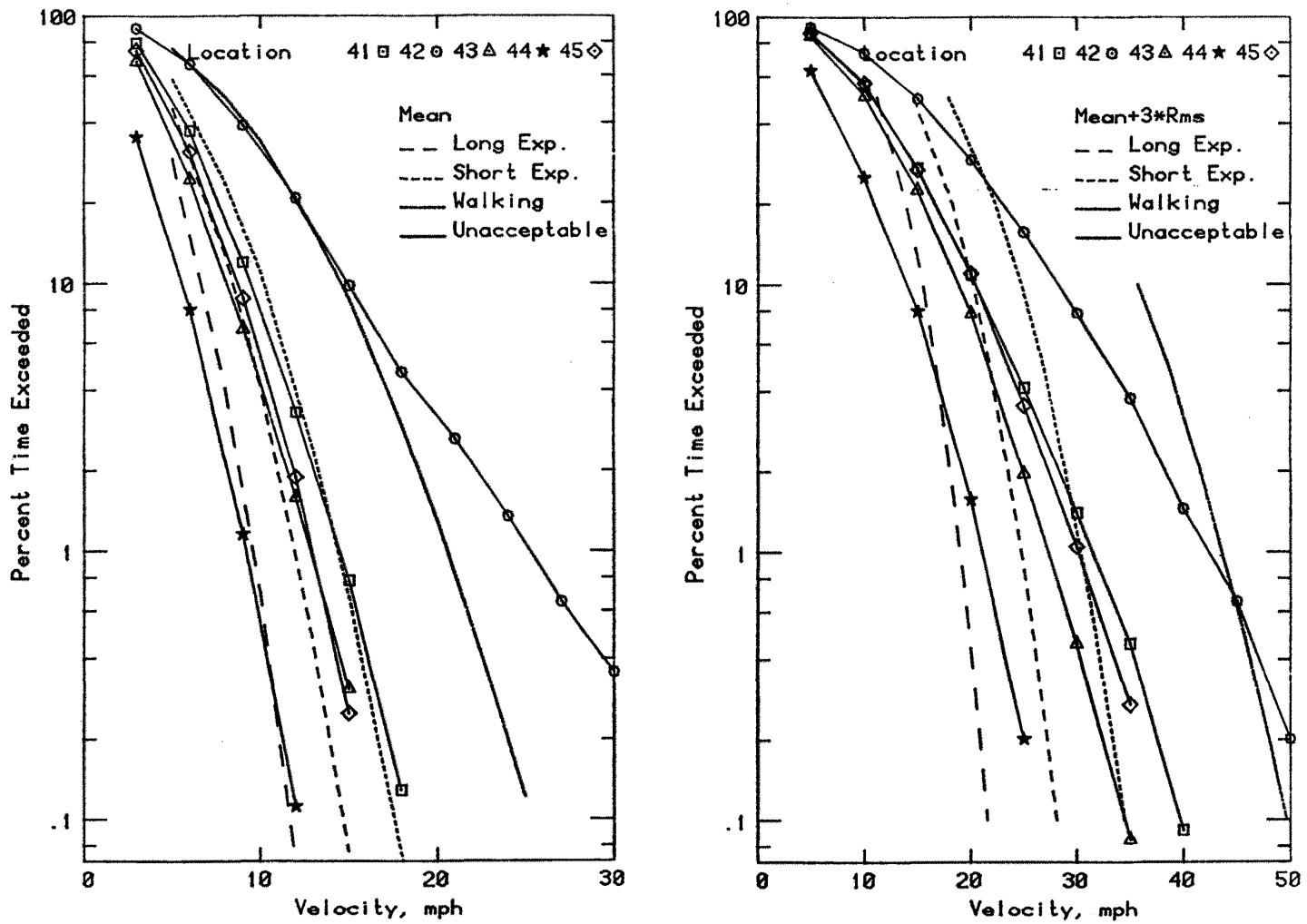


Figure 9i. Wind Velocity Probabilities
for Pedestrian Locations

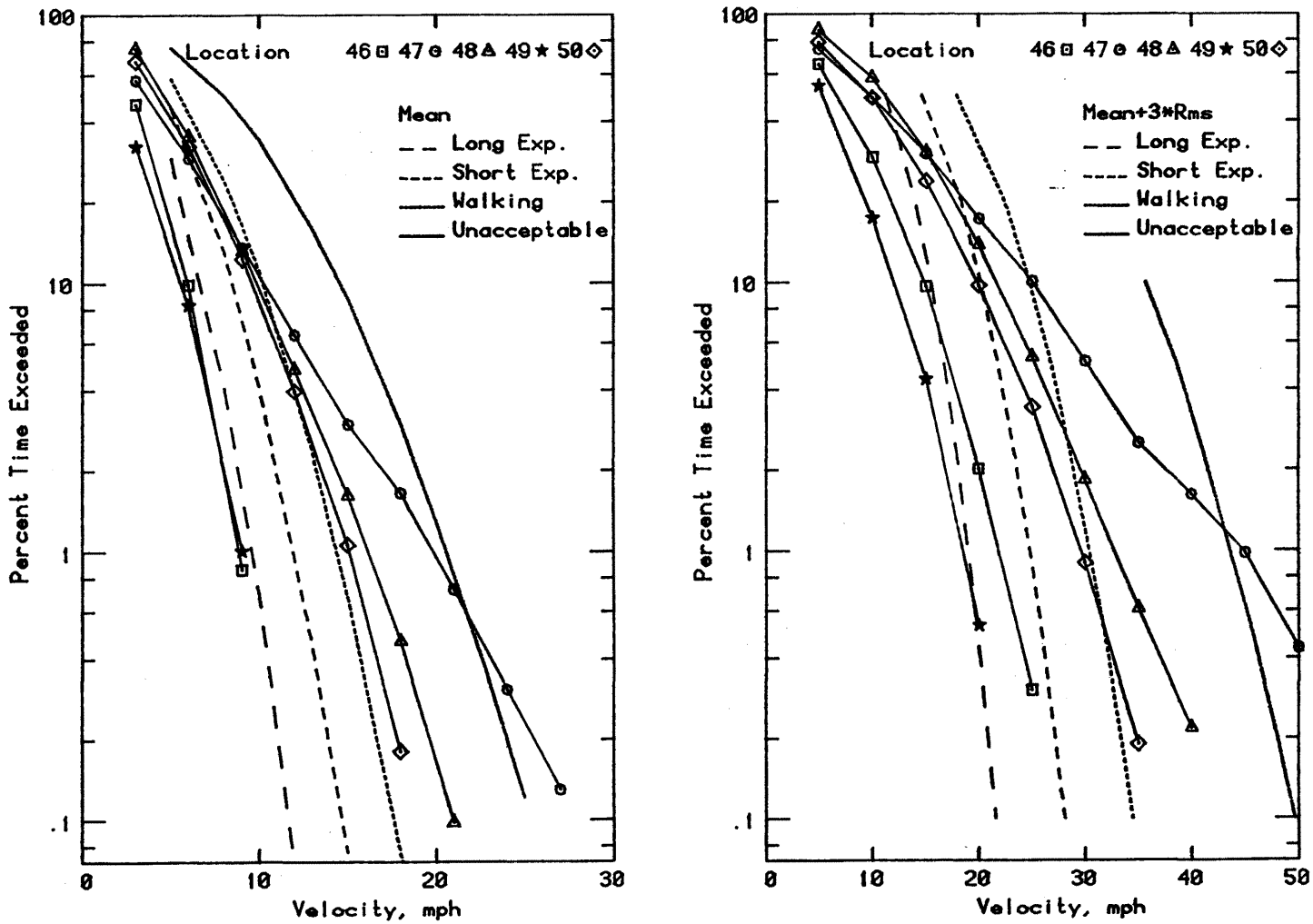


Figure 9j. Wind Velocity Probabilities for Pedestrian Locations

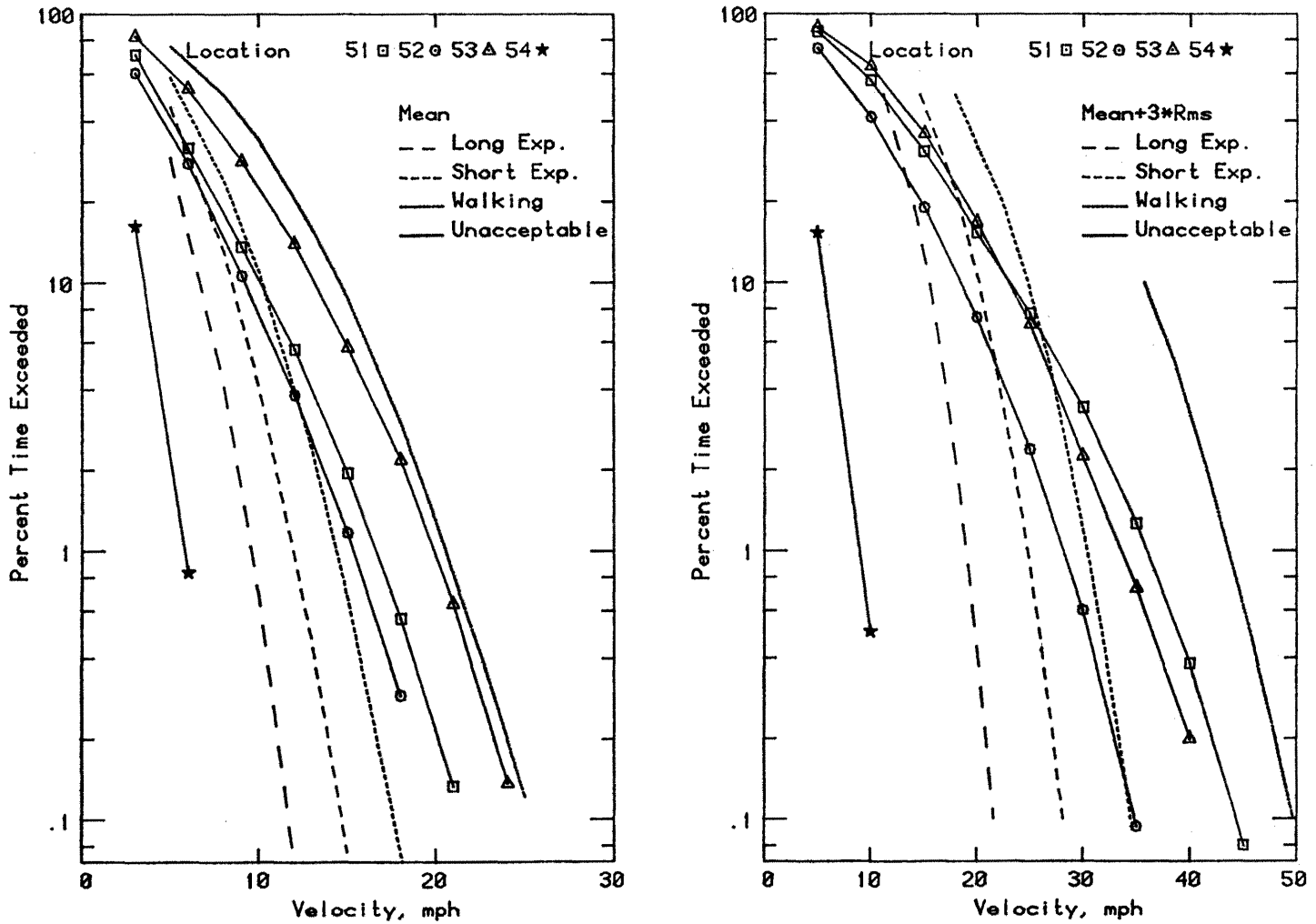


Figure 9k. Wind Velocity Probabilities
for Pedestrian Locations

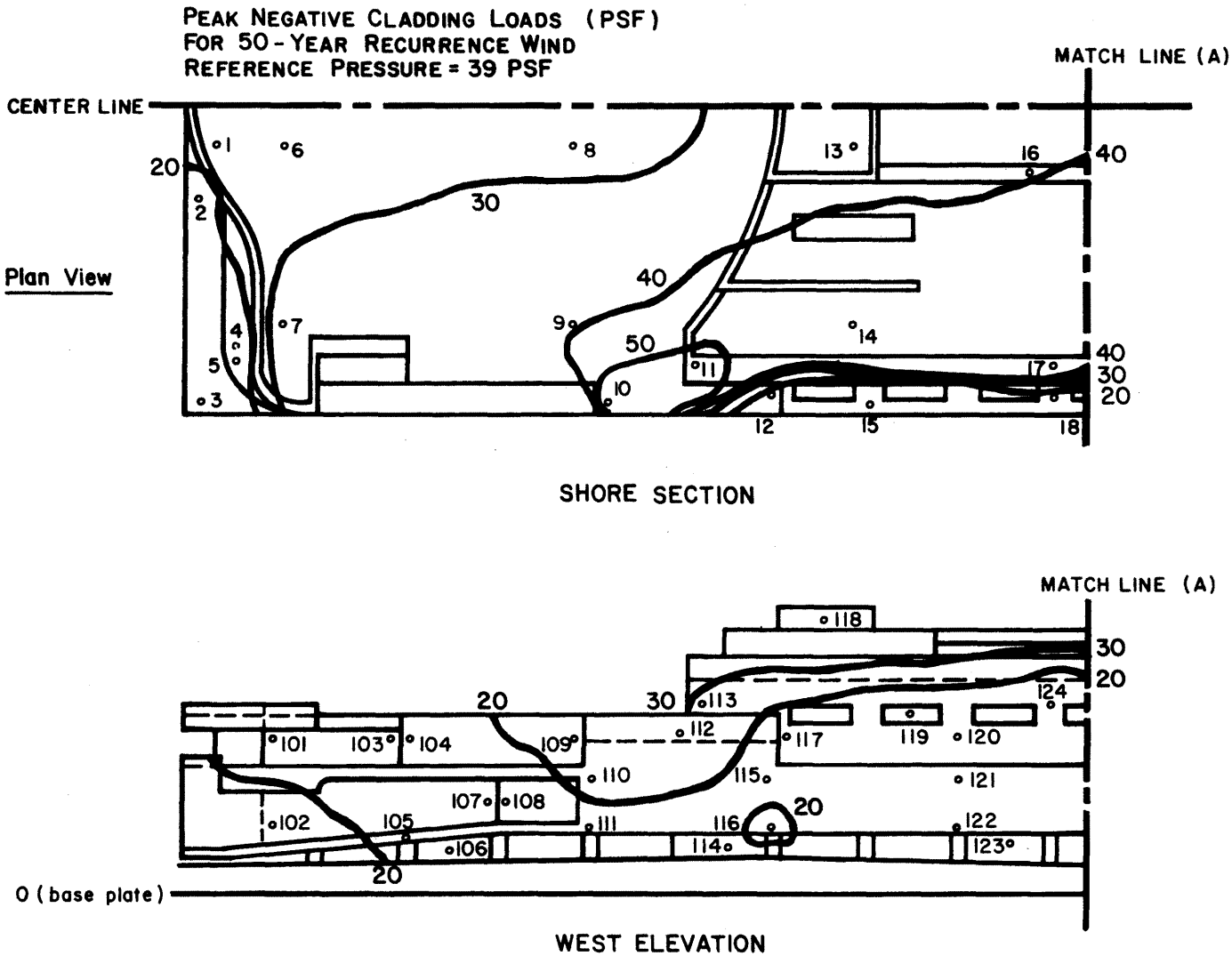


Figure 10a. Peak Pressure Contours on the Building for Cladding Loads

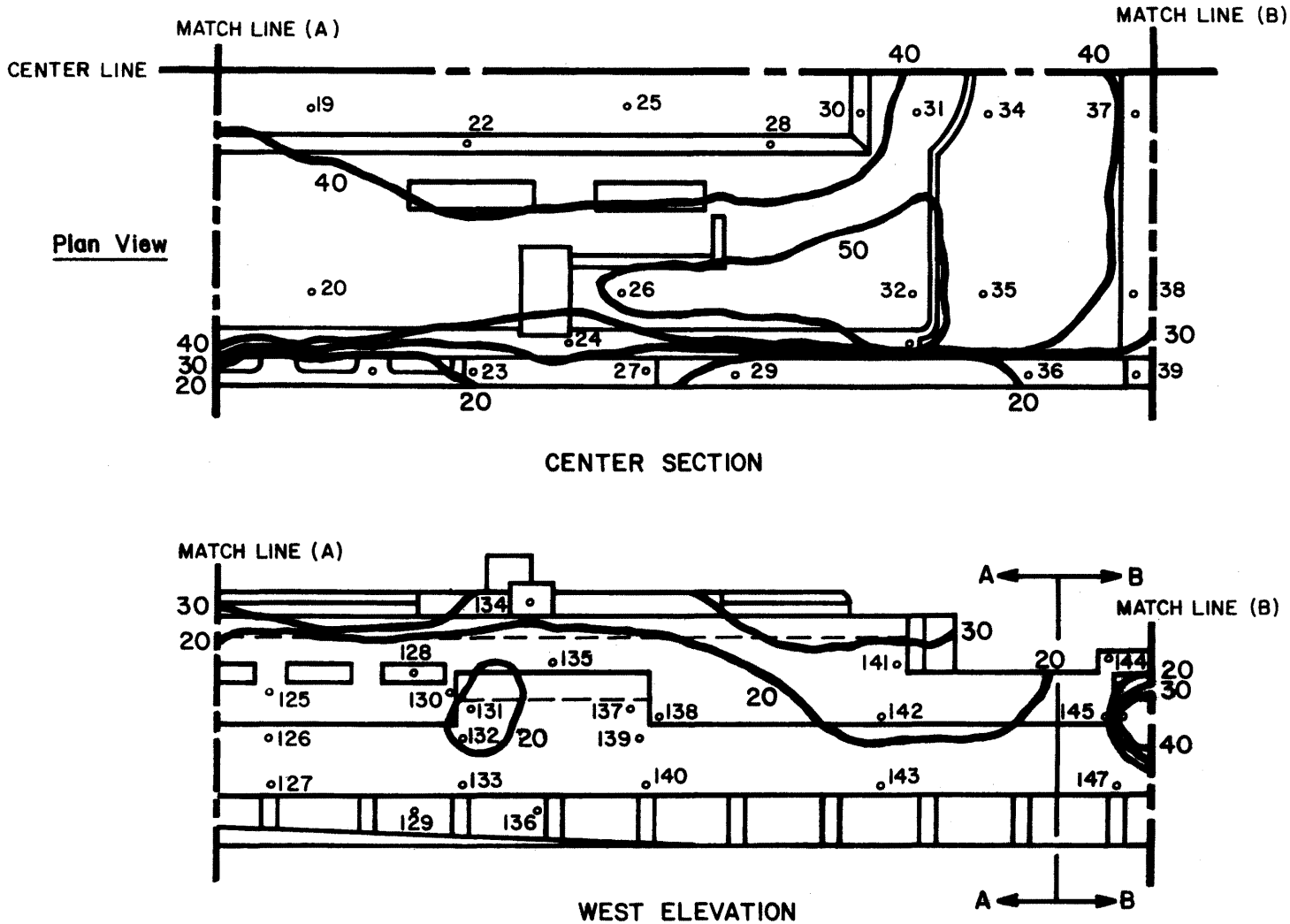


Figure 10b. Peak Pressure Contours on the Building for Cladding Loads

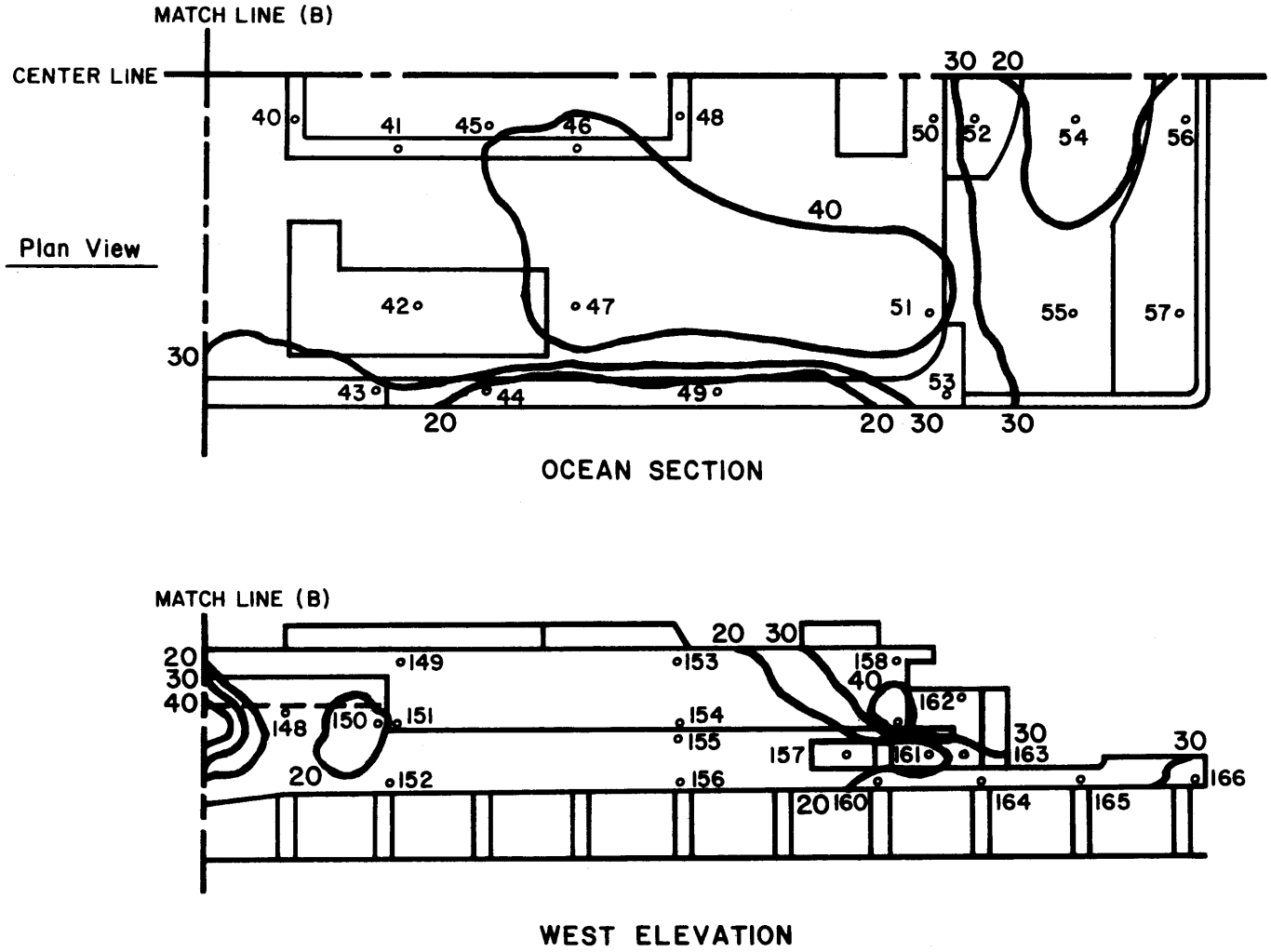


Figure 10c. Peak Pressure Contours on the Building for Cladding Loads

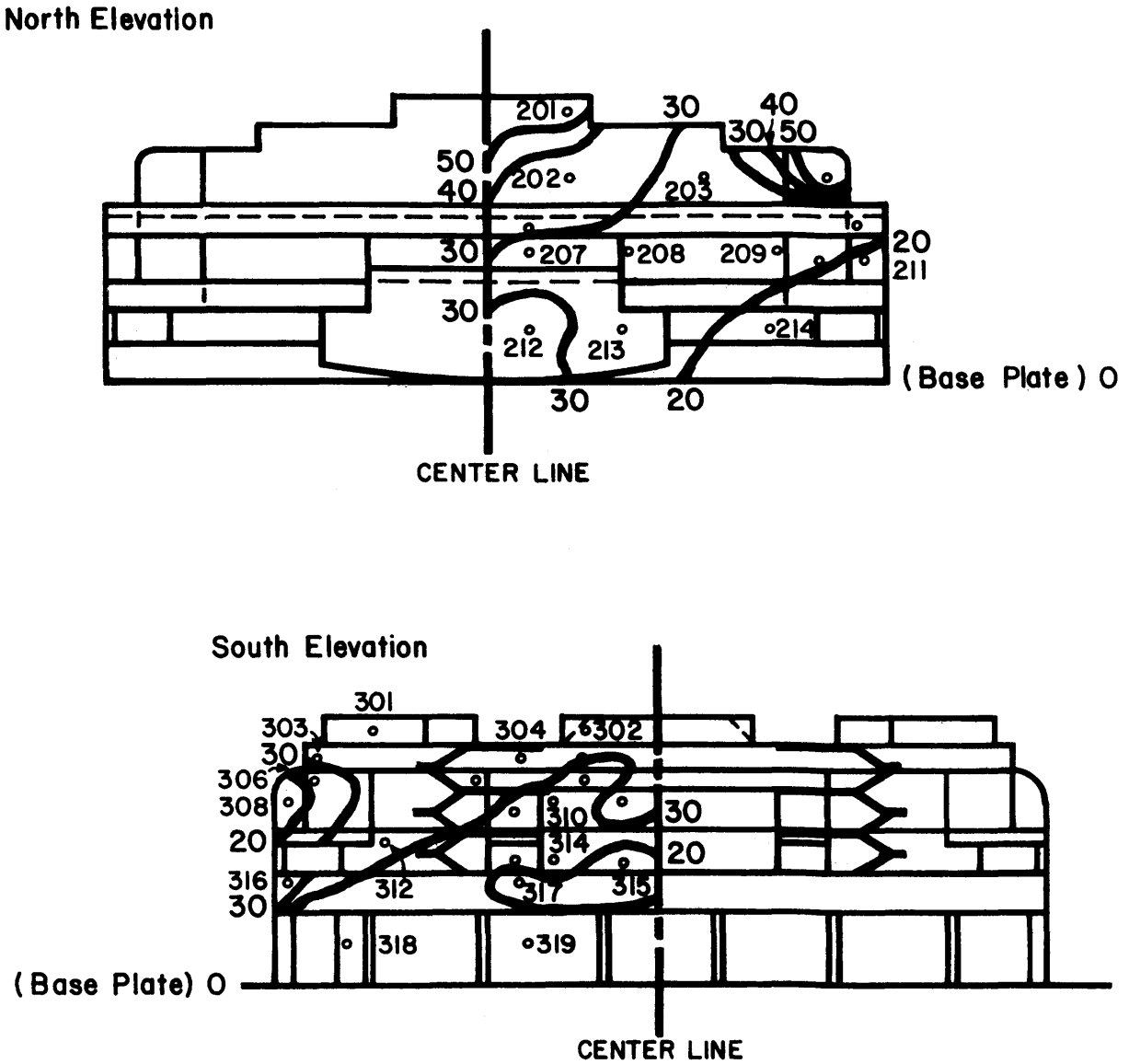
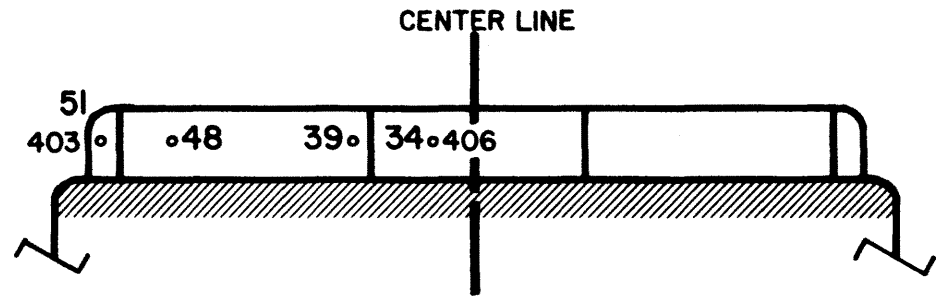
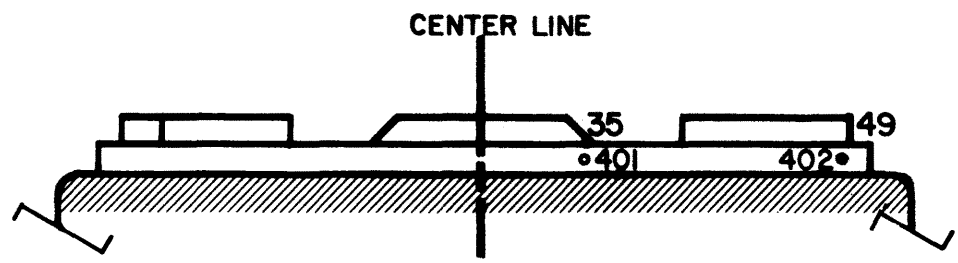


Figure 10d. Peak Pressure Contours on the Building for Cladding Loads



SECTION A-A



SECTION B-B

Figure 10e. Peak-Pressure Contours on the Building for Cladding Loads

TABLES

TABLE 1

MOTION PICTURE SCENE GUIDE

1. Introduction
2. Purposes for model testing
3. Procedures for conducting tests
4. Specific flow visualization scenes for Million Dollar Pier

Peak Pressure Areas

RUN	TAP	AZIMUTH
1	33	230°
2	33,204	240°
3	204	250°

High Pedestrian Wind Velocities

RUN	PEDESTRIAN LOCATION	AZIMUTH
4	14,22	90°
5	32,35	202.5°

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 1

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	18.4	8.5	43.8
22.50	35.5	13.2	75.0
45.00	35.3	10.8	67.7
67.50	45.5	10.4	76.7
90.00	46.4	9.0	73.4
112.50	43.2	8.7	69.4
135.00	45.7	8.3	70.6
157.50	43.7	8.5	69.1
180.00	39.5	8.8	65.9
202.50	42.7	11.3	76.4
225.00	22.6	9.8	52.0
247.50	39.1	14.6	82.7
270.00	48.3	12.7	86.5
292.50	38.5	12.1	74.9
315.00	26.8	9.1	54.2
337.50	18.1	8.6	43.9

LOCATION 2

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	17.1	10.4	48.3
22.50	12.5	9.5	41.1
45.00	19.8	12.5	57.3
67.50	46.9	14.2	89.6
90.00	44.5	11.1	77.7
112.50	51.3	7.7	74.4
135.00	43.3	7.5	65.7
157.50	36.7	8.6	62.5
180.00	30.1	9.9	59.9
202.50	21.4	9.3	49.4
225.00	31.5	13.1	70.7
247.50	28.8	14.1	71.1
270.00	42.4	15.4	88.6
292.50	41.1	14.0	83.0
315.00	31.9	11.3	65.7
337.50	18.7	10.8	51.0

LOCATION 3

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.9	9.8	60.4
22.50	39.9	12.2	76.6
45.00	36.5	10.2	67.0
67.50	56.3	8.7	82.4
90.00	50.6	8.5	76.1
112.50	45.1	8.3	70.1
135.00	32.4	10.2	63.0
157.50	47.6	11.2	81.2
180.00	56.7	12.6	94.6
202.50	55.3	12.3	92.1
225.00	58.3	11.4	92.6
247.50	63.9	11.3	97.8
270.00	47.0	13.6	87.9
292.50	17.7	10.4	49.1
315.00	19.6	9.0	46.7
337.50	23.5	8.1	47.8

LOCATION 4

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	20.1	10.6	51.9
22.50	22.9	12.5	60.2
45.00	35.5	14.1	77.7
67.50	48.0	17.7	101.2
90.00	39.3	16.9	89.8
112.50	28.1	15.5	74.7
135.00	14.9	7.4	37.0
157.50	24.7	10.4	55.9
180.00	15.3	7.7	38.5
202.50	34.6	16.8	85.1
225.00	48.8	16.1	97.2
247.50	55.8	17.1	107.0
270.00	40.0	18.9	96.7
292.50	16.9	9.8	45.5
315.00	12.7	7.6	35.5
337.50	12.9	7.7	35.9

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 5

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	10.9	7.3	32.8
22.50	14.0	8.9	40.6
45.00	29.3	12.7	67.4
67.50	45.3	11.2	79.0
90.00	39.5	11.3	73.3
112.50	29.6	10.0	59.5
135.00	12.0	5.6	28.7
157.50	12.3	5.1	27.7
180.00	14.3	6.8	34.7
202.50	10.8	4.9	25.4
225.00	8.1	3.4	18.4
247.50	45.5	13.2	85.1
270.00	51.2	13.9	92.9
292.50	15.8	9.0	42.8
315.00	12.9	6.8	33.2
337.50	10.6	6.4	29.9

LOCATION 6

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	16.3	9.7	45.3
22.50	18.7	10.1	49.1
45.00	30.5	14.7	74.7
67.50	52.5	15.5	99.0
90.00	50.5	15.3	96.5
112.50	48.4	15.7	95.4
135.00	25.0	10.8	57.4
157.50	11.7	5.2	27.3
180.00	10.7	4.8	25.1
202.50	9.8	3.7	21.0
225.00	9.6	4.3	22.5
247.50	54.1	12.9	92.8
270.00	49.3	13.2	88.9
292.50	16.3	8.7	42.5
315.00	25.1	10.6	57.0
337.50	24.6	10.9	57.4

LOCATION 7

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	9.1	7.0	30.1
22.50	14.0	9.8	43.3
45.00	22.3	13.7	63.3
67.50	40.5	13.5	81.0
90.00	45.2	12.9	83.8
112.50	37.3	11.5	71.7
135.00	21.0	7.4	43.0
157.50	8.8	2.9	17.5
180.00	8.4	3.1	17.9
202.50	7.8	3.1	17.1
225.00	8.6	3.6	19.5
247.50	7.9	3.0	17.0
270.00	16.6	7.7	39.7
292.50	9.0	5.9	26.6
315.00	7.1	4.0	19.2
337.50	7.5	4.2	20.2

LOCATION 8

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	35.1	13.6	75.8
22.50	39.0	15.7	86.1
45.00	23.2	13.5	63.7
67.50	27.6	14.0	69.7
90.00	56.1	20.3	117.1
112.50	35.5	17.0	86.6
135.00	14.2	6.9	34.8
157.50	17.3	7.9	41.0
180.00	16.2	8.5	41.7
202.50	20.4	11.6	55.2
225.00	36.0	15.3	81.9
247.50	45.3	13.3	85.2
270.00	41.8	13.8	83.3
292.50	20.3	10.0	50.3
315.00	32.7	11.6	67.7
337.50	35.3	10.4	66.5

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 9

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	20.4	12.2	56.9
22.50	19.3	9.5	47.9
45.00	19.2	9.8	48.7
67.50	24.6	9.5	53.0
90.00	15.4	7.3	37.4
112.50	8.8	4.2	21.4
135.00	6.8	2.4	14.0
157.50	8.8	3.9	20.4
180.00	14.4	6.1	32.7
202.50	23.1	8.2	47.8
225.00	21.3	8.9	48.1
247.50	20.9	10.6	52.6
270.00	22.3	11.3	56.3
292.50	19.1	10.9	51.8
315.00	16.2	9.3	44.0
337.50	14.7	8.5	40.3

LOCATION 10

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	21.3	12.5	58.7
22.50	24.9	13.0	63.9
45.00	56.2	21.2	120.0
67.50	35.1	19.3	93.0
90.00	15.2	7.6	38.0
112.50	9.5	4.0	21.4
135.00	7.8	3.1	17.1
157.50	10.8	6.4	29.9
180.00	23.3	8.7	49.5
202.50	18.0	6.9	38.8
225.00	22.4	12.0	58.4
247.50	49.4	14.6	93.3
270.00	53.7	12.7	91.8
292.50	32.6	13.1	71.8
315.00	27.9	11.0	61.1
337.50	21.4	10.0	51.2

LOCATION 11

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	36.4	14.4	79.7
22.50	25.9	10.5	57.4
45.00	29.9	11.5	64.2
67.50	26.2	12.1	62.5
90.00	20.5	9.1	47.9
112.50	23.3	9.8	52.7
135.00	32.5	9.5	60.9
157.50	30.9	9.0	58.0
180.00	43.7	11.6	78.6
202.50	37.5	14.8	82.0
225.00	18.9	12.2	55.5
247.50	30.2	15.0	75.2
270.00	35.4	11.5	70.0
292.50	29.1	11.4	63.4
315.00	18.4	7.6	41.1
337.50	29.1	10.5	60.6

LOCATION 12

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	22.5	10.0	52.6
22.50	16.7	8.0	40.8
45.00	16.5	6.4	35.7
67.50	15.4	10.6	47.2
90.00	24.7	12.2	61.3
112.50	29.4	9.7	58.5
135.00	26.6	8.2	51.2
157.50	18.1	7.0	39.2
180.00	10.1	6.0	28.0
202.50	2.8	1.8	8.2
225.00	4.0	2.5	11.5
247.50	5.1	3.4	15.4
270.00	11.0	6.3	30.9
292.50	15.7	4.9	30.3
315.00	14.2	3.9	25.9
337.50	20.5	5.3	36.4

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 13

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.6	10.7	62.7
22.50	26.2	10.1	56.4
45.00	23.1	8.4	48.3
67.50	18.7	10.5	50.1
90.00	28.3	13.4	68.6
112.50	37.0	13.5	77.6
135.00	23.2	11.6	57.9
157.50	17.5	9.7	46.4
180.00	15.3	8.5	40.8
202.50	24.6	11.6	59.4
225.00	14.8	9.3	42.8
247.50	14.3	9.8	43.8
270.00	27.3	10.0	57.2
292.50	33.1	10.3	64.0
315.00	25.2	7.9	49.0
337.50	34.5	8.2	59.0

LOCATION 14

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	40.3	10.7	72.5
22.50	35.7	11.2	69.3
45.00	37.4	14.3	80.4
67.50	36.0	18.9	92.6
90.00	80.1	13.7	121.2
112.50	60.0	15.3	105.8
135.00	39.6	13.1	78.8
157.50	46.1	11.2	79.7
180.00	38.8	11.2	72.8
202.50	60.6	16.2	109.3
225.00	66.5	17.1	117.8
247.50	45.1	18.1	99.3
270.00	36.8	13.6	77.5
292.50	42.2	13.0	81.2
315.00	27.5	8.8	53.8
337.50	40.2	10.4	71.4

LOCATION 15

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	32.3	9.8	61.6
22.50	32.4	13.0	71.3
45.00	23.3	10.5	54.7
67.50	46.4	20.4	107.5
90.00	45.3	20.6	107.1
112.50	22.8	11.0	55.7
135.00	24.3	10.3	55.3
157.50	32.1	10.9	64.7
180.00	34.0	11.1	67.3
202.50	31.5	12.2	68.0
225.00	41.6	19.5	100.3
247.50	31.7	15.9	79.4
270.00	21.6	8.3	46.5
292.50	16.3	5.5	33.0
315.00	14.0	4.4	27.3
337.50	21.4	6.5	40.9

LOCATION 16

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	27.5	10.3	58.4
22.50	25.9	11.0	59.0
45.00	24.5	8.9	51.1
67.50	26.3	10.8	58.6
90.00	31.7	12.2	68.2
112.50	28.3	12.2	64.9
135.00	23.7	10.1	54.1
157.50	21.3	9.1	48.6
180.00	28.0	11.5	62.6
202.50	30.0	11.8	65.4
225.00	38.2	15.1	83.4
247.50	30.9	12.8	69.3
270.00	24.2	9.9	52.9
292.50	25.5	9.4	53.8
315.00	17.9	6.1	36.1
337.50	23.7	7.8	47.0

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 17

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.5	14.0	72.5
22.50	23.3	11.0	56.2
45.00	21.9	10.4	53.3
67.50	25.8	13.3	65.5
90.00	36.4	17.5	88.8
112.50	21.4	10.9	54.2
135.00	15.8	7.8	39.2
157.50	23.5	8.7	49.7
180.00	40.3	11.2	73.9
202.50	35.1	11.2	68.7
225.00	21.4	11.4	55.7
247.50	21.9	11.9	57.7
270.00	19.9	8.3	44.8
292.50	17.8	7.7	40.8
315.00	13.2	4.1	25.5
337.50	18.4	7.4	40.6

LOCATION 18

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	37.7	11.0	70.8
22.50	28.8	11.1	62.1
45.00	25.0	10.4	56.3
67.50	25.7	11.0	58.8
90.00	17.9	9.0	45.0
112.50	44.6	16.2	93.1
135.00	41.8	9.1	69.1
157.50	30.2	9.9	60.1
180.00	34.6	9.3	62.4
202.50	32.1	10.4	63.4
225.00	20.5	10.2	50.9
247.50	23.0	12.3	59.9
270.00	28.8	12.1	65.1
292.50	31.4	11.7	66.5
315.00	20.6	7.4	42.8
337.50	27.6	9.2	55.0

LOCATION 19

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	41.5	10.9	74.2
22.50	35.0	13.4	75.2
45.00	26.6	10.6	58.4
67.50	24.2	11.6	59.0
90.00	56.5	19.8	115.9
112.50	55.5	10.7	87.6
135.00	48.4	11.5	82.9
157.50	26.1	11.0	59.0
180.00	37.1	10.9	69.8
202.50	27.3	11.3	61.2
225.00	23.2	10.0	53.1
247.50	15.4	7.1	36.6
270.00	25.8	8.7	51.9
292.50	41.6	11.0	74.5
315.00	28.2	7.4	50.6
337.50	39.7	8.0	63.8

LOCATION 20

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.1	11.7	65.3
22.50	23.1	11.1	56.5
45.00	20.6	10.0	50.5
67.50	46.3	21.6	110.9
90.00	63.5	11.9	99.2
112.50	44.5	14.7	88.5
135.00	36.0	12.6	73.8
157.50	22.9	11.4	57.2
180.00	51.9	13.6	92.7
202.50	57.2	11.6	92.0
225.00	65.2	12.6	103.1
247.50	20.5	11.1	53.9
270.00	26.1	11.7	61.2
292.50	26.9	11.4	61.0
315.00	17.4	7.6	40.3
337.50	17.9	7.5	40.4

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 21

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	42.9	11.8	78.2
22.50	25.4	11.0	58.5
45.00	21.6	9.0	48.7
67.50	21.9	10.8	54.3
90.00	74.6	19.2	132.3
112.50	70.7	13.8	112.1
135.00	33.0	18.2	87.7
157.50	28.0	14.8	72.6
180.00	56.9	15.1	102.1
202.50	44.6	13.1	84.0
225.00	45.2	11.1	78.4
247.50	35.2	15.4	81.3
270.00	39.8	13.1	79.2
292.50	44.2	9.9	73.9
315.00	32.6	8.2	57.1
337.50	41.3	9.2	69.0

LOCATION 22

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	42.3	11.3	76.0
22.50	26.0	13.1	65.4
45.00	30.3	14.6	74.1
67.50	67.2	19.2	124.9
90.00	82.8	12.9	121.5
112.50	41.7	18.5	97.3
135.00	35.5	14.7	79.6
157.50	37.1	19.7	96.2
180.00	76.5	11.9	112.3
202.50	79.4	13.2	118.9
225.00	76.4	11.7	111.4
247.50	61.3	20.0	121.2
270.00	24.2	11.2	57.9
292.50	36.0	11.1	69.3
315.00	29.3	7.6	51.9
337.50	41.0	8.8	67.3

LOCATION 23

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	9.9	3.8	21.4
22.50	13.2	6.0	31.2
45.00	15.8	6.6	35.7
67.50	36.9	12.8	75.4
90.00	66.2	13.4	106.5
112.50	52.7	16.0	100.8
135.00	29.4	14.9	74.2
157.50	22.0	10.5	53.4
180.00	29.0	13.6	69.9
202.50	52.3	15.3	98.3
225.00	48.3	11.1	81.6
247.50	35.4	15.4	81.5
270.00	14.8	6.0	32.8
292.50	11.7	4.7	25.7
315.00	8.7	3.1	18.0
337.50	10.5	3.6	21.2

LOCATION 24

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	15.3	4.6	29.1
22.50	31.0	13.0	70.1
45.00	57.3	19.1	114.6
67.50	52.0	19.6	110.9
90.00	37.0	18.5	92.5
112.50	18.6	8.9	45.3
135.00	36.9	11.8	72.4
157.50	48.3	12.0	84.4
180.00	55.9	11.9	91.6
202.50	61.3	10.9	94.1
225.00	52.5	9.5	80.9
247.50	24.1	8.4	49.1
270.00	11.3	4.6	25.2
292.50	19.8	7.3	41.6
315.00	12.7	4.4	25.6
337.50	11.6	2.7	19.6

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 25

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	16.6	5.1	32.0
22.50	30.4	13.2	70.1
45.00	39.4	16.0	87.3
67.50	46.0	18.3	100.9
90.00	32.6	12.5	70.1
112.50	18.2	9.3	46.0
135.00	27.2	12.5	64.7
157.50	41.4	12.4	78.8
180.00	57.6	12.8	96.0
202.50	60.3	10.9	92.9
225.00	49.4	9.5	77.9
247.50	30.9	8.6	56.7
270.00	9.6	3.5	20.2
292.50	14.5	5.0	29.4
315.00	12.1	4.0	24.0
337.50	13.9	4.4	27.1

LOCATION 26

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	6.8	3.5	17.3
22.50	8.8	5.8	26.3
45.00	28.0	17.8	81.5
67.50	73.7	12.3	110.6
90.00	54.4	13.7	95.7
112.50	31.7	12.0	67.8
135.00	23.2	12.7	61.2
157.50	22.2	12.7	60.3
180.00	33.4	12.3	70.4
202.50	32.2	10.2	62.8
225.00	26.3	6.2	44.9
247.50	31.6	5.9	49.4
270.00	9.6	5.0	24.6
292.50	18.5	7.5	41.0
315.00	14.9	6.3	34.0
337.50	8.2	3.9	20.0

LOCATION 27

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	34.9	12.8	73.4
22.50	42.9	14.7	86.9
45.00	25.5	16.0	73.5
67.50	16.5	7.7	39.7
90.00	15.3	7.7	38.5
112.50	48.6	15.9	96.2
135.00	14.2	7.5	36.8
157.50	20.2	10.5	51.7
180.00	45.0	12.4	82.9
202.50	56.5	11.3	90.5
225.00	57.7	9.4	85.9
247.50	45.1	10.6	76.8
270.00	8.3	5.9	26.2
292.50	8.6	5.5	25.1
315.00	7.5	4.6	21.3
337.50	25.2	12.0	61.2

LOCATION 28

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	9.5	3.5	20.1
22.50	3.3	2.2	9.9
45.00	1.5	.8	4.1
67.50	9.4	1.4	13.5
90.00	11.9	1.4	16.2
112.50	12.0	1.2	15.6
135.00	7.8	1.4	11.8
157.50	10.4	1.6	15.4
180.00	14.7	2.3	21.5
202.50	13.3	1.7	18.5
225.00	10.5	1.4	14.7
247.50	5.9	1.1	9.1
270.00	2.5	.8	4.9
292.50	.9	.6	2.8
315.00	.9	.4	2.0
337.50	4.2	.9	6.8

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 29

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	7.9	4.8	22.3
22.50	10.7	7.2	32.4
45.00	31.6	12.2	68.3
67.50	48.6	9.8	78.1
90.00	55.2	12.6	93.0
112.50	40.3	13.6	81.1
135.00	21.0	11.9	56.6
157.50	12.1	7.1	33.4
180.00	37.2	15.6	84.1
202.50	15.5	9.8	44.9
225.00	12.8	6.6	32.6
247.50	19.7	13.1	59.1
270.00	39.0	15.3	84.8
292.50	43.9	14.4	87.1
315.00	30.6	12.5	68.2
337.50	11.9	7.5	34.4

LOCATION 30

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.2	5.6	30.2
22.50	10.7	5.8	28.2
45.00	15.7	10.1	46.1
67.50	50.2	12.9	88.9
90.00	70.2	12.3	107.1
112.50	53.4	11.5	88.8
135.00	27.3	11.0	72.8
157.50	22.5	13.4	81.4
180.00	29.8	11.4	64.0
202.50	47.2	13.7	88.2
225.00	65.8	12.1	102.2
247.50	45.6	19.9	105.5
270.00	9.1	6.0	27.1
292.50	7.8	4.3	20.9
315.00	7.6	4.5	21.2
337.50	12.4	4.8	26.8

LOCATION 31

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	12.7	5.6	29.6
22.50	7.9	4.5	21.5
45.00	13.8	8.6	39.7
67.50	40.4	9.0	67.4
90.00	52.4	9.9	82.2
112.50	59.6	11.5	94.2
135.00	38.9	12.6	76.7
157.50	29.4	12.3	66.5
180.00	17.2	8.6	42.9
202.50	37.2	11.5	71.7
225.00	57.6	14.4	100.9
247.50	74.8	10.8	107.1
270.00	49.5	12.2	86.0
292.50	27.3	10.7	59.4
315.00	14.2	8.0	38.1
337.50	12.2	5.4	28.6

LOCATION 32

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	28.3	11.5	62.8
22.50	21.5	9.9	51.2
45.00	28.9	15.7	76.1
67.50	75.4	13.1	114.7
90.00	77.8	15.4	123.9
112.50	77.5	15.8	125.9
135.00	53.0	23.3	122.9
157.50	33.1	15.9	80.7
180.00	63.6	24.4	136.8
202.50	79.9	[illegible]	110.[illegible]
225.00	61.4	[illegible]	1[illegible]
247.50	43.4	19.6	102.2
270.00	18.2	10.9	48.8
292.50	29.6	13.9	71.[illegible]
315.00	19.3	8.1	43.[illegible]
337.50	26.0	10.7	59.1

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 33

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	8.2	2.8	16.8
22.50	13.4	5.2	29.1
45.00	17.0	9.1	44.4
67.50	42.9	12.9	81.6
90.00	38.6	12.2	75.3
112.50	18.6	13.6	59.5
135.00	21.0	10.6	52.7
157.50	23.4	12.2	60.0
180.00	53.8	16.5	103.2
202.50	65.2	12.7	103.3
225.00	46.1	14.8	90.5
247.50	19.1	8.6	44.8
270.00	13.8	6.1	32.1
292.50	10.2	3.9	22.0
315.00	8.8	3.3	18.7
337.50	8.8	2.8	17.2

LOCATION 34

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	23.3	7.7	46.5
22.50	13.3	8.4	38.4
45.00	6.2	4.4	19.4
67.50	40.3	7.8	63.9
90.00	53.4	8.7	79.5
112.50	64.4	10.8	96.8
135.00	57.4	13.9	99.2
157.50	53.1	13.7	94.2
180.00	30.4	13.9	72.2
202.50	33.9	17.9	87.5
225.00	64.8	13.1	104.0
247.50	72.4	13.6	113.1
270.00	61.9	13.9	103.7
292.50	38.7	14.6	82.5
315.00	25.6	14.1	67.8
337.50	21.5	9.9	51.3

LOCATION 35

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	48.7	12.7	86.8
22.50	38.5	12.6	76.3
45.00	30.3	14.4	73.5
67.50	44.8	10.4	75.9
90.00	39.6	10.6	71.5
112.50	48.1	18.5	103.5
135.00	50.4	18.1	104.9
157.50	24.3	11.2	57.9
180.00	61.0	20.6	122.8
202.50	81.8	10.0	111.7
225.00	41.4	17.0	92.3
247.50	22.7	10.0	52.7
270.00	16.7	7.6	39.5
292.50	28.4	12.4	65.6
315.00	22.8	9.8	52.2
337.50	28.8	12.2	65.5

LOCATION 36

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	18.2	9.7	47.3
22.50	23.5	12.3	60.4
45.00	24.6	15.3	70.5
67.50	53.3	19.5	111.8
90.00	63.8	11.9	99.6
112.50	50.4	13.1	89.8
135.00	34.6	13.0	73.6
157.50	26.0	12.6	64.0
180.00	41.1	14.3	84.1
202.50	73.7	9.6	102.4
225.00	67.0	14.8	111.3
247.50	21.5	9.9	51.1
270.00	19.2	9.2	46.8
292.50	31.3	12.8	69.7
315.00	14.2	9.1	41.5
337.50	10.5	5.8	27.9

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 37

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	44.6	10.8	77.0
22.50	29.3	9.6	58.0
45.00	23.4	9.3	51.4
67.50	18.7	9.6	47.6
90.00	24.0	10.0	54.1
112.50	32.0	10.5	63.5
135.00	32.2	12.1	68.6
157.50	38.4	10.9	71.1
180.00	54.7	10.2	85.2
202.50	59.9	15.7	107.0
225.00	34.6	15.8	82.0
247.50	23.2	10.8	55.5
270.00	41.4	15.8	88.8
292.50	39.1	11.3	73.0
315.00	30.3	8.4	55.5
337.50	36.2	8.4	61.3

LOCATION 38

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.3	11.0	63.2
22.50	28.3	9.9	58.1
45.00	26.9	12.0	63.0
67.50	18.7	9.7	47.7
90.00	31.1	12.5	68.5
112.50	33.2	9.5	61.7
135.00	38.0	10.6	69.8
157.50	37.3	9.7	66.4
180.00	51.8	12.3	88.8
202.50	24.2	16.5	73.6
225.00	20.9	9.0	48.0
247.50	21.9	10.7	54.0
270.00	27.1	12.6	64.8
292.50	34.7	11.4	68.9
315.00	26.3	9.4	54.7
337.50	20.5	7.4	42.6

LOCATION 39

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	20.6	8.3	45.4
22.50	18.9	8.1	43.1
45.00	20.2	7.9	44.0
67.50	24.8	14.1	67.1
90.00	26.1	10.8	58.6
112.50	41.2	10.8	73.7
135.00	27.3	9.0	54.4
157.50	14.6	6.7	34.8
180.00	15.5	7.6	38.4
202.50	24.7	12.3	61.5
225.00	23.5	11.3	57.5
247.50	22.8	10.4	54.1
270.00	21.4	9.5	49.6
292.50	20.0	8.6	45.8
315.00	15.9	6.5	35.5
337.50	12.8	4.0	24.9

LOCATION 40

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	14.6	5.0	29.5
22.50	20.4	9.4	48.6
45.00	29.0	13.0	68.1
67.50	45.8	21.4	110.0
90.00	30.5	17.2	82.2
112.50	29.7	11.5	64.2
135.00	33.2	13.5	73.8
157.50	20.5	10.5	52.0
180.00	17.6	9.5	46.1
202.50	26.7	17.0	77.8
225.00	39.5	19.7	98.6
247.50	23.5	15.0	68.4
270.00	22.2	9.4	50.2
292.50	24.7	9.7	53.9
315.00	13.1	4.6	26.9
337.50	14.3	5.9	26.0

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 41

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	29.2	10.3	59.9
22.50	24.8	8.3	49.7
45.00	27.5	9.6	56.4
67.50	40.7	14.3	83.5
90.00	32.5	14.5	75.9
112.50	28.5	11.8	63.9
135.00	27.5	11.1	61.0
157.50	24.8	10.4	55.9
180.00	27.5	11.9	63.2
202.50	41.2	17.3	93.2
225.00	26.3	10.8	58.6
247.50	28.7	10.6	60.6
270.00	22.5	8.7	48.7
292.50	31.1	11.8	66.7
315.00	23.2	7.2	44.9
337.50	23.8	7.6	46.7

LOCATION 42

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	43.6	10.9	76.3
22.50	37.1	12.4	74.4
45.00	44.1	14.8	88.6
67.50	51.8	18.7	107.9
90.000	75.5	23.4	145.8
112.50	44.2	13.5	84.5
135.00	56.4	10.8	88.9
157.50	45.5	11.1	78.7
180.00	44.0	14.0	86.0
202.50	77.6	14.1	119.8
225.00	51.6	22.3	118.6
247.50	37.6	18.6	93.4
270.00	38.1	13.2	77.7
292.50	36.6	11.2	70.1
315.00	24.4	7.9	48.0
337.50	34.9	8.4	60.1

LOCATION 43

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	31.9	10.5	63.2
22.50	25.5	11.0	58.7
45.00	18.0	11.2	51.5
67.50	11.2	7.3	33.1
90.00	25.8	13.1	65.0
112.50	26.7	10.2	57.4
135.00	26.2	11.3	60.0
157.50	20.8	11.3	54.6
180.00	33.6	12.7	71.6
202.50	39.4	14.3	82.2
225.00	22.2	12.5	59.7
247.50	17.1	10.3	48.0
270.00	16.8	10.2	47.4
292.50	19.0	11.2	52.6
315.00	16.7	9.8	46.1
337.50	21.6	9.5	50.3

LOCATION 44

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	13.3	7.5	35.7
22.50	15.6	8.3	40.3
45.00	8.6	5.5	25.2
67.50	7.8	3.4	18.0
90.000	4.8	2.8	13.2
112.50	6.8	4.5	20.2
135.00	12.8	7.5	35.4
157.50	12.7	7.4	34.9
180.00	12.7	7.8	36.4
202.50	16.8	12.0	52.7
225.00	17.8	11.6	52.6
247.50	11.1	7.1	32.5
270.00	12.0	9.5	40.4
292.50	13.9	9.7	43.1
315.00	8.9	6.4	28.1
337.50	10.9	6.1	30.9

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 45

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.5	14.2	73.1
22.50	35.4	13.2	75.0
45.00	31.8	12.6	69.6
67.50	22.2	13.3	62.3
90.00	26.4	14.0	68.5
112.50	43.0	11.5	77.5
135.00	31.4	9.0	58.4
157.50	31.1	8.5	56.5
180.00	27.2	10.6	58.9
202.50	18.1	8.9	44.8
225.00	23.9	10.7	55.9
247.50	27.5	12.8	66.0
270.00	31.8	14.7	76.0
292.50	26.2	13.6	67.1
315.00	16.0	9.3	43.8
337.50	14.9	9.5	43.5

LOCATION 46

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	21.4	10.2	51.9
22.50	21.0	9.8	50.4
45.00	22.6	11.9	58.1
67.50	20.2	9.1	47.5
90.00	23.9	8.6	49.8
112.50	14.8	6.9	35.7
135.00	9.9	4.3	22.9
157.50	6.8	2.5	14.2
180.00	6.7	2.8	15.2
202.50	12.8	5.9	30.5
225.00	23.0	8.8	49.6
247.50	23.2	10.0	53.2
270.00	20.7	11.3	54.6
292.50	16.4	10.4	47.4
315.00	11.3	6.7	31.3
337.50	16.4	9.8	45.8

LOCATION 47

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	38.5	15.5	85.0
22.50	39.3	12.3	76.3
45.00	40.4	12.0	84.4
67.50	27.8	14.1	70.2
90.00	13.3	8.0	37.4
112.50	18.9	9.6	47.6
135.00	13.9	10.1	44.2
157.50	5.3	3.2	14.9
180.00	6.3	3.7	17.4
202.50	10.4	6.1	28.7
225.00	29.3	19.3	87.3
247.50	67.0	28.4	152.3
270.00	30.3	19.0	87.2
292.50	21.7	15.0	66.6
315.00	13.9	8.0	37.7
337.50	25.2	11.1	58.5

LOCATION 48

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	38.1	12.1	74.5
22.50	42.7	13.9	84.4
45.00	39.6	11.4	73.7
67.50	42.1	14.6	85.8
90.00	20.6	12.0	56.6
112.50	14.9	7.2	36.5
135.00	15.3	7.2	37.0
157.50	14.3	6.9	35.0
180.00	24.5	12.5	62.0
202.50	50.9	16.9	101.6
225.00	27.6	14.4	70.9
247.50	22.5	9.9	52.3
270.00	25.5	14.1	67.9
292.50	18.4	10.0	48.5
315.00	25.3	11.5	59.9
337.50	35.4	10.6	67.2

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 49

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	10.1	5.9	27.8
22.50	21.2	9.0	48.3
45.00	14.0	6.2	32.5
67.50	9.2	3.5	19.8
90.00	7.9	3.1	17.2
112.50	7.9	2.7	15.9
135.00	8.4	2.8	16.8
157.50	15.4	5.1	30.6
180.00	24.2	8.0	48.2
202.50	26.2	9.2	53.8
225.00	24.0	9.1	51.1
247.50	19.8	8.5	45.2
270.00	10.4	7.5	32.8
292.50	8.1	6.0	26.2
315.00	5.8	4.5	19.4
337.50	2.7	2.1	8.9

LOCATION 50

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	37.1	12.3	74.1
22.50	55.3	13.6	96.2
45.00	42.6	10.2	73.1
67.50	11.8	6.6	31.7
90.00	8.9	3.1	18.0
112.50	9.3	3.3	19.2
135.00	13.5	4.9	28.1
157.50	24.6	7.9	48.2
180.00	32.2	10.6	64.0
202.50	36.5	12.1	72.9
225.00	39.2	14.2	81.7
247.50	40.1	15.3	86.1
270.00	21.1	12.2	57.6
292.50	16.3	7.8	39.5
315.00	13.9	7.6	36.7
337.50	22.0	10.5	53.4

LOCATION 51

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	26.6	12.5	63.9
22.50	36.1	15.0	81.0
45.00	37.5	12.8	76.0
67.50	45.7	15.3	91.4
90.00	33.7	15.4	80.0
112.50	15.3	8.0	39.2
135.00	21.1	8.4	46.2
157.50	22.0	8.8	48.3
180.00	21.5	12.5	59.0
202.50	38.8	18.4	94.1
225.00	45.6	18.5	101.0
247.50	50.5	17.3	102.2
270.00	24.5	15.2	70.2
292.50	13.1	8.2	37.8
315.00	13.8	8.0	37.8
337.50	14.7	8.5	40.2

LOCATION 52

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	30.8	12.9	69.4
22.50	50.2	14.3	93.0
45.00	34.3	10.8	66.8
67.50	12.6	6.9	33.4
90.00	8.7	3.6	19.4
112.50	11.9	5.2	27.4
135.00	10.4	4.7	24.6
157.50	15.6	6.6	35.4
180.00	25.7	9.5	54.1
202.50	36.3	11.2	70.0
225.00	46.9	12.1	83.0
247.50	44.5	11.1	77.7
270.00	20.2	10.6	52.0
292.50	17.6	8.6	43.6
315.00	9.6	4.8	23.9
337.50	10.8	5.9	28.4

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

LOCATION 53

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	39.3	14.4	82.7
22.50	47.0	15.5	93.5
45.00	29.7	11.1	63.1
67.50	43.1	15.5	89.5
90.00	26.9	12.9	65.6
112.50	38.5	13.5	78.8
135.00	24.7	9.9	54.5
157.50	37.5	9.0	64.3
180.00	45.6	8.5	71.2
202.50	50.2	8.1	74.4
225.00	56.7	7.7	79.9
247.50	59.1	10.2	89.8
270.00	39.3	13.5	79.9
292.50	23.0	10.2	53.5
315.00	14.8	8.2	39.3
337.50	17.9	9.8	47.3

LOCATION 54

WIND AZIMUTH	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3*URMS/UINF (PERCENT)
0.00	.5	2	1.2
22.50	3.1	.9	5.7
45.00	2.5	.6	4.4
67.50	10.1	[illegible]	13.7
90.00	15.3	[illegible]	23.0
112.50	17.3	2.8	25.7
135.00	12.9	2.1	19.3
157.50	6.4	1.7	11.4
180.00	15.1	2.8	23.5
202.50	17.9	3.4	27.9
225.00	12.1	3.1	21.5
247.50	5.8	2.0	11.7
270.00	4.2	3.6	14.9
292.50	6.7	1.9	12.2
315.00	3.9	1.4	8.1
337.50	1.6	.7	3.8

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

MILLION DOLLAR PIER, ATLANTIC CITY

* * GREATEST VALUES * *

UMEAN/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3RMS
22	90.0	82.8	12.9	121.5
35	202.5	81.8	10.0	111.7
14	90.0	80.1	13.7	121.2
32	202.5	79.9	10.0	110.0
22	202.5	79.4	13.2	118.9
32	90.0	77.8	15.4	123.9
42	202.5	77.6	14.1	119.8
32	112.5	77.5	15.8	125.0
22	180.0	76.5	11.9	112.3
22	225.0	76.4	11.7	111.4

URMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3RMS
47	247.5	67.0	28.4	152.3
32	180.0	63.6	24.4	136.8
32	135.0	53.0	23.3	123.0
42	225.0	51.6	22.3	118.6
20	67.5	46.3	21.6	110.9
40	67.5	45.8	21.4	110.0
10	45.0	56.2	21.2	120.0
35	180.0	61.0	20.6	122.8
15	90.0	45.3	20.6	107.1
15	67.5	46.4	20.4	107.5

UMEAN+3*RMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	M+3RMS
47	247.5	67.0	28.4	152.3
32	180.0	63.6	24.4	136.8
21	90.0	74.6	19.2	132.3
32	112.5	77.5	15.8	125.0
22	67.5	67.2	19.2	124.9
32	90.0	77.8	15.4	123.9
32	135.0	53.0	23.3	123.0
35	180.0	61.0	20.6	122.8
22	90.0	82.8	12.9	121.5
14	90.0	80.1	13.7	121.2

TABLE 3

PERCENTAGE FREQUENCY OF WIND DIRECTION AND SPEED

ATLANTIC CITY, NEW JERSEY NAT. AV FRC. EXP. CTR

SEASON : ANNUAL NO OF OBS.= 29216 HT. OF MEAS.= 20. FT.

VELOCITY LEVELS IN MPH.

DIRECTION	0- 3	4- 7	8-12	13-18	19-24	25-31	32-38	39 +	TOTAL
N	.30	2.40	3.30	1.50	.20	0.00	0.00	0.00	7.70
NNE	.20	1.00	1.10	.60	.10	0.00	0.00	0.00	2.90
NE	.10	1.00	1.10	.80	.20	0.00	0.00	0.00	3.20
ENE	.20	.90	1.20	1.30	.30	.10	0.00	0.00	4.00
E	.20	1.20	1.90	1.20	.20	.10	0.00	0.00	4.80
ESE	.20	.90	1.40	.70	.10	0.00	0.00	0.00	3.30
SE	.10	.80	1.20	.50	.10	0.00	0.00	0.00	2.80
SSE	.10	.80	1.40	.60	.10	0.00	0.00	0.00	3.10
S	.30	2.30	4.10	3.80	.60	.10	0.00	0.00	11.10
SSW	.20	1.60	2.70	1.90	.40	.10	0.00	0.00	6.90
SW	.20	1.70	2.30	1.30	.30	0.00	0.00	0.00	5.80
WSW	.20	2.20	3.00	1.60	.30	.10	0.00	0.00	7.40
W	.20	1.80	3.40	2.40	.80	.30	.10	0.00	9.00
WNW	.20	1.70	3.00	3.00	1.20	.40	.10	0.00	9.70
NW	.20	2.20	2.60	2.40	.90	.30	0.00	0.00	8.60
NNW	.20	1.50	1.80	1.40	.30	0.00	0.00	0.00	5.30
CALM	4.30	0.00	0.00	0.00	0.00	0.00	0.00	0.00	4.30
TOT	7.50	24.10	35.50	25.20	6.00	1.50	.30	0.00	100.00

TABLE 4

SUMMARY OF WIND EFFECTS ON PEOPLE

	Beaufort number	Speed (mph)	Effects
Calm, light air	0, 1	0- 3	Calm, no noticeable wind
Light breeze	2	4- 7	Wind felt on face
Gentle breeze	3	8-12	Wind extends light flag Hair is disturbed Clothing flaps
Moderate breeze	4	13-18	Raises dust, dry soil and loose paper Hair disarranged
Fresh breeze	5	19-24	Force of wind felt on body Drifting snow becomes airborne Limit of agreeable wind on land
Strong breeze	6	25-31	Umbrellas used with difficulty Hair blown straight Difficult to walk steadily Wind noise on ears unpleasant Windborne snow above head height (blizzard)
Near gale	7	32-38	Inconvenience felt when walking
Gale	8	39-46	Generally impedes progress Great difficulty with balance in gusts
Strong gale	9	47-54	People blown over by gusts

Note: Table from Reference 4, p. 40.

TABLE 5

CALCULATION OF REFERENCE PRESSURE

1. Basic wind speed from ANSI A58.1 (Ref. 6):

   50-yr fastest mile at 30 ft = 90 mph

   Mean hourly wind speed = $\frac{90}{1.28}$ = 70.3 mph

   Mean hourly gradient wind speed = $70.3 \left(\frac{1000}{30}\right)^{.16}$ = 123.2 mph

   Mean hourly wind at reference location = U_∞ = gradient wind = 123.2 mph

   Reference Pressure = $0.5 \rho U_\infty^2 = (.00256)\ (123.2)^2$ = 38.8 psf

   Use 39 psf

2. Loads for 100-yr recurrence wind:

   100-yr fastest mile at 30 ft = 105 mph

   Multiply 50-yr loads by $\left(\frac{105}{90}\right)^2$ = 1.36

3. Gust load factors to convert hourly mean integrated loads to various gust durations (see Sect. 4.4):

Gust Duration, sec	Gust Load Factor
10 - 15	$(1.4)^2$ = 1.96
30	$(1.32)^2$ = 1.74
45	$(1.26)^2$ = 1.59

   The 30 second gust load factor was used in Table 7.

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : MILLION DOLLAR PIER, ATLANTIC CITY
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 39.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF ----	POSITIVE PEAK ----
1	240	-.59	-23.2	11.8
2	240	-.47	-18.3	13.4
3	80	-.44	-17.0	13.0
4	50	-.58	-22.6	12.2
5	230	-.42	-16.6	16.4
6	90	-.56	-22.0	7.2
7	240	-.93	-36.3	13.9
8	220	-.72	-28.3	12.0
9	240	-1.02	-39.6	15.1
10	240	-1.41	-55.0	11.0
11	240	-1.36	-53.0	10.5
12	20	.61	-18.8	23.8
13	20	-.89	-34.6	7.7
14	240	-1.19	-46.5	10.8
15	30	.77	-17.9	30.2
16	220	-1.04	-40.4	10.3
17	230	-1.22	-47.4	7.6
18	20	.67	-11.6	26.0
19	240	-.86	-33.5	6.8
20	240	-1.23	-48.0	9.9
21	80	.63	-13.0	24.5
22	240	-.90	-35.2	10.8
23	260	-.58	-21.4	22.5
24	230	-.87	-33.7	10.3
25	230	-.83	-32.5	11.4
26	240	-1.39	-54.1	10.0
27	160	.63	-23.3	24.4
28	230	-.86	-33.7	8.3
29	110	.71	-15.5	27.8
30	240	-.90	-35.2	12.2
31	200	-1.09	-42.6	7.1
32	230	-1.38	-53.8	11.4
33	230	-1.51	-59.0	6.0
34	240	-1.08	-42.3	17.3
35	230	-1.15	-45.0	13.0
36	120	.60	-23.0	23.2
37	240	-.82	-31.9	9.0
38	230	-1.00	-39.1	7.1
39	290	-.73	-28.6	15.7
40	90	-.91	-35.5	20.4
41	220	-.97	-37.7	19.6
42	260	-.89	-34.6	8.0
43	200	-.76	-29.5	20.6
44	70	.70	-14.0	27.2
45	240	-.83	-32.5	6.1
46	240	-1.14	-44.3	11.4
47	270	-1.15	-44.9	12.5
48	240	-.82	-31.8	23.4
49	100	.72	-17.1	28.1
50	160	-.87	-34.0	.8
51	130	-1.13	-43.9	1.5
52	160	-.73	-28.4	21.8
53	240	-.83	-32.2	18.2
54	260	-.47	-18.2	17.6
55	240	-.60	-23.5	18.2
56	260	-.57	-22.2	12.2
57	180	-.53	-20.9	8.2
101	20	.63	-17.4	24.5
102	240	-.54	-21.2	17.1
103	230	.64	-19.1	25.1
104	270	.73	-16.0	28.5
105	290	.55	-16.1	21.4
106	30	.47	-14.8	18.4
107	60	.63	-13.6	24.4
108	20	.62	-14.5	24.4
109	210	.73	-20.7	28.7
110	20	.71	-21.7	27.7
111	20	.48	-15.6	18.7
112	10	-.75	-29.2	28.9
113	20	.88	-21.0	34.5
114	20	.62	-15.9	24.1
115	250	.74	-19.4	29.0
116	20	.52	-19.6	20.5
117	20	.69	-17.2	26.8
118	210	.92	-31.5	35.9
119	20	.83	-16.7	32.5
120	20	.81	-16.6	31.5
121	20	.69	-12.1	26.9
122	60	.50	-14.4	19.4
123	60	.52	-10.5	20.3
124	350	.72	-17.4	28.1
125	70	.77	-11.4	29.9
126	60	.79	-14.3	30.8
127	60	.66	-10.8	25.6
128	250	.76	-17.1	29.6
129	60	.47	-11.2	18.4
130	60	.66	-15.6	25.7
131	280	.72	-25.4	28.2
132	280	.78	-21.1	30.5
133	70	.51	-11.5	19.8
134	130	.77	-25.1	30.0
135	100	.71	-12.9	27.6
136	70	.42	-11.3	16.2
137	180	.66	-17.7	25.6
138	80	.74	-16.1	29.0
139	180	.73	-15.2	28.4
140	110	.51	-14.0	20.0
141	110	-.71	-27.5	23.5
142	110	.68	-22.4	26.6
143	100	.57	-15.2	22.3
144	70	-.48	-18.8	18.2
145	70	.65	-16.8	25.2
146	290	-1.12	-43.7	30.8
147	80	.65	-14.1	25.5
148	70	.84	-17.9	32.5
149	60	.51	-15.7	20.0
150	180	.78	-27.4	30.4
151	60	.75	-13.9	29.2
152	80	.54	-13.4	20.9
153	120	.49	-15.7	19.0
154	100	.74	-19.0	28.8
155	100	.81	-14.2	31.1
156	60	.57	-14.9	22.3
157	80	.76	-15.3	29.5
158	170	-.82	-32.0	25.2
159	170	-1.12	-43.9	30.1
160	130	.68	-22.8	26.5
161	70	.63	-14.9	24.5
162	240	-.90	-35.0	33.1
163	240	.78	-29.5	30.1
164	110	.67	-22.5	26.2
165	110	.71	-21.4	27.5
166	100	.89	-32.4	34.9
167	20	.54	-15.8	21.2
201	240	-1.30	-50.6	24.4
202	230	-.81	-31.5	23.1
203	240	-.75	-29.2	21.0
204	250	-1.50	-58.5	25.0
205	60	-.93	-36.5	24.0
206	200	-.70	-27.4	21.0
207	280	-.72	-28.0	11.3
208	60	-.65	-25.3	19.5
209	240	-.75	-29.4	19.1
210	20	.66	-19.5	25.6
211	240	.75	-18.8	29.8
212	250	-.83	-32.2	9.0
213	230	-.62	-24.2	19.0
214	30	.69	-14.9	26.7
301	250	-.98	-38.3	24.7
302	250	-.93	-36.4	22.8
303	240	-.88	-34.2	26.8
304	60	.91	-32.7	35.4
305	240	-.85	-27.5	33.3
306	250	-.95	-36.9	31.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : MILLION DOLLAR PIER, ATLANTIC CITY
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 39.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK (PSF)	POSITIVE PEAK (PSF)
307	250	.69	-20.7	27.0	314	240	.70	-26.5	27.3	401	250	-.89	-34.9	13.2
308	60	1.04	-13.8	40.4	315	260	.70	-18.6	27.4	402	230	-1.25	-48.9	20.0
309	240	.69	-24.5	26.8	316	240	.80	-30.2	31.2	403	230	-1.32	-51.4	36.5
310	250	.75	-28.6	29.1	317	240	.69	-11.3	27.1	404	250	-1.22	-47.7	21.3
311	30	.79	-30.6	30.6	318	240	-.64	-24.9	16.2	405	250	-.99	-38.7	23.5
312	240	-.83	-32.5	28.4	319	260	-.53	-20.7	10.2	406	230	-.87	-34.0	19.1
313	240	.68	-26.3	26.7	320	30	-.86	-33.6	31.0					

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : MILLION DOLLAR PIER, ATLANTIC CITY
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 39 0 PSF

* * 15 GREATEST PRESSURE COEFFICIENT MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
33	230	-1.51	-59 0	6 0
204	250	-1.50	-58.6	25.0
10	240	-1.41	-55 0	11 0
26	240	-1.39	-54.1	10.0
32	230	-1.38	-53.8	11.4
11	240	-1.36	-53.0	10.5
403	230	-1.32	-51.4	36.5
201	240	-1.30	-50.6	24.8
402	230	-1.25	-48.9	20.0
20	240	-1.23	-48.0	9 9
404	250	-1.22	-47.7	21.3
17	230	-1.22	-47.4	7.6
14	240	-1.19	-46.5	10.8
35	230	-1.15	-45.0	13.0
47	270	-1.15	-44 9	12.5

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : MILLION DOLLAR PIER, ATLANTIC CITY
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 39.0 PSF

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----	TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
10	240	-1.52	-59.1	1.4	32	230	-1.53	-59.5	.7	204	252	-1.47	-57.2	10.4
11	254	-1.40	-54.4	-3.9	33	226	-1.49	-58.1	-5.5	403	230	-1.46	-56.9	21.2
26	226	-1.54	-60.0	4.5										

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : MILLION DOLLAR PIER, ATLANTIC CITY
LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 39.0 PSF

* * 7 GREATEST PRESSURE COEFFICIENT MAGNITUDES * *

TAP	AZI-MUTH	PRESS COEFF	NEGATIVE PEAK ---- PSF	POSITIVE PEAK ----
26	226	-1.54	-60.0	4.5
32	230	-1.53	-59.5	.7
10	240	-1.52	-59.1	1.4
33	226	-1.49	-58.1	-5.5
204	252	-1.47	-57.2	10.4
403	230	-1.46	-56.9	21.2
11	254	-1.40	-54.4	-3.9

TABLE 6B. COMPARISON OF CONFIGURATIONS A AND B MILLION DOLLAR PIER, ATLANTIC CITY

TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. B EXCEEDED THAT FOR CONFIG. A BY 5 PSF
REF. PRESSURE = 39.0 PSF

TAP	AZIMUTH	A CONFIG PSF LOAD	AZIMUTH	B CONFIG PSF LOAD
26	240	-54.1	226	-60.0
32	230	-53.8	230	-59.5
403	230	-51.4	230	-56.9

TABLE 7. BASE SHEAR AND MOMENT SUMMARY   MILLION DOLLAR PIER, ATLANTIC CITY
CONFIGURATION A   REFERENCE PRESSURE 39.0   GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

AZIMUTH	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z	ECCEN (%) X	ECCEN (%) Y
0	-35.4	345.8	41.2	26	-12
10	-48.5	520.2	85.4	38	-15
20	-66.9	584.2	87.4	33	-17
30	-41.7	702.5	81.5	28	-7
40	-23.9	732.6	75.4	23	-3
50	13.7	787.9	61.5	17	1
60	62.0	1118.6	43.6	9	2
70	62.7	1147.6	29.4	6	1
80	72.9	1138.6	14.4	3	1
90	90.5	1010.4	-15.9	-3	-1
100	124.7	933.1	-18.8	-4	-3
110	155.6	825.0	-12.9	-3	-3
120	168.2	559.5	-19.0	-7	-9
130	150.3	342.7	-13.1	-7	-14
140	147.8	165.1	-5.0	-4	-15
150	146.1	.0	-.2	-0	-1
160	148.1	-165.1	4.6	-3	14
170	149.7	-342.7	12.8	-7	14
180	165.6	-559.5	18.8	-7	9
190	151.9	-825.0	12.8	-3	3
200	120.0	-933.1	18.8	-4	3
210	95.4	-1010.4	16.0	-4	1
220	68.4	-1138.6	-14.3	3	-1
230	60.1	-1147.6	-29.4	6	-1
240	61.2	-1118.6	-43.6	9	-2
250	13.2	-787.9	-61.4	17	-1
260	-24.3	-732.6	-75.4	23	3
270	-42.3	-702.5	-81.5	26	7
280	-67.7	-584.2	-87.4	33	17
290	-49.2	-520.2	-85.3	36	15
300	-35.0	-345.8	-41.2	26	12
310	-20.0	-186.1	-19.0	22	11
320	-17.3	-73.9	-5.8	16	17
330	-23.3	-.0	-.0	0	0
340	-17.0	73.9	5.8	16	-17
350	-19.5	186.1	19.0	22	-11

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 0 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-35.4	345.8	41.2
.10	8.85	-6.7	9.9	741	1325	-9.0	7.5	23	-70	-28.8	335.9	39.7
.20	17.70	.8	28.7	1514	4085	.5	7.0	43	5	-29.6	307.2	34.1
.30	26.55	-1.3	45.3	1770	7080	-.7	6.4	21	-3	-28.2	261.9	29.8
.40	35.40	-2.6	47.5	1770	7080	-1.5	6.7	21	-5	-25.6	214.4	25.3
.50	44.25	-2.7	51.9	1770	7013	-1.5	7.4	23	-5	-23.0	162.5	20.0
.60	53.10	-4.6	54.4	1770	7010	-2.6	7.8	27	-10	-18.3	108.2	13.4
.70	61.95	-6.8	42.6	1670	5842	-4.1	7.3	21	-15	-11.6	65.5	9.2
.80	70.80	-12.3	32.7	1390	4422	-8.8	7.4	20	-34	.7	32.8	5.8
.90	79.65	.4	25.1	668	3075	.6	8.1	37	3	.3	7.8	1.6
1.00	88.50	.3	7.8	234	506	1.3	15.3	47	8	0.0	0.0	0.0

TABLE 7 SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 10 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-48.5	520.2	85.4
.10	8.85	-9.8	19.9	741	1325	-13.3	15.0	29	-65	-38.6	500.3	82.1
.20	17.70	-1.8	55.2	1514	4085	-1.2	13.5	51	-7	-36.9	445.2	69.6
.30	26.55	-3.6	68.5	1770	7080	-2.1	9.7	33	-8	-33.2	376.6	59.4
.40	35.40	-4.6	69.8	1770	7080	-2.6	9.9	33	-10	-28.6	306.8	49.0
.50	44.25	-4.8	74.0	1770	7013	-2.7	10.6	35	-10	-23.8	232.8	37.4
.60	53.10	-6.4	77.5	1770	7010	-3.6	11.1	38	-14	-17.4	155.3	24.2
.70	61.95	-7.4	59.1	1670	5842	-4.4	10.1	31	-18	-10.0	96.2	15.7
.80	70.80	-11.2	46.9	1390	4422	-8.1	10.6	28	-30	1.2	49.2	9.4
.90	79.65	.9	37.2	668	3075	1.4	12.1	40	5	.2	12.0	2.6
1.00	88.50	.2	12.0	234	506	1.0	23.7	49	4	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 20 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-66.9	584.2	87.4
.10	8.85	-9.8	18.4	741	1325	-13.3	13.9	32	-77	-57.1	565.8	84.1
.20	17.70	-2.8	65.0	1514	4085	-1.8	15.9	55	-10	-54.3	500.8	68.0
.30	26.55	-6.0	84.6	1770	7080	-3.4	12.0	28	-9	-48.3	416.2	57.5
.40	35.40	-6.8	83.9	1770	7080	-3.8	11.9	27	-10	-41.5	332.3	47.3
.50	44.25	-6.0	88.7	1770	7013	-3.4	12.6	29	-9	-35.5	243.6	35.5
.60	53.10	-7.8	91.7	1770	7010	-4.4	13.1	34	-13	-27.6	151.9	21.3
.70	61.95	-10.1	64.7	1670	5842	-6.0	11.1	24	-17	-17.6	87.2	14.1
.80	70.80	-16.1	43.4	1390	4422	-11.6	9.8	24	-41	-1.4	43.6	8.7
.90	79.65	-1.2	32.7	668	3075	-1.7	10.6	42	-7	-.3	11.1	2.5
1.00	88.50	-.3	11.1	234	506	-1.2	21.9	50	-6	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 30 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-41.7	702.5	81.5
.10	8.85	-10.5	26.0	741	1325	-14.2	19.6	31	-56	-31.2	676.5	77.3
.20	17.70	-2.3	74.7	1514	4085	-1.5	18.3	49	-7	-28.9	601.8	61.0
.30	26.55	-6.0	105.2	1770	7080	-3.4	14.9	18	-5	-22.9	496.6	52.5
.40	35.40	-7.1	106.7	1770	7080	-4.0	15.1	19	-6	-15.8	389.9	43.2
.50	44.25	-6.0	108.2	1770	7013	-3.4	15.4	20	-5	-9.8	281.7	33.2
.60	53.10	-8.9	105.0	1770	7010	-5.0	15.0	24	-9	-1.0	176.7	22.0
.70	61.95	-9.3	78.7	1670	5842	-5.5	13.5	18	-10	8.3	98.0	15.5
.80	70.80	-4.4	50.4	1390	4422	-3.1	11.4	28	-11	12.6	47.6	9.0
.90	79.65	9.5	34.9	668	3075	14.2	11.4	37	45	3.2	12.7	2.8
1.00	88.50	3.2	12.7	234	506	13.6	25.1	46	51	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 40 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-23.9	732.6	75.4
.10	8.85	-10.4	23.3	741	1325	-14.0	17.5	30	-61	-13.5	709.3	71.6
.20	17.70	-2.5	73.8	1514	4085	-1.7	18.1	46	-7	-11.0	635.6	56.4
.30	26.55	-5.8	114.5	1770	7080	-3.3	16.2	13	-3	-5.2	521.1	50.0
.40	35.40	-6.6	112.0	1770	7080	-3.7	15.8	12	-3	1.3	409.1	43.7
.50	44.25	-4.5	116.6	1770	7013	-2.5	16.6	17	-3	5.8	292.5	34.7
.60	53.10	-6.4	115.2	1770	7010	-3.6	16.4	23	-6	12.2	177.3	22.6
.70	61.95	-6.4	84.0	1670	5842	-3.8	14.4	18	-6	18.6	93.3	15.7
.80	70.80	.7	47.7	1390	4422	.5	10.8	33	2	17.9	45.6	8.7
.90	79.65	13.6	33.9	668	3075	20.3	11.0	35	62	4.3	11.8	2.5
1.00	88.50	4.3	11.8	234	506	18.5	23.2	42	70	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 50 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									13.7	787.9	61.5
.10	8.85	-5.5	26.4	741	1325	-7.5	19.9	33	-31	19.2	761.5	57.4
.20	17.70	4.0	78.0	1514	4085	2.7	19.1	43	10	15.2	683.5	42.2
.30	26.55	-1.0	126.8	1770	7080	-.6	17.9	8	-0	16.2	556.7	37.7
.40	35.40	-3.6	124.9	1770	7080	-2.0	17.6	8	-1	19.8	431.8	33.2
.50	44.25	-1.6	128.5	1770	7013	-.9	18.3	12	-1	21.4	303.3	26.4
.60	53.10	-3.5	124.7	1770	7010	-2.0	17.8	17	-2	24.9	178.6	17.0
.70	61.95	-4.8	91.7	1670	5842	-2.8	15.7	10	-2	29.7	86.9	12.7
.80	70.80	4.6	47.0	1390	4422	3.3	10.6	28	12	25.1	39.8	6.7
.90	79.65	18.7	30.5	668	3075	27.9	9.9	25	70	6.5	9.4	1.9
1.00	88.50	6.5	9.4	234	506	27.7	18.5	31	97	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 60 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									62.0	1118.6	43.6
.10	8.85	-7.4	32.7	741	1325	-10.0	24.7	30	-31	69.4	1085.9	38.9
.20	17.70	7.9	98.3	1514	4085	4.6	24.1	39	13	62.4	987.6	21.5
.30	26.55	.8	179.7	1770	7080	.4	25.4	2	0	61.6	807.9	19.7
.40	35.40	-.7	183.3	1770	7080	-.4	25.9	-0	0	62.3	624.6	19.7
.50	44.25	3.9	194.4	1770	7013	2.2	27.7	2	0	58.4	430.2	18.0
.60	53.10	1.4	181.7	1770	7010	.8	25.9	5	0	57.0	248.5	13.7
.70	61.95	-.1	137.2	1670	5842	-.1	23.5	1	-0	57.1	111.4	13.2
.80	70.80	14.0	64.4	1390	4422	10.1	14.6	21	21	43.1	47.0	6.8
.90	79.65	31.6	36.4	668	3075	47.3	11.8	17	66	11.5	10.6	1.9
1.00	88.50	11.5	10.6	234	506	49.3	20.9	19	91	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 70 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									62.7	1147.6	29.4
.10	8.85	-13.3	37.2	741	1325	-17.9	28.0	29	-47	76.0	1110.5	23.9
.20	17.70	-.7	101.8	1514	4085	-.5	24.9	39	-1	76.7	1008.7	6.1
.30	26.55	-2.9	184.7	1770	7080	-1.6	26.1	-1	0	79.6	823.9	6.7
.40	35.40	1.0	188.4	1770	7080	.6	26.6	-3	-0	78.6	635.5	8.9
.50	44.25	9.3	196.5	1770	7013	5.2	28.0	-1	-0	69.3	439.0	10.2
.60	53.10	4.2	181.5	1770	7010	2.4	25.9	0	0	65.1	257.5	9.9
.70	61.95	3.4	140.1	1670	5842	2.0	24.0	-3	-0	61.8	117.4	11.8
.80	70.80	15.6	68.9	1390	4422	11.2	15.6	16	16	46.2	48.5	6.5
.90	79.65	33.7	37.9	668	3075	50.5	12.3	15	60	12.5	10.6	1.9
1.00	88.50	12.5	10.6	234	506	53.7	20.9	17	90	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 80 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									72.9	1138.6	14.4
.10	8.85	-17.1	35.6	741	1325	-23.1	26.9	27	-59	90.0	1103.0	9.1
.20	17.70	-2.9	98.1	1514	4085	-1.9	24.0	38	-5	92.9	1004.9	-7.8
.30	26.55	-1.6	182.1	1770	7080	-.9	25.7	-3	0	94.5	822.8	-5.0
.40	35.40	4.8	184.4	1770	7080	2.7	26.0	-6	-1	89.7	638.4	-.2
.50	44.25	14.6	190.2	1770	7013	8.2	27.1	-5	-2	75.1	448.2	4.4
.60	53.10	6.6	175.6	1770	7010	3.8	25.1	-4	-1	68.5	272.6	7.7
.70	61.95	6.7	141.2	1670	5842	4.0	24.2	-6	-1	61.7	131.4	11.6
.80	70.80	17.4	75.1	1390	4422	12.5	17.0	13	13	44.3	56.3	7.1
.90	79.65	32.4	43.8	668	3075	48.5	14.3	16	52	11.9	12.5	2.3
1.00	88.50	11.9	12.5	234	506	51.1	24.7	22	93	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 90 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									90.5	1010.4	-15.9
.10	8.85	-16.6	29.7	741	1325	-22.4	22.4	23	-58	107.0	980.7	-20.0
.20	17.70	-1.5	72.0	1514	4085	-1.0	17.6	28	-3	108.5	908.7	-29.0
.30	26.55	2.2	164.0	1770	7080	1.3	23.2	-9	-1	106.3	744.6	-22.2
.40	35.40	9.9	166.1	1770	7080	5.6	23.5	-11	-3	96.4	578.5	-13.8
.50	44.25	18.9	170.9	1770	7013	10.7	24.4	-11	-5	77.5	407.6	-5.3
.60	53.10	10.1	158.1	1770	7010	5.7	22.6	-10	-3	67.4	249.5	1.5
.70	61.95	10.7	130.4	1670	5842	6.4	22.3	-10	-4	56.7	119.1	7.2
.80	70.80	17.9	70.9	1390	4422	12.9	16.0	7	9	38.8	48.2	4.6
.90	79.65	28.4	39.1	668	3075	42.5	12.7	12	38	10.4	9.0	1.5
1.00	88.50	10.4	9.0	234	506	44.6	17.8	16	83	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 100 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									124.7	933.1	-18.8
		-13.1	27.3	741	1325	-17.7	20.6	25	-54			
.10	8.85									137.8	905.8	-22.6
		2.7	63.7	1514	4085	1.8	15.6	27	5			
.20	17.70									135.1	842.1	-30.4
		8.4	147.4	1770	7080	4.7	20.8	-10	-2			
.30	26.55									126.7	694.7	-24.0
		15.9	149.7	1770	7080	9.0	21.1	-12	-6			
.40	35.40									110.8	545.0	-15.7
		22.9	154.4	1770	7013	12.9	22.0	-13	-8			
.50	44.25									87.9	390.6	-6.8
		17.9	144.3	1770	7010	10.1	20.6	-11	-6			
.60	53.10									70.0	246.3	.5
		17.3	121.9	1670	5842	10.4	20.9	-10	-6			
.70	61.95									52.7	124.4	6.1
		19.7	73.1	1390	4422	14.1	16.5	4	5			
.80	70.80									33.0	51.3	4.5
		24.2	42.0	668	3075	36.2	13.7	12	31			
.90	79.65									8.8	9.3	1.5
		8.8	9.3	234	506	37.8	18.3	19	83			
1.00	88.50									0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 110 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									155.6	825.0	-12.9
.10	8.85	-9.7	24.3	741	1325	-13.1	18.3	29	-53	165.3	800.7	-16.6
.20	17.70	7.2	58.8	1514	4085	4.8	14.4	31	17	158.0	741.9	-24.9
.30	26.55	16.3	127.3	1770	7080	9.2	18.0	-8	-5	141.7	614.6	-20.0
.40	35.40	22.7	128.2	1770	7080	12.8	18.1	-11	-9	119.0	486.5	-13.4
.50	44.25	26.8	131.3	1770	7013	15.1	18.7	-12	-11	92.2	355.2	-6.3
.60	53.10	23.5	124.2	1770	7010	13.3	17.7	-10	-9	68.7	231.0	-.4
.70	61.95	21.3	107.3	1670	5842	12.8	18.4	-10	-9	47.4	123.7	4.5
.80	70.80	20.6	71.5	1390	4422	14.8	16.2	1	2	26.8	52.2	4.0
.90	79.65	19.8	43.1	668	3075	29.7	14.0	11	22	7.0	9.0	1.5
1.00	88.50	7.0	9.0	234	506	30.0	17.9	24	82	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 120 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									168.2	559.5	-19.0
.10	8.85	-8.8	14.8	741	1325	-11.9	11.2	25	-66	177.0	544.7	-21.2
.20	17.70	9.0	34.0	1514	4085	5.9	8.3	20	24	168.0	510.8	-24.5
.30	26.55	21.5	88.1	1770	7080	12.1	12.4	-14	-16	146.5	422.7	-18.5
.40	35.40	27.3	84.9	1770	7080	15.4	12.0	-15	-22	119.2	337.8	-12.2
.50	44.25	30.6	83.9	1770	7013	17.3	12.0	-14	-23	88.6	253.9	-6.2
.60	53.10	27.3	80.5	1770	7010	15.4	11.5	-12	-19	61.3	173.4	-1.2
.70	61.95	23.9	75.2	1670	5842	14.3	12.9	-9	-13	37.5	98.2	2.1
.80	70.80	15.5	56.1	1390	4422	11.1	12.7	-1	-1	22.0	42.1	2.4
.90	79.65	16.5	36.6	668	3075	24.7	11.9	8	16	5.5	5.5	.8
1.00	88.50	5.5	5.5	234	506	23.6	10.9	16	74	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 130 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									150.3	342.7	-13.1
.10	8.85	-14.1	9.3	741	1325	-19.0	7.0	10	-67	164.4	333.4	-14.4
.20	17.70	5.5	19.9	1514	4085	3.6	4.9	16	20	158.9	313.5	-16.0
.30	26.55	22.4	54.9	1770	7080	12.7	7.8	-16	-29	136.5	258.6	-11.4
.40	35.40	27.0	50.3	1770	7080	15.2	7.1	-14	-34	109.5	208.3	-7.2
.50	44.25	29.3	47.9	1770	7013	16.6	6.8	-11	-31	80.2	160.4	-3.9
.60	53.10	27.0	46.7	1770	7010	15.2	6.7	-11	-28	53.3	113.6	-.9
.70	61.95	24.4	46.6	1670	5842	14.6	8.0	-8	-18	26.8	67.0	1.1
.80	70.80	11.0	38.0	1390	4422	7.9	8.6	-3	-4	17.8	29.0	1.7
.90	79.65	13.4	25.1	668	3075	20.1	8.2	8	19	4.4	3.9	.6
1.00	88.50	4.4	3.9	234	506	19.0	7.6	15	77	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 140 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									147.8	165.1	-5.0
.10	8.85	-15.1	3.5	741	1325	-20.3	2.6	1	-29	162.9	161.6	-5.4
.20	17.70	5.5	7.4	1514	4085	3.6	1.8	8	26	157.5	154.2	-5.8
.30	26.55	24.3	25.4	1770	7080	13.8	3.6	-14	-59	133.1	128.8	-2.8
.40	35.40	28.0	22.2	1770	7080	15.8	3.1	-9	-54	105.1	106.7	-.4
.50	44.25	29.5	21.1	1770	7013	16.7	3.0	-5	-34	75.6	85.6	1.2
.60	53.10	28.9	22.0	1770	7010	16.3	3.1	-4	-22	46.7	63.6	2.2
.70	61.95	25.3	22.9	1670	5842	15.2	3.9	-1	-7	21.3	40.7	2.5
.80	70.80	7.4	20.8	1390	4422	5.3	4.7	2	4	14.0	19.8	2.2
.90	79.65	10.4	15.7	668	3075	15.6	5.1	14	42	3.6	4.1	.8
1.00	88.50	3.6	4.1	234	506	15.3	8.2	26	99	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 150 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									146.1	.0	-.2
.10	8.85	-15.3	-.0	741	1325	-20.7	-.0	0	0	161.4	.0	-.2
.20	17.70	4.5	.0	1514	4085	3.0	.0	0	0	156.9	.0	-.2
.30	26.55	24.3	.0	1770	7080	13.7	.0	-0	-0	132.6	.0	-.2
.40	35.40	28.2	.0	1770	7080	16.0	.0	0	0	104.3	.0	-.2
.50	44.25	29.7	.0	1770	7013	16.8	.0	-0	-0	74.6	.0	-.2
.60	53.10	29.3	.0	1770	7010	16.6	.0	0	0	45.3	.0	-.2
.70	61.95	25.6	.0	1670	5842	15.3	.0	0	0	19.7	.0	-.2
.80	70.80	7.2	.0	1390	4422	5.2	.0	-0	-26	12.5	-.0	.0
.90	79.65	9.3	-.0	668	3075	13.9	-.0	-0	0	3.2	.0	.0
1.00	88.50	3.2	.0	234	506	13.7	.0	0	0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 160 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									148.1	-165.1	4.6
.10	8.85	-15.1	-3.5	741	1325	-20.3	-2.6	1	29	163.2	-161.6	5.1
.20	17.70	5.5	-7.4	1514	4085	3.6	-1.8	8	-26	157.8	-154.2	5.5
.30	26.55	24.3	-25.4	1770	7080	13.8	-3.6	-14	59	133.4	-128.8	2.5
.40	35.40	28.0	-22.2	1770	7080	15.8	-3.1	-9	54	105.4	-106.7	.0
.50	44.25	29.5	-21.1	1770	7013	16.7	-3.0	-5	34	75.9	-85.6	-1.5
.60	53.10	28.9	-22.0	1770	7010	16.3	-3.1	-4	22	47.0	-63.6	-2.5
.70	61.95	25.3	-22.9	1670	5842	15.2	-3.9	-1	7	21.6	-40.7	-2.8
.80	70.80	7.7	-20.8	1390	4422	5.5	-4.7	5	-9	14.0	-19.8	-2.2
.90	79.65	10.4	-15.7	668	3075	15.6	-5.1	14	-42	3.6	-4.1	-.8
1.00	88.50	3.6	-4.1	234	506	15.3	-8.2	26	-99	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 170 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									149.7	-342.7	12.8
.10	8.85	-14.1	-9.3	741	1325	-19.0	-7.0	10	67	163.8	-333.4	14.2
.20	17.70	5.5	-19.9	1514	4085	3.6	-4.9	16	-20	158.3	-313.5	15.7
.30	26.55	22.4	-54.9	1770	7080	12.7	-7.8	-16	29	135.9	-258.6	11.1
.40	35.40	27.0	-50.3	1770	7080	15.2	-7.1	-14	34	108.9	-208.3	7.0
.50	44.25	29.3	-47.9	1770	7013	16.6	-6.8	-11	31	79.6	-160.4	3.7
.60	53.10	27.0	-46.7	1770	7010	15.2	-6.7	-11	28	52.6	-113.6	.6
.70	61.95	24.4	-46.6	1670	5842	14.6	-8.0	-8	18	28.2	-67.0	-1.4
.80	70.80	10.4	-38.0	1390	4422	7.5	-8.6	-2	2	17.8	-29.0	-1.7
.90	79.65	13.4	-25.1	668	3075	20.1	-8.2	8	-19	4.4	-3.9	-.6
1.00	88.50	4.4	-3.9	234	506	19.0	-7.6	15	-77	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 180 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									165.6	-559.5	18.8
		-8.8	-14.8	741	1325	-11.9	-11.2	25	66			
.10	8.85									174.4	-544.7	21.0
		9.0	-34.0	1514	4085	5.9	-8.3	20	-24			
.20	17.70									165.5	-510.8	24.3
		21.5	-88.1	1770	7080	12.1	-12.4	-14	16			
.30	26.55									144.0	-422.7	18.4
		27.3	-84.9	1770	7080	15.4	-12.0	-15	22			
.40	35.40									116.7	-337.8	12.0
		30.6	-83.9	1770	7013	17.3	-12.0	-14	23			
.50	44.25									86.1	-253.9	6.0
		27.3	-80.5	1770	7010	15.4	-11.5	-12	19			
.60	53.10									58.8	-173.4	1.1
		23.9	-75.2	1670	5842	14.3	-12.9	-9	13			
.70	61.95									34.9	-98.2	-2.3
		13.0	-56.1	1390	4422	9.3	-12.7	-0	0			
.80	70.80									22.0	-42.1	-2.4
		16.5	-36.6	668	3075	24.7	-11.9	8	-16			
.90	79.65									5.5	-5.5	-.8
		5.5	-5.5	234	506	23.6	-10.9	16	-74			
1.00	88.50									0.0	0.0	0.0

TABLE 7 SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 190 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									151.9	-825.0	12.8
.10	8.85	-9.7	-24.3	741	1325	-13.1	-18.3	29	53	161.6	-800.7	16.6
.20	17.70	7.2	-58.8	1514	4085	4.8	-14.4	31	-17	154.4	-741.9	24.9
.30	26.55	16.3	-127.3	1770	7080	9.2	-18.0	-8	5	138.0	-614.6	20.0
.40	35.40	22.7	-128.2	1770	7080	12.8	-18.1	-11	9	115.3	-486.5	13.3
.50	44.25	26.8	-131.3	1770	7013	15.1	-18.7	-12	11	88.5	-355.2	6.2
.60	53.10	23.5	-124.2	1770	7010	13.3	-17.7	-10	9	65.0	-231.0	.3
.70	61.95	21.3	-107.3	1670	5842	12.8	-18.4	-10	9	43.7	-123.7	-4.6
.80	70.80	16.9	-71.5	1390	4422	12.2	-16.2	2	-2	26.8	-52.2	-4.0
.90	79.65	19.8	-43.1	668	3075	29.7	-14.0	11	-22	7.0	-9.0	-1.5
1.00	88.50	7.0	-9.0	234	506	30.0	-17.9	24	-82	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 200 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									120.0	-933.1	18.8
.10	8.85	-13.1	-27.3	741	1325	-17.7	-20.6	25	54	133.1	-905.8	22.6
.20	17.70	2.7	-63.7	1514	4085	1.8	-15.6	27	-5	130.4	-842.1	30.5
.30	26.55	8.4	-147.4	1770	7080	4.7	-20.8	-10	2	122.0	-694.7	24.1
.40	35.40	15.9	-149.7	1770	7080	9.0	-21.1	-12	6	106.1	-545.0	15.8
.50	44.25	22.9	-154.4	1770	7013	12.9	-22.0	-13	8	83.3	-390.6	6.8
.60	53.10	17.9	-144.3	1770	7010	10.1	-20.6	-11	6	65.3	-246.3	-.4
.70	61.95	17.3	-121.9	1670	5842	10.4	-20.9	-10	6	48.0	-124.4	-6.0
.80	70.80	15.0	-73.1	1390	4422	10.8	-16.5	4	-4	33.0	-51.3	-4.5
.90	79.65	24.2	-42.0	668	3075	36.2	-13.7	12	-31	8.8	-9.3	-1.5
1.00	88.50	8.8	-9.3	234	506	37.8	-18.3	19	-83	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 210 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									85.4	-1010.4	16.0
.10	8.85	-16.6	-29.7	741	1325	-22.4	-22.4	23	58	101.9	-980.7	20.1
.20	17.70	-1.5	-72.0	1514	4085	-1.0	-17.6	28	3	103.4	-908.7	29.2
.30	26.55	2.2	-164.0	1770	7080	1.3	-23.2	-9	1	101.2	-744.6	22.4
.40	35.40	9.9	-166.1	1770	7080	5.6	-23.5	-11	3	91.3	-578.5	13.9
.50	44.25	18.9	-170.9	1770	7013	10.7	-24.4	-11	5	72.4	-407.6	5.5
.60	53.10	10.1	-158.1	1770	7010	5.7	-22.6	-10	3	62.3	-249.5	-1.4
.70	61.95	10.7	-130.4	1670	5842	6.4	-22.3	-10	4	51.6	-119.1	-7.0
.80	70.80	12.8	-70.9	1390	4422	9.2	-16.0	7	-6	38.8	-48.2	-4.6
.90	79.65	28.4	-39.1	668	3075	42.5	-12.7	12	-38	10.4	-9.0	-1.5
1.00	88.50	10.4	-9.0	234	506	44.6	-17.8	16	-83	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 220 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									68.4	-1138.6	-14.3
.10	8.85	-17.1	-35.6	741	1325	-23.1	-26.9	27	59	85.5	-1103.0	-9.0
.20	17.70	-2.9	-98.1	1514	4085	-1.9	-24.0	38	5	88.3	-1004.9	7.9
.30	26.55	-1.6	-182.1	1770	7080	-.9	-25.7	-3	-0	90.9	-822.8	5.1
.40	35.40	4.8	-184.4	1770	7080	2.7	-26.0	-6	1	85.1	-638.4	.3
.50	44.25	14.6	-190.2	1770	7013	8.2	-27.1	-5	2	70.6	-448.2	-4.3
.60	53.10	6.6	-175.6	1770	7010	3.8	-25.1	-4	1	63.9	-272.6	-7.7
.70	61.95	6.7	-141.2	1670	5842	4.0	-24.2	-6	1	57.2	-131.4	-11.5
.80	70.80	12.9	-75.1	1390	4422	9.3	-17.0	13	-10	44.3	-56.3	-7.1
.90	79.65	32.4	-43.8	668	3075	48.5	-14.3	16	-52	11.9	-12.5	-2.3
1.00	88.50	11.9	-12.5	234	506	51.1	-24.7	22	-93	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 230 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									60.1	-1147.6	-29.4
		-13.3	-37.2	741	1325	-17.9	-28.0	29	47			
.10	8.85									73.3	-1110.5	-23.9
		-.7	-101.8	1514	4085	-.5	-24.9	39	1			
.20	17.70									74.1	-1008.7	-6.0
		-2.9	-184.7	1770	7080	-1.6	-26.1	-1	-0			
.30	26.55									77.0	-823.9	-6.7
		1.0	-188.4	1770	7080	.6	-26.6	-3	0			
.40	35.40									76.0	-635.5	-8.9
		9.3	-196.5	1770	7013	5.2	-28.0	-1	0			
.50	44.25									66.7	-439.0	-10.2
		4.2	-181.5	1770	7010	2.4	-25.9	0	-0			
.60	53.10									62.5	-257.5	-9.9
		3.4	-140.1	1670	5842	2.0	-24.0	-3	0			
.70	61.95									59.1	-117.4	-11.7
		12.9	-68.9	1390	4422	9.3	-15.6	16	-14			
.80	70.80									46.2	-48.5	-6.5
		33.7	-37.9	668	3075	50.5	-12.3	15	-60			
.90	79.65									12.5	-10.6	-1.9
		12.5	-10.6	234	506	53.7	-20.9	17	-90			
1.00	88.50									0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 240 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									61.2	-1118.6	-43.6
.10	8.85	-7.4	-32.7	741	1325	-10.0	-24.7	30	31	68.6	-1085.9	-38.9
.20	17.70	7.0	-98.3	1514	4085	4.6	-24.1	39	-13	61.6	-987.6	-21.5
.30	26.55	.8	-179.7	1770	7080	.4	-25.4	2	-0	60.8	-807.9	-19.7
.40	35.40	-.7	-183.3	1770	7080	-.4	-25.9	-0	-0	61.5	-624.6	-19.7
.50	44.25	3.9	-194.4	1770	7013	2.2	-27.7	2	-0	57.6	-430.2	-18.0
.60	53.10	1.4	-181.7	1770	7010	.8	-25.9	5	-0	56.2	-248.5	-13.7
.70	61.95	-.1	-137.2	1670	5842	-.1	-23.5	1	0	56.4	-111.4	-13.2
.80	70.80	13.3	-64.4	1390	4422	9.5	-14.6	21	-20	43.1	-47.0	-6.8
.90	79.65	31.6	-36.4	668	3075	47.3	-11.8	17	-66	11.5	-10.6	-1.9
1.00	88.50	11.5	-10.6	234	506	49.3	-20.9	19	-91	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 250 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									13.2	-787.9	-61.4
.10	8.85	-5.5	-26.4	741	1325	-7.5	-19.9	33	31	18.7	-761.5	-57.4
.20	17.70	4.0	-78.0	1514	4085	2.7	-19.1	43	-10	14.7	-683.5	-42.2
.30	26.55	-1.0	-126.8	1770	7080	-.6	-17.9	8	0	15.7	-556.7	-37.7
.40	35.40	-3.6	-124.9	1770	7080	-2.0	-17.6	8	1	19.3	-431.8	-33.2
.50	44.25	-1.6	-128.5	1770	7013	-.9	-18.3	12	1	20.9	-303.3	-26.4
.60	53.10	-3.5	-124.7	1770	7010	-2.0	-17.8	17	2	24.4	-178.6	-17.0
.70	61.95	-4.8	-91.7	1670	5842	-2.8	-15.7	10	2	29.2	-86.9	-12.7
.80	70.80	4.1	-47.0	1390	4422	2.9	-10.6	28	-11	25.1	-39.8	-6.7
.90	79.65	18.7	-30.5	668	3075	27.9	-9.9	25	-79	6.5	-9.4	-1.9
1.00	88.50	6.5	-9.4	234	506	27.7	-18.5	31	-97	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 260 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-24.3	-732.6	-75.4
.10	8.85	-10.4	-23.3	741	1325	-14.0	-17.5	30	61	-13.9	-709.3	-71.6
.20	17.70	-2.5	-73.8	1514	4085	-1.7	-18.1	46	7	-11.3	-635.6	-56.4
.30	26.55	-5.8	-114.5	1770	7080	-3.3	-16.2	13	3	-5.6	-521.1	-49.9
.40	35.40	-6.6	-112.0	1770	7080	-3.7	-15.8	12	3	1.0	-409.1	-43.7
.50	44.25	-4.5	-116.6	1770	7013	-2.5	-16.6	17	3	5.4	-292.5	-34.7
.60	53.10	-6.4	-115.2	1770	7010	-3.6	-16.4	23	6	11.9	-177.3	-22.5
.70	61.95	-6.4	-84.0	1670	5842	-3.8	-14.4	18	6	18.2	-93.3	-15.7
.80	70.80	.4	-47.7	1390	4422	.3	-10.8	33	-1	17.9	-45.6	-8.7
.90	79.65	13.6	-33.9	668	3075	20.3	-11.0	35	-62	4.3	-11.8	-2.5
1.00	88.50	4.3	-11.8	234	506	18.5	-23.2	42	-70	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 270 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-42.3	-702.5	-81.5
.10	8.85	-10.5	-26.0	741	1325	-14.2	-19.6	31	56	-31.9	-676.5	-77.3
.20	17.70	-2.3	-74.7	1514	4085	-1.5	-18.3	49	7	-29.6	-601.8	-60.9
.30	26.55	-6.0	-105.2	1770	7080	-3.4	-14.9	18	5	-23.6	-496.6	-52.4
.40	35.40	-7.1	-106.7	1770	7080	-4.0	-15.1	19	6	-16.5	-389.9	-43.1
.50	44.25	-6.0	-108.2	1770	7013	-3.4	-15.4	20	5	-10.5	-281.7	-33.2
.60	53.10	-8.9	-105.0	1770	7010	-5.0	-15.0	24	9	-1.7	-176.7	-21.9
.70	61.95	-9.3	-78.7	1670	5842	-5.5	-13.5	18	10	7.6	-98.0	-15.4
.80	70.80	-5.0	-50.4	1390	4422	-3.6	-11.4	28	13	12.6	-47.6	-9.0
.90	79.65	9.5	-34.9	668	3075	14.2	-11.4	37	-45	3.2	-12.7	-2.8
1.00	88.50	3.2	-12.7	234	506	13.6	-25.1	46	-51	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 280 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-67.7	-584.2	-87.4
.10	8.85	-9.8	-18.4	741	1325	-13.3	-13.9	32	77	-57.8	-565.8	-84.0
.20	17.70	-2.8	-65.0	1514	4085	-1.8	-15.9	55	10	-55.1	-500.8	-68.0
.30	26.55	-6.0	-84.6	1770	7080	-3.4	-12.0	28	9	-49.0	-416.2	-57.4
.40	35.40	-6.8	-83.9	1770	7080	-3.8	-11.9	27	10	-42.3	-332.2	-47.2
.50	44.25	-6.0	-88.7	1770	7013	-3.4	-12.6	29	9	-36.2	-243.6	-35.4
.60	53.10	-7.8	-91.7	1770	7010	-4.4	-13.1	34	13	-28.4	-151.9	-21.2
.70	61.95	-10.1	-64.7	1670	5842	-6.0	-11.1	24	17	-18.3	-87.2	-14.0
.80	70.80	-16.9	-43.4	1390	4422	-12.1	-9.8	24	42	-1.4	-43.8	-8.7
.90	79.65	-1.2	-32.7	668	3075	-1.7	-10.6	42	7	-.3	-11.1	-2.5
1.00	88.50	-.3	-11.1	234	506	-1.2	-21.9	50	6	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 290 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-49.2	-520.2	-85.3
.10	8.85	-9.8	-19.9	741	1325	-13.3	-15.0	29	65	-39.3	-500.3	-82.1
.20	17.70	-1.8	-55.2	1514	4085	-1.2	-13.5	51	7	-37.6	-445.2	-69.5
.30	26.55	-3.6	-68.5	1770	7080	-2.1	-9.7	33	8	-33.9	-376.6	-59.4
.40	35.40	-4.6	-69.8	1770	7080	-2.6	-9.9	33	10	-29.3	-306.8	-49.0
.50	44.25	-4.8	-74.0	1770	7013	-2.7	-10.6	35	10	-24.5	-232.8	-37.4
.60	53.10	-6.4	-77.5	1770	7010	-3.6	-11.1	38	14	-18.1	-155.3	-24.1
.70	61.95	-7.4	-59.1	1670	5842	-4.4	-10.1	31	18	-10.7	-96.2	-15.7
.80	70.80	-11.9	-46.9	1390	4422	-8.6	-10.6	28	32	1.2	-49.2	-9.4
.90	79.65	.9	-37.2	668	3075	1.4	-12.1	40	-5	.2	-12.0	-2.6
1.00	88.50	.2	-12.0	234	506	1.0	-23.7	49	-4	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 300 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-36.0	-345.8	-41.2
.10	8.85	-6.7	-9.9	741	1325	-9.0	-7.5	23	70	-29.4	-335.9	-39.7
.20	17.70	.8	-28.7	1514	4085	.5	-7.0	43	-5	-30.1	-307.2	-34.1
.30	26.55	-1.3	-45.3	1770	7080	-.7	-6.4	21	3	-28.8	-261.9	-29.7
.40	35.40	-2.6	-47.5	1770	7080	-1.5	-6.7	21	5	-26.2	-214.4	-25.3
.50	44.25	-2.7	-51.9	1770	7013	-1.5	-7.4	23	5	-23.5	-162.5	-20.0
.60	53.10	-4.6	-54.4	1770	7010	-2.6	-7.8	27	10	-18.9	-108.2	-13.4
.70	61.95	-6.8	-42.6	1670	5842	-4.1	-7.3	21	15	-12.2	-65.5	-9.2
.80	70.80	-12.9	-32.7	1390	4422	-9.3	-7.4	20	36	.7	-32.8	-5.8
.90	79.65	.4	-25.1	668	3075	.6	-8.1	37	-3	.3	-7.8	-1.6
1.00	88.50	.3	-7.8	234	506	1.3	-15.3	47	-8	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 310 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-20.0	-186.1	-19.0
		-5.1	-3.9	741	1325	-6.9	-3.0	12	69			
.10	8.85									-14.9	-182.2	-18.5
		3.0	-12.3	1514	4085	2.0	-3.0	36	-39			
.20	17.70									-17.9	-169.9	-16.4
		1.7	-23.8	1770	7080	1.0	-3.4	14	-5			
.30	26.55									-19.6	-146.1	-14.9
		.1	-24.4	1770	7080	.1	-3.4	13	-0			
.40	35.40									-19.7	-121.7	-13.4
		-.6	-27.8	1770	7013	-.3	-4.0	18	2			
.50	44.25									-19.2	-93.9	-11.1
		-2.0	-30.5	1770	7010	-1.1	-4.3	26	8			
.60	53.10									-17.2	-63.4	-7.6
		-4.6	-24.5	1670	5842	-2.7	-4.2	20	16			
.70	61.95									-12.6	-38.9	-5.4
		-11.3	-19.4	1390	4422	-8.1	-4.4	16	42			
.80	70.80									-1.3	-19.5	-3.5
		-.9	-15.1	668	3075	-1.4	-4.9	37	10			
.90	79.65									-.4	-4.5	-.9
		-.4	-4.5	234	506	-1.7	-8.8	46	18			
1.00	88.50									0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 320 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-17.3	-73.9	-5.8
.10	8.85	-4.0	-.6	741	1325	-5.4	-.4	-0	-4	-13.3	-73.3	-5.8
.20	17.70	3.8	-1.6	1514	4085	2.5	-.4	-8	84	-17.0	-71.7	-6.1
.30	26.55	2.7	-9.0	1770	7080	1.5	-1.3	1	-1	-19.7	-62.8	-6.1
.40	35.40	.6	-9.1	1770	7080	.4	-1.3	-0	0	-20.4	-53.7	-6.1
.50	44.25	-.6	-11.2	1770	7013	-.3	-1.6	13	3	-19.8	-42.5	-5.5
.60	53.10	-1.9	-13.4	1770	7010	-1.1	-1.9	26	16	-17.9	-29.1	-3.9
.70	61.95	-4.4	-11.2	1670	5842	-2.6	-1.9	19	33	-13.6	-17.9	-2.8
.80	70.80	-11.1	-8.8	1390	4422	-8.0	-2.0	10	57	-2.5	-9.1	-1.8
.90	79.65	-1.8	-7.0	668	3075	-2.7	-2.3	39	46	-.7	-2.1	-.4
1.00	88.50	-.7	-2.1	234	506	-3.0	-4.1	41	64	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 330 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-23.3	-.0	-.0
.10	8.85	-3.1	-.0	741	1325	-4.2	-.0	-0	-0	-20.2	-.0	-.0
.20	17.70	3.2	-.0	1514	4085	2.1	-.0	0	-0	-23.3	-.0	-.0
.30	26.55	2.0	-.0	1770	7080	1.1	-.0	-0	0	-25.3	-.0	-.0
.40	35.40	-.4	-.0	1770	7080	-.2	-.0	-0	-0	-24.9	-.0	-.0
.50	44.25	-1.8	.0	1770	7013	-1.0	.0	0	-0	-23.1	-.0	-.0
.60	53.10	-2.7	.0	1770	7010	-1.5	.0	0	-0	-20.4	-.0	-.0
.70	61.95	-5.0	-.0	1670	5842	-3.0	-.0	0	0	-15.4	-.0	-.0
.80	70.80	-11.1	-.0	1390	4422	-8.0	-.0	0	1	-4.3	-.0	.0
.90	79.65	-2.9	-.0	668	3075	-4.4	-.0	-0	-0	-1.3	.0	.0
1.00	88.50	-1.3	.0	234	506	-5.7	.0	0	-0	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 340 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-17.0	73.9	5.8
.10	8.85	-4.0	.6	741	1325	-5.4	.4	-0	4	-13.0	73.3	5.8
.20	17.70	3.8	1.6	1514	4085	2.5	.4	-8	-84	-16.8	71.7	6.1
.30	26.55	2.7	9.0	1770	7080	1.5	1.3	1	1	-19.5	62.8	6.1
.40	35.40	.6	9.1	1770	7080	.4	1.3	-0	-0	-20.1	53.7	6.1
.50	44.25	-.6	11.2	1770	7013	-.3	1.6	13	-3	-19.6	42.5	5.5
.60	53.10	-1.9	13.4	1770	7010	-1.1	1.9	26	-16	-17.7	29.1	3.9
.70	61.95	-4.4	11.2	1670	5842	-2.6	1.9	19	-33	-13.3	17.9	2.8
80	70.80	-10.8	8.8	1390	4422	-7.8	2.0	10	-57	-2.5	9.1	1.8
90	79.65	-1.8	7.0	668	3075	-2.7	2.3	39	-46	-.7	2.1	.4
1 00	88.50	-.7	2.1	234	506	-3.0	4.1	41	-64	0.0	0.0	0.0

TABLE 7. SHEAR AND MOMENT DIAGRAMS : MILLION DOLLAR PIER, ATLANTIC CITY
WIND DIRECTION 350 CONFIGURATION A REFERENCE PRESSURE 39.0 PSF GUST FACTOR 1.32
ECCENTRICITIES BASED ON 450 FT IN THE X DIRECTION AND 100 FT IN THE Y DIRECTION

FLOOR	HEIGHT	FORCE (KIPS) X	FORCE (KIPS) Y	AREA (SQ FT) X	AREA (SQ FT) Y	PRESSURE (PSF) X	PRESSURE (PSF) Y	ECCEN (%) X	ECCEN (%) Y	SHEAR (KIPS) X	SHEAR (KIPS) Y	MOMENT (1000-FT-KIPS) Z
.00	0.00									-19.5	186.1	19.0
.10	8.85	-5.1	3.9	741	1325	-6.9	3.0	12	-69	-14.4	182.2	18.5
.20	17.70	3.0	12.3	1514	4085	2.0	3.0	36	39	-17.4	169.9	16.4
.30	26.55	1.7	23.8	1770	7080	1.0	3.4	14	5	-19.2	146.1	14.9
.40	35.40	.1	24.4	1770	7080	.1	3.4	13	0	-19.3	121.7	13.4
.50	44.25	-.6	27.8	1770	7013	-.3	4.0	18	-2	-18.7	93.9	11.1
.60	53.10	-2.0	30.5	1770	7010	-1.1	4.3	26	-8	-16.7	63.4	7.6
.70	61.95	-4.6	24.5	1670	5842	-2.7	4.2	20	-16	-12.2	38.9	5.4
.80	70.80	-10.8	19.4	1390	4422	-7.8	4.4	16	-41	-1.3	19.5	3.5
.90	79.65	-.9	15.1	668	3075	-1.4	4.9	37	-10	-.4	4.5	.9
1.00	88.50	-.4	4.5	234	506	-1.7	8.8	46	-18	0.0	0.0	0.0

TABLE 7. MILLION DOLLAR PIER, ATLANTIC CITY
PROJECT 7710 CONFIGURATION A
SCALE = 300 REF. PRESSURE = 30.0
GUST FACTOR = 1.32 STANDARD FLOOR HEIGHT = 8.85
NUMBER OF SIDES = 12 NO. OF FLOORS = 10

SIDE	ANGLE	Z-AXIS
1	90.0	18.000
2	90.0	10.000
3	90.0	2.000
4	90.0	-6.000
5	0.0	0.000
6	180.0	4.000
7	270.0	-10.000
8	270.0	-2.000
9	270.0	6.000
10	270.0	14.000
11	0.0	4.000
12	180.0	0.000

FLOOR #	LABEL	HEIGHT-FT
1	.00	8.85
2	.10	8.85
3	.20	8.85
4	.30	8.85
5	.40	8.85
6	.50	8.85
7	.60	8.85
8	.70	8.85
9	.80	8.85
10	.90	8.85

APPENDIX A

PRESSURE DATA

Note: Pressure coefficients are defined in Section 4.3.

Pressure tap designation is explained in Figure 3.

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	1	-.057	.045	.127	-.247
0	2	-.107	.035	.046	-.233
0	3	-.111	.023	-.013	-.214
0	4	-.127	.031	-.042	-.277
0	5	-.095	.028	.084	-.263
0	6	-.065	.031	.067	-.201
0	7	-.075	.045	.151	-.285
0	8	.000	.045	.182	-.153
0	9	-.039	.037	.172	-.191
0	10	-.197	.043	-.075	-.365
0	11	-.245	.071	.046	-.643
0	12	-.192	.050	-.006	-.403
0	13	-.182	.071	.026	-.619
0	14	-.199	.045	-.052	-.397
0	15	-.168	.038	-.060	-.346
0	16	-.111	.035	.040	-.270
0	17	-.166	.076	.033	-.565
0	18	-.134	.023	-.043	-.221
0	19	-.084	.028	.008	-.228
0	20	-.035	.031	.092	-.155
0	21	-.103	.025	-.012	-.263
0	22	-.094	.023	-.008	-.212
0	23	-.124	.027	-.022	-.258
0	24	-.130	.034	-.042	-.322
0	25	-.047	.046	.228	-.196
0	26	-.129	.029	-.020	-.283
0	27	-.104	.023	-.028	-.237
0	28	-.076	.023	.012	-.193
0	29	-.081	.023	.004	-.191
0	30	-.090	.022	-.013	-.208
0	31	-.064	.033	.096	-.196
0	32	-.013	.041	.223	-.162
0	33	-.084	.038	.028	-.296
0	34	-.110	.024	-.022	-.194
0	35	-.089	.025	.003	-.205
0	36	-.067	.023	.028	-.193
0	37	-.031	.044	.207	-.187
0	38	-.064	.036	.181	-.235
0	39	-.116	.027	-.001	-.289
0	40	.020	.066	.458	-.155
0	41	-.084	.024	.008	-.187
0	42	-.096	.024	-.018	-.210
0	43	-.100	.021	-.026	-.214
0	44	-.073	.022	.010	-.175
0	45	-.044	.030	.156	-.169
0	46	-.092	.019	-.022	-.201
0	47	-.110	.032	.006	-.285
0	48	-.073	.025	.010	-.196
0	49	-.072	.021	.010	-.247
0	50	-.165	.029	-.075	-.306
0	51	-.102	.022	-.002	-.189
0	52	-.118	.028	-.028	-.270
0	53	-.103	.026	-.034	-.303
0	54	-.121	.024	-.034	-.246
0	55	-.107	.030	.062	-.341
0	56	-.079	.034	.080	-.311
0	57	-.062	.038	.118	-.274
0	101	-.152	.028	-.029	-.285
0	102	-.141	.028	-.053	-.341
0	103	-.111	.031	.030	-.281
0	104	-.143	.033	-.016	-.285
0	105	-.134	.020	-.066	-.224
0	106	-.129	.021	-.060	-.230
0	107	-.107	.021	-.026	-.225
0	108	-.121	.027	-.034	-.247
0	109	-.139	.032	-.008	-.267
0	110	-.195	.044	-.076	-.380
0	111	-.128	.027	-.049	-.241
0	112	-.212	.056	-.081	-.527
0	113	-.232	.049	-.123	-.473
0	114	-.142	.026	-.062	-.251
0	115	-.166	.041	-.055	-.403
0	116	-.143	.046	-.012	-.473
0	117	-.192	.038	-.091	-.363
0	118	-.242	.061	-.085	-.607
0	119	-.127	.032	-.035	-.288
0	120	-.132	.035	-.031	-.280
0	121	-.118	.025	-.050	-.226
0	122	-.116	.031	.006	-.268
0	123	-.086	.026	.033	-.200
0	124	-.109	.028	-.022	-.238
0	125	-.101	.023	-.028	-.223
0	126	-.125	.025	-.016	-.236
0	127	-.086	.024	.002	-.216
0	128	-.100	.027	-.020	-.242
0	129	-.077	.018	-.015	-.150
0	130	-.114	.028	-.014	-.252
0	131	-.108	.026	-.032	-.234
0	132	-.099	.023	-.020	-.222
0	133	-.082	.019	-.001	-.179
0	134	-.175	.040	-.073	-.397
0	135	-.101	.025	.004	-.227
0	136	-.080	.020	-.007	-.165
0	137	-.087	.019	-.012	-.199
0	138	-.109	.022	-.034	-.245
0	139	-.086	.021	-.014	-.216
0	140	-.084	.023	-.011	-.173
0	141	-.061	.019	.001	-.155
0	142	-.092	.022	-.021	-.200
0	143	-.074	.021	.011	-.173
0	144	-.090	.027	.007	-.222
0	145	-.058	.021	.014	-.143
0	146	-.109	.026	-.030	-.252
0	147	-.068	.020	.002	-.155
0	148	-.085	.025	-.011	-.216
0	149	-.075	.020	-.010	-.192
0	150	-.102	.022	-.034	-.193
0	151	-.085	.022	-.018	-.182
0	152	-.080	.019	-.016	-.165
0	153	-.064	.021	-.001	-.175
0	154	-.093	.023	-.018	-.229
0	155	-.076	.022	-.009	-.180
0	156	-.082	.021	-.011	-.176
0	157	-.069	.021	.003	-.148
0	158	-.125	.027	-.025	-.302
0	159	-.095	.023	-.012	-.243
0	160	-.088	.023	-.022	-.265
0	161	-.095	.019	-.030	-.181
0	162	-.127	.025	-.057	-.218
0	163	-.097	.025	-.018	-.191
0	164	-.091	.026	-.018	-.205
0	165	-.078	.025	.010	-.217
0	166	-.089	.028	-.018	-.216
0	167	-.158	.026	-.072	-.255
0	201	.015	.080	.452	-.216
0	202	.067	.083	.511	-.167
0	203	.064	.071	.539	-.110
0	204	-.128	.081	.419	-.438
0	205	-.105	.047	.258	-.308
0	206	-.107	.034	.077	-.306
0	207	-.129	.039	-.006	-.339
0	208	-.094	.042	.322	-.282
0	209	-.087	.031	.056	-.227
0	210	-.104	.036	.047	-.274
0	211	-.111	.037	.128	-.312
0	212	-.137	.038	.002	-.352
0	213	-.136	.030	-.030	-.279
0	214	-.112	.023	-.036	-.220
0	301	-.097	.024	-.017	-.223
0	302	-.172	.036	-.062	-.409
0	303	-.123	.031	-.034	-.331
0	304	-.114	.025	-.022	-.220
0	305	-.112	.022	-.048	-.203
0	306	-.137	.025	-.064	-.243
0	307	-.112	.022	-.041	-.214
0	308	-.088	.023	.002	-.240
0	309	-.108	.019	-.037	-.190
0	310	-.133	.026	-.034	-.250
0	311	-.111	.030	-.006	-.277
0	312	-.119	.026	-.029	-.242

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0	313	-.093	.021	-.021	-.221
0	314	-.111	.026	-.016	-.234
0	315	-.097	.026	.002	-.257
0	316	-.071	.028	-.000	-.314
0	317	-.061	.021	.020	-.244
0	318	-.113	.020	-.051	-.183
0	319	-.075	.018	-.015	-.136
0	320	-.114	.025	-.028	-.216
0	401	-.059	.046	.191	-.283
0	402	-.052	.026	.092	-.148
0	403	-.102	.025	-.024	-.258
0	404	-.067	.023	.012	-.158
0	405	-.074	.026	.020	-.186
0	406	-.077	.022	-.011	-.177
10	1	-.024	.046	.203	-.221
10	2	-.098	.050	.138	-.293
10	3	-.118	.028	-.008	-.232
10	4	-.188	.047	-.085	-.468
10	5	-.098	.036	.067	-.228
10	6	-.054	.029	.067	-.173
10	7	-.051	.055	.186	-.293
10	8	-.004	.047	.228	-.146
10	9	-.058	.036	.089	-.185
10	10	-.244	.048	-.123	-.483
10	11	-.274	.073	-.086	-.631
10	12	-.220	.053	.026	-.457
10	13	-.165	.089	.031	-.629
10	14	-.242	.053	-.031	-.503
10	15	-.213	.043	-.109	-.401
10	16	-.120	.035	.044	-.287
10	17	-.242	.094	.017	-.746
10	18	-.168	.027	-.091	-.281
10	19	-.099	.028	.033	-.241
10	20	-.034	.034	.121	-.167
10	21	-.125	.028	-.021	-.275
10	22	-.105	.023	-.015	-.217
10	23	-.141	.027	-.058	-.255
10	24	-.137	.034	-.037	-.420
10	25	-.057	.053	.291	-.252
10	26	-.147	.030	-.020	-.320
10	27	-.122	.025	-.038	-.259
10	28	-.092	.026	.031	-.225
10	29	-.094	.021	-.017	-.178
10	30	-.109	.025	-.025	-.235
10	31	-.085	.035	.058	-.232
10	32	-.028	.042	.148	-.205
10	33	-.107	.039	.008	-.302
10	34	-.127	.025	-.045	-.233
10	35	-.109	.029	.003	-.296
10	36	-.083	.025	.010	-.205
10	37	-.060	.044	.125	-.221
10	38	-.076	.036	.097	-.233
10	39	-.131	.030	-.047	-.309
10	40	-.023	.061	.332	-.198
10	41	-.098	.024	-.005	-.201
10	42	-.112	.024	-.038	-.242
10	43	-.115	.024	-.029	-.248
10	44	-.085	.024	.012	-.196
10	45	-.069	.032	.053	-.207
10	46	-.112	.023	-.034	-.212
10	47	-.121	.032	-.006	-.344
10	48	-.099	.036	.017	-.361
10	49	-.082	.023	.006	-.198
10	50	-.171	.034	-.047	-.384
10	51	-.101	.024	-.004	-.201
10	52	-.126	.036	.017	-.321
10	53	-.110	.028	-.005	-.239
10	54	-.134	.027	-.043	-.247
10	55	-.112	.033	.008	-.282
10	56	-.089	.035	.058	-.239
10	57	-.065	.040	.107	-.216
10	101	-.202	.034	-.100	-.375
10	102	-.181	.037	-.074	-.389
10	103	-.153	.039	-.035	-.359
10	104	-.187	.034	-.091	-.367
10	105	-.175	.027	-.098	-.325
10	106	-.163	.027	-.083	-.275
10	107	-.136	.027	-.049	-.262
10	108	-.157	.032	-.077	-.293
10	109	-.171	.031	-.059	-.316
10	110	-.241	.050	-.102	-.453
10	111	-.168	.033	-.096	-.330
10	112	-.260	.065	-.104	-.748
10	113	-.278	.056	-.153	-.513
10	114	-.176	.034	-.051	-.316
10	115	-.211	.044	-.035	-.377
10	116	-.189	.057	.017	-.454
10	117	-.231	.040	-.125	-.405
10	118	-.273	.067	-.122	-.693
10	119	-.156	.036	-.031	-.330
10	120	-.168	.040	-.042	-.326
10	121	-.153	.030	-.062	-.285
10	122	-.135	.038	.025	-.342
10	123	-.107	.030	.056	-.226
10	124	-.137	.031	-.022	-.311
10	125	-.129	.026	-.057	-.281
10	126	-.153	.029	-.071	-.285
10	127	-.113	.028	-.034	-.226
10	128	-.120	.028	-.020	-.266
10	129	-.099	.020	-.006	-.187
10	130	-.133	.028	-.028	-.267
10	131	-.126	.027	-.036	-.235
10	132	-.122	.027	-.040	-.239
10	133	-.104	.025	-.028	-.234
10	134	-.182	.042	-.078	-.390
10	135	-.118	.026	-.050	-.235
10	136	-.102	.024	-.029	-.277
10	137	-.100	.020	-.028	-.218
10	138	-.123	.023	-.039	-.232
10	139	-.102	.024	-.012	-.249
10	140	-.104	.026	-.027	-.208
10	141	-.075	.020	-.010	-.169
10	142	-.107	.023	-.037	-.207
10	143	-.093	.021	-.018	-.179
10	144	-.104	.028	-.009	-.250
10	145	-.072	.021	.012	-.160
10	146	-.121	.027	-.030	-.283
10	147	-.086	.020	-.000	-.167
10	148	-.096	.025	-.009	-.273
10	149	-.086	.020	-.017	-.205
10	150	-.111	.022	-.039	-.210
10	151	-.095	.023	-.030	-.242
10	152	-.095	.019	-.027	-.190
10	153	-.076	.021	-.003	-.182
10	154	-.101	.023	-.023	-.214
10	155	-.088	.022	-.023	-.179
10	156	-.094	.024	-.009	-.257
10	157	-.074	.023	.048	-.167
10	158	-.125	.027	-.030	-.415
10	159	-.098	.024	-.005	-.204
10	160	-.095	.023	-.022	-.206
10	161	-.094	.019	-.024	-.173
10	162	-.122	.024	-.034	-.221
10	163	-.096	.024	.004	-.201
10	164	-.094	.028	.007	-.239
10	165	-.079	.025	.005	-.214
10	166	-.095	.030	.011	-.314
10	167	-.204	.037	-.100	-.360
10	201	.023	.087	.452	-.283
10	202	.076	.084	.530	-.127
10	203	.067	.070	.441	-.102
10	204	-.186	.072	.202	-.490
10	205	-.080	.046	.115	-.321
10	206	-.161	.043	.080	-.358
10	207	-.097	.039	.019	-.269
10	208	-.076	.047	.202	-.244
10	209	-.077	.038	.090	-.217
10	210	-.135	.051	.022	-.373
10	211	-.139	.038	.099	-.298
10	212	-.129	.043	.059	-.353

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
10	213	-.160	.038	-.030	-.355
10	214	-.136	.029	-.031	-.270
10	301	-.101	.025	-.028	-.292
10	302	-.176	.042	-.048	-.385
10	303	-.116	.030	-.018	-.292
10	304	-.117	.030	-.007	-.259
10	305	-.112	.026	-.005	-.225
10	306	-.135	.027	-.034	-.239
10	307	-.124	.029	-.034	-.262
10	308	-.100	.024	-.002	-.241
10	309	-.103	.021	-.030	-.189
10	310	-.132	.031	-.030	-.305
10	311	-.119	.039	.025	-.676
10	312	-.113	.025	-.049	-.253
10	313	.091	.019	-.030	-.180
10	314	-.114	.024	-.046	-.235
10	315	-.105	.027	.004	-.265
10	316	-.079	.027	.004	-.234
10	317	.070	.021	-.002	-.286
10	318	-.137	.022	-.068	-.214
10	319	-.096	.022	-.028	-.177
10	320	-.125	.037	-.003	-.409
10	401	.065	.045	.130	-.272
10	402	.055	.029	.117	-.237
10	403	-.120	.027	-.036	-.260
10	404	.080	.024	.008	-.193
10	405	.092	.027	.026	-.212
10	406	.092	.023	.000	-.200
20	1	-.028	.045	.208	-.218
20	2	-.132	.056	.138	-.341
20	3	.088	.032	.057	-.217
20	4	.244	.064	-.092	-.573
20	5	-.090	.046	.131	-.366
20	6	.058	.030	.063	-.183
20	7	.034	.060	.186	-.265
20	8	.002	.049	.227	-.157
20	9	-.071	.035	.084	-.227
20	10	-.266	.052	-.146	-.472
20	11	-.254	.072	-.080	-.629
20	12	-.231	.053	-.042	-.483
20	13	-.159	.091	.057	-.888
20	14	-.264	.056	-.036	-.502
20	15	-.209	.042	-.091	-.409
20	16	-.127	.035	.037	-.315
20	17	-.223	.074	.022	-.583
20	18	-.174	.026	-.100	-.298
20	19	-.104	.031	-.003	-.436
20	20	.056	.037	.137	-.205
20	21	-.123	.026	-.028	-.225
20	22	-.124	.027	-.013	-.263

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	23	-.116	.024	-.028	-.256
20	24	-.127	.033	-.026	-.397
20	25	-.094	.045	.084	-.341
20	26	-.148	.031	-.029	-.302
20	27	-.103	.025	-.015	-.247
20	28	-.108	.030	-.015	-.300
20	29	-.100	.020	-.017	-.171
20	30	-.131	.029	.001	-.348
20	31	-.077	.044	.181	-.247
20	32	-.060	.036	.101	-.200
20	33	-.114	.035	-.003	-.359
20	34	-.149	.029	-.054	-.295
20	35	-.120	.031	-.010	-.267
20	36	-.098	.024	-.026	-.234
20	37	-.091	.040	.073	-.321
20	38	-.100	.035	.067	-.243
20	39	-.156	.031	-.037	-.319
20	40	-.058	.054	.207	-.300
20	41	-.115	.029	-.001	-.263
20	42	-.135	.026	-.052	-.245
20	43	-.136	.027	-.053	-.303
20	44	-.104	.025	-.015	-.254
20	45	-.091	.041	.060	-.312
20	46	-.142	.028	-.048	-.355
20	47	-.146	.036	.001	-.301
20	48	-.138	.057	.033	-.523
20	49	-.103	.022	-.039	-.220
20	50	-.197	.048	-.013	-.550
20	51	-.113	.030	.037	-.274
20	52	-.148	.051	.078	-.487
20	53	-.119	.031	-.039	-.297
20	54	-.161	.033	-.031	-.332
20	55	-.139	.037	.051	-.296
20	56	-.108	.041	.112	-.408
20	57	-.079	.038	.138	-.274
20	101	-.252	.044	-.132	-.447
20	102	-.237	.050	-.114	-.492
20	103	-.199	.053	-.053	-.465
20	104	-.221	.042	-.104	-.400
20	105	-.223	.043	-.119	-.413
20	106	-.206	.038	-.109	-.377
20	107	-.168	.040	-.067	-.322
20	108	-.196	.046	-.077	-.373
20	109	-.206	.042	-.082	-.401
20	110	-.302	.061	-.150	-.557
20	111	-.210	.050	-.092	-.399
20	112	-.264	.058	-.117	-.552
20	113	-.290	.052	-.165	-.539
20	114	-.237	.035	-.145	-.406
20	115	-.216	.042	-.107	-.417

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	116	-.206	.056	-.046	-.503
20	117	-.246	.037	-.139	-.440
20	118	-.321	.065	-.143	-.722
20	119	-.164	.037	-.042	-.429
20	120	-.163	.037	-.049	-.426
20	121	-.153	.028	-.068	-.310
20	122	-.142	.041	-.000	-.337
20	123	-.114	.029	-.045	-.233
20	124	-.139	.033	-.029	-.284
20	125	-.127	.025	-.017	-.252
20	126	-.149	.027	-.053	-.271
20	127	-.115	.027	-.018	-.231
20	128	-.114	.025	-.034	-.222
20	129	-.101	.018	-.033	-.178
20	130	-.123	.025	-.019	-.226
20	131	-.116	.023	-.036	-.247
20	132	-.116	.024	-.018	-.273
20	133	-.106	.022	-.012	-.187
20	134	-.166	.044	-.048	-.490
20	135	-.110	.024	-.025	-.229
20	136	-.105	.021	-.038	-.179
20	137	-.099	.018	-.046	-.178
20	138	-.121	.022	-.053	-.212
20	139	-.100	.021	-.034	-.188
20	140	-.107	.022	-.002	-.190
20	141	-.090	.020	-.008	-.172
20	142	-.115	.022	-.030	-.207
20	143	-.102	.020	-.036	-.206
20	144	-.129	.030	-.025	-.291
20	145	-.094	.023	-.023	-.203
20	146	-.148	.031	-.055	-.321
20	147	-.107	.023	-.025	-.206
20	148	-.121	.029	-.018	-.289
20	149	-.106	.022	-.028	-.243
20	150	-.128	.024	-.041	-.232
20	151	-.114	.025	-.014	-.294
20	152	-.117	.024	-.040	-.235
20	153	-.095	.020	-.033	-.198
20	154	-.117	.023	-.048	-.235
20	155	-.101	.024	-.032	-.263
20	156	-.106	.023	-.034	-.202
20	157	-.085	.022	-.006	-.187
20	158	-.131	.028	-.019	-.253
20	159	-.109	.025	-.023	-.211
20	160	-.106	.026	-.020	-.255
20	161	-.099	.020	-.019	-.196
20	162	-.131	.028	-.019	-.267
20	163	-.107	.027	-.016	-.238
20	164	-.103	.027	-.022	-.251
20	165	-.090	.023	-.021	-.223

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
20	166	-.110	.026	-.012	-.235
20	167	-.239	.042	-.125	-.405
20	201	.017	.083	.445	-.195
20	202	.086	.095	.567	-.163
20	203	.078	.082	.449	-.151
20	204	-.209	.068	.113	-.522
20	205	-.085	.054	.111	-.387
20	206	-.230	.053	-.090	-.465
20	207	-.098	.046	.095	-.297
20	208	-.080	.055	.227	-.269
20	209	-.077	.050	.210	-.260
20	210	-.189	.062	.020	-.499
20	211	-.167	.040	-.039	-.346
20	212	-.141	.058	-.070	-.437
20	213	-.192	.053	-.061	-.457
20	214	-.163	.041	-.016	-.340
20	301	-.123	.029	-.028	-.295
20	302	-.200	.064	-.023	-.631
20	303	-.125	.036	.002	-.331
20	304	-.136	.039	.027	-.349
20	305	-.125	.031	-.037	-.263
20	306	-.145	.032	-.028	-.301
20	307	-.150	.043	.027	-.387
20	308	-.119	.024	-.036	-.244
20	309	-.114	.024	-.006	-.263
20	310	-.150	.041	-.009	-.553
20	311	-.148	.051	-.000	-.514
20	312	-.120	.028	.011	-.264
20	313	-.104	.021	-.003	-.189
20	314	-.135	.031	-.005	-.360
20	315	-.132	.033	-.007	-.340
20	316	-.093	.026	-.011	-.278
20	317	-.091	.025	-.011	-.238
20	318	-.141	.020	-.077	-.224
20	319	-.102	.025	-.024	-.200
20	320	-.158	.055	.079	-.806
20	401	-.067	.053	.316	-.267
20	402	-.067	.031	.126	-.236
20	403	-.137	.028	-.036	-.295
20	404	-.096	.027	.014	-.233
20	405	-.115	.031	-.009	-.378
20	406	-.115	.029	-.022	-.333
30	1	-.045	.055	.203	-.516
30	2	-.144	.059	.217	-.363
30	3	-.162	.037	.023	-.313
30	4	-.270	.068	-.058	-.566
30	5	-.104	.047	.079	-.282
30	6	-.082	.035	.059	-.270
30	7	-.121	.078	.269	-.413
30	8	-.063	.041	.113	-.251
30	9	-.096	.036	.063	-.257
30	10	-.253	.042	-.155	-.454
30	11	-.311	.062	-.147	-.664
30	12	-.210	.039	-.102	-.418
30	13	-.144	.061	.049	-.550
30	14	-.226	.047	-.051	-.514
30	15	-.275	.036	-.177	-.459
30	16	-.151	.033	-.042	-.317
30	17	-.207	.065	-.073	-.543
30	18	-.179	.026	-.102	-.295
30	19	-.217	.036	-.089	-.406
30	20	-.068	.041	.118	-.235
30	21	-.124	.025	-.042	-.257
30	22	-.144	.031	-.048	-.321
30	23	-.200	.024	-.121	-.294
30	24	-.116	.028	-.013	-.294
30	25	-.122	.043	.074	-.366
30	26	-.161	.034	-.023	-.321
30	27	-.189	.024	-.091	-.291
30	28	-.131	.030	-.042	-.283
30	29	-.108	.021	-.021	-.194
30	30	-.167	.039	-.046	-.405
30	31	-.183	.057	.069	-.425
30	32	-.072	.040	.129	-.223
30	33	-.141	.043	.024	-.580
30	34	-.183	.038	-.046	-.367
30	35	-.203	.041	-.011	-.471
30	36	-.122	.036	-.026	-.479
30	37	-.128	.048	.026	-.521
30	38	-.132	.036	.012	-.325
30	39	-.255	.038	-.140	-.469
30	40	-.091	.058	.170	-.413
30	41	-.133	.033	-.003	-.430
30	42	-.154	.030	.008	-.342
30	43	-.225	.027	-.155	-.384
30	44	-.118	.022	-.035	-.248
30	45	-.104	.044	.054	-.360
30	46	-.171	.030	-.090	-.374
30	47	-.205	.042	.016	-.591
30	48	-.162	.062	-.008	-.566
30	49	-.118	.022	-.039	-.246
30	50	-.219	.053	.003	-.435
30	51	-.119	.035	.023	-.282
30	52	-.161	.056	.063	-.415
30	53	-.122	.028	-.042	-.287
30	54	-.174	.032	-.055	-.321
30	55	-.193	.036	-.009	-.505
30	56	-.121	.038	.038	-.372
30	57	-.087	.038	.131	-.221
30	101	-.271	.044	-.153	-.423
30	102	-.306	.054	-.172	-.522
30	103	-.220	.051	-.042	-.379
30	104	-.201	.035	-.110	-.332
30	105	-.226	.037	-.132	-.365
30	106	-.260	.033	-.174	-.379
30	107	-.168	.034	-.070	-.299
30	108	-.192	.033	-.096	-.337
30	109	-.209	.033	-.113	-.358
30	110	-.311	.041	-.208	-.488
30	111	-.197	.036	-.095	-.381
30	112	-.220	.040	-.094	-.444
30	113	-.249	.036	-.160	-.421
30	114	-.260	.032	-.162	-.391
30	115	-.193	.033	-.097	-.363
30	116	-.183	.044	-.058	-.405
30	117	-.231	.031	-.155	-.360
30	118	-.300	.050	-.147	-.556
30	119	-.165	.033	-.070	-.338
30	120	-.159	.030	-.056	-.306
30	121	-.141	.025	-.059	-.290
30	122	-.142	.036	-.021	-.366
30	123	-.119	.026	-.030	-.260
30	124	-.137	.029	-.022	-.255
30	125	-.116	.023	-.041	-.232
30	126	-.140	.025	-.066	-.274
30	127	-.113	.025	-.030	-.226
30	128	-.112	.024	-.036	-.206
30	129	-.095	.017	-.041	-.168
30	130	-.115	.024	-.025	-.229
30	131	-.114	.023	-.043	-.206
30	132	-.110	.021	-.047	-.219
30	133	-.094	.019	-.035	-.161
30	134	-.139	.032	-.050	-.326
30	135	-.105	.023	-.025	-.228
30	136	-.107	.022	-.034	-.212
30	137	-.097	.017	-.041	-.172
30	138	-.125	.022	-.052	-.247
30	139	-.108	.021	-.023	-.201
30	140	-.129	.027	-.031	-.255
30	141	-.098	.021	-.021	-.201
30	142	-.123	.022	-.059	-.222
30	143	-.111	.021	-.043	-.206
30	144	-.156	.032	-.049	-.348
30	145	-.107	.024	-.005	-.217
30	146	-.175	.040	-.082	-.430
30	147	-.129	.029	-.018	-.260
30	148	-.149	.030	-.060	-.293
30	149	-.120	.021	-.057	-.206
30	150	-.145	.023	-.064	-.242
30	151	-.132	.023	-.059	-.242

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	152	-.143	.025	-.063	-.235
30	153	-.106	.019	-.032	-.203
30	154	-.129	.022	-.039	-.235
30	155	-.114	.021	-.027	-.197
30	156	-.116	.022	-.047	-.197
30	157	-.094	.019	-.028	-.174
30	158	-.129	.028	-.039	-.262
30	159	-.113	.024	-.030	-.215
30	160	-.114	.025	-.038	-.235
30	161	-.100	.019	-.035	-.170
30	162	-.137	.028	-.014	-.256
30	163	-.117	.026	-.005	-.222
30	164	-.111	.026	-.038	-.232
30	165	-.101	.022	-.035	-.199
30	166	-.119	.025	-.043	-.256
30	167	-.189	.028	-.103	-.353
30	201	-.054	.065	.341	-.305
30	202	-.011	.075	.433	-.371
30	203	.012	.068	.423	-.170
30	204	-.164	.059	.079	-.436
30	205	-.102	.053	-.183	-.447
30	206	-.248	.051	-.091	-.496
30	207	-.117	.046	.043	-.328
30	208	-.090	.057	.174	-.326
30	209	-.094	.052	.189	-.273
30	210	-.205	.050	-.031	-.384
30	211	-.170	.035	-.070	-.312
30	212	-.160	.062	.029	-.403
30	213	-.204	.055	-.077	-.438
30	214	-.168	.039	-.056	-.382
30	301	-.152	.036	-.030	-.392
30	302	-.210	.066	-.012	-.597
30	303	-.125	.036	-.007	-.348
30	304	-.143	.041	-.007	-.351
30	305	-.120	.030	-.037	-.272
30	306	-.147	.032	-.023	-.290
30	307	-.159	.041	-.000	-.404
30	308	-.135	.023	-.049	-.275
30	309	-.119	.024	-.026	-.234
30	310	-.165	.046	-.003	-.633
30	311	-.167	.051	.011	-.784
30	312	-.127	.029	-.002	-.277
30	313	-.115	.023	-.012	-.212
30	314	-.153	.034	-.003	-.292
30	315	-.154	.038	-.021	-.380
30	316	-.102	.024	-.032	-.216
30	317	-.103	.021	-.038	-.216
30	318	-.108	.021	-.034	-.196
30	319	-.104	.031	.009	-.226
30	320	-.171	.062	.099	-.861

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
30	401	-.086	.058	.224	-.359
30	402	-.081	.034	.097	-.236
30	403	-.118	.033	-.001	-.435
30	404	-.117	.037	-.006	-.353
30	405	-.140	.040	-.005	-.311
30	406	-.150	.038	-.020	-.326
40	1	-.074	.035	.082	-.446
40	2	-.138	.033	.046	-.275
40	3	-.105	.029	.021	-.242
40	4	-.218	.043	-.097	-.419
40	5	-.131	.046	.017	-.327
40	6	-.088	.029	.025	-.220
40	7	-.112	.052	.095	-.407
40	8	-.097	.041	.126	-.287
40	9	-.126	.032	.037	-.274
40	10	-.222	.037	-.142	-.457
40	11	-.232	.056	-.029	-.600
40	12	-.201	.036	-.082	-.378
40	13	-.129	.034	.004	-.338
40	14	-.189	.045	.003	-.441
40	15	-.183	.030	-.078	-.314
40	16	-.179	.037	.041	-.326
40	17	-.196	.057	-.054	-.513
40	18	-.141	.022	-.074	-.239
40	19	-.171	.042	.007	-.402
40	20	-.079	.044	.106	-.267
40	21	-.121	.022	-.048	-.213
40	22	-.152	.036	-.036	-.457
40	23	-.133	.024	-.051	-.238
40	24	-.135	.033	.004	-.342
40	25	-.149	.046	.035	-.365
40	26	-.163	.039	-.036	-.374
40	27	-.129	.023	-.053	-.218
40	28	-.162	.032	-.068	-.317
40	29	-.124	.020	-.063	-.204
40	30	-.173	.038	-.045	-.374
40	31	-.121	.057	.118	-.386
40	32	-.090	.041	.111	-.263
40	33	-.165	.047	-.050	-.399
40	34	-.186	.042	.000	-.401
40	35	-.149	.047	.037	-.377
40	36	-.142	.031	-.041	-.326
40	37	-.153	.052	.064	-.419
40	38	-.123	.036	.050	-.322
40	39	-.170	.025	-.098	-.292
40	40	-.123	.060	.129	-.464
40	41	-.149	.039	-.032	-.410
40	42	-.136	.033	.007	-.293
40	43	-.146	.023	-.067	-.267
40	44	-.126	.021	-.055	-.206

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	45	-.141	.055	.037	-.415
40	46	-.173	.038	-.049	-.349
40	47	-.138	.045	.025	-.346
40	48	-.197	.070	.052	-.701
40	49	-.120	.020	-.043	-.233
40	50	-.183	.053	.005	-.518
40	51	-.133	.041	.011	-.298
40	52	-.167	.056	.095	-.487
40	53	-.132	.032	-.019	-.410
40	54	-.162	.036	-.045	-.421
40	55	-.119	.036	.133	-.393
40	56	-.126	.037	.007	-.312
40	57	-.092	.032	-.084	-.267
40	101	-.220	.031	-.124	-.356
40	102	-.204	.033	-.107	-.391
40	103	-.201	.032	-.111	-.380
40	104	-.197	.033	-.106	-.399
40	105	-.187	.027	-.112	-.322
40	106	-.177	.026	-.105	-.305
40	107	-.167	.026	-.093	-.281
40	108	-.181	.026	-.122	-.305
40	109	-.187	.026	-.117	-.308
40	110	-.223	.035	-.130	-.380
40	111	-.191	.030	-.104	-.324
40	112	-.208	.038	-.119	-.421
40	113	-.218	.037	-.106	-.489
40	114	-.174	.028	-.094	-.337
40	115	-.186	.032	-.097	-.401
40	116	-.176	.041	-.041	-.401
40	117	-.197	.027	-.126	-.329
40	118	-.213	.043	-.121	-.458
40	119	-.156	.032	-.052	-.310
40	120	-.150	.029	-.057	-.271
40	121	-.134	.022	-.065	-.250
40	122	-.138	.030	-.031	-.285
40	123	-.125	.023	-.043	-.237
40	124	-.129	.025	-.053	-.254
40	125	-.110	.020	-.043	-.188
40	126	-.133	.022	-.056	-.216
40	127	-.129	.022	-.043	-.194
40	128	-.119	.023	-.035	-.223
40	129	-.105	.017	-.054	-.164
40	130	-.120	.023	-.027	-.207
40	131	-.122	.021	-.036	-.203
40	132	-.120	.020	-.057	-.218
40	133	-.105	.017	-.054	-.170
40	134	-.146	.033	-.056	-.352
40	135	-.117	.023	-.007	-.235
40	136	-.116	.020	-.038	-.210
40	137	-.109	.018	-.041	-.195

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
40	138	-.136	.023	-.049	-.254
40	139	-.123	.021	-.049	-.226
40	140	-.134	.022	-.071	-.245
40	141	-.112	.021	-.036	-.201
40	142	-.133	.021	-.060	-.209
40	143	-.126	.020	-.054	-.203
40	144	-.160	.027	-.084	-.302
40	145	-.125	.021	-.043	-.219
40	146	-.172	.029	-.087	-.347
40	147	-.146	.027	-.056	-.259
40	148	-.145	.023	-.075	-.285
40	149	-.120	.019	-.063	-.208
40	150	-.140	.021	-.076	-.227
40	151	-.128	.019	-.065	-.217
40	152	-.135	.018	-.079	-.201
40	153	-.106	.018	-.036	-.197
40	154	-.126	.021	-.029	-.221
40	155	-.116	.019	-.038	-.201
40	156	-.121	.022	-.044	-.245
40	157	-.106	.017	-.052	-.188
40	158	-.133	.030	-.038	-.381
40	159	-.122	.025	-.049	-.250
40	160	-.123	.025	-.042	-.252
40	161	-.112	.021	-.045	-.230
40	162	-.150	.030	-.020	-.330
40	163	-.131	.026	-.011	-.248
40	164	-.123	.024	-.040	-.289
40	165	-.114	.020	-.045	-.206
40	166	-.132	.024	-.056	-.265
40	167	-.236	.026	-.149	-.342
40	201	-.097	.073	.259	-.476
40	202	-.068	.068	.274	-.324
40	203	-.028	.055	.357	-.210
40	204	-.200	.044	.020	-.445
40	205	-.144	.059	.058	-.453
40	206	-.209	.035	-.129	-.437
40	207	-.132	.041	.032	-.337
40	208	-.123	.051	.095	-.325
40	209	-.119	.048	.064	-.299
40	210	-.194	.032	-.102	-.430
40	211	-.165	.025	-.096	-.289
40	212	-.160	.035	-.004	-.301
40	213	-.176	.030	-.076	-.322
40	214	-.165	.025	-.086	-.271
40	301	-.151	.037	-.058	-.364
40	302	-.194	.061	-.016	-.783
40	303	-.129	.034	.006	-.302
40	304	-.153	.043	.031	-.455
40	305	-.119	.025	-.030	-.239
40	306	-.150	.032	-.034	-.303
40	307	-.159	.039	-.013	-.369
40	308	-.129	.020	-.057	-.207
40	309	-.125	.023	-.034	-.221
40	310	-.167	.042	-.031	-.378
40	311	-.169	.045	-.005	-.373
40	312	-.131	.031	-.022	-.307
40	313	-.119	.024	-.030	-.223
40	314	-.153	.034	-.020	-.347
40	315	-.155	.038	-.018	-.317
40	316	-.139	.024	-.052	-.231
40	317	-.109	.020	-.042	-.185
40	318	-.174	.027	-.084	-.309
40	319	-.133	.043	-.012	-.323
40	320	-.176	.061	-.006	-.622
40	401	-.117	.068	.267	-.431
40	402	-.088	.039	.114	-.225
40	403	-.192	.042	-.023	-.455
40	404	-.145	.048	-.026	-.441
40	405	-.173	.048	-.067	-.395
40	406	-.180	.044	-.009	-.524
50	1	-.094	.032	-.079	-.246
50	2	-.171	.031	-.032	-.322
50	3	-.128	.031	-.005	-.338
50	4	-.245	.047	-.143	-.579
50	5	-.173	.049	-.035	-.402
50	6	-.111	.029	-.019	-.301
50	7	-.152	.040	-.017	-.363
50	8	-.133	.040	-.036	-.322
50	9	-.144	.031	-.019	-.341
50	10	-.220	.032	-.121	-.356
50	11	-.231	.054	-.089	-.608
50	12	-.193	.032	-.097	-.349
50	13	-.154	.035	-.037	-.391
50	14	-.206	.045	-.002	-.497
50	15	-.188	.030	-.098	-.315
50	16	-.206	.042	-.094	-.400
50	17	-.195	.060	-.026	-.645
50	18	-.145	.021	-.084	-.246
50	19	-.203	.048	-.024	-.565
50	20	-.099	.040	-.096	-.303
50	21	-.130	.022	-.057	-.218
50	22	-.183	.038	-.043	-.392
50	23	-.152	.027	-.038	-.265
50	24	-.150	.036	-.025	-.347
50	25	-.176	.048	-.036	-.373
50	26	-.184	.042	-.013	-.443
50	27	-.155	.026	-.057	-.322
50	28	-.191	.036	-.087	-.363
50	29	-.142	.021	-.076	-.237
50	30	-.199	.045	-.045	-.424
50	31	-.174	.060	.024	-.453
50	32	-.107	.046	.165	-.324
50	33	-.186	.052	-.010	-.563
50	34	-.211	.047	-.032	-.406
50	35	-.163	.044	-.067	-.402
50	36	-.158	.027	-.076	-.322
50	37	-.199	.070	-.026	-.520
50	38	-.148	.041	-.016	-.358
50	39	-.172	.025	-.102	-.315
50	40	-.170	.078	-.115	-.498
50	41	-.172	.047	-.024	-.436
50	42	-.144	.039	-.026	-.422
50	43	-.158	.024	-.075	-.269
50	44	-.137	.021	-.067	-.232
50	45	-.192	.067	-.002	-.570
50	46	-.191	.043	-.057	-.459
50	47	-.153	.033	-.051	-.489
50	48	-.199	.072	-.094	-.556
50	49	-.138	.023	-.062	-.323
50	50	-.171	.051	-.004	-.433
50	51	-.133	.038	-.014	-.357
50	52	-.151	.057	-.092	-.409
50	53	-.152	.029	-.064	-.298
50	54	-.162	.032	-.050	-.322
50	55	-.122	.032	-.047	-.276
50	56	-.127	.026	-.025	-.322
50	57	-.102	.024	-.015	-.246
50	101	-.228	.032	-.155	-.406
50	102	-.220	.034	-.127	-.361
50	103	-.212	.032	-.122	-.370
50	104	-.207	.030	-.123	-.375
50	105	-.205	.026	-.130	-.337
50	106	-.195	.025	-.125	-.329
50	107	-.185	.025	-.122	-.301
50	108	-.191	.027	-.130	-.300
50	109	-.201	.028	-.127	-.308
50	110	-.217	.031	-.141	-.340
50	111	-.196	.031	-.122	-.310
50	112	-.207	.032	-.112	-.359
50	113	-.215	.031	-.121	-.376
50	114	-.188	.026	-.116	-.304
50	115	-.188	.030	-.106	-.317
50	116	-.179	.036	-.060	-.314
50	117	-.193	.024	-.118	-.292
50	118	-.224	.041	-.089	-.425
50	119	-.159	.029	-.062	-.294
50	120	-.160	.028	-.061	-.290
50	121	-.155	.022	-.077	-.260
50	122	-.144	.026	-.061	-.251
50	123	-.137	.020	-.068	-.222

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	124	-.137	.024	-.058	-.263
50	125	-.132	.018	-.077	-.214
50	126	-.136	.021	-.074	-.216
50	127	-.132	.020	-.064	-.207
50	128	-.134	.022	-.056	-.217
50	129	-.138	.015	-.083	-.201
50	130	-.128	.022	-.050	-.212
50	131	-.145	.022	-.076	-.237
50	132	-.144	.020	-.061	-.223
50	133	-.144	.016	-.087	-.212
50	134	-.164	.034	-.057	-.320
50	135	-.140	.023	-.061	-.232
50	136	-.139	.019	-.073	-.207
50	137	-.149	.018	-.081	-.231
50	138	-.158	.024	-.069	-.314
50	139	-.150	.021	-.076	-.241
50	140	-.154	.021	-.096	-.232
50	141	-.146	.022	-.069	-.248
50	142	-.150	.021	-.084	-.235
50	143	-.148	.019	-.087	-.220
50	144	-.163	.028	-.065	-.332
50	145	-.154	.020	-.069	-.256
50	146	-.162	.026	-.057	-.278
50	147	-.156	.026	-.047	-.266
50	148	-.155	.024	-.063	-.257
50	149	-.148	.022	-.054	-.256
50	150	-.149	.022	-.067	-.243
50	151	-.142	.022	-.051	-.249
50	152	-.145	.018	-.088	-.232
50	153	-.138	.023	-.062	-.264
50	154	-.144	.024	-.069	-.253
50	155	-.139	.022	-.066	-.248
50	156	-.142	.027	-.044	-.305
50	157	-.153	.021	-.087	-.248
50	158	-.162	.027	-.080	-.314
50	159	-.157	.027	-.072	-.310
50	160	-.156	.025	-.077	-.265
50	161	-.156	.024	-.054	-.279
50	162	-.163	.030	-.059	-.293
50	163	-.149	.028	-.040	-.262
50	164	-.169	.023	-.088	-.261
50	165	-.163	.018	-.100	-.239
50	166	-.168	.026	-.082	-.278
50	167	-.193	.025	-.127	-.290
50	201	-.149	.085	-.122	-.774
50	202	-.118	.068	-.334	-.453
50	203	-.060	.058	-.205	-.248
50	204	-.203	.036	-.080	-.419
50	205	-.236	.083	-.045	-.838
50	206	-.234	.038	-.138	-.398

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
50	207	-.213	.048	-.038	-.445
50	208	-.180	.047	-.011	-.348
50	209	-.164	.036	-.015	-.321
50	210	-.213	.032	-.127	-.346
50	211	-.192	.026	-.119	-.321
50	212	-.204	.040	-.105	-.421
50	213	-.200	.033	-.112	-.376
50	214	-.183	.026	-.106	-.277
50	301	-.162	.045	-.022	-.437
50	302	-.186	.054	-.029	-.672
50	303	-.163	.032	-.064	-.338
50	304	-.189	.071	-.015	-.557
50	305	-.147	.024	-.077	-.254
50	306	-.154	.033	-.023	-.295
50	307	-.152	.042	-.012	-.342
50	308	-.143	.023	-.065	-.246
50	309	-.150	.025	-.062	-.266
50	310	-.172	.034	-.030	-.331
50	311	-.192	.044	-.051	-.391
50	312	-.137	.031	-.025	-.321
50	313	-.140	.025	-.056	-.231
50	314	-.160	.031	-.053	-.301
50	315	-.176	.036	-.038	-.308
50	316	-.157	.023	-.090	-.253
50	317	-.122	.019	-.063	-.229
50	318	-.119	.021	-.057	-.220
50	319	-.116	.041	-.025	-.272
50	320	-.174	.055	-.013	-.517
50	401	-.155	.070	.178	-.450
50	402	-.122	.034	.142	-.254
50	403	-.154	.041	.002	-.456
50	404	-.162	.050	.065	-.542
50	405	-.194	.053	.046	-.466
50	406	-.215	.048	-.047	-.448
60	1	-.167	.046	-.043	-.391
60	2	-.244	.035	-.010	-.373
60	3	-.196	.039	.014	-.362
60	4	-.290	.051	-.137	-.519
60	5	-.255	.041	-.076	-.423
60	6	-.181	.035	-.065	-.330
60	7	-.222	.040	.037	-.399
60	8	-.241	.058	.009	-.535
60	9	-.203	.042	.002	-.446
60	10	-.230	.030	-.143	-.366
60	11	-.250	.053	-.087	-.509
60	12	-.217	.034	-.072	-.361
60	13	-.251	.047	-.124	-.522
60	14	-.238	.049	-.003	-.492
60	15	-.213	.029	-.104	-.318
60	16	-.296	.057	-.086	-.595

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	17	-.224	.063	-.070	-.600
60	18	-.175	.023	-.106	-.279
60	19	-.306	.074	-.069	-.666
60	20	-.184	.066	.071	-.433
60	21	-.184	.026	-.069	-.295
60	22	-.264	.050	-.097	-.503
60	23	-.215	.036	-.078	-.364
60	24	-.210	.044	-.063	-.535
60	25	-.292	.065	-.014	-.570
60	26	-.232	.044	-.063	-.467
60	27	-.218	.029	-.113	-.362
60	28	-.301	.050	-.148	-.612
60	29	-.207	.024	-.122	-.300
60	30	-.284	.056	-.097	-.583
60	31	-.299	.079	-.016	-.662
60	32	-.175	.063	-.113	-.459
60	33	-.297	.073	-.071	-.750
60	34	-.325	.073	-.058	-.701
60	35	-.239	.061	-.007	-.579
60	36	-.213	.030	-.109	-.396
60	37	-.363	.091	-.042	-.773
60	38	-.211	.060	-.003	-.615
60	39	-.226	.034	-.117	-.383
60	40	-.349	.105	-.034	-.836
60	41	-.292	.074	-.053	-.622
60	42	-.202	.062	-.047	-.455
60	43	-.226	.038	-.115	-.433
60	44	-.209	.031	-.107	-.343
60	45	-.342	.092	-.002	-.725
60	46	-.281	.063	-.067	-.599
60	47	-.210	.067	-.049	-.503
60	48	-.278	.083	-.021	-.700
60	49	-.209	.025	-.133	-.325
60	50	-.186	.035	-.013	-.437
60	51	-.176	.030	-.079	-.375
60	52	-.188	.054	-.037	-.380
60	53	-.239	.025	-.154	-.325
60	54	-.204	.022	-.124	-.289
60	55	-.163	.019	-.092	-.242
60	56	-.169	.023	-.088	-.290
60	57	-.153	.021	-.092	-.259
60	101	-.240	.029	-.147	-.378
60	102	-.255	.035	-.127	-.403
60	103	-.251	.031	-.153	-.412
60	104	-.248	.027	-.153	-.369
60	105	-.225	.024	-.136	-.321
60	106	-.228	.024	-.143	-.311
60	107	-.241	.027	-.139	-.348
60	108	-.234	.026	-.135	-.337
60	109	-.218	.026	-.122	-.336

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
60	110	-.237	.030	-.120	-.360
60	111	-.219	.028	-.122	-.336
60	112	-.219	.032	-.106	-.364
60	113	-.205	.032	-.083	-.359
60	114	-.208	.024	-.122	-.297
60	115	-.207	.028	-.107	-.334
60	116	-.200	.024	-.124	-.277
60	117	-.189	.024	-.111	-.291
60	118	-.290	.045	-.175	-.514
60	119	-.194	.028	-.093	-.301
60	120	-.197	.026	-.082	-.289
60	121	-.201	.021	-.115	-.285
60	122	-.258	.027	-.150	-.369
60	123	-.194	.022	-.105	-.268
60	124	-.198	.029	-.086	-.328
60	125	-.189	.022	-.115	-.287
60	126	-.247	.026	-.160	-.366
60	127	-.175	.023	-.077	-.277
60	128	-.191	.030	-.078	-.393
60	129	-.204	.019	-.148	-.287
60	130	-.246	.028	-.148	-.401
60	131	-.203	.031	-.112	-.380
60	132	-.199	.025	-.099	-.284
60	133	-.215	.018	-.150	-.278
60	134	-.281	.044	-.114	-.568
60	135	-.200	.028	-.081	-.303
60	136	-.195	.023	-.086	-.267
60	137	-.219	.020	-.133	-.296
60	138	-.279	.027	-.178	-.398
60	139	-.207	.023	-.114	-.286
60	140	-.212	.021	-.132	-.313
60	141	-.224	.025	-.122	-.340
60	142	-.278	.025	-.182	-.398
60	143	-.210	.022	-.123	-.308
60	144	-.227	.036	-.119	-.413
60	145	-.229	.025	-.148	-.367
60	146	-.283	.030	-.182	-.389
60	147	-.215	.028	-.119	-.332
60	148	-.220	.034	-.112	-.411
60	149	-.229	.032	-.126	-.402
60	150	-.277	.030	-.180	-.408
60	151	-.209	.030	-.114	-.356
60	152	-.210	.025	-.141	-.319
60	153	-.214	.025	-.135	-.369
60	154	-.274	.030	-.182	-.403
60	155	-.203	.027	-.121	-.295
60	156	-.207	.030	-.099	-.382
60	157	-.250	.021	-.179	-.318
60	158	-.308	.028	-.203	-.419
60	159	-.229	.026	-.127	-.352
60	160	-.249	.026	-.163	-.369
60	161	-.255	.024	-.166	-.353
60	162	-.287	.030	-.192	-.414
60	163	-.201	.030	-.114	-.330
60	164	-.250	.026	-.169	-.343
60	165	-.248	.020	-.186	-.334
60	166	-.333	.034	-.238	-.472
60	167	-.217	.022	-.133	-.302
60	201	-.275	.126	.117	-1.019
60	202	-.249	.083	-.151	-.600
60	203	-.167	.069	-.139	-.400
60	204	-.292	.041	-.157	-.486
60	205	-.369	.082	-.119	-.935
60	206	-.254	.035	-.124	-.474
60	207	-.341	.047	-.201	-.596
60	208	-.343	.050	-.150	-.649
60	209	-.222	.034	-.083	-.376
60	210	-.255	.029	-.141	-.385
60	211	-.249	.025	-.166	-.373
60	212	-.391	.061	-.215	-.699
60	213	-.255	.038	-.088	-.449
60	214	-.243	.025	-.154	-.359
60	301	-.211	.060	-.044	-.532
60	302	-.290	.041	-.114	-.545
60	303	-.247	.032	-.143	-.394
60	304	-.265	.080	-.049	-.838
60	305	-.244	.022	-.175	-.336
60	306	-.267	.032	-.150	-.437
60	307	-.188	.044	-.048	-.358
60	308	-.211	.033	-.084	-.354
60	309	-.230	.026	-.148	-.327
60	310	-.317	.037	-.210	-.474
60	311	-.301	.052	-.160	-.506
60	312	-.140	.053	.099	-.293
60	313	-.215	.026	-.135	-.300
60	314	-.284	.032	-.171	-.394
60	315	-.277	.044	-.130	-.451
60	316	-.229	.023	-.160	-.331
60	317	-.160	.019	-.094	-.238
60	318	-.156	.021	-.087	-.237
60	319	-.123	.030	-.040	-.304
60	320	-.208	.048	-.054	-.510
60	401	-.292	.091	.037	-.733
60	402	-.196	.042	-.010	-.392
60	403	-.232	.057	-.011	-.612
60	404	-.239	.068	-.007	-.626
60	405	-.298	.069	-.060	-.664
60	406	-.326	.065	-.099	-.648
70	1	-.172	.026	-.023	-.314
70	2	-.205	.022	-.132	-.290
70	3	-.211	.030	-.078	-.331
70	4	-.218	.026	-.098	-.320
70	5	-.216	.030	-.113	-.351
70	6	-.196	.031	-.095	-.357
70	7	-.198	.031	-.080	-.381
70	8	-.293	.069	.004	-.568
70	9	-.192	.053	.013	-.459
70	10	-.197	.033	-.095	-.444
70	11	-.204	.052	-.004	-.448
70	12	-.194	.035	-.049	-.353
70	13	-.290	.060	-.088	-.584
70	14	-.224	.051	-.008	-.495
70	15	-.193	.029	-.078	-.340
70	16	-.302	.062	-.002	-.568
70	17	-.222	.058	-.005	-.595
70	18	-.177	.023	-.084	-.272
70	19	-.315	.071	-.039	-.620
70	20	-.203	.060	-.025	-.551
70	21	-.206	.025	-.125	-.309
70	22	-.271	.050	-.118	-.504
70	23	-.241	.031	-.147	-.413
70	24	-.230	.040	-.103	-.432
70	25	-.300	.064	-.088	-.618
70	26	-.235	.038	-.084	-.423
70	27	-.228	.027	-.138	-.333
70	28	-.321	.049	-.185	-.649
70	29	-.223	.023	-.153	-.316
70	30	-.308	.059	-.065	-.621
70	31	-.361	.077	-.078	-.781
70	32	-.216	.067	-.032	-.572
70	33	-.300	.071	-.083	-.674
70	34	-.315	.061	-.084	-.566
70	35	-.296	.054	-.073	-.540
70	36	-.237	.032	-.117	-.390
70	37	-.377	.080	-.007	-.667
70	38	-.237	.057	-.015	-.534
70	39	-.295	.038	-.177	-.510
70	40	-.393	.096	-.024	-.822
70	41	-.316	.073	-.051	-.676
70	42	-.204	.058	-.022	-.462
70	43	-.293	.039	-.138	-.455
70	44	-.228	.029	-.133	-.360
70	45	-.355	.083	-.047	-.715
70	46	-.302	.058	-.127	-.662
70	47	-.208	.058	-.081	-.436
70	48	-.178	.076	-.095	-.488
70	49	-.244	.026	-.171	-.344
70	50	-.207	.035	-.114	-.352
70	51	-.198	.026	-.118	-.303
70	52	-.224	.050	-.063	-.418

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
70	53	-.281	.030	-.201	-.441
70	54	-.199	.022	-.125	-.290
70	55	-.218	.019	-.140	-.298
70	56	-.167	.031	-.087	-.353
70	57	-.173	.026	-.100	-.286
70	101	-.196	.022	-.121	-.279
70	102	-.281	.025	-.190	-.377
70	103	-.206	.023	-.131	-.297
70	104	-.205	.024	-.120	-.314
70	105	-.188	.022	-.116	-.279
70	106	-.250	.021	-.156	-.347
70	107	-.198	.021	-.124	-.290
70	108	-.194	.023	-.106	-.286
70	109	-.195	.032	-.072	-.391
70	110	-.257	.030	-.135	-.370
70	111	-.191	.022	-.105	-.271
70	112	-.192	.035	-.033	-.356
70	113	-.182	.036	-.077	-.371
70	114	-.247	.024	-.112	-.342
70	115	-.188	.029	-.056	-.308
70	116	-.188	.025	-.090	-.291
70	117	-.172	.026	-.070	-.279
70	118	-.353	.050	-.186	-.579
70	119	-.182	.032	-.070	-.315
70	120	-.183	.027	-.097	-.295
70	121	-.184	.021	-.106	-.291
70	122	-.236	.024	-.141	-.335
70	123	-.178	.021	-.092	-.261
70	124	-.186	.030	-.028	-.317
70	125	-.201	.022	-.093	-.293
70	126	-.256	.025	-.113	-.365
70	127	-.188	.023	-.064	-.272
70	128	-.213	.027	-.115	-.356
70	129	-.216	.018	-.159	-.287
70	130	-.264	.026	-.182	-.369
70	131	-.220	.027	-.125	-.360
70	132	-.219	.024	-.145	-.313
70	133	-.221	.019	-.166	-.296
70	134	-.285	.037	-.154	-.502
70	135	-.210	.026	-.123	-.325
70	136	-.208	.021	-.108	-.291
70	137	-.222	.020	-.157	-.298
70	138	-.278	.025	-.205	-.374
70	139	-.213	.022	-.136	-.290
70	140	-.222	.021	-.162	-.315
70	141	-.245	.024	-.132	-.377
70	142	-.299	.027	-.175	-.426
70	143	-.229	.024	-.134	-.336
70	144	-.242	.040	-.117	-.482
70	145	-.247	.030	-.161	-.430
70	146	-.294	.033	-.200	-.445
70	147	-.224	.030	-.112	-.356
70	148	-.236	.037	-.130	-.458
70	149	-.243	.031	-.130	-.368
70	150	-.297	.033	-.195	-.429
70	151	-.218	.029	-.114	-.331
70	152	-.226	.025	-.149	-.339
70	153	-.225	.020	-.163	-.331
70	154	-.289	.026	-.207	-.415
70	155	-.223	.025	-.149	-.325
70	156	-.237	.027	-.152	-.376
70	157	-.279	.022	-.212	-.388
70	158	-.353	.031	-.264	-.497
70	159	-.285	.027	-.215	-.421
70	160	-.289	.029	-.208	-.397
70	161	-.276	.024	-.203	-.381
70	162	-.281	.031	-.186	-.424
70	163	-.200	.028	-.116	-.314
70	164	-.292	.033	-.191	-.439
70	165	-.275	.027	-.192	-.419
70	166	-.378	.039	-.285	-.621
70	167	-.197	.022	-.119	-.293
70	201	-.357	.139	.024	-1.056
70	202	-.322	.081	-.009	-.641
70	203	-.229	.072	-.070	-.514
70	204	-.262	.052	-.065	-.545
70	205	-.303	.049	-.145	-.617
70	206	-.177	.027	-.097	-.314
70	207	-.281	.028	-.174	-.426
70	208	-.303	.030	-.200	-.422
70	209	-.214	.031	-.107	-.369
70	210	-.217	.025	-.130	-.315
70	211	-.222	.032	-.139	-.390
70	212	-.310	.037	-.182	-.507
70	213	-.235	.031	-.090	-.384
70	214	-.202	.022	-.134	-.278
70	301	-.136	.063	-.110	-.456
70	302	-.283	.031	-.184	-.420
70	303	-.306	.036	-.206	-.474
70	304	-.232	.063	-.038	-.691
70	305	-.276	.024	-.205	-.377
70	306	-.262	.034	-.136	-.410
70	307	-.206	.042	-.037	-.360
70	308	-.214	.033	-.056	-.350
70	309	-.223	.024	-.152	-.315
70	310	-.321	.038	-.223	-.504
70	311	-.312	.044	-.191	-.525
70	312	-.067	.069	-.240	-.284
70	313	-.211	.024	-.135	-.304
70	314	-.289	.029	-.186	-.397
70	315	-.316	.040	-.208	-.476
70	316	-.250	.027	-.171	-.368
70	317	-.213	.018	-.024	-.200
70	318	-.169	.018	-.106	-.242
70	319	-.104	.023	-.019	-.222
70	320	-.208	.043	-.070	-.427
70	401	-.314	.082	-.041	-.689
70	402	-.206	.045	-.037	-.401
70	403	-.233	.048	-.036	-.491
70	404	-.242	.060	-.028	-.621
70	405	-.302	.070	-.010	-.581
70	406	-.314	.062	-.115	-.596
80	1	-.164	.043	-.102	-.303
80	2	-.182	.022	-.101	-.268
80	3	-.285	.030	-.192	-.436
80	4	-.192	.025	-.116	-.308
80	5	-.194	.028	-.103	-.368
80	6	-.184	.033	-.054	-.374
80	7	-.271	.039	-.094	-.545
80	8	-.301	.065	-.026	-.593
80	9	-.190	.063	-.202	-.509
80	10	-.181	.041	-.038	-.425
80	11	-.291	.068	-.035	-.595
80	12	-.179	.038	-.031	-.367
80	13	-.297	.064	-.089	-.591
80	14	-.214	.050	-.080	-.462
80	15	-.265	.030	-.152	-.408
80	16	-.295	.059	-.019	-.560
80	17	-.228	.053	-.061	-.528
80	18	-.184	.021	-.098	-.263
80	19	-.398	.063	-.119	-.660
80	20	-.195	.057	-.028	-.475
80	21	-.207	.024	-.126	-.333
80	22	-.263	.046	-.112	-.539
80	23	-.302	.029	-.209	-.438
80	24	-.227	.038	-.129	-.504
80	25	-.290	.060	-.070	-.539
80	26	-.238	.034	-.133	-.409
80	27	-.310	.028	-.214	-.448
80	28	-.318	.041	-.193	-.576
80	29	-.231	.024	-.154	-.340
80	30	-.303	.057	-.119	-.594
80	31	-.425	.073	-.164	-.760
80	32	-.246	.065	-.054	-.555
80	33	-.285	.060	-.089	-.598
80	34	-.288	.051	-.082	-.457
80	35	-.338	.052	-.070	-.717
80	36	-.248	.033	-.153	-.414
80	37	-.345	.062	-.047	-.649
80	38	-.239	.050	-.006	-.467

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
80	39	-.333	.038	-.207	-.535
80	40	-.402	.091	-.038	-.823
80	41	-.291	.065	-.068	-.616
80	42	-.178	.040	.001	-.358
80	43	-.337	.032	-.222	-.491
80	44	-.237	.025	-.141	-.337
80	45	-.298	.073	-.117	-.688
80	46	-.286	.048	-.133	-.525
80	47	-.192	.044	-.017	-.379
80	48	-.141	.049	.080	-.461
80	49	-.288	.030	-.189	-.402
80	50	-.228	.030	-.142	-.358
80	51	-.225	.030	-.148	-.371
80	52	-.222	.033	-.087	-.407
80	53	-.317	.031	-.230	-.428
80	54	-.178	.022	-.087	-.272
80	55	-.240	.021	-.132	-.316
80	56	-.166	.039	-.045	-.351
80	57	-.188	.031	-.096	-.340
80	101	-.181	.023	-.085	-.305
80	102	-.278	.026	-.179	-.401
80	103	-.186	.026	-.080	-.285
80	104	-.185	.028	-.100	-.337
80	105	-.169	.021	-.096	-.256
80	106	-.259	.025	-.167	-.351
80	107	-.175	.021	-.104	-.240
80	108	-.175	.026	-.089	-.321
80	109	-.176	.032	-.066	-.325
80	110	-.265	.035	-.142	-.438
80	111	-.174	.024	-.085	-.287
80	112	-.179	.035	-.047	-.326
80	113	-.179	.038	-.024	-.504
80	114	-.257	.025	-.149	-.344
80	115	-.171	.026	-.066	-.278
80	116	-.171	.023	-.091	-.256
80	117	-.168	.027	-.075	-.295
80	118	-.382	.057	-.184	-.643
80	119	-.181	.031	-.066	-.327
80	120	-.187	.026	-.100	-.292
80	121	-.185	.021	-.108	-.267
80	122	-.239	.024	-.132	-.338
80	123	-.184	.020	-.117	-.267
80	124	-.194	.028	-.078	-.419
80	125	-.205	.020	-.137	-.287
80	126	-.258	.023	-.182	-.356
80	127	-.195	.021	-.117	-.273
80	128	-.211	.025	-.128	-.355
80	129	-.211	.017	-.163	-.287
80	130	-.262	.023	-.187	-.345
80	131	-.212	.023	-.139	-.311
80	132	-.213	.023	-.135	-.312
80	133	-.215	.019	-.148	-.293
80	134	-.278	.032	-.152	-.448
80	135	-.213	.024	-.132	-.329
80	136	-.205	.020	-.148	-.283
80	137	-.221	.020	-.157	-.311
80	138	-.278	.027	-.200	-.413
80	139	-.213	.023	-.139	-.320
80	140	-.228	.024	-.119	-.320
80	141	-.263	.030	-.157	-.472
80	142	-.304	.030	-.180	-.409
80	143	-.236	.025	-.126	-.342
80	144	-.249	.040	-.119	-.471
80	145	-.252	.029	-.168	-.425
80	146	-.297	.032	-.189	-.452
80	147	-.236	.029	-.130	-.362
80	148	-.237	.030	-.135	-.360
80	149	-.244	.024	-.163	-.337
80	150	-.300	.029	-.207	-.439
80	151	-.227	.026	-.130	-.318
80	152	-.241	.021	-.176	-.344
80	153	-.258	.020	-.190	-.350
80	154	-.331	.029	-.228	-.443
80	155	-.251	.024	-.172	-.357
80	156	-.252	.027	-.159	-.377
80	157	-.290	.024	-.212	-.392
80	158	-.403	.036	-.287	-.590
80	159	-.329	.031	-.238	-.476
80	160	-.323	.032	-.235	-.469
80	161	-.283	.024	-.210	-.381
80	162	-.261	.031	-.168	-.400
80	163	-.180	.028	-.070	-.287
80	164	-.341	.036	-.231	-.506
80	165	-.311	.032	-.229	-.434
80	166	-.423	.051	-.301	-.652
80	167	-.187	.025	-.070	-.286
80	201	-.376	.136	.069	-1.207
80	202	-.331	.072	-.069	-.696
80	203	-.272	.066	.092	-.529
80	204	-.266	.067	-.017	-.693
80	205	-.231	.037	-.104	-.428
80	206	-.143	.029	-.035	-.312
80	207	-.221	.026	-.150	-.331
80	208	-.263	.030	-.152	-.388
80	209	-.204	.037	-.097	-.397
80	210	-.192	.029	-.080	-.318
80	211	-.195	.033	-.049	-.350
80	212	-.262	.031	-.166	-.413
80	213	-.201	.029	-.106	-.329
80	214	-.180	.023	-.076	-.272
90	301	-.097	.045	.189	-.304
90	302	-.288	.038	-.134	-.439
90	303	-.365	.040	-.256	-.521
90	304	-.182	.052	.044	-.539
90	305	-.297	.024	-.227	-.381
90	306	-.251	.034	-.102	-.379
90	307	-.197	.026	-.099	-.300
90	308	-.222	.029	-.106	-.322
90	309	-.207	.024	-.130	-.317
90	310	-.306	.038	-.152	-.450
90	311	-.282	.044	-.165	-.505
90	312	-.212	.075	.296	-.233
90	313	-.188	.025	-.062	-.269
90	314	-.258	.031	-.122	-.379
90	315	-.299	.045	-.190	-.465
90	316	-.264	.032	-.167	-.371
90	317	-.056	.021	.063	-.127
90	318	-.156	.019	-.096	-.218
90	319	-.080	.024	.012	-.164
90	320	-.205	.038	.012	-.387
90	401	-.304	.066	-.071	-.640
90	402	-.203	.043	-.079	-.397
90	403	-.235	.047	.003	-.457
90	404	-.234	.054	.000	-.493
90	405	-.271	.071	.079	-.675
90	406	-.266	.056	-.074	-.495
90	1	-.129	.052	-.134	-.314
90	2	-.161	.021	-.083	-.263
90	3	-.167	.027	-.052	-.260
90	4	-.158	.024	-.074	-.241
90	5	-.170	.032	-.020	-.352
90	6	-.176	.048	.033	-.564
90	7	-.164	.046	.037	-.451
90	8	-.272	.059	-.024	-.610
90	9	-.178	.059	.053	-.432
90	10	-.178	.047	.003	-.395
90	11	-.200	.058	.014	-.501
90	12	-.164	.033	-.024	-.370
90	13	-.273	.064	-.067	-.579
90	14	-.205	.043	-.038	-.400
90	15	-.174	.025	-.068	-.279
90	16	-.270	.049	-.106	-.498
90	17	-.224	.055	-.070	-.570
90	18	-.184	.019	-.115	-.265
90	19	-.279	.051	-.088	-.580
90	20	-.172	.049	.022	-.406
90	21	-.190	.022	-.094	-.273
90	22	-.246	.038	-.124	-.438
90	23	-.209	.025	-.097	-.313
90	24	-.217	.030	-.113	-.370

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	25	-.264	.046	-.099	-.493
90	26	-.240	.034	-.083	-.409
90	27	-.227	.026	-.145	-.338
90	28	-.295	.041	-.184	-.488
90	29	-.230	.023	-.151	-.368
90	30	-.289	.049	-.120	-.502
90	31	-.310	.057	-.086	-.617
90	32	-.259	.060	-.015	-.516
90	33	-.281	.053	-.092	-.669
90	34	-.250	.042	-.035	-.470
90	35	-.224	.040	-.065	-.369
90	36	-.237	.033	-.138	-.379
90	37	-.294	.051	-.090	-.522
90	38	-.205	.040	-.047	-.382
90	39	-.238	.030	-.161	-.413
90	40	-.382	.097	-.065	-.909
90	41	-.218	.063	-.063	-.565
90	42	-.167	.029	-.013	-.372
90	43	-.243	.022	-.176	-.349
90	44	-.237	.021	-.180	-.319
90	45	-.207	.049	-.065	-.477
90	46	-.280	.039	-.161	-.443
90	47	-.108	.035	.089	-.258
90	48	-.125	.039	.033	-.292
90	49	-.294	.030	-.214	-.416
90	50	-.233	.030	-.129	-.402
90	51	-.237	.034	-.158	-.535
90	52	-.175	.034	-.033	-.285
90	53	-.309	.032	-.219	-.452
90	54	-.142	.025	-.001	-.238
90	55	-.140	.024	-.052	-.233
90	56	-.151	.037	-.042	-.280
90	57	-.180	.031	-.076	-.321
90	101	-.163	.027	-.065	-.281
90	102	-.166	.023	-.083	-.254
90	103	-.153	.028	-.033	-.271
90	104	-.151	.031	-.058	-.303
90	105	-.144	.023	-.056	-.231
90	106	-.148	.022	-.070	-.233
90	107	-.142	.022	-.068	-.221
90	108	-.144	.026	-.013	-.280
90	109	-.153	.030	-.029	-.309
90	110	-.155	.029	-.009	-.354
90	111	-.143	.022	-.038	-.235
90	112	-.161	.033	-.038	-.307
90	113	-.170	.033	-.051	-.375
90	114	-.158	.021	-.079	-.254
90	115	-.155	.024	-.052	-.262
90	116	-.154	.022	-.063	-.242
90	117	-.163	.026	-.070	-.272

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	118	-.270	.049	-.115	-.467
90	119	-.172	.028	-.074	-.310
90	120	-.179	.022	-.099	-.272
90	121	-.177	.018	-.116	-.252
90	122	-.219	.021	-.134	-.293
90	123	-.171	.018	-.109	-.241
90	124	-.183	.025	-.103	-.285
90	125	-.189	.018	-.125	-.259
90	126	-.236	.021	-.159	-.317
90	127	-.182	.020	-.112	-.267
90	128	-.197	.023	-.108	-.311
90	129	-.195	.017	-.138	-.270
90	130	-.244	.021	-.161	-.345
90	131	-.201	.023	-.118	-.309
90	132	-.195	.022	-.121	-.298
90	133	-.194	.018	-.134	-.270
90	134	-.259	.026	-.166	-.381
90	135	-.209	.023	-.127	-.298
90	136	-.191	.020	-.138	-.277
90	137	-.220	.019	-.158	-.300
90	138	-.264	.026	-.155	-.367
90	139	-.211	.023	-.129	-.306
90	140	-.226	.022	-.153	-.296
90	141	-.302	.044	-.186	-.572
90	142	-.304	.031	-.211	-.439
90	143	-.238	.027	-.155	-.381
90	144	-.232	.031	-.112	-.368
90	145	-.235	.023	-.143	-.340
90	146	-.273	.026	-.173	-.367
90	147	-.221	.024	-.136	-.315
90	148	-.232	.025	-.147	-.322
90	149	-.243	.020	-.191	-.318
90	150	-.295	.023	-.216	-.394
90	151	-.231	.023	-.142	-.324
90	152	-.242	.019	-.181	-.324
90	153	-.258	.022	-.186	-.331
90	154	-.332	.031	-.229	-.455
90	155	-.251	.027	-.140	-.346
90	156	-.246	.028	-.160	-.350
90	157	-.273	.025	-.208	-.359
90	158	-.400	.038	-.274	-.541
90	159	-.331	.031	-.232	-.446
90	160	-.328	.034	-.227	-.431
90	161	-.264	.026	-.182	-.359
90	162	-.198	.037	-.012	-.335
90	163	-.123	.036	.070	-.252
90	164	-.350	.040	-.238	-.533
90	165	-.329	.038	-.237	-.482
90	166	-.443	.062	-.288	-.758
90	167	-.158	.023	-.053	-.235

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
90	201	-.326	.110	-.011	-.985
90	202	-.293	.061	-.047	-.578
90	203	-.270	.056	-.024	-.497
90	204	-.255	.067	-.044	-.724
90	205	-.173	.031	-.074	-.324
90	206	-.114	.038	-.010	-.364
90	207	-.172	.020	-.086	-.248
90	208	-.219	.027	-.082	-.324
90	209	-.178	.041	-.041	-.471
90	210	-.163	.033	-.027	-.331
90	211	-.160	.029	-.029	-.316
90	212	-.221	.027	-.130	-.331
90	213	-.171	.026	-.085	-.278
90	214	-.147	.023	-.069	-.238
90	301	-.091	.033	.094	-.208
90	302	-.276	.044	-.119	-.437
90	303	-.368	.044	-.254	-.587
90	304	-.105	.059	.226	-.368
90	305	-.292	.029	-.197	-.423
90	306	-.213	.048	.010	-.446
90	307	-.147	.033	.015	-.271
90	308	-.229	.026	-.064	-.337
90	309	-.155	.031	-.033	-.272
90	310	-.243	.045	-.064	-.437
90	311	-.216	.047	-.063	-.427
90	312	.045	.078	.430	-.201
90	313	-.134	.033	-.005	-.243
90	314	-.200	.037	-.053	-.326
90	315	-.244	.049	-.107	-.475
90	316	-.243	.037	-.142	-.393
90	317	.019	.029	.140	-.070
90	318	-.141	.016	-.076	-.212
90	319	-.051	.022	.028	-.115
90	320	-.148	.044	.113	-.301
90	401	-.272	.053	-.110	-.463
90	402	-.183	.037	-.081	-.382
90	403	-.204	.066	.187	-.407
90	404	-.198	.061	.189	-.426
90	405	-.232	.057	.116	-.577
90	406	-.199	.041	-.043	-.426
100	1	-.112	.052	.124	-.344
100	2	-.134	.022	-.052	-.215
100	3	-.133	.027	-.020	-.234
100	4	-.122	.024	-.033	-.216
100	5	-.136	.033	.005	-.226
100	6	-.166	.056	.061	-.356
100	7	-.144	.045	.063	-.256
100	8	-.243	.048	-.027	-.488
100	9	-.164	.052	.117	-.405
100	10	-.178	.043	-.024	-.411

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	11	-.227	.060	-.029	-.536
100	12	-.167	.029	-.054	-.301
100	13	-.263	.064	-.066	-.624
100	14	-.188	.040	-.029	-.341
100	15	-.183	.023	-.108	-.262
100	16	-.240	.039	-.130	-.453
100	17	-.233	.052	-.088	-.485
100	18	-.180	.018	-.114	-.249
100	19	-.245	.039	-.122	-.423
100	20	-.155	.036	-.008	-.301
100	21	-.184	.022	-.120	-.294
100	22	-.223	.034	-.130	-.371
100	23	-.211	.023	-.140	-.306
100	24	-.234	.033	-.144	-.391
100	25	-.243	.030	-.143	-.353
100	26	-.224	.033	-.102	-.357
100	27	-.241	.027	-.140	-.350
100	28	-.258	.034	-.169	-.402
100	29	-.241	.028	-.159	-.378
100	30	-.266	.046	-.063	-.474
100	31	-.288	.033	-.057	-.529
100	32	-.288	.075	-.031	-.900
100	33	-.306	.070	-.102	-.718
100	34	-.200	.047	-.077	-.465
100	35	-.158	.039	-.058	-.460
100	36	-.233	.035	-.123	-.389
100	37	-.217	.051	-.025	-.415
100	38	-.167	.027	-.068	-.304
100	39	-.232	.024	-.151	-.331
100	40	-.338	.097	-.040	-.718
100	41	-.142	.036	-.013	-.362
100	42	-.171	.027	-.070	-.281
100	43	-.243	.024	-.165	-.336
100	44	-.233	.024	-.158	-.329
100	45	-.169	.027	-.059	-.321
100	46	-.260	.034	-.160	-.415
100	47	-.086	.040	.097	-.216
100	48	-.080	.041	.093	-.227
100	49	-.296	.037	-.186	-.437
100	50	-.245	.036	-.123	-.389
100	51	-.275	.059	-.148	-.717
100	52	-.115	.039	.022	-.273
100	53	-.285	.031	-.182	-.421
100	54	-.080	.036	.042	-.180
100	55	-.132	.029	-.016	-.248
100	56	-.108	.038	.029	-.276
100	57	-.169	.037	-.020	-.346
100	101	-.136	.027	-.038	-.270
100	102	-.139	.023	-.052	-.202
100	103	-.127	.027	-.006	-.262
100	104	-.124	.026	-.020	-.241
100	105	-.124	.020	-.027	-.194
100	106	-.136	.021	-.041	-.202
100	107	-.117	.020	-.022	-.190
100	108	-.124	.025	-.015	-.225
100	109	-.156	.030	-.029	-.268
100	110	-.154	.027	-.048	-.248
100	111	-.131	.020	-.054	-.197
100	112	-.164	.030	-.047	-.275
100	113	-.183	.033	-.079	-.323
100	114	-.159	.020	-.092	-.227
100	115	-.155	.023	-.052	-.232
100	116	-.149	.022	-.077	-.228
100	117	-.167	.024	-.072	-.268
100	118	-.258	.040	-.117	-.442
100	119	-.172	.024	-.086	-.269
100	120	-.183	.022	-.089	-.264
100	121	-.174	.018	-.104	-.239
100	122	-.213	.022	-.131	-.292
100	123	-.169	.018	-.099	-.228
100	124	-.183	.024	-.098	-.269
100	125	-.178	.018	-.126	-.241
100	126	-.227	.021	-.165	-.299
100	127	-.178	.021	-.108	-.245
100	128	-.191	.021	-.113	-.271
100	129	-.180	.015	-.135	-.227
100	130	-.237	.019	-.170	-.302
100	131	-.194	.020	-.130	-.268
100	132	-.189	.020	-.093	-.267
100	133	-.184	.017	-.115	-.252
100	134	-.268	.028	-.167	-.399
100	135	-.205	.022	-.137	-.330
100	136	-.188	.019	-.113	-.262
100	137	-.222	.020	-.150	-.307
100	138	-.252	.029	-.069	-.363
100	139	-.213	.026	-.119	-.316
100	140	-.223	.023	-.150	-.313
100	141	-.343	.066	-.203	-.627
100	142	-.315	.037	-.192	-.509
100	143	-.234	.032	-.130	-.389
100	144	-.216	.027	-.126	-.370
100	145	-.220	.021	-.164	-.300
100	146	-.259	.023	-.165	-.347
100	147	-.213	.022	-.141	-.299
100	148	-.218	.022	-.142	-.310
100	149	-.227	.019	-.155	-.302
100	150	-.282	.024	-.183	-.384
100	151	-.217	.023	-.115	-.296
100	152	-.243	.021	-.186	-.326
100	153	-.252	.025	-.183	-.349
100	154	-.329	.037	-.222	-.486
100	155	-.245	.031	-.139	-.365
100	156	-.234	.030	-.129	-.354
100	157	-.267	.024	-.190	-.355
100	158	-.396	.043	-.283	-.588
100	159	-.330	.035	-.232	-.451
100	160	-.324	.032	-.242	-.455
100	161	-.256	.025	-.183	-.344
100	162	-.131	.049	.074	-.274
100	163	-.067	.045	.155	-.208
100	164	-.372	.047	-.249	-.554
100	165	-.331	.041	-.221	-.488
100	166	-.464	.071	-.286	-.832
100	167	-.138	.019	-.072	-.200
100	201	-.280	.083	-.060	-.867
100	202	-.256	.046	-.111	-.457
100	203	-.252	.047	-.086	-.490
100	204	-.271	.077	-.051	-.629
100	205	-.146	.033	-.004	-.394
100	206	-.157	.037	-.039	-.447
100	207	-.145	.021	-.064	-.254
100	208	-.188	.028	-.076	-.299
100	209	-.162	.052	-.004	-.422
100	210	-.134	.030	-.010	-.240
100	211	-.151	.027	-.029	-.227
100	212	-.192	.028	-.049	-.338
100	213	-.143	.026	-.018	-.228
100	214	-.123	.021	-.036	-.190
100	301	-.062	.050	.194	-.183
100	302	-.256	.053	-.010	-.484
100	303	-.374	.050	-.208	-.564
100	304	-.014	.076	.336	-.253
100	305	-.259	.033	-.159	-.393
100	306	-.128	.064	.211	-.343
100	307	-.077	.043	.084	-.219
100	308	-.218	.028	-.113	-.310
100	309	-.078	.041	.125	-.210
100	310	-.155	.052	.063	-.379
100	311	-.125	.056	.091	-.380
100	312	.096	.089	.450	-.199
100	313	-.063	.040	.112	-.227
100	314	-.127	.045	.065	-.286
100	315	-.171	.056	.005	-.389
100	316	-.205	.046	-.041	-.381
100	317	.027	.043	.214	-.099
100	318	-.130	.016	-.074	-.200
100	319	-.027	.024	.074	-.101
100	320	-.091	.058	.205	-.369
100	401	-.240	.047	-.025	-.507
100	402	-.230	.029	-.146	-.435

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
100	403	-.154	.090	.217	-.500
100	404	-.102	.089	.227	-.357
100	405	-.168	.073	.253	-.449
100	406	-.224	.051	.070	-.435
110	1	-.103	.049	.128	-.311
110	2	-.108	.023	-.032	-.191
110	3	-.103	.028	-.008	-.225
110	4	-.090	.024	-.004	-.185
110	5	-.107	.029	.037	-.219
110	6	-.150	.051	.055	-.419
110	7	-.126	.038	.066	-.311
110	8	-.209	.041	-.018	-.377
110	9	-.162	.049	.051	-.424
110	10	-.185	.046	-.020	-.443
110	11	-.265	.063	-.030	-.541
110	12	-.157	.026	-.046	-.281
110	13	-.269	.077	-.057	-.669
110	14	-.160	.036	-.013	-.284
110	15	-.169	.024	-.084	-.264
110	16	-.176	.029	-.087	-.311
110	17	-.234	.057	-.076	-.567
110	18	-.163	.019	-.106	-.270
110	19	-.206	.035	-.056	-.393
110	20	-.128	.027	-.008	-.246
110	21	-.165	.023	-.078	-.281
110	22	-.211	.036	-.113	-.450
110	23	-.203	.025	-.119	-.342
110	24	-.240	.041	-.125	-.423
110	25	-.210	.028	-.110	-.413
110	26	-.190	.032	-.050	-.303
110	27	-.246	.033	-.135	-.419
110	28	-.218	.030	-.115	-.391
110	29	-.238	.034	-.115	-.396
110	30	-.219	.051	.024	-.405
110	31	-.277	.076	-.016	-.874
110	32	-.295	.082	-.041	-.745
110	33	-.328	.090	-.080	-.745
110	34	-.105	.071	.204	-.450
110	35	-.072	.057	.113	-.314
110	36	-.222	.047	-.071	-.489
110	37	-.122	.047	.026	-.325
110	38	-.130	.025	-.020	-.228
110	39	-.198	.025	-.128	-.295
110	40	-.266	.075	-.046	-.701
110	41	-.110	.026	.024	-.256
110	42	-.156	.030	-.055	-.284
110	43	-.226	.025	-.154	-.354
110	44	-.217	.029	-.127	-.349
110	45	-.148	.019	-.078	-.246
110	46	-.218	.031	-.134	-.377
110	47	-.047	.045	.174	-.185
110	48	-.051	.043	.190	-.258
110	49	-.274	.036	-.152	-.410
110	50	-.263	.050	-.111	-.534
110	51	-.368	.106	-.150	-.802
110	52	-.044	.046	.202	-.178
110	53	-.249	.034	-.145	-.383
110	54	-.036	.047	.172	-.212
110	55	-.121	.034	.090	-.274
110	56	-.074	.041	.118	-.300
110	57	-.150	.039	-.002	-.343
110	101	-.114	.025	.017	-.237
110	102	-.109	.024	.036	-.189
110	103	-.104	.026	.029	-.176
110	104	-.105	.025	-.023	-.200
110	105	-.107	.021	-.029	-.186
110	106	-.118	.021	-.035	-.187
110	107	-.088	.021	-.015	-.160
110	108	-.104	.028	.007	-.200
110	109	-.152	.030	-.041	-.247
110	110	-.148	.027	-.032	-.246
110	111	-.114	.022	-.032	-.211
110	112	-.156	.030	-.059	-.288
110	113	-.190	.035	-.078	-.342
110	114	-.150	.020	-.086	-.220
110	115	-.140	.023	-.064	-.239
110	116	-.137	.023	-.064	-.219
110	117	-.158	.023	-.060	-.235
110	118	-.234	.037	-.098	-.422
110	119	-.152	.024	-.076	-.239
110	120	-.159	.020	-.072	-.242
110	121	-.150	.017	-.084	-.219
110	122	-.190	.022	-.101	-.268
110	123	-.143	.018	-.078	-.205
110	124	-.158	.024	-.083	-.337
110	125	-.149	.018	-.084	-.250
110	126	-.199	.021	-.126	-.304
110	127	-.153	.020	-.087	-.229
110	128	-.166	.025	-.079	-.262
110	129	-.148	.019	-.084	-.228
110	130	-.214	.022	-.140	-.309
110	131	-.173	.024	-.073	-.276
110	132	-.168	.024	-.083	-.299
110	133	-.158	.021	-.091	-.255
110	134	-.268	.037	-.149	-.519
110	135	-.188	.026	-.109	-.285
110	136	-.165	.021	-.101	-.242
110	137	-.198	.024	-.115	-.332
110	138	-.207	.026	-.054	-.345
110	139	-.188	.033	-.089	-.334
110	140	-.213	.029	-.125	-.359
110	141	-.367	.072	-.184	-.706
110	142	-.329	.049	-.140	-.574
110	143	-.198	.040	-.067	-.376
110	144	-.176	.029	-.096	-.301
110	145	-.181	.021	-.120	-.279
110	146	-.224	.025	-.138	-.350
110	147	-.189	.024	-.113	-.303
110	148	-.188	.025	-.070	-.295
110	149	-.194	.021	-.120	-.301
110	150	-.250	.033	-.140	-.405
110	151	-.187	.027	-.047	-.316
110	152	-.224	.026	-.140	-.341
110	153	-.231	.028	-.144	-.343
110	154	-.297	.042	-.170	-.482
110	155	-.217	.035	-.105	-.352
110	156	-.214	.033	-.105	-.343
110	157	-.257	.027	-.177	-.345
110	158	-.376	.046	-.266	-.669
110	159	-.311	.036	-.218	-.443
110	160	-.318	.036	-.220	-.451
110	161	-.246	.027	-.171	-.343
110	162	-.031	.058	.218	-.218
110	163	.013	.054	.263	-.158
110	164	-.359	.056	-.213	-.586
110	165	-.306	.047	-.206	-.544
110	166	-.446	.080	-.261	-.822
110	167	-.122	.019	-.058	-.188
110	201	-.225	.056	-.031	-.586
110	202	-.215	.036	-.063	-.412
110	203	-.214	.036	-.080	-.396
110	204	-.319	.092	-.056	-.697
110	205	-.126	.038	.000	-.314
110	206	-.134	.032	-.016	-.301
110	207	-.123	.025	-.038	-.235
110	208	-.147	.027	-.035	-.241
110	209	-.117	.036	.040	-.312
110	210	-.116	.029	.027	-.211
110	211	-.143	.028	-.040	-.241
110	212	-.158	.032	-.042	-.277
110	213	-.105	.027	-.002	-.198
110	214	-.091	.022	-.015	-.167
110	301	.010	.063	.320	-.140
110	302	-.197	.076	.227	-.528
110	303	-.350	.052	-.178	-.586
110	304	-.090	.108	.636	-.244
110	305	-.205	.032	-.089	-.328
110	306	-.024	.085	.499	-.238
110	307	-.001	.050	.227	-.158
110	308	-.186	.030	-.043	-.290

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
110	309	.009	.048	.234	-.140
110	310	-.059	.058	.211	-.300
110	311	-.023	.065	.267	-.238
110	312	.123	.092	.567	-.213
110	313	.012	.047	.205	-.120
110	314	-.046	.053	.179	-.204
110	315	-.067	.063	.172	-.307
110	316	-.122	.053	.093	-.332
110	317	.109	.058	.460	-.018
110	318	-.111	.018	-.042	-.176
110	319	-.000	.026	.115	-.088
110	320	-.052	.074	.375	-.393
110	401	-.173	.042	-.020	-.370
110	402	-.191	.023	-.118	-.306
110	403	-.169	.100	.317	-.520
110	404	-.005	.084	.351	-.326
110	405	-.047	.106	.381	-.346
110	406	-.121	.082	.240	-.376
120	1	-.085	.036	.084	-.248
120	2	-.085	.024	.006	-.198
120	3	-.074	.026	.038	-.205
120	4	-.057	.023	.036	-.157
120	5	-.076	.027	.042	-.237
120	6	-.123	.036	.118	-.322
120	7	-.101	.039	.159	-.219
120	8	-.181	.035	-.004	-.346
120	9	-.138	.047	.155	-.364
120	10	-.171	.041	-.027	-.386
120	11	-.271	.054	-.096	-.490
120	12	-.138	.023	-.059	-.241
120	13	-.257	.064	-.050	-.566
120	14	-.124	.029	-.001	-.273
120	15	-.141	.021	-.070	-.221
120	16	-.115	.024	-.036	-.269
120	17	-.173	.054	-.066	-.467
120	18	-.138	.018	-.079	-.222
120	19	-.149	.031	-.025	-.282
120	20	-.106	.023	-.006	-.208
120	21	-.135	.025	-.046	-.230
120	22	-.189	.031	-.074	-.334
120	23	-.187	.025	-.108	-.301
120	24	-.242	.051	-.094	-.513
120	25	-.155	.030	-.055	-.271
120	26	-.135	.036	.022	-.336
120	27	-.241	.035	-.136	-.400
120	28	-.160	.033	-.055	-.334
120	29	-.196	.036	-.080	-.370
120	30	-.134	.072	.151	-.386
120	31	-.263	.091	.017	-.650
120	32	-.272	.069	-.083	-.620

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
120	33	-.290	.075	-.034	-.684
120	34	-.062	.066	.261	-.318
120	35	-.046	.042	.114	-.245
120	36	-.168	.047	-.020	-.590
120	37	-.051	.034	.093	-.193
120	38	-.093	.027	.020	-.231
120	39	-.166	.025	-.077	-.294
120	40	-.195	.048	-.041	-.529
120	41	-.089	.022	-.004	-.202
120	42	-.123	.035	-.011	-.254
120	43	-.204	.029	-.113	-.339
120	44	-.189	.035	-.092	-.334
120	45	-.115	.019	-.043	-.179
120	46	-.185	.028	-.086	-.301
120	47	-.029	.060	.213	-.256
120	48	-.017	.086	.471	-.269
120	49	-.226	.039	-.110	-.380
120	50	-.295	.070	-.128	-.627
120	51	-.469	.129	-.143	-1.109
120	52	-.031	.068	.329	-.415
120	53	-.207	.039	-.041	-.396
120	54	-.040	.060	.132	-.285
120	55	-.104	.043	.095	-.292
120	56	-.031	.048	.157	-.234
120	57	-.110	.044	.081	-.479
120	101	-.098	.022	-.020	-.182
120	102	-.087	.021	-.009	-.164
120	103	-.076	.023	.006	-.166
120	104	-.069	.023	.005	-.163
120	105	-.077	.021	.010	-.161
120	106	-.089	.021	-.006	-.160
120	107	-.055	.019	.010	-.125
120	108	-.067	.030	.033	-.188
120	109	-.136	.027	.001	-.245
120	110	-.131	.024	-.021	-.233
120	111	-.088	.022	.010	-.173
120	112	-.134	.026	-.050	-.258
120	113	-.186	.027	-.058	-.313
120	114	-.126	.020	-.054	-.197
120	115	-.114	.021	-.041	-.185
120	116	-.104	.023	-.020	-.207
120	117	-.127	.022	-.046	-.203
120	118	-.195	.030	-.108	-.311
120	119	-.118	.020	-.043	-.204
120	120	-.125	.019	-.067	-.217
120	121	-.114	.016	-.062	-.183
120	122	-.153	.022	-.033	-.221
120	123	-.108	.017	-.040	-.167
120	124	-.121	.021	-.054	-.250
120	125	-.109	.017	-.051	-.174

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
120	126	-.156	.021	-.071	-.235
120	127	-.116	.021	-.031	-.198
120	128	-.134	.025	-.045	-.233
120	129	-.108	.020	-.033	-.185
120	130	-.180	.021	-.094	-.264
120	131	-.145	.023	-.051	-.240
120	132	-.137	.026	-.030	-.292
120	133	-.125	.024	-.042	-.238
120	134	-.267	.044	-.162	-.491
120	135	-.164	.028	-.076	-.271
120	136	-.135	.022	-.059	-.213
120	137	-.169	.025	-.091	-.269
120	138	-.158	.039	.044	-.330
120	139	-.151	.036	-.042	-.363
120	140	-.184	.033	-.096	-.316
120	141	-.351	.057	-.185	-.619
120	142	-.287	.054	-.099	-.514
120	143	-.148	.038	-.035	-.325
120	144	-.131	.031	-.028	-.330
120	145	-.135	.020	-.066	-.218
120	146	-.173	.025	-.074	-.273
120	147	-.156	.026	-.071	-.256
120	148	-.148	.028	-.061	-.264
120	149	-.155	.025	-.064	-.258
120	150	-.185	.031	-.094	-.346
120	151	-.142	.034	-.018	-.314
120	152	-.189	.032	-.109	-.312
120	153	-.208	.032	-.091	-.403
120	154	-.246	.047	-.110	-.455
120	155	-.184	.037	-.053	-.320
120	156	-.193	.033	-.092	-.336
120	157	-.232	.028	-.157	-.350
120	158	-.332	.050	-.198	-.577
120	159	-.273	.037	-.167	-.421
120	160	-.309	.041	-.204	-.528
120	161	-.231	.027	-.150	-.353
120	162	.061	.067	.380	-.167
120	163	.075	.060	.310	-.147
120	164	-.322	.054	-.182	-.539
120	165	-.276	.048	-.146	-.483
120	166	-.402	.079	-.194	-.702
120	167	-.103	.019	-.025	-.160
120	201	-.180	.033	-.051	-.349
120	202	-.181	.026	-.103	-.334
120	203	-.190	.030	-.104	-.335
120	204	-.340	.091	-.071	-.707
120	205	-.095	.034	.031	-.289
120	206	-.114	.030	-.016	-.255
120	207	-.093	.020	-.011	-.165
120	208	-.114	.023	-.006	-.185

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
120	209	-.091	.027	.065	-.202
120	210	-.087	.026	.012	-.195
120	211	-.116	.026	-.020	-.212
120	212	-.122	.032	.004	-.244
120	213	-.075	.027	.047	-.169
120	214	-.063	.020	.018	-.149
120	301	.049	.070	.352	-.159
120	302	-.151	.103	.314	-.473
120	303	-.326	.056	-.182	-.661
120	304	.222	.133	.736	-.275
120	305	-.157	.037	.059	-.324
120	306	.089	.097	.591	-.353
120	307	.081	.062	.336	-.105
120	308	-.149	.034	.034	-.268
120	309	.095	.061	.392	-.119
120	310	.025	.068	.308	-.326
120	311	.075	.084	.441	-.283
120	312	.116	.101	.474	-.224
120	313	.072	.048	.297	-.082
120	314	.028	.059	.269	-.149
120	315	.026	.064	.294	-.202
120	316	-.026	.061	.310	-.230
120	317	.180	.074	.508	.006
120	318	-.093	.018	-.030	-.162
120	319	.011	.024	.105	-.066
120	320	-.006	.096	.520	-.354
120	401	-.088	.034	-.041	-.251
120	402	-.136	.020	-.072	-.221
120	403	-.185	.087	.323	-.461
120	404	.024	.067	.358	-.218
120	405	.059	.091	.397	-.237
120	406	-.004	.073	.264	-.275
130	1	-.061	.029	.053	-.162
130	2	-.072	.024	.036	-.182
130	3	-.065	.027	.041	-.191
130	4	-.041	.024	.047	-.173
130	5	-.051	.024	.035	-.160
130	6	-.103	.030	.013	-.194
130	7	-.066	.036	.107	-.188
130	8	-.155	.033	-.017	-.314
130	9	-.111	.041	.056	-.305
130	10	-.150	.036	-.032	-.354
130	11	-.232	.041	-.132	-.427
130	12	-.118	.024	-.020	-.214
130	13	-.240	.053	-.071	-.518
130	14	-.105	.026	.001	-.199
130	15	-.117	.025	-.036	-.214
130	16	-.071	.022	.003	-.191
130	17	-.102	.032	-.009	-.284
130	18	-.114	.021	-.044	-.201

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
130	19	-.110	.028	-.004	-.231
130	20	-.076	.025	.045	-.175
130	21	-.100	.027	.014	-.197
130	22	-.150	.022	-.081	-.307
130	23	-.150	.024	-.056	-.243
130	24	-.252	.055	-.008	-.532
130	25	-.101	.024	-.020	-.217
130	26	-.088	.033	.076	-.204
130	27	-.191	.032	-.099	-.356
130	28	-.101	.023	-.015	-.207
130	29	-.133	.027	-.016	-.245
130	30	-.051	.062	.192	-.307
130	31	-.184	.095	.166	-.597
130	32	-.213	.055	-.031	-.509
130	33	-.204	.056	-.020	-.475
130	34	-.055	.052	.279	-.215
130	35	-.027	.048	.222	-.217
130	36	-.126	.035	-.006	-.296
130	37	-.019	.026	.088	-.105
130	38	-.090	.026	.008	-.197
130	39	-.131	.026	-.023	-.302
130	40	-.129	.029	-.045	-.268
130	41	-.067	.021	.003	-.188
130	42	-.090	.033	.043	-.220
130	43	-.186	.032	-.084	-.328
130	44	-.130	.039	-.024	-.314
130	45	-.081	.020	.010	-.201
130	46	-.153	.027	-.060	-.277
130	47	-.069	.060	.253	-.283
130	48	.046	.099	.474	-.251
130	49	-.169	.032	-.077	-.314
130	50	-.312	.065	-.081	-.644
130	51	-.475	.135	-.148	-1.126
130	52	.095	.083	.455	-.444
130	53	-.154	.056	.037	-.394
130	54	-.065	.070	.389	-.286
130	55	-.061	.067	.258	-.323
130	56	.002	.071	.302	-.523
130	57	-.097	.054	.090	-.424
130	101	-.080	.023	.018	-.171
130	102	-.073	.024	.001	-.167
130	103	-.052	.023	.041	-.133
130	104	-.050	.024	.028	-.158
130	105	-.062	.023	.039	-.145
130	106	-.075	.021	.001	-.148
130	107	-.036	.021	.038	-.124
130	108	-.048	.029	.060	-.172
130	109	-.122	.026	-.030	-.220
130	110	-.116	.023	-.035	-.200
130	111	-.067	.021	.010	-.161

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
130	112	-.110	.026	-.013	-.266
130	113	-.166	.023	-.098	-.288
130	114	-.106	.020	-.030	-.174
130	115	-.089	.021	-.004	-.180
130	116	-.077	.021	.012	-.151
130	117	-.100	.026	.032	-.192
130	118	-.159	.028	-.025	-.285
130	119	-.089	.024	.010	-.210
130	120	-.092	.023	-.004	-.199
130	121	-.079	.019	-.013	-.163
130	122	-.118	.023	-.039	-.215
130	123	-.084	.019	-.013	-.160
130	124	-.095	.026	.007	-.232
130	125	-.081	.019	-.005	-.156
130	126	-.128	.022	-.051	-.208
130	127	-.099	.021	-.011	-.195
130	128	-.098	.027	.001	-.199
130	129	-.078	.022	-.000	-.147
130	130	-.137	.023	-.064	-.226
130	131	-.105	.024	-.020	-.191
130	132	-.103	.028	-.004	-.221
130	133	-.096	.025	-.008	-.180
130	134	-.260	.050	-.105	-.643
130	135	-.115	.025	-.020	-.217
130	136	-.106	.023	-.034	-.186
130	137	-.119	.021	-.044	-.213
130	138	-.111	.031	-.024	-.231
130	139	-.122	.042	-.018	-.359
130	140	-.139	.029	-.045	-.265
130	141	-.264	.049	-.147	-.511
130	142	-.188	.034	-.057	-.319
130	143	-.191	.032	-.009	-.235
130	144	-.092	.035	.036	-.274
130	145	-.094	.022	-.018	-.195
130	146	-.125	.025	-.039	-.229
130	147	-.106	.023	-.038	-.206
130	148	-.115	.031	.005	-.241
130	149	-.101	.028	-.027	-.235
130	150	-.157	.033	-.030	-.332
130	151	-.094	.039	.089	-.233
130	152	-.123	.022	-.032	-.221
130	153	-.150	.058	-.046	-.371
130	154	-.176	.038	-.066	-.368
130	155	-.156	.039	-.022	-.353
130	156	-.186	.031	-.069	-.317
130	157	-.191	.032	-.064	-.299
130	158	-.280	.054	-.120	-.494
130	159	-.230	.039	-.100	-.384
130	160	-.275	.053	-.135	-.585
130	161	-.191	.032	-.101	-.338

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
130	162	.103	.099	.607	-.181
130	163	.072	.085	.499	-.184
130	164	-.259	.060	-.109	-.557
130	165	-.213	.053	-.084	-.454
130	166	-.330	.078	-.154	-.686
130	167	-.082	.019	-.025	-.161
130	201	-.149	.022	-.086	-.286
130	202	-.154	.021	-.085	-.241
130	203	-.165	.023	-.081	-.252
130	204	-.300	.075	-.102	-.611
130	205	-.067	.029	.107	-.177
130	206	-.079	.028	.018	-.262
130	207	-.064	.020	.039	-.145
130	208	-.075	.024	.035	-.159
130	209	-.057	.025	.049	-.151
130	210	-.060	.023	.027	-.148
130	211	-.088	.022	-.009	-.187
130	212	-.086	.032	.121	-.251
130	213	-.046	.026	.053	-.155
130	214	-.038	.020	.038	-.120
130	301	-.013	.075	.506	-.209
130	302	-.103	.131	.418	-.461
130	303	-.293	.065	-.120	-.572
130	304	-.275	.142	.876	-.157
130	305	-.090	.068	.228	-.303
130	306	.122	.128	.783	-.325
130	307	-.155	.084	.550	-.071
130	308	-.089	.050	.148	-.234
130	309	.140	.078	.449	-.136
130	310	.070	.092	.418	-.276
130	311	.132	.112	.610	-.277
130	312	.071	.126	.595	-.385
130	313	.086	.070	.410	-.086
130	314	.051	.084	.456	-.208
130	315	.060	.086	.508	-.182
130	316	.075	.071	.549	-.146
130	317	.252	.079	.685	.044
130	318	-.076	.019	-.011	-.144
130	319	-.004	.022	.090	-.068
130	320	.095	.121	.638	-.384
130	401	-.033	.028	.092	-.144
130	402	-.086	.019	-.002	-.166
130	403	-.070	.101	.426	-.357
130	404	.034	.068	.400	-.153
130	405	.109	.078	.496	-.123
130	406	.054	.049	.273	-.109
140	1	-.027	.029	.161	-.119
140	2	-.079	.020	.025	-.141
140	3	-.080	.023	.012	-.163
140	4	-.047	.019	.024	-.108
140	5	-.065	.021	.014	-.142
140	6	-.063	.027	.065	-.167
140	7	-.068	.029	.062	-.189
140	8	-.120	.029	-.017	-.256
140	9	-.108	.031	.023	-.238
140	10	-.148	.025	-.051	-.315
140	11	-.182	.033	-.099	-.343
140	12	-.120	.027	-.038	-.244
140	13	-.213	.051	-.068	-.433
140	14	-.095	.020	.003	-.155
140	15	-.090	.026	.022	-.281
140	16	-.038	.021	.057	-.119
140	17	-.065	.027	.023	-.210
140	18	-.088	.024	.011	-.183
140	19	-.086	.024	.005	-.189
140	20	-.047	.025	.061	-.165
140	21	-.071	.029	.056	-.213
140	22	-.126	.018	-.067	-.212
140	23	-.128	.024	-.044	-.258
140	24	-.205	.062	-.036	-.543
140	25	-.068	.023	.017	-.190
140	26	-.071	.031	.077	-.190
140	27	-.173	.033	-.035	-.355
140	28	-.070	.022	.006	-.145
140	29	-.091	.029	.017	-.203
140	30	-.054	.052	.313	-.209
140	31	-.113	.073	.098	-.459
140	32	-.168	.050	-.006	-.415
140	33	-.157	.054	.003	-.417
140	34	-.043	.043	.268	-.075
140	35	-.020	.054	.254	-.239
140	36	-.067	.041	.066	-.270
140	37	-.091	.027	.131	-.089
140	38	-.069	.027	.058	-.190
140	39	-.096	.026	.015	-.232
140	40	-.083	.025	-.001	-.196
140	41	-.059	.023	.028	-.162
140	42	-.079	.033	.088	-.207
140	43	-.145	.030	-.037	-.352
140	44	-.076	.028	.024	-.242
140	45	-.058	.023	.026	-.240
140	46	-.121	.033	.029	-.266
140	47	-.061	.068	.228	-.286
140	48	-.040	.077	.577	-.279
140	49	-.132	.028	-.025	-.242
140	50	-.324	.066	-.098	-.703
140	51	-.466	.121	-.130	-.962
140	52	-.116	.093	.450	-.443
140	53	-.076	.057	.136	-.295
140	54	-.056	.086	.358	-.382
140	55	-.056	.073	.271	-.326
140	56	.003	.064	.304	-.351
140	57	-.066	.055	.124	-.435
140	101	-.094	.021	-.013	-.183
140	102	-.089	.020	-.007	-.153
140	103	-.056	.021	.036	-.138
140	104	-.053	.020	.040	-.160
140	105	-.074	.023	.027	-.157
140	106	-.089	.019	-.014	-.163
140	107	-.052	.018	.022	-.110
140	108	-.042	.027	.099	-.121
140	109	-.139	.022	-.063	-.247
140	110	-.122	.021	-.016	-.229
140	111	-.063	.019	.017	-.133
140	112	-.089	.026	.003	-.215
140	113	-.143	.021	-.077	-.240
140	114	-.091	.021	-.004	-.156
140	115	-.077	.023	.013	-.196
140	116	-.058	.020	.019	-.139
140	117	-.070	.031	.065	-.186
140	118	-.118	.027	-.014	-.224
140	119	-.064	.024	.027	-.179
140	120	-.064	.023	.027	-.166
140	121	-.047	.019	.030	-.146
140	122	-.089	.024	.012	-.179
140	123	-.060	.019	.011	-.122
140	124	-.067	.026	.027	-.188
140	125	-.047	.019	.030	-.120
140	126	-.098	.022	.003	-.210
140	127	-.075	.021	.029	-.149
140	128	-.073	.027	.034	-.236
140	129	-.046	.019	.024	-.116
140	130	-.107	.022	-.026	-.304
140	131	-.080	.024	.016	-.257
140	132	-.074	.025	.021	-.192
140	133	-.058	.021	.024	-.140
140	134	-.210	.056	-.057	-.464
140	135	-.087	.027	-.025	-.208
140	136	-.074	.018	-.004	-.142
140	137	-.086	.020	-.026	-.183
140	138	-.078	.033	.136	-.228
140	139	-.083	.026	.011	-.215
140	140	-.089	.022	.003	-.192
140	141	-.198	.049	-.066	-.419
140	142	-.130	.040	.010	-.298
140	143	-.056	.024	.020	-.197
140	144	-.050	.033	.089	-.339
140	145	-.050	.020	.028	-.157
140	146	-.086	.024	.010	-.201
140	147	-.076	.020	.000	-.171

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
140	148	-.068	.025	.034	-.206
140	149	-.064	.025	.024	-.207
140	150	-.120	.027	-.010	-.264
140	151	-.051	.031	.100	-.177
140	152	-.089	.018	-.021	-.175
140	153	-.094	.038	.041	-.288
140	154	-.134	.031	.015	-.286
140	155	-.115	.035	-.015	-.275
140	156	-.155	.032	-.052	-.333
140	157	-.147	.033	.021	-.271
140	158	-.234	.054	-.093	-.520
140	159	-.189	.042	-.062	-.461
140	160	-.247	.054	-.076	-.451
140	161	-.163	.035	-.040	-.343
140	162	.175	.109	.655	-.102
140	163	.110	.097	.675	-.166
140	164	-.197	.055	-.039	-.467
140	165	-.157	.066	.024	-.404
140	166	-.265	.076	-.050	-.655
140	167	-.086	.017	-.026	-.145
140	201	-.119	.020	-.051	-.222
140	202	-.122	.019	-.058	-.188
140	203	-.121	.020	-.053	-.207
140	204	-.175	.033	-.071	-.329
140	205	-.051	.024	.045	-.184
140	206	-.105	.025	-.014	-.246
140	207	-.041	.019	.043	-.101
140	208	-.076	.023	.033	-.145
140	209	-.063	.024	.031	-.135
140	210	-.059	.021	.012	-.146
140	211	-.081	.019	-.013	-.173
140	212	-.078	.027	.028	-.190
140	213	-.055	.020	.016	-.133
140	214	-.048	.020	.021	-.111
140	301	.041	.091	.414	-.159
140	302	-.094	.144	.540	-.495
140	303	-.226	.067	.098	-.648
140	304	.320	.141	.883	-.131
140	305	.008	.077	.370	-.214
140	306	.205	.126	.709	-.246
140	307	.207	.090	.593	-.027
140	308	-.045	.042	.183	-.181
140	309	.224	.090	.538	-.061
140	310	.157	.111	.558	-.170
140	311	.216	.132	.661	-.191
140	312	.099	.125	.646	-.418
140	313	.141	.078	.510	-.050
140	314	.105	.093	.516	-.158
140	315	.122	.094	.504	-.146
140	316	.169	.089	.538	-.054
140	317	-.290	.092	.678	-.047
140	318	-.052	.018	.022	-.126
140	319	.003	.022	.078	-.067
140	320	.166	.142	.794	-.288
140	401	-.007	.025	.122	-.120
140	402	-.048	.021	.047	-.144
140	403	-.003	.094	.432	-.352
140	404	.053	.074	.546	-.168
140	405	.096	.074	.543	-.094
140	406	.055	.048	.289	-.062
150	1	-.017	.030	.139	-.110
150	2	-.070	.028	.056	-.183
150	3	-.080	.023	.015	-.169
150	4	-.047	.021	.022	-.122
150	5	-.065	.019	.014	-.140
150	6	-.057	.025	.056	-.166
150	7	-.071	.031	.063	-.220
150	8	-.106	.027	-.011	-.248
150	9	-.111	.029	.017	-.274
150	10	-.138	.020	-.059	-.235
150	11	-.159	.029	-.076	-.366
150	12	-.113	.032	.027	-.292
150	13	-.208	.052	-.053	-.454
150	14	-.083	.020	.001	-.156
150	15	-.077	.026	.101	-.184
150	16	-.025	.022	.080	-.122
150	17	-.046	.023	.056	-.210
150	18	-.073	.021	.027	-.154
150	19	-.082	.022	.015	-.165
150	20	-.038	.024	.059	-.141
150	21	-.052	.027	.063	-.214
150	22	-.115	.019	-.054	-.188
150	23	-.114	.022	-.043	-.270
150	24	-.180	.066	.017	-.548
150	25	-.051	.024	.038	-.140
150	26	-.050	.035	.113	-.166
150	27	-.166	.044	-.016	-.428
150	28	-.053	.025	.052	-.192
150	29	-.049	.024	.033	-.163
150	30	-.041	.055	.254	-.199
150	31	-.141	.072	.108	-.478
150	32	-.158	.056	.010	-.434
150	33	-.148	.061	.035	-.577
150	34	-.035	.047	.357	-.092
150	35	-.030	.051	.333	-.217
150	36	-.023	.030	.132	-.162
150	37	.002	.026	.114	-.096
150	38	-.052	.026	.058	-.195
150	39	-.080	.023	.001	-.191
150	40	-.064	.024	.034	-.174
150	41	-.043	.024	.054	-.186
150	42	-.047	.038	.161	-.183
150	43	-.137	.037	.013	-.380
150	44	-.043	.026	.078	-.146
150	45	-.046	.025	.065	-.163
150	46	-.084	.029	.032	-.242
150	47	-.002	.058	.321	-.380
150	48	-.063	.069	.423	-.295
150	49	-.093	.031	.040	-.212
150	50	-.349	.074	-.145	-.705
150	51	-.424	.105	-.137	-.869
150	52	.127	.091	.434	-.555
150	53	-.018	.066	.252	-.244
150	54	-.050	.088	.352	-.371
150	55	-.040	.073	.276	-.380
150	56	.012	.067	.285	-.467
150	57	-.035	.055	.137	-.369
150	101	-.099	.023	-.004	-.209
150	102	-.091	.020	-.019	-.160
150	103	-.058	.020	.013	-.129
150	104	-.052	.021	.042	-.143
150	105	-.087	.023	.013	-.199
150	106	-.093	.020	-.007	-.160
150	107	-.050	.020	.038	-.118
150	108	-.054	.024	.074	-.147
150	109	-.137	.019	-.073	-.223
150	110	-.119	.019	-.040	-.205
150	111	-.060	.016	-.001	-.118
150	112	-.070	.023	.010	-.186
150	113	-.129	.021	-.044	-.216
150	114	-.089	.020	-.014	-.167
150	115	-.086	.033	.015	-.253
150	116	-.050	.020	.021	-.117
150	117	-.044	.036	.147	-.154
150	118	-.092	.027	.015	-.184
150	119	-.046	.024	.048	-.167
150	120	-.051	.023	.049	-.148
150	121	-.030	.019	.043	-.114
150	122	-.077	.023	.055	-.199
150	123	-.052	.018	.020	-.110
150	124	-.054	.026	.047	-.226
150	125	-.028	.019	.051	-.110
150	126	-.091	.022	-.005	-.203
150	127	-.071	.024	.071	-.185
150	128	-.052	.031	.090	-.185
150	129	-.029	.018	.069	-.095
150	130	-.085	.022	.012	-.188
150	131	-.058	.024	.038	-.159
150	132	-.053	.025	.053	-.130
150	133	-.037	.019	.058	-.101

APPENDIX A -- PRESSURE DATA: CONFIGURATION A) MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
150	134	-.160	.059	-.008	-.468
150	135	-.053	.026	.064	-.192
150	136	-.061	.021	.029	-.137
150	137	-.061	.026	.030	-.188
150	138	-.028	.041	.217	-.177
150	139	-.068	.034	.069	-.254
150	140	-.059	.026	.075	-.145
150	141	-.136	.051	.094	-.405
150	142	-.072	.033	.039	-.261
150	143	-.029	.025	.071	-.128
150	144	-.026	.024	.084	-.200
150	145	-.019	.016	.049	-.086
150	146	-.055	.021	.037	-.137
150	147	-.049	.022	.049	-.128
150	148	-.043	.025	.068	-.174
150	149	-.029	.023	.086	-.183
150	150	-.093	.036	.026	-.355
150	151	-.017	.036	.207	-.161
150	152	-.054	.022	.029	-.156
150	153	-.044	.032	.127	-.248
150	154	-.090	.031	.072	-.257
150	155	-.069	.030	.049	-.234
150	156	-.107	.041	.042	-.294
150	157	-.103	.040	.086	-.291
150	158	-.238	.077	-.059	-.744
150	159	-.196	.076	.000	-.761
150	160	-.169	.057	.023	-.386
150	161	-.121	.043	.088	-.321
150	162	.200	.107	.799	-.085
150	163	-.127	.101	.558	-.143
150	164	-.128	.061	.090	-.440
150	165	-.062	.061	.120	-.317
150	166	-.190	.079	.070	-.515
150	167	-.070	.018	-.018	-.123
150	201	-.100	.019	-.037	-.172
150	202	-.102	.018	-.034	-.170
150	203	-.089	.016	-.033	-.155
150	204	-.139	.024	-.068	-.254
150	205	-.052	.026	.049	-.148
150	206	-.126	.032	-.035	-.308
150	207	-.039	.019	.017	-.099
150	208	-.073	.021	-.010	-.150
150	209	-.060	.020	.005	-.123
150	210	-.060	.022	.023	-.150
150	211	-.073	.018	-.000	-.162
150	212	-.049	.036	.132	-.161
150	213	-.045	.023	.095	-.139
150	214	-.048	.019	.025	-.111
150	301	-.138	.092	.540	-.106
150	302	-.085	.163	.564	-.664

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
150	303	-.162	.082	.205	-.626
150	304	.315	.135	.863	-.137
150	305	.082	.090	.467	-.201
150	306	.234	.127	.728	-.148
150	307	.220	.092	.693	-.121
150	308	-.005	.049	.285	-.174
150	309	.259	.088	.611	.034
150	310	.194	.119	.635	-.194
150	311	.254	.136	.759	-.134
150	312	.114	.136	.671	-.383
150	313	.170	.087	.516	-.033
150	314	.135	.105	.568	-.134
150	315	.154	.103	.585	-.134
150	316	.227	.099	.657	-.020
150	317	.305	.092	.695	.068
150	318	-.033	.023	.106	-.092
150	319	.026	.027	.145	-.052
150	320	.189	.150	.704	-.304
150	401	.003	.027	.151	-.106
150	402	-.023	.021	.054	-.124
150	403	.027	.103	.528	-.233
150	404	.056	.075	.467	-.117
150	405	.101	.081	.579	-.111
150	406	.068	.056	.377	-.117
160	1	-.032	.028	.136	-.123
160	2	-.070	.032	.125	-.201
160	3	-.110	.025	-.009	-.210
160	4	-.069	.023	.010	-.172
160	5	-.086	.023	.010	-.174
160	6	-.084	.028	.091	-.194
160	7	-.105	.043	.034	-.329
160	8	-.119	.026	-.020	-.216
160	9	-.123	.031	-.013	-.290
160	10	-.158	.023	-.082	-.272
160	11	-.158	.026	-.071	-.260
160	12	-.156	.047	-.022	-.380
160	13	-.227	.057	-.050	-.469
160	14	-.101	.027	.003	-.248
160	15	-.059	.027	.053	-.147
160	16	-.026	.025	.121	-.137
160	17	-.064	.028	.040	-.249
160	18	-.059	.021	.015	-.144
160	19	-.097	.021	.003	-.181
160	20	-.064	.034	.073	-.237
160	21	-.036	.027	.078	-.141
160	22	-.122	.020	-.030	-.215
160	23	-.100	.023	-.004	-.176
160	24	-.149	.065	.059	-.426
160	25	-.050	.026	.065	-.148
160	26	-.059	.040	.191	-.277

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
160	27	-.207	.061	-.047	-.599
160	28	-.053	.030	.061	-.184
160	29	-.002	.030	.111	-.119
160	30	-.022	.065	.269	-.201
160	31	-.194	.074	.096	-.475
160	32	-.181	.063	.038	-.505
160	33	-.204	.091	.065	-.657
160	34	.063	.060	.400	-.087
160	35	-.046	.049	.213	-.324
160	36	-.004	.027	.144	-.103
160	37	-.009	.026	.120	-.107
160	38	-.057	.029	.065	-.177
160	39	-.081	.021	.005	-.157
160	40	-.076	.023	.013	-.179
160	41	-.035	.024	.083	-.119
160	42	-.022	.050	.172	-.244
160	43	-.200	.060	-.023	-.494
160	44	-.002	.031	.121	-.126
160	45	-.055	.027	.030	-.201
160	46	-.069	.027	.075	-.149
160	47	.018	.065	.273	-.214
160	48	.048	.101	.599	-.216
160	49	-.044	.034	.065	-.183
160	50	-.371	.082	-.068	-.871
160	51	-.410	.107	-.133	-.978
160	52	.117	.094	.560	-.729
160	53	.028	.072	.317	-.283
160	54	-.037	.090	.452	-.400
160	55	-.023	.067	.402	-.245
160	56	.013	.068	.258	-.396
160	57	-.016	.053	.172	-.304
160	101	-.108	.027	.003	-.229
160	102	-.113	.025	-.047	-.229
160	103	-.080	.023	-.006	-.177
160	104	-.062	.020	.010	-.139
160	105	-.098	.021	-.008	-.170
160	106	-.093	.019	-.014	-.150
160	107	-.056	.019	.017	-.112
160	108	-.065	.018	.007	-.123
160	109	-.163	.022	-.103	-.258
160	110	-.124	.019	-.047	-.205
160	111	-.053	.016	.029	-.117
160	112	-.066	.022	.023	-.167
160	113	-.127	.020	-.063	-.208
160	114	-.083	.020	-.011	-.152
160	115	-.098	.041	.029	-.288
160	116	-.039	.019	.040	-.116
160	117	-.002	.044	.184	-.127
160	118	-.087	.033	.044	-.233
160	119	-.030	.023	.061	-.135

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
160	120	-.034	.024	.070	-.132
160	121	-.017	.019	.077	-.114
160	122	-.059	.027	.127	-.160
160	123	-.030	.024	.071	-.112
160	124	-.033	.030	.103	-.158
160	125	-.003	.022	.092	-.080
160	126	-.068	.021	.012	-.171
160	127	-.042	.030	.119	-.138
160	128	-.009	.033	.131	-.208
160	129	.031	.031	.144	-.058
160	130	-.058	.021	.041	-.182
160	131	-.027	.025	.104	-.143
160	132	-.011	.030	.110	-.117
160	133	.025	.033	.135	-.069
160	134	-.122	.046	.083	-.361
160	135	-.017	.029	.126	-.141
160	136	.002	.036	.136	-.091
160	137	-.065	.041	.045	-.261
160	138	.048	.057	.337	-.094
160	139	-.046	.043	.095	-.260
160	140	-.002	.034	.129	-.123
160	141	-.048	.072	.195	-.319
160	142	-.022	.033	.131	-.153
160	143	-.001	.028	.112	-.108
160	144	-.018	.024	.090	-.121
160	145	-.016	.016	.049	-.073
160	146	-.037	.020	.072	-.114
160	147	-.017	.029	.101	-.130
160	148	-.024	.025	.090	-.106
160	149	-.014	.022	.109	-.089
160	150	-.121	.068	.098	-.577
160	151	.047	.053	.337	-.079
160	152	-.015	.024	.066	-.099
160	153	-.002	.026	.097	-.177
160	154	-.037	.035	.096	-.180
160	155	-.019	.032	.101	-.165
160	156	-.031	.039	.125	-.208
160	157	-.025	.055	.150	-.196
160	158	-.269	.101	.014	-.780
160	159	-.241	.124	.099	-1.001
160	160	-.086	.064	.094	-.428
160	161	-.089	.070	.204	-.373
160	162	.215	.121	.849	-.167
160	163	.136	.113	.698	-.163
160	164	-.046	.072	.179	-.515
160	165	.014	.046	.148	-.254
160	166	-.072	.092	.348	-.449
160	167	-.059	.016	.005	-.110
160	201	-.106	.019	-.044	-.178
160	202	-.107	.018	-.047	-.182
160	203	-.081	.016	-.022	-.151
160	204	-.129	.023	-.043	-.231
160	205	-.053	.026	.038	-.277
160	206	-.170	.040	-.054	-.362
160	207	-.035	.018	.026	-.114
160	208	-.070	.026	-.003	-.162
160	209	-.059	.022	.011	-.132
160	210	-.082	.024	-.012	-.228
160	211	-.092	.021	-.020	-.190
160	212	-.056	.032	.118	-.202
160	213	-.051	.021	.044	-.134
160	214	-.059	.020	.014	-.128
160	301	.181	.093	.634	-.052
160	302	-.110	.173	.584	-.612
160	303	-.068	.100	.269	-.528
160	304	.286	.141	.797	-.202
160	305	.173	.108	.587	-.172
160	306	.232	.122	.798	-.171
160	307	.203	.100	.607	-.088
160	308	.081	.079	.451	-.084
160	309	.269	.090	.606	.043
160	310	.188	.142	.734	-.259
160	311	.232	.146	.731	-.262
160	312	.129	.130	.643	-.382
160	313	.178	.087	.574	-.009
160	314	.136	.112	.687	-.202
160	315	.143	.104	.702	-.185
160	316	.275	.107	.744	.010
160	317	.282	.091	.664	.072
160	318	.011	.031	.142	-.068
160	319	.026	.027	.143	-.042
160	320	.160	.148	.773	-.342
160	401	.001	.027	.128	-.091
160	402	-.017	.022	.075	-.140
160	403	.070	.128	.636	-.304
160	404	.035	.062	.348	-.137
160	405	.128	.085	.603	-.124
160	406	.108	.071	.440	-.076
170	1	-.054	.029	.088	-.197
170	2	-.105	.022	-.035	-.195
170	3	-.113	.027	-.004	-.225
170	4	-.064	.022	.006	-.163
170	5	-.106	.027	-.020	-.234
170	6	-.107	.029	.018	-.279
170	7	-.159	.052	.051	-.386
170	8	-.131	.027	-.022	-.258
170	9	-.143	.041	.017	-.432
170	10	-.185	.032	-.090	-.415
170	11	-.186	.029	-.103	-.425
170	12	-.115	.042	.036	-.305
170	13	-.253	.079	-.004	-.547
170	14	-.152	.036	.006	-.326
170	15	-.062	.035	.159	-.197
170	16	-.055	.038	.096	-.247
170	17	-.132	.040	-.013	-.349
170	18	-.075	.031	.073	-.200
170	19	-.127	.026	-.043	-.302
170	20	-.172	.045	-.029	-.428
170	21	-.066	.027	.134	-.149
170	22	-.149	.025	-.052	-.255
170	23	-.095	.027	.118	-.185
170	24	-.169	.071	.263	-.441
170	25	-.080	.029	.019	-.218
170	26	-.146	.073	.099	-.432
170	27	-.204	.066	-.004	-.552
170	28	-.092	.035	.050	-.238
170	29	.055	.035	.208	-.057
170	30	-.102	.080	.176	-.314
170	31	-.249	.070	-.002	-.545
170	32	-.300	.086	-.050	-.643
170	33	-.330	.088	-.062	-.740
170	34	.054	.063	.443	-.135
170	35	-.079	.053	.157	-.317
170	36	.017	.031	.173	-.082
170	37	-.031	.026	.074	-.158
170	38	-.103	.034	.015	-.236
170	39	-.090	.021	.039	-.165
170	40	-.110	.026	-.027	-.207
170	41	-.037	.027	.072	-.156
170	42	-.066	.074	.204	-.386
170	43	-.242	.066	-.091	-.653
170	44	.047	.039	.210	-.066
170	45	-.087	.030	.017	-.269
170	46	-.044	.035	.123	-.164
170	47	-.029	.087	.272	-.444
170	48	.048	.092	.478	-.235
170	49	.018	.038	.189	-.144
170	50	-.357	.071	-.099	-.711
170	51	-.404	.099	-.147	-.863
170	52	.063	.094	.467	-.532
170	53	.096	.063	.313	-.181
170	54	-.033	.075	.274	-.355
170	55	.043	.079	.368	-.235
170	56	.014	.068	.314	-.321
170	57	-.041	.074	.189	-.400
170	101	-.082	.031	.078	-.185
170	102	-.118	.023	-.040	-.225
170	103	-.114	.030	-.017	-.256
170	104	-.057	.023	.037	-.144
170	105	-.105	.023	-.011	-.188

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
170	106	-.082	.022	.003	-.153
170	107	-.077	.019	-.010	-.140
170	108	-.072	.018	-.014	-.149
170	109	-.195	.030	-.104	-.322
170	110	-.116	.031	.010	-.233
170	111	-.030	.020	.068	-.110
170	112	-.065	.039	.099	-.186
170	113	-.135	.033	.015	-.286
170	114	-.041	.033	.073	-.151
170	115	-.023	.052	.198	-.261
170	116	.015	.036	.157	-.108
170	117	-.065	.053	.245	-.133
170	118	-.142	.050	.068	-.324
170	119	-.032	.034	.152	-.170
170	120	-.023	.030	.126	-.139
170	121	-.016	.021	.086	-.093
170	122	-.011	.046	.173	-.140
170	123	.021	.030	.201	-.070
170	124	.002	.035	.167	-.131
170	125	.023	.023	.135	-.067
170	126	-.025	.023	.073	-.114
170	127	.004	.029	.114	-.098
170	128	.025	.035	.290	-.107
170	129	.066	.025	.219	-.011
170	130	-.036	.026	.134	-.107
170	131	-.003	.029	.240	-.096
170	132	.019	.030	.259	-.081
170	133	.057	.027	.191	-.030
170	134	-.103	.075	.249	-.370
170	135	.012	.035	.177	-.085
170	136	.047	.032	.206	-.051
170	137	-.073	.069	.127	-.371
170	138	.121	.067	.555	-.062
170	139	-.026	.062	.177	-.292
170	140	.051	.031	.221	-.051
170	141	.063	.059	.299	-.248
170	142	.030	.034	.188	-.099
170	143	.043	.029	.179	-.067
170	144	-.026	.023	.113	-.124
170	145	-.033	.015	.032	-.091
170	146	-.021	.020	.069	-.097
170	147	.021	.027	.129	-.096
170	148	.011	.034	.175	-.094
170	149	-.011	.023	.131	-.093
170	150	-.112	.100	.182	-.670
170	151	.121	.071	.438	-.085
170	152	.020	.028	.137	-.062
170	153	.022	.025	.116	-.071
170	154	.018	.039	.169	-.140
170	155	.034	.040	.223	-.094
170	156	.027	.035	.182	-.090
170	157	.048	.050	.245	-.110
170	158	-.239	.115	.190	-.820
170	159	-.215	.139	.233	-1.125
170	160	-.000	.053	.199	-.260
170	161	-.023	.098	.338	-.379
170	162	.281	.127	.814	-.121
170	163	.217	.122	.779	-.115
170	164	.049	.060	.255	-.256
170	165	.077	.034	.217	-.119
170	166	.076	.103	.486	-.247
170	167	-.069	.015	-.002	-.131
170	201	-.131	.021	-.059	-.288
170	202	-.133	.021	-.068	-.228
170	203	-.110	.018	-.054	-.198
170	204	-.147	.026	-.060	-.264
170	205	-.073	.028	-.026	-.200
170	206	-.226	.051	-.081	-.437
170	207	-.055	.019	-.015	-.129
170	208	-.083	.022	-.016	-.173
170	209	-.078	.027	.007	-.194
170	210	-.114	.028	-.019	-.230
170	211	-.125	.024	-.046	-.237
170	212	-.078	.029	.147	-.210
170	213	-.075	.022	.011	-.200
170	214	-.078	.019	-.012	-.148
170	301	.133	.091	.377	-.168
170	302	-.138	.156	.531	-.566
170	303	.034	.100	.473	-.436
170	304	.244	.120	.699	-.180
170	305	.250	.100	.658	-.078
170	306	.234	.105	.773	-.194
170	307	.139	.096	.554	-.146
170	308	.182	.110	.779	-.088
170	309	.306	.090	.654	.071
170	310	.204	.151	.747	-.368
170	311	.215	.139	.785	-.251
170	312	.212	.132	.729	-.219
170	313	.223	.089	.641	.008
170	314	.160	.114	.701	-.175
170	315	.116	.102	.598	-.174
170	316	.294	.106	.799	.022
170	317	.269	.088	.644	.025
170	318	.072	.038	.286	-.051
170	319	.050	.032	.167	-.033
170	320	.132	.151	.688	-.436
170	401	-.017	.028	.114	-.107
170	402	-.048	.029	.051	-.162
170	403	.254	.143	.849	-.254
170	404	.044	.062	.368	-.135
170	405	.091	.090	.569	-.222
170	406	.118	.084	.489	-.262
180	1	-.085	.042	.098	-.267
180	2	-.102	.022	-.035	-.220
180	3	-.143	.029	-.028	-.261
180	4	-.082	.023	.001	-.178
180	5	-.144	.028	-.041	-.260
180	6	-.150	.046	.056	-.424
180	7	-.225	.063	.090	-.530
180	8	-.170	.032	-.062	-.357
180	9	-.184	.060	.014	-.807
180	10	-.213	.040	-.061	-.419
180	11	-.237	.038	-.123	-.496
180	12	-.114	.052	.106	-.359
180	13	-.248	.080	.058	-.590
180	14	-.233	.048	-.100	-.506
180	15	-.027	.053	.316	-.164
180	16	-.134	.066	.059	-.436
180	17	-.210	.044	-.066	-.456
180	18	-.044	.033	.076	-.157
180	19	-.179	.038	-.045	-.365
180	20	-.258	.046	-.073	-.585
180	21	-.024	.037	.134	-.147
180	22	-.206	.043	-.081	-.373
180	23	-.067	.038	.102	-.188
180	24	-.138	.080	.220	-.487
180	25	-.100	.033	.047	-.249
180	26	-.284	.078	.008	-.590
180	27	-.184	.075	.146	-.549
180	28	-.125	.045	.097	-.487
180	29	.091	.044	.257	-.029
180	30	-.190	.058	.037	-.388
180	31	-.295	.064	.025	-.552
180	32	-.395	.079	-.162	-.825
180	33	-.399	.086	-.173	-.842
180	34	-.048	.076	.270	-.340
180	35	-.149	.070	.107	-.564
180	36	.059	.042	.250	-.078
180	37	-.070	.038	.067	-.244
180	38	-.175	.044	-.033	-.431
180	39	-.091	.029	.085	-.179
180	40	-.169	.034	-.080	-.352
180	41	-.062	.049	.125	-.323
180	42	-.196	.107	.186	-.515
180	43	-.248	.064	.032	-.569
180	44	.107	.052	.357	-.029
180	45	-.125	.031	-.039	-.260
180	46	-.039	.043	.229	-.184
180	47	-.168	.096	.168	-.501
180	48	.050	.067	.394	-.148

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
180	49	.070	.046	.278	-.083
180	50	-.345	.060	-.174	-.623
180	51	-.437	.092	-.154	-.881
180	52	-.029	.074	.329	-.341
180	53	.137	.062	.404	-.036
180	54	.024	.070	.284	-.229
180	55	-.103	.073	.439	-.113
180	56	-.020	.051	.236	-.313
180	57	-.128	.074	.211	-.535
180	101	-.082	.035	.044	-.246
180	102	-.151	.027	-.043	-.273
180	103	-.147	.036	-.006	-.297
180	104	-.062	.030	.086	-.161
180	105	-.114	.028	.023	-.232
180	106	-.081	.024	.003	-.171
180	107	-.098	.023	-.004	-.197
180	108	-.081	.022	.035	-.159
180	109	-.223	.034	-.119	-.407
180	110	-.108	.033	.039	-.254
180	111	-.024	.021	.059	-.113
180	112	-.042	.051	.162	-.216
180	113	-.136	.046	.157	-.316
180	114	-.016	.035	.119	-.128
180	115	.024	.061	.245	-.299
180	116	.049	.037	.190	-.078
180	117	.038	.068	.469	-.124
180	118	-.215	.060	.163	-.484
180	119	-.011	.051	.343	-.171
180	120	-.009	.041	.175	-.115
180	121	.000	.030	.129	-.079
180	122	.045	.058	.264	-.111
180	123	.068	.036	.254	-.053
180	124	.033	.050	.311	-.191
180	125	.054	.032	.225	-.055
180	126	.020	.033	.207	-.062
180	127	.049	.036	.199	-.057
180	128	.060	.050	.274	-.091
180	129	.103	.032	.231	.019
180	130	-.001	.041	.179	-.117
180	131	.031	.043	.270	-.079
180	132	.063	.045	.350	-.054
180	133	.094	.036	.262	-.011
180	134	-.011	.113	.376	-.365
180	135	.048	.048	.334	-.119
180	136	.078	.045	.252	-.082
180	137	-.023	.083	.225	-.453
180	138	.155	.072	.622	-.043
180	139	.030	.074	.292	-.389
180	140	.102	.041	.291	-.069
180	141	.139	.060	.406	-.147
180	142	.081	.047	.310	-.027
180	143	.090	.037	.256	.002
180	144	-.027	.036	.158	-.143
180	145	-.057	.022	.061	-.140
180	146	.018	.036	.231	-.071
180	147	.074	.037	.256	-.037
180	148	.050	.043	.291	-.071
180	149	-.014	.028	.105	-.112
180	150	-.037	.116	.326	-.703
180	151	.172	.071	.497	-.031
180	152	.064	.036	.208	-.052
180	153	.035	.032	.199	-.055
180	154	.080	.050	.343	-.078
180	155	.098	.053	.382	-.099
180	156	.073	.041	.258	-.054
180	157	.108	.060	.308	-.086
180	158	-.105	.136	.302	-.679
180	159	-.047	.171	.517	-.629
180	160	.070	.066	.372	-.183
180	161	.113	.122	.483	-.300
180	162	.286	.113	.791	-.111
180	163	.243	.106	.720	-.029
180	164	.113	.060	.381	-.239
180	165	.121	.040	.293	.006
180	166	.200	.101	.668	-.135
180	167	-.066	.023	.024	-.144
180	201	-.167	.027	-.082	-.318
180	202	-.170	.024	-.082	-.294
180	203	-.158	.020	-.092	-.247
180	204	-.178	.033	-.067	-.358
180	205	-.103	.036	.031	-.320
180	206	-.285	.055	-.108	-.498
180	207	-.097	.023	-.024	-.184
180	208	-.117	.026	-.032	-.209
180	209	-.121	.029	-.015	-.230
180	210	-.152	.033	.001	-.285
180	211	-.166	.032	-.051	-.306
180	212	-.101	.033	-.126	-.255
180	213	-.113	.027	-.015	-.234
180	214	-.100	.022	-.006	-.172
180	301	.016	.091	.487	-.291
180	302	-.093	.171	.545	-.639
180	303	.148	.113	.614	-.417
180	304	.205	.109	.907	-.174
180	305	.321	.108	.743	-.055
180	306	.229	.099	.745	-.019
180	307	.032	.080	.464	-.234
180	308	.241	.121	.800	-.073
180	309	.288	.086	.684	.050
180	310	.203	.137	.692	-.280
180	311	.193	.109	.731	-.172
180	312	.219	.096	.728	-.104
180	313	.240	.078	.684	.041
180	314	.203	.107	.696	-.212
180	315	.123	.093	.590	-.152
180	316	.249	.103	.707	-.006
180	317	.202	.074	.506	.013
180	318	.129	.044	.361	.010
180	319	.097	.034	.218	.003
180	320	.039	.132	.557	-.334
180	401	-.051	.039	.070	-.228
180	402	-.118	.033	-.002	-.273
180	403	.287	.128	.936	-.130
180	404	.043	.086	.405	-.252
180	405	.019	.069	.374	-.224
180	406	-.016	.091	.329	-.380
190	1	-.111	.047	.123	-.301
190	2	-.116	.021	-.039	-.189
190	3	-.109	.029	-.009	-.224
190	4	-.102	.023	.006	-.202
190	5	-.176	.029	-.071	-.312
190	6	-.150	.060	.119	-.468
190	7	-.247	.062	.005	-.468
190	8	-.229	.042	-.080	-.426
190	9	-.235	.075	.007	-.645
190	10	-.205	.045	-.057	-.402
190	11	-.254	.060	-.103	-.559
190	12	-.093	.067	.176	-.424
190	13	-.257	.064	.007	-.501
190	14	-.270	.055	-.112	-.562
190	15	-.061	.064	.295	-.176
190	16	-.247	.078	.063	-.546
190	17	-.310	.054	-.153	-.597
190	18	.050	.043	.265	-.082
190	19	-.193	.053	-.043	-.495
190	20	-.369	.055	-.202	-.622
190	21	.059	.053	.324	-.082
190	22	-.239	.049	.007	-.530
190	23	.033	.050	.231	-.114
190	24	-.159	.078	.167	-.479
190	25	-.119	.039	.002	-.335
190	26	-.380	.073	-.116	-.788
190	27	-.080	.078	.192	-.447
190	28	-.149	.064	.091	-.433
190	29	.142	.054	.353	-.027
190	30	-.198	.056	.023	-.438
190	31	-.276	.063	-.059	-.639
190	32	-.499	.095	-.225	-.862
190	33	-.481	.104	-.207	-.992
190	34	-.114	.065	.160	-.363

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
190	35	-.182	.078	.094	-.584
190	36	.099	.053	.317	-.055
190	37	-.153	.049	.032	-.365
190	38	-.215	.045	-.075	-.400
190	39	-.021	.039	.217	-.180
190	40	-.241	.043	-.096	-.430
190	41	-.164	.083	.116	-.574
190	42	-.309	.082	.096	-.585
190	43	-.154	.075	.160	-.438
190	44	.153	.065	.480	-.015
190	45	-.116	.042	.039	-.285
190	46	.017	.054	.210	-.226
190	47	-.252	.073	.121	-.623
190	48	.051	.058	.312	-.188
190	49	.144	.063	.440	-.023
190	50	-.281	.055	-.123	-.614
190	51	-.498	.098	-.210	-.894
190	52	-.086	.050	.157	-.313
190	53	.163	.067	.467	-.091
190	54	.047	.060	.265	-.116
190	55	.100	.062	.466	-.110
190	56	-.052	.039	.167	-.262
190	57	-.132	.078	.119	-.433
190	101	-.040	.033	.105	-.176
190	102	-.125	.026	-.039	-.246
190	103	-.171	.043	.056	-.318
190	104	-.054	.038	.237	-.160
190	105	-.069	.032	.105	-.173
190	106	-.019	.025	.130	-.105
190	107	-.111	.028	.063	-.223
190	108	-.076	.031	.105	-.171
190	109	-.204	.039	.007	-.356
190	110	-.039	.038	.285	-.171
190	111	-.012	.025	.130	-.094
190	112	-.001	.053	.226	-.217
190	113	-.078	.053	.117	-.288
190	114	.068	.037	.205	-.041
190	115	.076	.063	.335	-.244
190	116	.083	.038	.219	-.073
190	117	.131	.078	.498	-.055
190	118	-.224	.074	.194	-.482
190	119	.022	.082	.413	-.195
190	120	.044	.061	.357	-.126
190	121	.098	.052	.341	-.047
190	122	.128	.061	.365	-.071
190	123	.113	.046	.307	-.038
190	124	.066	.063	.341	-.112
190	125	.126	.045	.396	-.012
190	126	.090	.043	.290	-.020
190	127	.092	.044	.298	-.043
190	128	.095	.058	.350	-.096
190	129	.168	.036	.297	.073
190	130	.059	.046	.252	-.060
190	131	.068	.051	.303	-.068
190	132	.099	.056	.403	-.048
190	133	.159	.046	.352	.036
190	134	.099	.100	.499	-.311
190	135	.065	.059	.358	-.114
190	136	.144	.061	.416	-.055
190	137	.097	.089	.374	-.427
190	138	.217	.075	.510	-.069
190	139	.112	.085	.448	-.266
190	140	.155	.046	.348	-.055
190	141	.228	.072	.561	-.050
190	142	.161	.061	.439	-.008
190	143	.137	.044	.317	-.006
190	144	-.037	.052	.202	-.199
190	145	-.025	.041	.166	-.166
190	146	.089	.054	.370	-.073
190	147	.119	.047	.367	-.029
190	148	.097	.058	.435	-.067
190	149	.029	.040	.209	-.111
190	150	.089	.121	.610	-.576
190	151	.224	.081	.692	-.015
190	152	.102	.040	.305	-.003
190	153	.091	.044	.291	-.041
190	154	.159	.058	.405	.009
190	155	.160	.062	.423	.008
190	156	.123	.052	.348	-.019
190	157	.217	.062	.460	.003
190	158	.112	.112	.525	-.440
190	159	.190	.146	.738	-.566
190	160	.147	.063	.571	-.162
190	161	.274	.085	.583	-.287
190	162	.262	.096	.812	-.017
190	163	.189	.083	.605	-.045
190	164	.176	.068	.599	-.041
190	165	.199	.055	.534	.078
190	166	.279	.095	.895	.054
190	167	-.054	.035	.070	-.149
190	201	-.217	.040	-.073	-.471
190	202	-.219	.035	-.092	-.365
190	203	-.170	.031	-.072	-.304
190	204	-.195	.038	-.084	-.382
190	205	-.133	.034	-.033	-.354
190	206	-.362	.055	-.193	-.611
190	207	-.088	.024	.012	-.181
190	208	-.121	.026	-.015	-.231
190	209	-.158	.029	-.052	-.268
190	210	-.175	.039	-.019	-.315
190	211	-.156	.039	.014	-.304
190	212	-.101	.028	-.006	-.240
190	213	-.157	.028	-.077	-.301
190	214	-.110	.029	.052	-.242
190	301	-.093	.090	.475	-.548
190	302	.051	.148	.539	-.473
190	303	.218	.109	.688	-.218
190	304	.131	.082	.517	-.153
190	305	.356	.100	.853	-.168
190	306	.175	.068	.550	.003
190	307	-.054	.059	.218	-.250
190	308	.267	.117	.886	-.012
190	309	.252	.082	.686	.047
190	310	.105	.120	.559	-.251
190	311	.076	.095	.446	-.172
190	312	.195	.080	.510	-.135
190	313	.230	.068	.532	.058
190	314	.152	.078	.610	-.069
190	315	.035	.096	.448	-.289
190	316	.194	.097	.636	-.084
190	317	.152	.066	.448	-.011
190	318	.157	.049	.403	-.035
190	319	.104	.039	.261	-.014
190	320	-.081	.113	.582	-.373
190	401	-.151	.047	.001	-.335
190	402	-.209	.045	-.072	-.587
190	403	.250	.140	.760	-.378
190	404	-.042	.100	.381	-.389
190	405	-.040	.074	.240	-.300
190	406	-.137	.079	.180	-.568
200	1	-.139	.046	.051	-.314
200	2	-.189	.021	-.104	-.260
200	3	-.188	.033	-.077	-.327
200	4	-.116	.024	-.031	-.212
200	5	-.195	.028	-.110	-.304
200	6	-.223	.051	-.023	-.352
200	7	-.376	.057	-.177	-.650
200	8	-.270	.050	-.112	-.604
200	9	-.294	.092	.030	-.818
200	10	-.326	.062	-.164	-.624
200	11	-.430	.087	-.213	-.822
200	12	-.077	.072	.225	-.445
200	13	-.282	.060	-.061	-.525
200	14	-.435	.074	-.248	-.811
200	15	.068	.063	.396	-.179
200	16	-.335	.078	.045	-.692
200	17	-.386	.067	-.222	-.811
200	18	.050	.062	.327	-.090
200	19	-.331	.072	-.101	-.677
200	20	-.431	.064	-.258	-.773

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
200	21	-.093	.064	.425	-.075
200	22	-.359	.065	-.083	-.746
200	23	-.006	.067	.389	-.230
200	24	-.235	.093	.232	-.704
200	25	-.166	.066	.056	-.497
200	26	-.575	.087	-.320	-1.057
200	27	-.097	.100	.287	-.485
200	28	-.164	.069	.103	-.431
200	29	.182	.069	.501	-.002
200	30	-.321	.065	-.095	-.607
200	31	-.397	.067	-.179	-1.092
200	32	-.613	.130	-.306	-1.259
200	33	-.585	.132	-.286	-1.123
200	34	-.253	.053	-.061	-.533
200	35	-.336	.091	.030	-.825
200	36	.126	.057	.396	-.073
200	37	-.255	.052	-.057	-.497
200	38	-.366	.051	-.135	-.650
200	39	-.053	.052	.173	-.279
200	40	-.306	.053	-.128	-.542
200	41	-.289	.098	.150	-.827
200	42	-.477	.066	-.246	-.746
200	43	-.176	.098	.146	-.757
200	44	.202	.072	.537	-.017
200	45	-.126	.053	.033	-.454
200	46	-.071	.082	.166	-.588
200	47	-.428	.077	-.186	-.914
200	48	.007	.056	.218	-.198
200	49	.206	.082	.521	-.029
200	50	-.308	.061	-.068	-.732
200	51	-.512	.101	-.087	-.971
200	52	-.133	.047	.128	-.309
200	53	.111	.080	.418	-.185
200	54	-.064	.051	.214	-.193
200	55	-.027	.067	.304	-.276
200	56	-.089	.039	.068	-.288
200	57	-.091	.078	.191	-.394
200	101	-.092	.039	.061	-.222
200	102	-.216	.030	-.109	-.317
200	103	-.165	.063	.098	-.369
200	104	-.034	.053	.308	-.201
200	105	-.107	.042	.176	-.289
200	106	-.063	.032	.178	-.150
200	107	-.100	.038	.209	-.205
200	108	-.067	.040	.088	-.190
200	109	-.276	.050	-.049	-.437
200	110	-.079	.053	.170	-.228
200	111	.002	.033	.133	-.094
200	112	.025	.058	.310	-.146
200	113	-.108	.052	.181	-.322
200	114	.032	.042	.287	-.096
200	115	.070	.082	.433	-.299
200	116	.091	.043	.285	-.034
200	117	.138	.084	.526	-.095
200	118	-.349	.094	.217	-.698
200	119	.096	.097	.537	-.216
200	120	.126	.084	.445	-.065
200	121	.166	.061	.412	-.006
200	122	.160	.051	.388	-.040
200	123	.146	.046	.342	-.004
200	124	.091	.080	.459	-.145
200	125	.158	.057	.499	-.012
200	126	.139	.058	.551	-.002
200	127	.144	.054	.579	-.038
200	128	.133	.074	.470	-.170
200	129	.205	.043	.408	.094
200	130	.107	.062	.410	-.073
200	131	.116	.067	.439	-.073
200	132	.143	.061	.489	-.012
200	133	.191	.045	.365	.036
200	134	.138	.109	.517	-.371
200	135	.085	.069	.393	-.122
200	136	.170	.056	.410	-.003
200	137	.151	.085	.459	-.404
200	138	.246	.086	.636	-.067
200	139	.169	.085	.505	-.166
200	140	.170	.052	.401	.045
200	141	.217	.078	.576	.036
200	142	.181	.071	.513	.018
200	143	.150	.050	.377	.027
200	144	-.059	.064	.298	-.253
200	145	-.015	.061	.234	-.184
200	146	.138	.068	.430	-.033
200	147	.150	.054	.384	-.017
200	148	.143	.070	.468	-.046
200	149	.052	.054	.399	-.095
200	150	.189	.115	.609	-.329
200	151	.261	.088	.674	.017
200	152	.149	.050	.332	-.010
200	153	.113	.058	.343	-.037
200	154	.220	.077	.551	.047
200	155	.228	.083	.609	.017
200	156	.163	.057	.440	.016
200	157	.265	.066	.612	.110
200	158	.206	.098	.645	-.208
200	159	.280	.115	.737	-.180
200	160	.202	.077	.528	.027
200	161	.281	.078	.601	.083
200	162	.235	.087	.690	-.020
200	163	.149	.077	.549	-.075
200	164	.230	.086	.596	.045
200	165	.244	.073	.630	.063
200	166	.276	.098	.694	-.026
200	167	.033	.045	.189	-.169
200	168	.278	.067	.075	-.716
200	169	.271	.047	.102	-.487
200	170	.226	.040	.110	-.397
200	171	.243	.047	.120	-.445
200	172	.155	.034	.043	-.338
200	173	.392	.059	.247	-.703
200	174	.115	.025	.024	-.230
200	175	.149	.026	.058	-.246
200	176	.207	.038	.106	-.431
200	177	.271	.049	.032	-.343
200	178	.183	.051	.076	-.366
200	179	.183	.027	.004	-.258
200	180	.137	.030	.103	-.230
200	181	.103	.042	.117	-.233
200	182	.224	.084	.092	-.553
200	183	.272	.180	.499	-.553
200	184	.205	.113	.681	-.145
200	185	.205	.067	.365	-.145
200	186	.244	.148	.765	-.317
200	187	.115	.059	.444	-.080
200	188	.135	.054	.101	-.301
200	189	.280	.112	.945	-.079
200	190	.225	.075	.519	-.010
200	191	.205	.096	.450	-.322
200	192	.205	.079	.356	-.354
200	193	.205	.095	.390	-.278
200	194	.205	.063	.401	-.046
200	195	.205	.056	.358	-.094
200	196	.205	.071	.363	-.345
200	197	.205	.086	.440	-.274
200	198	.205	.048	.304	-.053
200	199	.205	.068	.356	-.248
200	200	.205	.038	.216	-.026
200	201	.205	.064	.197	-.387
200	202	.205	.047	.075	-.457
200	203	.205	.084	.155	-.938
200	204	.205	.169	.913	-.696
200	205	.205	.098	.322	-.562
200	206	.205	.085	.176	-.588
200	207	.205	.047	.176	-.353
200	208	.205	.027	.011	-.345
200	209	.205	.038	.068	-.311
200	210	.205	.027	.010	-.384
200	211	.205	.028	.135	-.396
200	212	.205	.033	.011	-.489
200	213	.205	.040	.135	-.145
200	214	.205	.042	.117	-.315
200	301	.205	.084	.092	-.080
200	302	.205	.180	.499	-.301
200	303	.205	.113	.681	-.079
200	304	.205	.067	.365	-.010
200	305	.205	.148	.765	-.322
200	306	.205	.059	.444	-.354
200	307	.205	.054	.101	-.278
200	308	.205	.112	.945	-.046
200	309	.205	.075	.519	-.094
200	310	.205	.096	.450	-.345
200	311	.205	.079	.356	-.274
200	312	.205	.095	.390	-.053
200	313	.205	.063	.401	-.248
200	314	.205	.056	.358	-.026
200	315	.205	.071	.363	-.387
200	316	.205	.086	.440	-.457
200	317	.205	.048	.304	-.938
200	318	.205	.068	.356	-.696
200	319	.205	.038	.216	-.562
200	320	.205	.064	.197	-.588
200	401	.205	.047	.075	-.353
200	402	.205	.084	.155	-.345
200	403	.205	.169	.913	-.311
200	404	.205	.098	.322	-.384
200	405	.205	.085	.176	-.396
200	406	.205	.047	.176	-.489
200	1	.205	.027	.011	-.145
200	2	.205	.028	.135	-.315
200	3	.205	.033	.011	-.080
200	4	.205	.040	.135	-.301
200	5	.205	.042	.117	-.079
200	6	.205	.084	.092	-.010

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
210	7	-.445	.071	-.254	-.751
210	8	-.322	.063	-.031	-.614
210	9	-.345	.099	-.022	-.801
210	10	-.413	.086	-.204	-.835
210	11	-.518	.106	-.278	-1.049
210	12	-.053	.094	.384	-.458
210	13	-.334	.078	-.055	-.676
210	14	-.570	.097	-.340	-1.004
210	15	-.117	.074	.497	-.122
210	16	-.417	.098	.129	-.827
210	17	-.472	.082	-.283	-1.102
210	18	-.132	.077	.528	-.110
210	19	-.433	.086	-.178	-.795
210	20	-.507	.076	-.275	-1.043
210	21	.143	.074	.505	-.041
210	22	-.437	.088	-.062	-.850
210	23	-.038	.076	.377	-.195
210	24	-.334	.093	.101	-.718
210	25	-.264	.089	.012	-.637
210	26	-.676	.094	-.405	-1.137
210	27	-.047	.106	.353	-.455
210	28	-.171	.064	.059	-.507
210	29	.223	.080	.546	.017
210	30	-.371	.069	-.156	-.806
210	31	-.451	.076	-.171	-.770
210	32	-.745	.146	-.205	-1.343
210	33	-.746	.144	-.336	-1.248
210	34	-.333	.051	-.125	-.535
210	35	-.460	.096	-.117	-1.000
210	36	.152	.068	.440	-.045
210	37	-.335	.054	-.138	-.658
210	38	-.448	.056	-.284	-.714
210	39	-.041	.058	.174	-.308
210	40	-.356	.057	-.166	-.591
210	41	-.382	.097	.116	-.723
210	42	-.528	.063	-.323	-.854
210	43	-.108	.106	.294	-.526
210	44	.234	.081	.570	-.017
210	45	-.238	.097	.001	-.656
210	46	-.264	.141	.083	-.806
210	47	-.523	.084	-.234	-1.039
210	48	-.020	.060	.259	-.247
210	49	.240	.084	.579	.054
210	50	-.292	.042	-.154	-.487
210	51	-.488	.122	-.051	-.935
210	52	-.185	.037	-.029	-.326
210	53	-.031	.088	.268	-.379
210	54	-.140	.032	.066	-.260
210	55	-.140	.057	.098	-.396
210	56	-.125	.039	.050	-.333

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
210	57	-.072	.056	.113	-.409
210	101	-.129	.046	.078	-.308
210	102	-.249	.034	-.122	-.389
210	103	-.152	.072	.113	-.458
210	104	-.001	.070	.443	-.218
210	105	-.088	.054	.144	-.274
210	106	-.047	.041	.135	-.171
210	107	-.080	.051	.254	-.231
210	108	-.051	.050	.120	-.202
210	109	-.280	.072	.025	-.531
210	110	-.054	.071	.289	-.242
210	111	.019	.042	.178	-.094
210	112	.062	.074	.355	-.225
210	113	-.089	.066	.231	-.378
210	114	.053	.049	.267	-.078
210	115	.092	.098	.512	-.389
210	116	.100	.043	.288	-.011
210	117	.151	.080	.499	-.081
210	118	-.401	.111	.262	-.807
210	119	.127	.082	.470	-.187
210	120	.193	.082	.595	-.065
210	121	.206	.061	.474	-.006
210	122	.182	.052	.436	-.011
210	123	.177	.051	.381	-.015
210	124	.121	.087	.497	-.124
210	125	.180	.068	.642	.028
210	126	.177	.070	.581	.000
210	127	.169	.056	.436	-.017
210	128	.159	.095	.595	-.140
210	129	.225	.052	.412	.101
210	130	.156	.078	.577	-.035
210	131	.160	.083	.490	-.117
210	132	.193	.080	.586	-.012
210	133	.223	.058	.497	.054
210	134	.147	.134	.659	-.390
210	135	.118	.084	.603	-.105
210	136	.157	.055	.375	-.014
210	137	.208	.091	.602	-.158
210	138	.275	.091	.668	-.082
210	139	.226	.094	.707	-.152
210	140	.200	.058	.465	.057
210	141	.224	.090	.575	-.024
210	142	.232	.086	.597	.007
210	143	.185	.059	.485	-.045
210	144	-.071	.069	.286	-.287
210	145	.035	.088	.356	-.245
210	146	.196	.076	.541	.003
210	147	.178	.056	.441	-.038
210	148	.178	.082	.522	-.021
210	149	.074	.066	.381	-.095

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
210	150	.254	.111	.659	-.323
210	151	.288	.097	.749	-.041
210	152	.188	.061	.506	.045
210	153	.128	.065	.399	-.057
210	154	.260	.082	.624	.016
210	155	.276	.086	.652	.071
210	156	.204	.070	.527	-.005
210	157	.310	.087	.727	.101
210	158	.227	.102	.633	-.138
210	159	.233	.117	.772	-.055
210	160	.244	.088	.680	.006
210	161	.252	.089	.629	-.015
210	162	.182	.093	.673	-.140
210	163	.052	.083	.494	-.224
210	164	.247	.084	.570	.009
210	165	.258	.072	.624	.063
210	166	.209	.103	.695	-.172
210	167	-.006	.050	.162	-.144
210	201	-.331	.087	.020	-.895
210	202	-.331	.059	-.117	-.603
210	203	-.293	.048	-.153	-.486
210	204	-.301	.052	-.145	-.542
210	205	-.188	.035	-.068	-.339
210	206	-.399	.062	-.194	-.638
210	207	-.147	.024	-.048	-.234
210	208	-.182	.028	-.058	-.288
210	209	-.300	.053	-.175	-.525
210	210	-.159	.061	.071	-.372
210	211	-.163	.069	.101	-.363
210	212	-.156	.027	-.078	-.261
210	213	-.233	.035	-.145	-.372
210	214	-.082	.052	.153	-.232
210	301	-.342	.080	-.100	-.723
210	302	-.261	.123	.358	-.674
210	303	.088	.127	.606	-.490
210	304	-.007	.065	.263	-.324
210	305	-.049	.175	.600	-.555
210	306	.032	.060	.286	-.373
210	307	-.204	.040	.010	-.360
210	308	.289	.111	.793	-.051
210	309	.138	.071	.474	-.102
210	310	-.036	.071	.239	-.344
210	311	-.138	.059	.108	-.321
210	312	-.044	.111	.300	-.408
210	313	.074	.070	.361	-.140
210	314	.029	.059	.275	-.172
210	315	-.162	.052	.089	-.360
210	316	-.083	.087	.231	-.387
210	317	-.010	.037	.155	-.096
210	318	.041	.142	.415	-.402

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
210	319	-.039	.049	.193	-.227
210	320	-.226	.044	-.011	-.368
210	401	-.334	.063	-.119	-.669
210	402	-.478	.142	-.248	-1.130
210	403	-.042	.241	.628	-.946
210	404	-.325	.099	.072	-.767
210	405	-.214	.098	.137	-.674
210	406	-.297	.059	-.043	-.588
220	1	-.214	.052	-.048	-.431
220	2	-.208	.025	-.132	-.303
220	3	-.132	.037	.023	-.299
220	4	-.137	.035	.028	-.293
220	5	-.248	.037	-.132	-.388
220	6	-.233	.037	-.082	-.399
220	7	-.417	.081	-.201	-.753
220	8	-.361	.075	.017	-.725
220	9	-.381	.089	-.107	-.804
220	10	-.431	.107	-.153	-.996
220	11	-.484	.104	-.224	-.992
220	12	-.021	.104	.497	-.413
220	13	-.348	.077	-.043	-.652
220	14	-.552	.089	-.321	-.973
220	15	-.172	.076	.529	-.052
220	16	-.448	.105	.070	-1.037
220	17	-.517	.091	-.302	-1.122
220	18	.198	.074	.595	-.077
220	19	-.388	.088	-.048	-.730
220	20	-.547	.090	-.332	-1.030
220	21	.179	.076	.606	-.025
220	22	-.424	.086	.094	-.750
220	23	.117	.083	.475	-.173
220	24	-.385	.085	.025	-.773
220	25	-.331	.097	-.034	-.729
220	26	-.671	.098	-.401	-1.126
220	27	.086	.113	.625	-.347
220	28	-.198	.091	.113	-.656
220	29	.231	.080	.559	.036
220	30	-.327	.074	-.086	-.688
220	31	-.377	.080	-.098	-.744
220	32	-.736	.136	-.123	-1.209
220	33	-.823	.144	-.406	-1.358
220	34	-.328	.068	-.096	-.631
220	35	-.461	.100	-.176	-.899
220	36	.171	.074	.506	-.013
220	37	-.374	.069	-.064	-.731
220	38	-.434	.070	-.285	-.839
220	39	.028	.067	.319	-.210
220	40	-.393	.072	-.144	-.876
220	41	-.439	.087	-.089	-.967
220	42	-.478	.066	-.296	-.784
220	43	.009	.107	.349	-.347
220	44	.255	.089	.696	.019
220	45	-.356	.098	.048	-.756
220	46	-.400	.119	.144	-.861
220	47	-.484	.081	-.244	-.867
220	48	-.012	.075	.285	-.321
220	49	.256	.089	.679	.016
220	50	-.241	.035	-.116	-.456
220	51	-.378	.132	-.123	-.964
220	52	-.220	.035	-.110	-.358
220	53	-.163	.087	.136	-.497
220	54	-.139	.027	-.043	-.267
220	55	-.143	.051	.057	-.358
220	56	-.141	.040	-.020	-.302
220	57	-.109	.050	.089	-.347
220	101	-.090	.056	.160	-.262
220	102	-.219	.044	-.059	-.406
220	103	-.110	.088	.239	-.401
220	104	.038	.086	.359	-.202
220	105	-.017	.061	.228	-.214
220	106	.034	.043	.192	-.084
220	107	-.054	.062	.235	-.229
220	108	-.009	.065	.263	-.223
220	109	-.185	.090	.242	-.472
220	110	.047	.080	.436	-.210
220	111	.049	.051	.258	-.093
220	112	.084	.087	.484	-.204
220	113	-.032	.075	.476	-.296
220	114	.123	.053	.365	-.073
220	115	.106	.113	.591	-.390
220	116	.126	.050	.334	-.007
220	117	.217	.089	.663	-.061
220	118	-.353	.123	.308	-.805
220	119	.158	.097	.602	-.144
220	120	.204	.084	.568	-.014
220	121	.204	.068	.456	.014
220	122	.181	.052	.410	.036
220	123	.179	.053	.436	.038
220	124	.181	.100	.722	-.136
220	125	.242	.085	.767	.023
220	126	.237	.082	.790	.021
220	127	.200	.065	.656	.057
220	128	.195	.108	.630	-.129
220	129	.234	.055	.451	.093
220	130	.208	.095	.604	-.006
220	131	.206	.099	.633	-.217
220	132	.215	.080	.568	.020
220	133	.222	.052	.418	.066
220	134	.159	.141	.636	-.445
220	135	.151	.087	.617	-.133
220	136	.126	.060	.371	-.065
220	137	.233	.093	.636	-.121
220	138	.279	.097	.700	.007
220	139	.254	.096	.696	-.087
220	140	.206	.065	.481	.032
220	141	.201	.094	.602	-.119
220	142	.254	.091	.682	.032
220	143	.194	.063	.480	.029
220	144	-.063	.073	.348	-.303
220	145	.091	.097	.454	-.213
220	146	.234	.080	.575	-.026
220	147	.187	.058	.441	-.029
220	148	.221	.096	.660	-.051
220	149	.112	.081	.512	-.121
220	150	.302	.108	.750	-.199
220	151	.289	.108	.737	-.045
220	152	.205	.062	.440	.057
220	153	.133	.073	.418	-.076
220	154	.281	.089	.642	.074
220	155	.302	.096	.723	.071
220	156	.208	.072	.545	.011
220	157	.324	.091	.722	.077
220	158	.168	.110	.593	-.243
220	159	.141	.107	.640	-.217
220	160	.239	.085	.589	.018
220	161	.158	.090	.591	-.101
220	162	.078	.121	.535	-.471
220	163	-.079	.087	.304	-.399
220	164	.265	.097	.641	.050
220	165	.278	.084	.677	.035
220	166	.075	.106	.488	-.317
220	167	.022	.066	.282	-.167
220	201	-.378	.102	-.045	-1.004
220	202	-.384	.073	-.168	-.716
220	203	-.356	.059	-.200	-.621
220	204	-.357	.063	-.178	-.682
220	205	-.244	.038	-.124	-.416
220	206	-.365	.074	-.136	-.616
220	207	-.195	.032	-.067	-.337
220	208	-.223	.038	-.033	-.382
220	209	-.389	.057	-.207	-.626
220	210	-.132	.069	.144	-.379
220	211	-.136	.087	.201	-.414
220	212	-.213	.033	-.123	-.328
220	213	-.307	.045	-.182	-.480
220	214	-.051	.068	.247	-.246
220	301	-.433	.073	-.213	-.918
220	302	-.351	.103	.038	-.722
220	303	-.112	.153	.492	-.825
220	304	-.117	.089	.217	-.457

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
220	305	-.250	.104	.228	-.655
220	306	-.080	.098	.188	-.552
220	307	-.230	.035	-.089	-.360
220	308	-.286	.115	.926	-.046
220	309	-.004	.089	.298	-.357
220	310	-.056	.064	.287	-.382
220	311	-.217	.049	-.013	-.395
220	312	-.211	.096	.252	-.649
220	313	-.063	.070	.296	-.287
220	314	-.055	.055	.258	-.232
220	315	-.215	.045	-.064	-.388
220	316	-.205	.071	.017	-.518
220	317	-.071	.027	.063	-.173
220	318	-.118	.139	.301	-.520
220	319	-.017	.048	.150	-.308
220	320	-.239	.043	-.086	-.457
220	401	-.405	.077	-.095	-.757
220	402	-.538	.150	-.293	-1.201
220	403	-.226	.289	.618	-1.288
220	404	-.420	.104	-.052	-1.005
220	405	-.313	.111	.170	-.931
220	406	-.355	.076	.035	-.765
230	1	-.261	.065	-.086	-.577
230	2	-.262	.027	-.174	-.365
230	3	-.119	.037	.023	-.295
230	4	-.118	.042	.042	-.245
230	5	-.229	.043	-.095	-.425
230	6	-.269	.044	-.122	-.480
230	7	-.500	.093	-.265	-.849
230	8	-.374	.086	-.096	-.723
230	9	-.458	.090	-.175	-.852
230	10	-.560	.131	-.255	-1.137
230	11	-.590	.116	-.304	-1.103
230	12	.027	.121	.419	-.452
230	13	-.368	.074	-.066	-.682
230	14	-.637	.101	-.370	-1.118
230	15	.200	.086	.551	-.018
230	16	-.476	.124	.106	-.957
230	17	-.557	.096	-.273	-1.216
230	18	.189	.080	.616	-.018
230	19	-.401	.097	-.073	-.808
230	20	-.574	.094	-.296	-1.028
230	21	.215	.085	.580	.002
230	22	-.467	.084	-.117	-.845
230	23	.137	.090	.577	-.172
230	24	-.430	.082	-.162	-.865
230	25	-.392	.097	-.018	-.834
230	26	-.715	.101	-.452	-1.222
230	27	.130	.110	.545	-.279
230	28	-.311	.126	.076	-.863
230	29	-.262	.091	.714	.034
230	30	-.372	.087	-.103	-.868
230	31	-.418	.103	.046	-.862
230	32	-.743	.141	-.302	-1.380
230	33	-.827	.137	-.461	-1.514
230	34	-.432	.082	-.115	-.802
230	35	-.516	.102	-.208	-1.153
230	36	.198	.082	.584	-.045
230	37	-.425	.079	-.077	-.743
230	38	-.517	.083	-.312	-1.001
230	39	.021	.080	.325	-.389
230	40	-.425	.085	-.066	-.787
230	41	-.488	.084	-.200	-.850
230	42	-.517	.063	-.351	-.765
230	43	.052	.100	.403	-.302
230	44	.268	.084	.634	.037
230	45	-.437	.084	-.045	-.761
230	46	-.509	.096	.058	-.880
230	47	-.532	.079	-.286	-1.018
230	48	-.171	.123	.237	-.642
230	49	.265	.103	.720	.032
230	50	-.254	.036	-.128	-.526
230	51	-.366	.113	-.109	-.924
230	52	-.238	.046	-.041	-.452
230	53	-.306	.083	-.018	-.804
230	54	-.195	.025	-.117	-.315
230	55	-.203	.053	-.046	-.471
230	56	-.155	.032	-.075	-.392
230	57	-.176	.049	-.005	-.391
230	101	-.072	.069	.319	-.335
230	102	-.251	.062	-.016	-.490
230	103	-.062	.095	.364	-.491
230	104	.098	.097	.575	-.186
230	105	.021	.066	.278	-.181
230	106	.063	.048	.270	-.071
230	107	.002	.073	.364	-.192
230	108	-.053	.076	.336	-.164
230	109	-.115	.118	.292	-.468
230	110	.106	.099	.641	-.140
230	111	.091	.058	.320	-.057
230	112	.143	.111	.657	-.300
230	113	.031	.112	.464	-.326
230	114	.174	.068	.590	.016
230	115	.191	.114	.653	-.401
230	116	.171	.060	.427	.023
230	117	.230	.099	.584	-.027
230	118	-.354	.146	.323	-.794
230	119	.194	.118	.669	-.123
230	120	.234	.097	.808	-.012
230	121	.222	.081	.690	.019
230	122	.200	.058	.465	.016
230	123	.201	.058	.508	.054
230	124	.190	.103	.616	-.099
230	125	.253	.091	.606	.019
230	126	.247	.090	.634	-.111
230	127	.200	.065	.448	.022
230	128	.206	.110	.760	-.122
230	129	.219	.053	.473	.058
230	130	.236	.096	.659	.000
230	131	.218	.101	.723	-.098
230	132	.221	.092	.637	-.055
230	133	.202	.057	.432	.039
230	134	.140	.153	.771	-.468
230	135	.161	.094	.610	-.070
230	136	.088	.063	.338	-.087
230	137	.264	.093	.604	-.185
230	138	.293	.096	.744	-.027
230	139	.286	.096	.727	-.034
230	140	.190	.066	.513	.018
230	141	.172	.093	.559	-.101
230	142	.262	.089	.659	.043
230	143	.192	.061	.469	.017
230	144	-.031	.089	.374	-.307
230	145	.163	.113	.634	-.224
230	146	.277	.096	.791	-.080
230	147	.196	.068	.653	.033
230	148	.217	.094	.653	-.122
230	149	.114	.078	.502	-.076
230	150	.304	.101	.704	-.049
230	151	.269	.112	.690	-.043
230	152	.208	.066	.443	.013
230	153	.127	.077	.486	-.115
230	154	.280	.091	.717	.063
230	155	.302	.098	.808	.079
230	156	.203	.075	.573	.006
230	157	.319	.087	.695	.105
230	158	.098	.103	.563	-.283
230	159	.082	.093	.441	-.250
230	160	.224	.084	.669	-.014
230	161	.042	.078	.570	-.181
230	162	-.124	.167	.440	-.723
230	163	-.228	.092	.165	-.582
230	164	.261	.095	.641	.020
230	165	.275	.085	.706	.046
230	166	-.079	.112	.313	-.578
230	167	.073	.068	.436	-.120
230	201	-.436	.136	-.061	-1.145
230	202	-.412	.080	-.138	-.807
230	203	-.408	.063	-.224	-.718
230	204	-.402	.076	-.194	-.986

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
230	205	-.283	.040	-.133	-.455
230	206	-.270	.087	.082	-.676
230	207	-.243	.041	-.119	-.380
230	208	-.242	.062	.058	-.406
230	209	-.415	.066	-.209	-.667
230	210	-.099	.079	.271	-.393
230	211	-.102	.107	.366	-.430
230	212	-.284	.047	-.162	-.558
230	213	-.362	.052	-.181	-.621
230	214	-.005	.066	.265	-.236
230	301	-.477	.072	-.298	-.936
230	302	-.376	.106	-.024	-.792
230	303	-.298	.146	.285	-.808
230	304	-.255	.102	.052	-.629
230	305	-.337	.072	.128	-.611
230	306	-.260	.147	.054	-.846
230	307	-.246	.034	-.105	-.423
230	308	.288	.118	1.037	-.080
230	309	-.191	.104	.119	-.571
230	310	-.098	.107	.248	-.616
230	311	-.255	.048	-.040	-.448
230	312	-.328	.080	-.062	-.640
230	313	-.187	.068	.035	-.480
230	314	-.135	.067	.125	-.468
230	315	-.233	.041	-.017	-.393
230	316	-.330	.073	-.156	-.699
230	317	-.130	.020	-.062	-.230
230	318	-.227	.099	.211	-.534
230	319	-.082	.062	.095	-.398
230	320	-.263	.060	-.094	-.668
230	401	-.467	.084	-.185	-.854
230	402	-.530	.111	-.278	-1.255
230	403	-.429	.270	.360	-1.319
230	404	-.483	.106	-.208	-.962
230	405	-.427	.115	.074	-.985
230	406	-.439	.090	-.088	-.873
240	1	-.299	.073	-.142	-.594
240	2	-.313	.036	-.183	-.468
240	3	-.111	.042	.062	-.313
240	4	-.101	.048	.072	-.242
240	5	-.215	.047	-.002	-.397
240	6	-.267	.042	-.141	-.496
240	7	-.535	.093	-.278	-.930
240	8	-.345	.087	-.039	-.694
240	9	-.524	.110	-.258	-1.016
240	10	-.641	.135	-.290	-1.411
240	11	-.670	.131	-.304	-1.358
240	12	.075	.117	.497	-.422
240	13	-.365	.067	-.144	-.687
240	14	-.693	.108	-.271	-1.193
240	15	.206	.096	.631	-.060
240	16	-.473	.128	.077	-1.001
240	17	-.610	.101	-.354	-1.210
240	18	.209	.081	.668	.019
240	19	-.429	.107	-.034	-.859
240	20	-.606	.093	-.352	-1.232
240	21	.225	.089	.559	-.018
240	22	-.474	.097	-.058	-.901
240	23	.119	.100	.486	-.258
240	24	-.442	.084	-.175	-.856
240	25	-.388	.093	-.046	-.781
240	26	-.733	.112	-.443	-1.388
240	27	.148	.100	.520	-.193
240	28	-.404	.120	.111	-.846
240	29	.259	.097	.621	.021
240	30	-.392	.089	-.095	-.901
240	31	-.433	.112	-.069	-.925
240	32	-.707	.135	-.302	-1.206
240	33	-.740	.148	-.326	-1.400
240	34	-.475	.097	-.016	-1.085
240	35	-.557	.111	-.131	-1.040
240	36	.205	.081	.596	-.025
240	37	-.446	.089	-.137	-.817
240	38	-.599	.100	-.345	-.989
240	39	-.008	.092	.276	-.458
240	40	-.416	.100	-.057	-.856
240	41	-.513	.091	-.071	-.950
240	42	-.558	.071	-.368	-.864
240	43	.071	.094	.527	-.368
240	44	.255	.090	.698	.040
240	45	-.451	.091	-.036	-.833
240	46	-.542	.104	-.079	-1.135
240	47	-.550	.085	-.343	-.997
240	48	-.360	.115	.028	-.816
240	49	.247	.088	.596	.018
240	50	-.248	.046	-.074	-.487
240	51	-.481	.107	-.204	-.974
240	52	-.235	.066	.049	-.500
240	53	-.384	.085	-.068	-.827
240	54	-.234	.030	-.157	-.410
240	55	-.233	.048	-.099	-.603
240	56	-.170	.023	-.096	-.311
240	57	-.221	.045	-.080	-.450
240	101	-.037	.083	.399	-.278
240	102	-.269	.084	.101	-.543
240	103	.002	.100	.531	-.399
240	104	.139	.105	.562	-.196
240	105	.047	.068	.332	-.167
240	106	.083	.050	.295	-.051
240	107	.049	.078	.377	-.172
240	108	.116	.093	.528	-.155
240	109	-.036	.138	.450	-.419
240	110	.160	.110	.700	-.159
240	111	.126	.063	.381	-.076
240	112	.127	.109	.557	-.169
240	113	.016	.111	.447	-.345
240	114	.162	.067	.430	.009
240	115	.183	.110	.605	-.410
240	116	.169	.058	.429	.021
240	117	.227	.098	.647	-.025
240	118	-.351	.148	.357	-.799
240	119	.191	.124	.672	-.179
240	120	.225	.095	.653	-.000
240	121	.211	.083	.579	-.015
240	122	.192	.055	.420	.036
240	123	.194	.057	.453	.073
240	124	.194	.104	.680	-.080
240	125	.253	.092	.613	.001
240	126	.249	.090	.664	.021
240	127	.199	.059	.476	.010
240	128	.200	.108	.708	-.158
240	129	.200	.053	.453	.076
240	130	.249	.094	.648	-.002
240	131	.219	.106	.667	-.308
240	132	.250	.104	.776	-.197
240	133	.206	.060	.465	.051
240	134	.169	.160	.767	-.468
240	135	.196	.106	.706	-.093
240	136	.042	.063	.313	-.124
240	137	.244	.107	.657	-.125
240	138	.260	.113	.693	-.026
240	139	.262	.109	.709	-.036
240	140	.159	.063	.491	-.010
240	141	.121	.092	.565	-.193
240	142	.246	.092	.637	.025
240	143	.171	.063	.573	-.024
240	144	-.021	.095	.404	-.288
240	145	.200	.112	.609	-.161
240	146	.284	.101	.682	-.262
240	147	.186	.067	.437	-.013
240	148	.224	.100	.710	-.115
240	149	.108	.079	.460	-.116
240	150	.300	.101	.738	-.078
240	151	.239	.112	.727	-.075
240	152	.196	.066	.473	.029
240	153	.120	.079	.456	-.077
240	154	.272	.096	.738	.061
240	155	.292	.099	.750	.059
240	156	.175	.069	.509	-.014
240	157	.275	.097	.757	-.031

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
240	158	.007	.094	.350	-.385
240	159	.004	.083	.324	-.356
240	160	.208	.085	.610	-.058
240	161	-.062	.063	.188	-.267
240	162	-.351	.137	.173	-.898
240	163	-.375	.088	-.144	-.757
240	164	.210	.091	.671	-.039
240	165	.238	.083	.597	.028
240	166	-.246	.109	.119	-.694
240	167	.104	.063	.354	-.070
240	201	-.454	.155	.024	-1.297
240	202	-.414	.088	-.101	-.798
240	203	-.454	.074	-.246	-.749
240	204	-.456	.107	-.239	-1.425
240	205	-.314	.054	-.087	-.548
240	206	-.164	.086	.134	-.468
240	207	-.276	.046	-.111	-.468
240	208	-.230	.083	.155	-.475
240	209	-.397	.071	-.140	-.755
240	210	-.051	.090	.363	-.350
240	211	-.027	.124	.405	-.481
240	212	-.416	.065	-.237	-.658
240	213	-.402	.062	-.190	-.621
240	214	.057	.080	.447	-.199
240	301	-.525	.082	-.308	-.929
240	302	-.284	.101	.032	-.795
240	303	-.452	.131	.123	-.877
240	304	-.391	.083	-.124	-.727
240	305	-.392	.058	-.223	-.705
240	306	-.460	.119	-.080	-.891
240	307	-.273	.047	-.093	-.490
240	308	.225	.110	.644	-.064
240	309	-.349	.085	-.036	-.628
240	310	-.214	.132	.151	-.712
240	311	-.249	.053	-.073	-.481
240	312	-.433	.070	-.240	-.832
240	313	-.338	.070	-.136	-.673
240	314	-.263	.095	.016	-.679
240	315	-.237	.052	.047	-.469
240	316	-.418	.076	-.243	-.774
240	317	-.171	.021	-.104	-.289
240	318	-.270	.072	.033	-.639
240	319	-.141	.079	.022	-.474
240	320	-.321	.087	-.089	-.786
240	401	-.489	.102	-.041	-.883
240	402	-.516	.083	-.304	-1.079
240	403	-.539	.216	.251	-1.290
240	404	-.496	.107	-.185	-1.218
240	405	-.479	.113	-.039	-.969
240	406	-.482	.097	-.090	-.863

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
250	1	-.243	.066	-.072	-.518
250	2	-.178	.031	-.066	-.288
250	3	-.009	.038	.147	-.153
250	4	-.017	.053	.185	-.205
250	5	-.101	.041	.060	-.262
250	6	-.146	.033	-.044	-.400
250	7	-.316	.076	-.064	-.636
250	8	-.187	.055	-.017	-.506
250	9	-.380	.096	-.135	-.887
250	10	-.428	.099	-.122	-.957
250	11	-.518	.130	-.195	-1.100
250	12	.049	.112	.511	-.336
250	13	-.235	.054	-.070	-.551
250	14	-.487	.100	-.140	-.997
250	15	.155	.089	.547	-.079
250	16	-.282	.114	.260	-.796
250	17	-.451	.099	-.222	-.939
250	18	.171	.082	.578	-.015
250	19	-.274	.089	.118	-.707
250	20	-.434	.101	-.186	-.966
250	21	.158	.089	.629	-.045
250	22	-.291	.074	.081	-.735
250	23	.079	.101	.502	-.267
250	24	-.321	.079	.090	-.669
250	25	-.243	.067	-.009	-.580
250	26	-.505	.096	-.051	-1.001
250	27	.098	.089	.535	-.249
250	28	-.253	.106	.189	-.642
250	29	.174	.090	.602	-.061
250	30	-.265	.070	-.044	-.594
250	31	-.266	.087	.037	-.658
250	32	-.464	.120	-.078	-1.108
250	33	-.472	.127	-.202	-1.344
250	34	-.273	.072	.016	-.579
250	35	-.421	.111	-.135	-1.040
250	36	.120	.074	.500	-.098
250	37	-.283	.080	-.027	-.666
250	38	-.434	.096	-.147	-.847
250	39	-.028	.096	.386	-.414
250	40	-.241	.096	.085	-.696
250	41	-.343	.116	.226	-.811
250	42	-.451	.082	-.259	-.782
250	43	.066	.093	.455	-.320
250	44	.181	.095	.613	-.089
250	45	-.275	.081	.009	-.632
250	46	-.330	.089	.188	-.711
250	47	-.389	.092	-.093	-.917
250	48	-.258	.091	.103	-.723
250	49	.161	.084	.656	-.103
250	50	-.202	.060	.010	-.482

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
250	51	-.366	.098	-.033	-.848
250	52	-.219	.073	.065	-.630
250	53	-.287	.074	.020	-.594
250	54	-.176	.040	-.011	-.409
250	55	-.167	.046	.046	-.376
250	56	-.139	.026	-.044	-.322
250	57	-.172	.048	-.016	-.464
250	101	.082	.102	.629	-.176
250	102	-.091	.092	.218	-.419
250	103	.065	.113	.613	-.365
250	104	.128	.104	.568	-.269
250	105	.090	.058	.365	-.096
250	106	.095	.053	.325	-.050
250	107	.093	.081	.468	-.121
250	108	.129	.084	.624	-.103
250	109	.052	.108	.490	-.277
250	110	.127	.093	.582	-.110
250	111	.100	.060	.439	-.039
250	112	.108	.098	.689	-.316
250	113	.064	.102	.497	-.228
250	114	.145	.065	.618	-.001
250	115	.151	.098	.744	-.497
250	116	.120	.058	.394	-.021
250	117	.163	.079	.618	-.013
250	118	-.097	.150	.526	-.698
250	119	.121	.104	.674	-.162
250	120	.156	.090	.699	-.066
250	121	.138	.072	.655	-.045
250	122	.093	.061	.405	-.066
250	123	.136	.061	.497	-.005
250	124	.124	.095	.572	-.104
250	125	.151	.074	.469	-.029
250	126	.115	.082	.462	-.176
250	127	.125	.057	.430	-.025
250	128	.134	.108	.651	-.438
250	129	.129	.053	.363	-.026
250	130	.141	.103	.638	-.153
250	131	.146	.109	.634	-.287
250	132	.160	.097	.669	-.138
250	133	.126	.059	.503	-.026
250	134	.071	.144	.687	-.519
250	135	.122	.100	.653	-.163
250	136	.023	.057	.231	-.166
250	137	.162	.085	.545	-.084
250	138	.140	.100	.642	-.136
250	139	.183	.094	.628	-.103
250	140	.106	.065	.388	-.086
250	141	.040	.078	.370	-.233
250	142	.123	.090	.497	-.129
250	143	.111	.062	.385	-.071

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
250	144	-.025	.087	.370	-.324
250	145	.138	.095	.607	-.210
250	146	.148	.108	.598	-.434
250	147	.124	.066	.511	-.106
250	148	.146	.100	.844	-.177
250	149	.060	.077	.448	-.139
250	150	.159	.097	.778	-.148
250	151	.142	.102	.648	-.115
250	152	.130	.061	.535	-.052
250	153	.050	.066	.416	-.187
250	154	.120	.087	.483	-.125
250	155	.178	.085	.550	-.080
250	156	.123	.069	.483	-.107
250	157	.119	.086	.574	-.111
250	158	-.113	.093	.349	-.451
250	159	-.061	.077	.279	-.385
250	160	.104	.069	.454	-.116
250	161	-.108	.044	.152	-.270
250	162	-.361	.074	-.066	-.648
250	163	-.293	.056	-.133	-.520
250	164	.125	.085	.506	-.095
250	165	.145	.074	.464	-.052
250	166	-.336	.093	.023	-.760
250	167	.114	.074	.398	-.088
250	201	-.263	.114	.057	-1.031
250	202	-.225	.073	.088	-.549
250	203	-.321	.069	-.125	-.694
250	204	-.490	.165	-.132	-1.501
250	205	-.232	.038	-.042	-.511
250	206	-.026	.092	.393	-.509
250	207	-.239	.058	.061	-.540
250	208	-.148	.104	.330	-.406
250	209	-.278	.073	-.012	-.745
250	210	.020	.097	.408	-.304
250	211	.040	.115	.565	-.325
250	212	-.405	.083	-.188	-.826
250	213	-.234	.072	.016	-.509
250	214	.099	.089	.517	-.120
250	301	-.409	.079	-.221	-.983
250	302	-.306	.089	.040	-.934
250	303	-.371	.089	-.028	-.802
250	304	-.316	.069	-.070	-.658
250	305	-.317	.050	-.189	-.556
250	306	-.424	.090	-.218	-.946
250	307	-.246	.048	-.080	-.532
250	308	.124	.097	.656	-.107
250	309	-.319	.057	-.157	-.538
250	310	-.319	.100	.082	-.732
250	311	-.212	.066	.041	-.532
250	312	-.329	.061	-.143	-.656
250	313	-.308	.048	-.176	-.490
250	314	-.329	.069	-.075	-.591
250	315	-.202	.052	.020	-.426
250	316	-.307	.070	-.147	-.653
250	317	-.131	.022	-.061	-.218
250	318	-.194	.064	.107	-.509
250	319	-.146	.073	.008	-.490
250	320	-.275	.082	-.048	-.752
250	401	-.326	.108	.116	-.894
250	402	-.387	.084	-.163	-.917
250	403	-.447	.167	.250	-1.229
250	404	-.409	.110	.014	-1.224
250	405	-.326	.099	.020	-.993
250	406	-.288	.076	.000	-.677
260	1	-.169	.063	.073	-.457
260	2	-.146	.047	.076	-.330
260	3	.000	.038	.165	-.157
260	4	-.007	.046	.237	-.164
260	5	-.088	.054	.147	-.343
260	6	-.099	.040	.032	-.388
260	7	-.285	.103	.001	-.875
260	8	-.133	.064	.214	-.356
260	9	-.337	.116	.020	-.828
260	10	-.368	.108	-.077	-1.058
260	11	-.517	.159	-.108	-1.316
260	12	-.129	.111	.586	-.288
260	13	-.223	.060	-.050	-.508
260	14	-.473	.107	-.064	-.914
260	15	-.187	.098	.580	-.077
260	16	-.228	.104	.149	-.703
260	17	-.412	.091	-.150	-.922
260	18	-.176	.071	.538	-.026
260	19	-.250	.073	.053	-.618
260	20	-.375	.088	-.094	-.809
260	21	-.153	.088	.606	-.045
260	22	-.249	.070	.078	-.594
260	23	-.032	.110	.478	-.549
260	24	-.299	.075	.013	-.612
260	25	-.211	.069	.038	-.519
260	26	-.464	.107	-.135	-1.001
260	27	.095	.095	.551	-.359
260	28	-.204	.100	.203	-.669
260	29	.141	.079	.489	-.081
260	30	-.246	.067	-.050	-.585
260	31	-.224	.076	.102	-.582
260	32	-.382	.107	-.046	-.993
260	33	-.391	.103	-.146	-.940
260	34	-.221	.058	-.002	-.459
260	35	-.399	.109	-.010	-.907
260	36	.092	.074	.491	-.191
260	37	-.234	.073	-.012	-.649
260	38	-.386	.090	-.117	-.854
260	39	-.073	.118	.404	-.542
260	40	-.183	.091	.128	-.533
260	41	-.230	.132	.378	-.821
260	42	-.442	.083	-.219	-.887
260	43	.046	.082	.368	-.307
260	44	.147	.085	.593	-.062
260	45	-.210	.074	.004	-.566
260	46	-.273	.078	.074	-.621
260	47	-.360	.084	-.117	-.810
260	48	-.253	.073	.049	-.569
260	49	.125	.078	.483	-.050
260	50	-.212	.055	.021	-.410
260	51	-.308	.086	-.046	-.757
260	52	-.234	.063	.128	-.508
260	53	-.254	.078	.029	-.665
260	54	-.189	.050	-.053	-.466
260	55	-.161	.050	.073	-.417
260	56	-.154	.044	.020	-.569
260	57	-.140	.050	.035	-.360
260	101	.071	.076	.509	-.110
260	102	-.105	.093	.390	-.462
260	103	.096	.105	.590	-.193
260	104	.157	.115	.731	-.191
260	105	.115	.065	.440	-.068
260	106	.116	.065	.437	-.061
260	107	.116	.086	.613	-.123
260	108	.171	.090	.548	-.047
260	109	.136	.100	.556	-.215
260	110	.186	.111	.710	-.128
260	111	.139	.069	.436	-.028
260	112	.155	.114	.711	-.177
260	113	.140	.117	.649	-.161
260	114	.169	.081	.587	-.057
260	115	.179	.102	.615	-.261
260	116	.169	.071	.501	-.012
260	117	.213	.086	.686	-.013
260	118	.052	.175	.697	-.475
260	119	.171	.109	.665	-.146
260	120	.161	.087	.643	-.065
260	121	.142	.073	.612	-.104
260	122	.101	.063	.499	-.075
260	123	.136	.060	.520	-.018
260	124	.127	.091	.508	-.124
260	125	.141	.071	.485	-.063
260	126	.107	.079	.517	-.112
260	127	.117	.057	.370	-.018
260	128	.113	.099	.616	-.126
260	129	.099	.049	.299	-.022

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
260	130	.145	.099	.603	-.112
260	131	.097	.121	.624	-.511
260	132	.121	.110	.686	-.517
260	133	.102	.058	.408	-.038
260	134	.067	.135	.631	-.427
260	135	.110	.092	.610	-.159
260	136	-.007	.047	.259	-.153
260	137	.119	.083	.567	-.224
260	138	.079	.094	.554	-.232
260	139	.137	.090	.629	-.277
260	140	.064	.064	.351	-.133
260	141	.003	.075	.356	-.217
260	142	.087	.088	.529	-.177
260	143	.079	.061	.368	-.134
260	144	-.024	.085	.364	-.306
260	145	.150	.094	.646	-.135
260	146	.109	.128	.675	-.699
260	147	.089	.063	.392	-.089
260	148	.107	.092	.531	-.124
260	149	.040	.074	.428	-.147
260	150	.110	.090	.636	-.123
260	151	.086	.091	.540	-.211
260	152	.106	.057	.364	-.049
260	153	.040	.064	.333	-.174
260	154	.099	.083	.550	-.119
260	155	.152	.083	.583	-.084
260	156	.095	.066	.391	-.128
260	157	.072	.066	.433	-.099
260	158	-.139	.077	.267	-.416
260	159	-.077	.062	.181	-.343
260	160	.078	.071	.492	-.166
260	161	-.117	.040	-.126	-.315
260	162	-.320	.066	-.140	-.625
260	163	-.261	.056	-.102	-.513
260	164	.078	.073	.416	-.146
260	165	.099	.065	.444	-.081
260	166	-.348	.066	-.086	-.680
260	167	.119	.076	.472	-.079
260	201	-.178	.117	.254	-.906
260	202	-.154	.076	.200	-.513
260	203	-.273	.068	.008	-.544
260	204	-.493	.207	.116	-1.404
260	205	-.199	.070	.295	-.516
260	206	-.037	.083	.324	-.532
260	207	-.211	.060	.010	-.485
260	208	-.125	.094	.283	-.439
260	209	-.231	.078	.070	-.629
260	210	.072	.094	.465	-.245
260	211	.136	.114	.567	-.308
260	212	-.379	.102	-.037	-.734

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
260	213	-.209	.089	.274	-.500
260	214	.168	.099	.686	-.085
260	301	-.379	.071	-.183	-.931
260	302	-.295	.076	-.051	-.764
260	303	-.316	.069	-.100	-.629
260	304	-.278	.069	-.027	-.742
260	305	-.269	.047	-.101	-.499
260	306	-.346	.080	-.135	-.801
260	307	-.243	.049	-.107	-.468
260	308	.082	.086	.506	-.189
260	309	-.275	.046	-.147	-.501
260	310	-.310	.067	-.079	-.632
260	311	-.224	.059	.052	-.588
260	312	-.259	.056	-.083	-.506
260	313	-.264	.049	-.115	-.531
260	314	-.302	.063	-.121	-.655
260	315	-.217	.053	-.028	-.477
260	316	-.267	.059	-.138	-.626
260	317	-.140	.023	-.068	-.246
260	318	-.171	.056	.005	-.457
260	319	-.152	.062	.039	-.532
260	320	-.257	.074	.003	-.809
260	401	-.264	.103	.118	-.795
260	402	-.355	.082	-.019	-.937
260	403	-.434	.133	.102	-1.107
260	404	-.388	.108	-.097	-1.193
260	405	-.284	.081	.059	-.803
260	406	-.255	.067	-.059	-.545
270	1	-.119	.071	.201	-.518
270	2	-.022	.057	.323	-.169
270	3	.014	.051	.249	-.143
270	4	.011	.061	.288	-.280
270	5	-.023	.064	.378	-.296
270	6	-.070	.055	.149	-.376
270	7	-.124	.088	.149	-.734
270	8	-.083	.060	.191	-.379
270	9	-.134	.083	.130	-.481
270	10	-.168	.084	.213	-.669
270	11	-.258	.130	.149	-.873
270	12	.017	.101	.508	-.419
270	13	-.159	.054	.023	-.536
270	14	-.294	.136	.164	-.786
270	15	.115	.104	.774	-.172
270	16	-.157	.106	.263	-.648
270	17	-.326	.103	-.004	-.953
270	18	.150	.087	.556	-.070
270	19	-.191	.074	.094	-.603
270	20	-.315	.107	.052	-.920
270	21	.146	.105	.589	-.114
270	22	-.185	.082	.153	-.579

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
270	23	.082	.097	.499	-.262
270	24	-.244	.079	.021	-.738
270	25	-.172	.065	.121	-.549
270	26	-.394	.110	-.032	-.914
270	27	.100	.083	.510	-.282
270	28	-.146	.087	.214	-.489
270	29	.129	.078	.474	-.086
270	30	-.210	.061	.063	-.522
270	31	-.170	.065	.059	-.486
270	32	-.312	.098	-.017	-.960
270	33	-.341	.100	-.103	-.929
270	34	-.188	.056	.063	-.471
270	35	-.333	.095	-.065	-.774
270	36	.089	.071	.391	-.112
270	37	-.184	.061	-.015	-.469
270	38	-.312	.080	-.039	-.755
270	39	-.102	.108	.260	-.661
270	40	-.129	.081	.223	-.433
270	41	-.124	.114	.476	-.714
270	42	-.417	.089	-.120	-.764
270	43	.028	.070	.380	-.369
270	44	.098	.072	.499	-.130
270	45	-.155	.060	.070	-.660
270	46	-.184	.091	.120	-.585
270	47	-.334	.080	-.072	-1.152
270	48	-.223	.064	.001	-.579
270	49	.091	.073	.456	-.081
270	50	-.181	.051	.005	-.436
270	51	-.236	.075	-.020	-.665
270	52	-.207	.058	.016	-.514
270	53	-.186	.058	.010	-.458
270	54	-.150	.039	.030	-.352
270	55	-.138	.051	.034	-.366
270	56	-.150	.050	.025	-.518
270	57	-.105	.051	.094	-.381
270	101	.070	.085	.543	-.332
270	102	.029	.091	.439	-.311
270	103	.027	.086	.611	-.258
270	104	.015	.103	.511	-.410
270	105	.071	.058	.367	-.158
270	106	.055	.056	.320	-.090
270	107	.070	.078	.513	-.100
270	108	.054	.075	.536	-.168
270	109	.038	.096	.735	-.290
270	110	.047	.089	.466	-.486
270	111	.047	.060	.400	-.116
270	112	.042	.094	.742	-.203
270	113	.052	.093	.885	-.220
270	114	.079	.074	.501	-.079
270	115	.070	.104	.652	-.347

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
270	116	.069	.072	.525	-.097
270	117	.131	.090	.671	-.107
270	118	-.012	.131	.754	-.583
270	119	.084	.115	.834	-.280
270	120	.196	.104	.669	-.106
270	121	.177	.088	.593	-.111
270	122	.126	.078	.486	-.140
270	123	.162	.075	.435	-.059
270	124	.172	.115	.699	-.140
270	125	.179	.082	.536	-.042
270	126	.138	.095	.563	-.175
270	127	.142	.068	.444	-.055
270	128	.136	.096	.631	-.104
270	129	.109	.050	.327	-.026
270	130	.170	.107	.660	-.089
270	131	.101	.108	.687	-.444
270	132	.114	.108	.782	-.424
270	133	.101	.056	.368	-.054
270	134	.083	.125	.737	-.356
270	135	.114	.089	.580	-.157
270	136	-.013	.039	.156	-.144
270	137	.110	.067	.411	-.101
270	138	.058	.076	.456	-.165
270	139	.121	.075	.453	-.123
270	140	.044	.060	.356	-.119
270	141	-.017	.063	.315	-.234
270	142	.063	.077	.435	-.121
270	143	.049	.056	.271	-.116
270	144	-.027	.075	.334	-.228
270	145	.145	.080	.491	-.086
270	146	.047	.136	.458	-.935
270	147	.046	.056	.349	-.135
270	148	.074	.076	.476	-.149
270	149	.023	.063	.331	-.161
270	150	.057	.079	.430	-.179
270	151	.036	.080	.394	-.228
270	152	.067	.053	.336	-.092
270	153	.021	.060	.318	-.161
270	154	.061	.079	.449	-.112
270	155	.110	.080	.494	-.167
270	156	.060	.067	.379	-.126
270	157	.026	.063	.429	-.170
270	158	-.145	.061	.095	-.359
270	159	-.075	.052	.218	-.255
270	160	.046	.068	.354	-.151
270	161	-.103	.057	.078	-.284
270	162	-.251	.057	-.103	-.584
270	163	-.202	.052	-.080	-.453
270	164	.041	.068	.390	-.149
270	165	.057	.063	.372	-.127

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
270	166	-.342	.057	-.200	-.605
270	167	-.034	.066	.400	-.148
270	201	-.151	.110	.266	-.829
270	202	-.113	.082	.214	-.478
270	203	-.206	.082	.076	-.571
270	204	-.377	.185	.323	-1.403
270	205	-.088	.074	.357	-.417
270	206	-.067	.094	.517	-.292
270	207	-.097	.055	.176	-.320
270	208	-.069	.093	.321	-.405
270	209	-.112	.095	.316	-.506
270	210	-.010	.075	.340	-.280
270	211	.042	.102	.475	-.254
270	212	-.191	.078	.198	-.524
270	213	-.090	.102	.407	-.440
270	214	-.077	.073	.532	-.097
270	301	-.374	.072	-.172	-.703
270	302	-.273	.074	-.042	-.759
270	303	-.248	.067	-.100	-.561
270	304	-.210	.053	-.070	-.464
270	305	-.206	.038	-.101	-.384
270	306	-.254	.056	-.126	-.568
270	307	-.200	.044	-.075	-.417
270	308	-.041	.079	.433	-.180
270	309	-.215	.038	-.076	-.375
270	310	-.256	.054	-.072	-.535
270	311	-.205	.051	-.025	-.510
270	312	-.197	.046	-.070	-.431
270	313	-.206	.042	-.092	-.391
270	314	-.244	.053	-.110	-.524
270	315	-.198	.051	.004	-.463
270	316	-.252	.048	-.127	-.522
270	317	-.146	.025	-.063	-.274
270	318	-.160	.060	.165	-.482
270	319	-.140	.061	.063	-.505
270	320	-.208	.060	-.043	-.576
270	401	-.190	.094	.173	-.608
270	402	-.294	.093	.064	-.857
270	403	-.377	.117	.005	-1.012
270	404	-.334	.100	-.079	-1.090
270	405	-.246	.074	-.044	-.696
270	406	-.228	.068	-.026	-.563
280	1	-.090	.060	.303	-.498
280	2	-.029	.053	.242	-.192
280	3	.029	.051	.334	-.160
280	4	.025	.058	.314	-.197
280	5	.018	.058	.419	-.236
280	6	-.017	.043	.185	-.278
280	7	-.107	.087	.287	-.515
280	8	-.019	.060	.307	-.269

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
280	9	-.091	.103	.388	-.628
280	10	-.116	.110	.237	-.701
280	11	-.181	.120	.209	-.808
280	12	-.089	.087	.611	-.124
280	13	-.129	.061	.167	-.415
280	14	-.101	.087	.243	-.510
280	15	-.101	.079	.492	-.104
280	16	-.079	.060	.175	-.383
280	17	-.186	.075	.034	-.579
280	18	-.107	.058	.443	-.036
280	19	-.123	.042	.030	-.370
280	20	-.162	.078	.125	-.566
280	21	-.058	.066	.446	-.136
280	22	-.055	.056	.276	-.240
280	23	-.056	.102	.515	-.546
280	24	-.152	.060	.123	-.378
280	25	-.130	.041	.086	-.317
280	26	-.153	.070	.144	-.506
280	27	-.000	.064	.410	-.352
280	28	-.103	.052	.158	-.305
280	29	-.037	.065	.390	-.151
280	30	-.121	.035	.014	-.322
280	31	-.110	.044	.070	-.309
280	32	-.170	.077	.230	-.528
280	33	-.196	.070	.046	-.782
280	34	-.096	.035	.049	-.261
280	35	-.209	.077	.059	-.647
280	36	-.022	.063	.515	-.203
280	37	-.108	.048	.106	-.483
280	38	-.169	.071	.077	-.525
280	39	-.108	.108	.267	-.703
280	40	-.057	.069	.502	-.385
280	41	-.094	.086	.502	-.709
280	42	-.259	.089	.025	-.707
280	43	-.002	.076	.343	-.341
280	44	.055	.084	.422	-.179
280	45	-.119	.042	.061	-.451
280	46	-.075	.076	.291	-.389
280	47	-.247	.079	-.028	-.694
280	48	-.168	.047	-.042	-.460
280	49	.045	.077	.451	-.138
280	50	-.134	.042	.012	-.337
280	51	-.171	.055	-.042	-.462
280	52	-.170	.050	-.006	-.452
280	53	-.149	.052	.030	-.402
280	54	-.101	.032	.001	-.313
280	55	-.132	.055	.050	-.461
280	56	-.128	.044	.051	-.471
280	57	-.083	.059	.106	-.290
280	101	.118	.085	.553	-.207

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
280	102	-.006	.092	.419	-.325
280	103	.123	.105	.645	-.183
280	104	.140	.113	.679	-.218
280	105	.156	.070	.549	-.021
280	106	.125	.072	.472	-.066
280	107	.134	.092	.627	-.097
280	108	.144	.101	.607	-.080
280	109	.188	.098	.625	-.112
280	110	.136	.112	.651	-.318
280	111	.124	.078	.479	-.056
280	112	.121	.094	.572	-.167
280	113	.196	.121	.768	-.354
280	114	.124	.071	.452	-.046
280	115	.113	.084	.522	-.124
280	116	.098	.070	.435	-.089
280	117	.123	.067	.466	-.068
280	118	.060	.140	.921	-.571
280	119	.067	.080	.443	-.244
280	120	.064	.071	.425	-.140
280	121	.048	.058	.311	-.242
280	122	.024	.060	.312	-.142
280	123	.052	.054	.309	-.088
280	124	.045	.081	.483	-.199
280	125	.042	.060	.360	-.082
280	126	.004	.066	.337	-.206
280	127	.032	.054	.329	-.114
280	128	.023	.070	.425	-.228
280	129	.012	.040	.226	-.093
280	130	.054	.094	.604	-.185
280	131	-.040	.097	.396	-.651
280	132	-.021	.089	.616	-.540
280	133	-.006	.044	.507	-.119
280	134	-.036	.100	.483	-.436
280	135	.011	.069	.552	-.249
280	136	-.042	.039	.148	-.206
280	137	-.013	.065	.579	-.209
280	138	-.025	.079	.549	-.317
280	139	.021	.073	.702	-.264
280	140	-.017	.050	.175	-.215
280	141	-.048	.058	.215	-.211
280	142	-.008	.069	.351	-.201
280	143	.002	.055	.342	-.170
280	144	-.015	.085	.467	-.394
280	145	.095	.089	.581	-.284
280	146	.005	.146	.476	-.778
280	147	.015	.067	.344	-.215
280	148	.050	.094	.483	-.350
280	149	.019	.076	.344	-.166
280	150	.028	.088	.460	-.208
280	151	.022	.078	.427	-.208
280	152	.031	.058	.295	-.124
280	153	.007	.057	.353	-.184
280	154	.027	.073	.355	-.267
280	155	.063	.074	.400	-.262
280	156	.015	.059	.337	-.219
280	157	-.010	.042	.262	-.146
280	158	-.145	.054	.095	-.379
280	159	-.087	.046	.150	-.296
280	160	-.008	.053	.319	-.177
280	161	-.111	.029	.021	-.231
280	162	-.203	.042	-.087	-.422
280	163	-.163	.039	-.052	-.383
280	164	-.006	.060	.290	-.179
280	165	.003	.056	.264	-.168
280	166	-.297	.059	-.139	-.550
280	167	.103	.085	.543	-.123
280	201	-.006	.092	.635	-.524
280	202	-.035	.085	.509	-.217
280	203	-.022	.071	.373	-.302
280	204	-.053	.181	.640	-1.204
280	205	-.109	.097	.615	-.779
280	206	-.035	.084	.559	-.394
280	207	-.125	.078	.233	-.717
280	208	-.033	.090	.499	-.347
280	209	-.097	.109	.490	-.490
280	210	.073	.094	.655	-.166
280	211	.118	.100	.748	-.115
280	212	-.195	.086	.251	-.659
280	213	-.067	.090	.488	-.475
280	214	.121	.089	.538	-.146
280	301	-.297	.070	-.104	-.709
280	302	-.260	.071	-.087	-.634
280	303	-.189	.056	-.061	-.466
280	304	-.171	.046	-.031	-.438
280	305	-.171	.039	-.035	-.336
280	306	-.206	.046	-.055	-.438
280	307	-.169	.043	-.043	-.354
280	308	.019	.080	.421	-.199
280	309	-.174	.036	-.061	-.347
280	310	-.212	.049	-.060	-.481
280	311	-.169	.050	.002	-.464
280	312	-.161	.039	-.055	-.357
280	313	-.170	.033	-.077	-.298
280	314	-.203	.041	-.094	-.386
280	315	-.163	.041	-.032	-.401
280	316	-.224	.049	-.120	-.418
280	317	-.127	.027	-.043	-.274
280	318	-.124	.039	-.038	-.329
280	319	-.113	.038	-.036	-.315
280	320	-.170	.051	-.021	-.552
290	401	-.093	.062	.199	-.368
290	402	-.156	.103	.408	-.701
290	403	-.248	.079	.003	-.811
290	404	-.220	.070	.001	-.689
290	405	-.158	.045	.011	-.454
290	406	-.141	.039	-.015	-.355
290	1	-.069	.059	.242	-.337
290	2	-.006	.040	.342	-.120
290	3	-.006	.054	.188	-.307
290	4	-.010	.054	.262	-.187
290	5	-.034	.058	.268	-.306
290	6	-.012	.036	.145	-.177
290	7	-.082	.075	.356	-.512
290	8	-.039	.051	.224	-.268
290	9	-.080	.090	.211	-.633
290	10	-.070	.098	.188	-1.028
290	11	-.151	.132	.254	-.840
290	12	.080	.100	.591	-.317
290	13	-.096	.058	.198	-.381
290	14	-.083	.100	.277	-.561
290	15	.116	.092	.512	-.124
290	16	-.062	.069	.233	-.431
290	17	-.170	.093	.195	-.797
290	18	.151	.071	.438	-.046
290	19	-.094	.052	.133	-.534
290	20	-.143	.096	.180	-.635
290	21	.092	.078	.524	-.185
290	22	-.018	.056	.253	-.315
290	23	-.010	.082	.389	-.393
290	24	-.125	.057	.106	-.465
290	25	-.104	.043	.045	-.406
290	26	-.129	.074	.120	-.561
290	27	.028	.061	.367	-.138
290	28	-.073	.049	.146	-.393
290	29	.060	.063	.414	-.138
290	30	-.091	.035	.009	-.317
290	31	-.069	.043	.166	-.314
290	32	-.129	.081	.191	-.639
290	33	-.170	.075	.080	-.695
290	34	-.073	.035	.069	-.241
290	35	-.181	.067	.045	-.510
290	36	.033	.059	.343	-.165
290	37	-.058	.045	.118	-.262
290	38	-.099	.056	.071	-.447
290	39	-.141	.107	.221	-.734
290	40	-.092	.074	.392	-.302
290	41	-.054	.064	.293	-.253
290	42	-.152	.072	.086	-.530
290	43	-.022	.052	.261	-.188
290	44	.016	.058	.323	-.187

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
290	45	-.099	.029	.005	-.231
290	46	.004	.052	.258	-.192
290	47	-.182	.060	.036	-.552
290	48	-.135	.033	.007	-.313
290	49	-.010	.047	.275	-.174
290	50	-.128	.039	.009	-.332
290	51	-.140	.038	-.002	-.364
290	52	-.147	.036	-.015	-.357
290	53	-.123	.034	.023	-.280
290	54	-.076	.025	.018	-.205
290	55	-.122	.044	.089	-.435
290	56	-.107	.033	.025	-.272
290	57	-.079	.048	.144	-.284
290	101	.065	.070	.421	-.364
290	102	-.014	.071	.331	-.285
290	103	.016	.068	.433	-.190
290	104	.032	.083	.496	-.331
290	105	.083	.053	.381	-.171
290	106	.062	.058	.397	-.089
290	107	.048	.065	.381	-.147
290	108	.063	.071	.418	-.158
290	109	.095	.086	.487	-.154
290	110	.083	.101	.664	-.204
290	111	.069	.073	.433	-.118
290	112	.091	.099	.580	-.313
290	113	.120	.101	.684	-.143
290	114	.118	.079	.543	-.050
290	115	.119	.100	.672	-.172
290	116	.107	.083	.483	-.178
290	117	.154	.077	.521	-.052
290	118	.048	.136	.803	-.576
290	119	.109	.098	.549	-.156
290	120	.131	.093	.613	-.135
290	121	.113	.077	.505	-.204
290	122	.084	.076	.416	-.151
290	123	.110	.069	.402	-.085
290	124	.096	.091	.611	-.162
290	125	.094	.070	.458	-.151
290	126	.054	.083	.489	-.276
290	127	.074	.066	.474	-.119
290	128	.071	.076	.431	-.228
290	129	.048	.045	.282	-.050
290	130	.104	.101	.612	-.132
290	131	.000	.097	.349	-.629
290	132	.065	.092	.381	-.429
290	133	.036	.044	.289	-.082
290	134	.014	.101	.528	-.449
290	135	.045	.069	.441	-.148
290	136	-.027	.034	.161	-.139
290	137	.020	.051	.282	-.117
290	138	-.028	.058	.245	-.185
290	139	.027	.059	.326	-.126
290	140	-.014	.043	.237	-.162
290	141	-.062	.042	.204	-.189
290	142	-.018	.057	.343	-.207
290	143	-.016	.041	.309	-.168
290	144	-.015	.067	.323	-.409
290	145	.095	.076	.559	-.111
290	146	-.134	.148	.389	-1.120
290	147	-.035	.042	.170	-.202
290	148	-.002	.053	.334	-.204
290	149	-.026	.047	.258	-.184
290	150	-.047	.049	.248	-.228
290	151	-.045	.049	.226	-.231
290	152	-.021	.039	.292	-.144
290	153	-.034	.046	.213	-.276
290	154	-.036	.055	.266	-.194
290	155	-.007	.059	.313	-.278
290	156	-.027	.047	.303	-.193
290	157	-.051	.038	.193	-.175
290	158	-.150	.044	.095	-.305
290	159	-.096	.037	.156	-.229
290	160	-.049	.044	.252	-.177
290	161	-.113	.025	.028	-.211
290	162	-.168	.027	-.075	-.339
290	163	-.130	.025	-.034	-.242
290	164	-.053	.048	.339	-.217
290	165	-.047	.044	.231	-.224
290	166	-.221	.041	-.121	-.490
290	167	.019	.067	.378	-.166
290	201	-.042	.089	.438	-.569
290	202	-.008	.077	.593	-.272
290	203	-.062	.075	.414	-.432
290	204	-.183	.262	.471	-1.031
290	205	-.090	.074	.423	-.446
290	206	.007	.085	.431	-.349
290	207	-.101	.057	.289	-.345
290	208	-.048	.088	.359	-.349
290	209	-.061	.110	.405	-.685
290	210	.011	.071	.469	-.221
290	211	.063	.086	.470	-.334
290	212	-.148	.057	.230	-.426
290	213	-.068	.076	.369	-.372
290	214	.058	.071	.476	-.146
290	301	-.230	.054	-.026	-.559
290	302	-.250	.059	-.107	-.583
290	303	-.148	.037	-.027	-.363
290	304	-.135	.028	-.018	-.266
290	305	-.135	.024	-.048	-.244
290	306	-.168	.027	-.073	-.294
290	307	-.139	.025	-.043	-.271
290	308	-.054	.046	.190	-.246
290	309	-.136	.021	-.073	-.273
290	310	-.173	.028	-.089	-.344
290	311	-.141	.034	-.034	-.282
290	312	-.135	.029	-.035	-.263
290	313	-.137	.023	-.041	-.236
290	314	-.169	.029	-.053	-.312
290	315	-.135	.030	-.023	-.305
290	316	-.178	.035	-.075	-.405
290	317	-.104	.022	-.033	-.228
290	318	-.106	.037	.007	-.310
290	319	-.095	.035	.028	-.324
290	320	-.148	.032	-.041	-.305
290	401	-.051	.062	.333	-.294
290	402	-.065	.118	.514	-.590
290	403	-.220	.062	-.006	-.546
290	404	-.199	.058	.001	-.455
290	405	-.133	.046	.072	-.384
290	406	-.116	.041	.031	-.349
300	1	-.083	.035	.113	-.236
300	2	-.054	.022	.073	-.142
300	3	-.090	.044	.124	-.390
300	4	-.064	.039	.191	-.233
300	5	-.069	.047	.186	-.358
300	6	-.049	.029	.079	-.186
300	7	-.103	.048	.133	-.344
300	8	-.049	.032	.263	-.168
300	9	-.054	.047	.159	-.465
300	10	-.055	.054	.281	-.453
300	11	-.127	.073	.270	-.624
300	12	-.009	.064	.371	-.332
300	13	-.085	.040	.100	-.376
300	14	-.053	.066	.268	-.488
300	15	-.011	.062	.336	-.219
300	16	-.062	.051	.204	-.307
300	17	-.101	.074	.193	-.618
300	18	-.044	.053	.373	-.098
300	19	-.108	.049	.174	-.322
300	20	-.079	.078	.254	-.452
300	21	.031	.066	.484	-.171
300	22	-.034	.046	.213	-.229
300	23	-.023	.065	.404	-.319
300	24	-.086	.056	.132	-.413
300	25	-.074	.040	.075	-.309
300	26	-.083	.074	.257	-.518
300	27	-.006	.062	.313	-.176
300	28	-.049	.052	.202	-.271
300	29	.051	.073	.422	-.169
300	30	-.085	.037	.009	-.317

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
300	31	-.079	.048	.136	-.294
300	32	-.092	.090	.292	-.553
300	33	-.120	.066	.155	-.487
300	34	-.068	.030	.053	-.212
300	35	-.160	.060	.083	-.440
300	36	.030	.058	.297	-.197
300	37	-.044	.050	.197	-.298
300	38	-.090	.062	.147	-.367
300	39	-.102	.079	.245	-.579
300	40	.005	.077	.522	-.258
300	41	-.041	.057	.239	-.380
300	42	-.143	.080	.047	-.536
300	43	-.036	.048	.204	-.176
300	44	.026	.059	.362	-.152
300	45	-.078	.032	.051	-.247
300	46	-.012	.052	.206	-.234
300	47	-.184	.068	.020	-.549
300	48	-.119	.037	-.008	-.289
300	49	.003	.044	.255	-.123
300	50	-.145	.037	.018	-.293
300	51	-.118	.041	.024	-.399
300	52	-.133	.034	-.012	-.305
300	53	-.108	.034	-.011	-.276
300	54	-.095	.025	-.008	-.210
300	55	-.145	.046	.004	-.388
300	56	-.098	.033	.071	-.233
300	57	-.066	.045	.139	-.262
300	101	-.003	.065	.368	-.284
300	102	-.069	.060	.267	-.256
300	103	-.005	.059	.385	-.206
300	104	-.034	.053	.319	-.249
300	105	.007	.036	.202	-.122
300	106	-.035	.038	.133	-.153
300	107	-.004	.051	.279	-.181
300	108	-.005	.043	.182	-.156
300	109	.023	.050	.384	-.140
300	110	-.042	.048	.427	-.194
300	111	-.004	.038	.225	-.095
300	112	-.008	.056	.475	-.271
300	113	.007	.062	.480	-.275
300	114	-.018	.050	.297	-.151
300	115	.002	.057	.342	-.282
300	116	.013	.050	.328	-.125
300	117	.026	.045	.309	-.098
300	118	-.068	.076	.388	-.417
300	119	.009	.068	.434	-.282
300	120	.032	.070	.420	-.195
300	121	.023	.057	.314	-.184
300	122	.002	.062	.337	-.183
300	123	.034	.058	.299	-.115
300	124	.022	.072	.560	-.193
300	125	.036	.063	.397	-.164
300	126	.000	.072	.496	-.245
300	127	.031	.062	.391	-.115
300	128	.037	.076	.409	-.242
300	129	.033	.045	.229	-.073
300	130	.040	.092	.584	-.160
300	131	.021	.071	.393	-.295
300	132	.019	.082	.411	-.431
300	133	.030	.049	.271	-.104
300	134	.001	.105	.563	-.407
300	135	.034	.074	.431	-.173
300	136	-.014	.039	.209	-.138
300	137	.025	.058	.332	-.171
300	138	-.013	.061	.232	-.247
300	139	.030	.065	.328	-.232
300	140	.003	.051	.275	-.124
300	141	-.033	.040	.160	-.184
300	142	-.000	.059	.278	-.167
300	143	.001	.048	.251	-.216
300	144	.013	.075	.380	-.438
300	145	.096	.080	.506	-.117
300	146	-.053	.114	.331	-1.062
300	147	-.011	.046	.206	-.212
300	148	.023	.063	.293	-.295
300	149	.002	.051	.236	-.200
300	150	-.019	.054	.201	-.199
300	151	-.018	.049	.193	-.200
300	152	-.007	.042	.224	-.153
300	153	-.018	.041	.218	-.158
300	154	-.024	.053	.223	-.206
300	155	-.004	.057	.276	-.256
300	156	-.025	.043	.295	-.153
300	157	-.060	.028	.086	-.147
300	158	-.141	.035	-.007	-.288
300	159	-.087	.031	.056	-.229
300	160	-.056	.036	.113	-.207
300	161	-.107	.024	-.015	-.234
300	162	-.155	.028	-.067	-.249
300	163	-.119	.026	-.029	-.216
300	164	-.062	.035	.102	-.249
300	165	-.060	.032	.093	-.287
300	166	-.195	.043	-.080	-.404
300	167	-.021	.047	.263	-.193
300	201	-.039	.063	.384	-.481
300	202	-.018	.052	.238	-.211
300	203	-.034	.047	.211	-.307
300	204	-.061	.117	.586	-1.059
300	205	-.107	.043	.184	-.295
300	206	-.003	.071	.443	-.280
300	207	-.094	.032	.160	-.341
300	208	-.071	.058	.374	-.263
300	209	-.058	.081	.384	-.468
300	210	-.014	.059	.326	-.318
300	211	.001	.056	.363	-.164
300	212	-.128	.029	-.016	-.304
300	213	-.088	.037	.105	-.212
300	214	.013	.053	.340	-.184
300	301	-.172	.048	-.037	-.408
300	302	-.234	.055	-.126	-.591
300	303	-.122	.032	-.027	-.281
300	304	-.127	.031	-.027	-.262
300	305	-.125	.026	-.039	-.249
300	306	-.159	.029	-.048	-.286
300	307	-.136	.028	-.038	-.268
300	308	-.019	.047	.231	-.158
300	309	-.123	.023	-.048	-.227
300	310	-.161	.031	-.055	-.306
300	311	-.133	.040	.024	-.427
300	312	-.118	.029	-.009	-.253
300	313	-.120	.023	-.039	-.211
300	314	-.152	.029	-.044	-.276
300	315	-.126	.032	-.016	-.241
300	316	-.159	.043	-.053	-.399
300	317	-.090	.025	-.011	-.225
300	318	-.082	.031	.023	-.255
300	319	-.066	.030	.023	-.247
300	320	-.129	.032	-.032	-.287
300	401	-.028	.061	.320	-.261
300	402	-.039	.104	.342	-.606
300	403	-.174	.065	-.028	-.540
300	404	-.140	.060	.028	-.573
300	405	-.087	.040	.083	-.259
300	406	-.068	.032	.044	-.300
310	1	-.097	.042	.116	-.324
310	2	-.061	.021	.082	-.143
310	3	-.126	.043	.115	-.424
310	4	-.085	.037	.156	-.279
310	5	-.086	.043	.198	-.304
310	6	-.056	.032	.124	-.246
310	7	-.118	.043	.177	-.419
310	8	-.045	.033	.097	-.162
310	9	-.053	.038	.102	-.317
310	10	-.042	.043	.108	-.409
310	11	-.133	.057	.145	-.585
310	12	-.035	.034	.185	-.177
310	13	-.092	.043	.102	-.364
310	14	-.041	.038	.139	-.380
310	15	-.055	.042	.200	-.246
310	16	-.052	.037	.146	-.329

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
310	17	-.074	.049	.089	-.409
310	18	-.006	.035	.238	-.094
310	19	-.095	.040	.071	-.380
310	20	-.060	.051	.237	-.438
310	21	-.004	.052	.328	-.148
310	22	-.031	.032	.232	-.178
310	23	-.060	.055	.274	-.278
310	24	-.066	.043	.187	-.288
310	25	-.064	.031	.116	-.264
310	26	-.048	.048	.153	-.360
310	27	-.055	.048	.225	-.278
310	28	-.049	.038	.160	-.250
310	29	-.007	.048	.225	-.163
310	30	-.052	.026	.034	-.169
310	31	-.084	.034	.059	-.248
310	32	-.056	.056	.214	-.368
310	33	-.085	.053	.100	-.478
310	34	-.048	.024	.064	-.206
310	35	-.130	.049	.057	-.387
310	36	-.000	.051	.262	-.141
310	37	-.033	.042	.232	-.183
310	38	-.047	.047	.179	-.297
310	39	-.099	.060	.214	-.472
310	40	.006	.067	.393	-.202
310	41	-.034	.052	.272	-.230
310	42	-.078	.057	.102	-.411
310	43	-.060	.043	.124	-.241
310	44	.003	.052	.237	-.186
310	45	-.062	.029	.064	-.208
310	46	-.014	.042	.234	-.187
310	47	-.140	.052	.052	-.442
310	48	-.089	.034	.011	-.297
310	49	-.017	.040	.171	-.141
310	50	-.109	.030	-.024	-.246
310	51	-.087	.030	-.013	-.287
310	52	-.102	.028	-.014	-.270
310	53	-.084	.027	.051	-.246
310	54	-.069	.023	-.001	-.200
310	55	-.129	.035	-.010	-.334
310	56	-.072	.031	.079	-.202
310	57	-.057	.037	.122	-.226
310	101	-.043	.054	.366	-.338
310	102	-.118	.049	.258	-.253
310	103	-.042	.051	.366	-.207
310	104	-.053	.046	.196	-.275
310	105	-.019	.039	.197	-.191
310	106	-.069	.035	.149	-.183
310	107	-.022	.052	.301	-.202
310	108	-.026	.041	.145	-.177
310	109	.005	.044	.254	-.145
310	110	-.078	.040	.131	-.218
310	111	-.029	.033	.219	-.141
310	112	-.038	.038	.305	-.253
310	113	-.029	.048	.373	-.259
310	114	-.060	.033	.128	-.156
310	115	-.026	.034	.235	-.184
310	116	-.021	.036	.225	-.117
310	117	-.015	.029	.254	-.136
310	118	-.123	.051	.246	-.398
310	119	-.028	.041	.380	-.214
310	120	-.015	.041	.271	-.208
310	121	-.014	.034	.249	-.179
310	122	-.040	.040	.289	-.171
310	123	-.011	.037	.258	-.102
310	124	-.020	.041	.299	-.177
310	125	-.012	.033	.242	-.133
310	126	-.045	.038	.296	-.299
310	127	-.014	.035	.263	-.131
310	128	-.013	.048	.306	-.201
310	129	-.010	.030	.157	-.085
310	130	-.017	.059	.540	-.191
310	131	-.027	.047	.274	-.241
310	132	-.022	.047	.227	-.254
310	133	-.010	.034	.168	-.096
310	134	-.045	.071	.374	-.424
310	135	-.010	.052	.442	-.215
310	136	-.028	.028	.157	-.114
310	137	-.019	.037	.271	-.194
310	138	-.051	.041	.309	-.240
310	139	-.015	.041	.378	-.164
310	140	-.021	.036	.210	-.153
310	141	-.038	.032	.124	-.170
310	142	-.033	.048	.213	-.184
310	143	-.017	.036	.152	-.144
310	144	-.011	.067	.355	-.387
310	145	.037	.064	.460	-.166
310	146	-.067	.080	.318	-.987
310	147	-.024	.038	.283	-.175
310	148	-.011	.047	.234	-.219
310	149	-.018	.038	.168	-.175
310	150	-.042	.039	.157	-.195
310	151	-.030	.037	.161	-.177
310	152	-.020	.035	.162	-.127
310	153	-.022	.035	.168	-.183
310	154	-.038	.044	.175	-.184
310	155	-.018	.048	.219	-.246
310	156	-.027	.038	.179	-.168
310	157	-.049	.025	.098	-.212
310	158	-.111	.030	.006	-.281
310	159	-.067	.027	.055	-.199
310	160	-.045	.034	.125	-.208
310	161	-.078	.021	-.001	-.214
310	162	-.121	.027	-.025	-.254
310	163	-.089	.025	.011	-.204
310	164	-.047	.033	.135	-.219
310	165	-.043	.030	.117	-.245
310	166	-.138	.034	-.036	-.364
310	167	-.032	.041	.171	-.152
310	201	-.018	.063	.437	-.277
310	202	-.004	.051	.441	-.190
310	203	-.018	.041	.209	-.315
310	204	-.051	.065	.343	-.586
310	205	-.111	.047	.084	-.327
310	206	-.029	.064	.380	-.263
310	207	-.092	.033	.040	-.254
310	208	-.096	.048	.309	-.225
310	209	-.079	.062	.307	-.562
310	210	-.039	.058	.302	-.354
310	211	-.012	.048	.262	-.223
310	212	-.121	.028	-.018	-.258
310	213	-.091	.033	.123	-.221
310	214	-.017	.049	.271	-.173
310	301	-.110	.039	.001	-.425
310	302	-.169	.045	-.056	-.420
310	303	-.088	.030	-.007	-.292
310	304	-.092	.026	-.013	-.216
310	305	-.086	.024	-.021	-.188
310	306	-.120	.026	-.041	-.231
310	307	-.097	.025	-.020	-.206
310	308	-.030	.042	.186	-.229
310	309	-.091	.021	-.030	-.201
310	310	-.128	.028	-.043	-.258
310	311	-.100	.032	-.017	-.303
310	312	-.086	.025	-.000	-.221
310	313	-.085	.019	-.019	-.179
310	314	-.116	.024	-.041	-.225
310	315	-.089	.025	-.000	-.206
310	316	-.110	.034	-.013	-.379
310	317	-.061	.021	.000	-.211
310	318	-.067	.022	.010	-.206
310	319	-.049	.021	.030	-.155
310	320	-.100	.026	-.010	-.237
310	401	-.026	.050	.337	-.302
310	402	-.011	.078	.398	-.371
310	403	-.128	.051	.008	-.487
310	404	-.099	.046	.034	-.380
310	405	-.068	.032	.053	-.236
310	406	-.050	.026	.040	-.217
320	1	-.080	.048	.144	-.305
320	2	-.061	.021	.052	-.151

APPENDIX A -- PRESSURE DATA: CONFIGURATION A) MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
320	3	-.140	.035	-.010	-.332
320	4	-.091	.029	.047	-.215
320	5	-.086	.036	.142	-.246
320	6	-.046	.035	.105	-.180
320	7	-.120	.044	.140	-.494
320	8	-.019	.043	.228	-.231
320	9	-.037	.037	.144	-.230
320	10	-.035	.034	.134	-.247
320	11	-.165	.062	.027	-.517
320	12	-.057	.036	.152	-.211
320	13	-.122	.063	.171	-.541
320	14	-.056	.036	.090	-.240
320	15	-.083	.033	.076	-.271
320	16	-.055	.043	.102	-.320
320	17	-.061	.034	.115	-.287
320	18	-.017	.023	.096	-.111
320	19	-.090	.034	.069	-.240
320	20	-.047	.033	.125	-.179
320	21	-.027	.030	.124	-.228
320	22	-.030	.026	.079	-.133
320	23	-.100	.034	.170	-.285
320	24	-.069	.031	.116	-.247
320	25	-.058	.028	.060	-.201
320	26	-.037	.030	.076	-.213
320	27	-.084	.030	.083	-.224
320	28	-.047	.029	.091	-.183
320	29	-.029	.031	.187	-.149
320	30	-.042	.022	.043	-.186
320	31	-.087	.032	.058	-.226
320	32	-.040	.044	.244	-.275
320	33	-.061	.035	.083	-.323
320	34	-.041	.019	.032	-.108
320	35	-.119	.032	-.001	-.430
320	36	-.024	.032	.132	-.151
320	37	-.076	.035	.157	-.199
320	38	-.033	.036	.170	-.278
320	39	-.118	.043	.072	-.510
320	40	-.009	.050	.250	-.172
320	41	-.047	.032	.108	-.330
320	42	-.056	.036	.047	-.376
320	43	-.088	.029	.100	-.250
320	44	-.027	.035	.234	-.167
320	45	-.056	.025	.047	-.167
320	46	-.032	.025	.112	-.135
320	47	-.124	.034	-.010	-.311
320	48	-.071	.025	.015	-.193
320	49	-.033	.031	.169	-.208
320	50	-.094	.022	-.033	-.211
320	51	-.076	.022	-.002	-.197
320	52	-.090	.022	-.019	-.229
320	53	-.081	.024	.006	-.199
320	54	-.065	.018	-.006	-.155
320	55	-.130	.030	-.024	-.261
320	56	-.063	.026	.088	-.183
320	57	-.054	.029	.133	-.188
320	101	-.059	.042	.486	-.229
320	102	-.131	.038	.180	-.290
320	103	-.056	.044	.305	-.204
320	104	-.060	.043	.137	-.298
320	105	-.038	.034	.110	-.160
320	106	-.091	.031	.069	-.184
320	107	-.041	.045	.212	-.158
320	108	-.034	.042	.216	-.169
320	109	-.012	.043	.194	-.178
320	110	-.100	.038	.074	-.283
320	111	-.041	.031	.123	-.181
320	112	-.059	.040	.108	-.302
320	113	-.075	.047	.230	-.322
320	114	-.080	.029	.039	-.161
320	115	-.046	.031	.104	-.177
320	116	-.038	.028	.085	-.133
320	117	-.043	.022	.058	-.166
320	118	-.183	.061	.100	-.517
320	119	-.045	.028	.077	-.167
320	120	-.034	.031	.158	-.167
320	121	-.033	.024	.095	-.129
320	122	-.058	.030	.114	-.169
320	123	-.029	.027	.160	-.111
320	124	-.035	.034	.189	-.332
320	125	-.028	.026	.129	-.158
320	126	-.055	.029	.112	-.188
320	127	-.025	.030	.216	-.111
320	128	-.033	.030	.134	-.145
320	129	-.029	.018	.064	-.080
320	130	-.040	.038	.162	-.153
320	131	-.048	.028	.081	-.216
320	132	-.038	.029	.216	-.229
320	133	-.028	.021	.176	-.124
320	134	-.087	.046	.201	-.322
320	135	-.036	.030	.175	-.153
320	136	-.035	.021	.078	-.102
320	137	-.039	.023	.095	-.138
320	138	-.070	.026	.048	-.160
320	139	-.033	.027	.115	-.131
320	140	-.035	.024	.114	-.127
320	141	-.051	.022	.070	-.138
320	142	-.057	.031	.171	-.156
320	143	-.029	.024	.151	-.111
320	144	-.032	.044	.205	-.339
320	145	.004	.044	.283	-.154
320	146	-.081	.051	.203	-.489
320	147	-.032	.026	.088	-.144
320	148	-.033	.033	.174	-.180
320	149	-.039	.027	.100	-.151
320	150	-.063	.028	.091	-.197
320	151	-.048	.027	.103	-.185
320	152	-.030	.027	.111	-.158
320	153	-.035	.028	.144	-.174
320	154	-.057	.033	.146	-.192
320	155	-.033	.034	.133	-.273
320	156	-.036	.027	.116	-.147
320	157	-.056	.018	.044	-.156
320	158	-.106	.022	-.021	-.265
320	159	-.068	.021	.038	-.171
320	160	-.049	.026	.089	-.196
320	161	-.074	.018	-.015	-.165
320	162	-.108	.021	-.037	-.229
320	163	-.077	.020	-.009	-.169
320	164	-.053	.026	.096	-.238
320	165	-.050	.023	.075	-.254
320	166	-.116	.031	-.032	-.334
320	167	-.047	.042	.202	-.200
320	201	.005	.071	.385	-.282
320	202	.024	.060	.338	-.169
320	203	.004	.047	.312	-.187
320	204	-.062	.064	.313	-.265
320	205	-.102	.044	.110	-.327
320	206	-.053	.046	.190	-.224
320	207	-.096	.031	.032	-.234
320	208	-.101	.038	.308	-.222
320	209	-.078	.045	.362	-.345
320	210	-.058	.047	.247	-.283
320	211	-.027	.046	.317	-.245
320	212	-.123	.031	.002	-.347
320	213	-.093	.025	.038	-.230
320	214	-.039	.047	.281	-.178
320	301	-.089	.029	-.001	-.265
320	302	-.147	.032	-.057	-.359
320	303	-.084	.026	-.002	-.219
320	304	-.080	.021	-.013	-.156
320	305	-.080	.019	-.010	-.154
320	306	-.108	.021	-.037	-.210
320	307	-.084	.020	-.014	-.169
320	308	-.051	.028	.107	-.223
320	309	-.082	.018	-.024	-.167
320	310	-.114	.023	-.037	-.233
320	311	-.083	.024	.011	-.212
320	312	-.082	.022	-.009	-.198
320	313	-.079	.017	-.024	-.154
320	314	-.106	.022	-.035	-.208

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
320	315	-.075	.021	-.009	-.180
320	316	-.081	.025	-.018	-.248
320	317	-.044	.017	.007	-.125
320	318	-.063	.017	.001	-.137
320	319	-.042	.016	.017	-.117
320	320	-.085	.021	-.015	-.182
320	401	-.034	.037	.150	-.270
320	402	-.003	.056	.384	-.405
320	403	-.104	.033	-.020	-.370
320	404	-.076	.030	.014	-.243
320	405	-.058	.024	.029	-.151
320	406	-.042	.019	.031	-.147
330	1	-.068	.043	.134	-.302
330	2	-.078	.020	.059	-.180
330	3	-.086	.030	.019	-.209
330	4	-.081	.027	.048	-.227
330	5	-.077	.030	.105	-.260
330	6	-.049	.029	.077	-.169
330	7	-.058	.042	.271	-.223
330	8	-.005	.037	.225	-.182
330	9	-.019	.036	.150	-.191
330	10	-.064	.035	.117	-.250
330	11	-.158	.069	.090	-.535
330	12	-.078	.034	.115	-.274
330	13	-.148	.066	.083	-.530
330	14	-.104	.041	.081	-.308
330	15	-.062	.030	.061	-.203
330	16	-.059	.044	.155	-.366
330	17	-.051	.033	.068	-.258
330	18	-.048	.020	.039	-.187
330	19	-.036	.034	.107	-.209
330	20	-.034	.032	.182	-.261
330	21	-.036	.027	.088	-.180
330	22	-.047	.024	.056	-.160
330	23	-.067	.030	.052	-.256
330	24	-.074	.032	.039	-.296
330	25	-.052	.027	.059	-.169
330	26	-.056	.029	.126	-.203
330	27	-.053	.024	.067	-.176
330	28	-.043	.026	.068	-.182
330	29	-.041	.025	.063	-.158
330	30	-.058	.021	.016	-.214
330	31	-.036	.031	.107	-.203
330	32	-.016	.039	.142	-.189
330	33	-.050	.031	.092	-.244
330	34	-.060	.020	.001	-.167
330	35	-.073	.028	.014	-.254
330	36	-.033	.027	.135	-.167
330	37	-.035	.035	.148	-.174
330	38	-.037	.029	.153	-.160

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
330	39	-.078	.032	.059	-.311
330	40	-.099	.055	.379	-.185
330	41	-.047	.030	.114	-.205
330	42	-.063	.025	.068	-.183
330	43	-.058	.022	.043	-.185
330	44	-.042	.026	.113	-.173
330	45	-.049	.024	.041	-.160
330	46	-.056	.021	.027	-.158
330	47	-.076	.025	.036	-.207
330	48	-.065	.023	.003	-.162
330	49	-.048	.022	.074	-.134
330	50	-.117	.021	-.048	-.216
330	51	-.086	.021	-.018	-.171
330	52	-.095	.021	-.028	-.205
330	53	-.093	.022	-.025	-.236
330	54	-.089	.018	-.026	-.167
330	55	-.089	.025	-.006	-.256
330	56	-.061	.027	.061	-.173
330	57	-.050	.026	.077	-.154
330	101	-.078	.036	.146	-.281
330	102	-.082	.028	.087	-.189
330	103	-.055	.038	.160	-.178
330	104	-.064	.037	.074	-.233
330	105	-.056	.027	.079	-.196
330	106	-.050	.024	.083	-.130
330	107	-.037	.037	.167	-.135
330	108	-.040	.035	.210	-.205
330	109	-.042	.043	.217	-.408
330	110	-.072	.035	.087	-.260
330	111	-.049	.025	.088	-.182
330	112	-.086	.043	.112	-.304
330	113	-.131	.036	.054	-.281
330	114	-.051	.023	.070	-.163
330	115	-.062	.027	.059	-.216
330	116	-.050	.024	.063	-.147
330	117	-.080	.022	.003	-.191
330	118	-.166	.064	.132	-.568
330	119	-.055	.027	.037	-.261
330	120	-.045	.030	.093	-.189
330	121	-.041	.023	.043	-.157
330	122	-.068	.026	.063	-.184
330	123	-.040	.022	.058	-.110
330	124	-.046	.029	.084	-.284
330	125	-.037	.022	.061	-.166
330	126	-.065	.024	.038	-.198
330	127	-.036	.023	.076	-.124
330	128	-.044	.028	.107	-.220
330	129	-.036	.017	.052	-.102
330	130	-.051	.034	.195	-.205
330	131	-.057	.024	.049	-.202

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
330	132	-.048	.024	.042	-.173
330	133	-.037	.018	.043	-.110
330	134	-.122	.046	.050	-.382
330	135	-.049	.027	.096	-.211
330	136	-.039	.018	.060	-.102
330	137	-.050	.018	.012	-.128
330	138	-.078	.021	-.000	-.182
330	139	-.043	.021	.042	-.155
330	140	-.042	.022	.060	-.160
330	141	-.055	.020	.026	-.162
330	142	-.068	.024	.022	-.173
330	143	-.035	.022	.094	-.128
330	144	-.046	.035	.149	-.357
330	145	-.014	.032	.246	-.171
330	146	-.091	.037	.145	-.362
330	147	-.038	.022	.060	-.148
330	148	-.047	.027	.147	-.200
330	149	-.055	.022	.095	-.173
330	150	-.077	.024	.093	-.196
330	151	-.061	.024	.092	-.204
330	152	-.042	.019	.082	-.115
330	153	-.049	.021	.059	-.222
330	154	-.073	.024	.047	-.178
330	155	-.046	.023	.069	-.225
330	156	-.046	.023	.067	-.200
330	157	-.068	.016	-.019	-.157
330	158	-.119	.022	-.053	-.262
330	159	-.084	.020	-.018	-.198
330	160	-.060	.022	.073	-.206
330	161	-.091	.017	-.030	-.200
330	162	-.122	.022	-.046	-.216
330	163	-.089	.021	-.005	-.180
330	164	-.066	.025	.029	-.222
330	165	-.062	.022	.032	-.164
330	166	-.095	.024	-.016	-.205
330	167	-.065	.036	.096	-.215
330	201	-.042	.083	.561	-.211
330	202	-.049	.064	.431	-.160
330	203	-.027	.051	.315	-.148
330	204	-.071	.063	.268	-.300
330	205	-.089	.042	.123	-.238
330	206	-.060	.038	.191	-.206
330	207	-.088	.028	.023	-.220
330	208	-.094	.033	.066	-.219
330	209	-.067	.036	.110	-.234
330	210	-.057	.034	.147	-.255
330	211	-.040	.029	.168	-.260
330	212	-.115	.025	-.007	-.228
330	213	-.084	.021	-.000	-.187
330	214	-.044	.035	.182	-.149

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
330	301	-.079	.022	-.008	-.217
330	302	-.142	.028	-.073	-.319
330	303	-.099	.024	-.025	-.216
330	304	-.094	.021	-.022	-.202
330	305	-.098	.019	-.041	-.175
330	306	-.125	.023	-.046	-.239
330	307	-.093	.019	-.014	-.184
330	308	-.063	.022	.011	-.162
330	309	-.099	.017	-.039	-.166
330	310	-.123	.022	-.046	-.205
330	311	-.087	.022	-.000	-.187
330	312	-.102	.023	-.027	-.204
330	313	-.090	.019	-.032	-.175
330	314	-.112	.024	-.025	-.228
330	315	-.076	.022	-.000	-.162
330	316	-.068	.022	.027	-.187
330	317	-.042	.016	.043	-.106
330	318	-.065	.017	-.006	-.131
330	319	-.040	.015	.008	-.098
330	320	-.092	.021	-.024	-.203
330	401	-.038	.037	.147	-.233
330	402	-.000	.044	.419	-.184
330	403	-.098	.032	-.020	-.327
330	404	-.069	.029	.017	-.268
330	405	-.054	.021	.020	-.153
330	406	-.042	.018	.020	-.122
340	1	-.065	.042	.173	-.208
340	2	-.084	.020	.041	-.164
340	3	-.091	.026	.026	-.206
340	4	-.085	.024	.024	-.267
340	5	-.074	.038	.182	-.186
340	6	-.053	.030	.080	-.171
340	7	-.061	.052	.199	-.361
340	8	.003	.038	.184	-.130
340	9	-.014	.039	.177	-.188
340	10	-.089	.036	.055	-.241
340	11	-.204	.082	-.006	-.682
340	12	-.103	.036	.035	-.267
340	13	-.155	.057	.033	-.429
340	14	-.126	.039	.055	-.333
340	15	-.087	.030	.014	-.244
340	16	-.076	.040	.098	-.295
340	17	-.061	.034	.115	-.228
340	18	-.070	.021	.007	-.184
340	19	-.049	.029	.100	-.185
340	20	-.041	.031	.096	-.200
340	21	-.050	.025	.108	-.201
340	22	-.058	.022	.075	-.178
340	23	-.080	.030	.032	-.280
340	24	-.087	.032	.012	-.227
340	25	-.048	.031	.177	-.255
340	26	-.073	.030	.075	-.209
340	27	-.067	.026	.023	-.203
340	28	-.051	.024	.048	-.164
340	29	-.050	.024	.046	-.168
340	30	-.064	.019	.003	-.162
340	31	-.047	.027	.095	-.176
340	32	-.016	.035	.170	-.134
340	33	-.049	.029	.059	-.262
340	34	-.067	.018	-.011	-.139
340	35	-.074	.025	.008	-.260
340	36	-.040	.024	.067	-.170
340	37	-.038	.033	.162	-.139
340	38	-.049	.029	.116	-.166
340	39	-.086	.031	.082	-.343
340	40	-.004	.051	.369	-.170
340	41	-.055	.026	.073	-.186
340	42	-.072	.023	.001	-.275
340	43	-.069	.022	.039	-.215
340	44	-.050	.024	.069	-.195
340	45	-.045	.023	.064	-.137
340	46	-.066	.019	.021	-.155
340	47	-.084	.028	.014	-.244
340	48	-.062	.020	.003	-.157
340	49	-.056	.022	.046	-.195
340	50	-.127	.021	-.058	-.218
340	51	-.090	.019	-.031	-.166
340	52	-.098	.020	-.028	-.184
340	53	-.099	.023	-.034	-.244
340	54	-.099	.019	-.040	-.173
340	55	-.094	.026	-.015	-.280
340	56	-.065	.028	.048	-.182
340	57	-.050	.029	.075	-.181
340	101	-.104	.038	.086	-.342
340	102	-.093	.022	-.017	-.170
340	103	-.060	.036	.098	-.200
340	104	-.089	.036	.033	-.326
340	105	-.080	.023	.007	-.168
340	106	-.072	.021	.019	-.163
340	107	-.062	.027	.073	-.177
340	108	-.060	.025	.064	-.177
340	109	-.065	.036	.080	-.320
340	110	-.102	.030	-.003	-.271
340	111	-.067	.029	-.001	-.161
340	112	-.131	.052	.015	-.504
340	113	-.176	.042	-.038	-.432
340	114	-.075	.023	.014	-.165
340	115	-.088	.029	.010	-.243
340	116	-.079	.025	.015	-.197
340	117	-.107	.025	-.033	-.243
340	118	-.181	.065	.030	-.621
340	119	-.074	.030	.019	-.335
340	120	-.069	.026	.022	-.186
340	121	-.063	.020	.010	-.150
340	122	-.086	.023	.013	-.175
340	123	-.057	.019	.015	-.119
340	124	-.065	.031	.078	-.333
340	125	-.053	.022	.032	-.172
340	126	-.081	.024	.013	-.186
340	127	-.051	.022	.038	-.133
340	128	-.057	.029	.044	-.317
340	129	-.044	.016	.014	-.119
340	130	-.067	.029	.036	-.259
340	131	-.065	.024	.022	-.254
340	132	-.058	.023	.058	-.202
340	133	-.046	.018	.034	-.137
340	134	-.142	.049	-.021	-.568
340	135	-.061	.029	.065	-.274
340	136	-.047	.017	.016	-.122
340	137	-.057	.019	.003	-.143
340	138	-.086	.023	-.009	-.205
340	139	-.054	.022	.022	-.150
340	140	-.052	.021	.031	-.166
340	141	-.053	.020	.017	-.170
340	142	-.076	.024	.027	-.202
340	143	-.046	.020	.040	-.144
340	144	-.055	.033	.071	-.368
340	145	-.028	.027	.134	-.159
340	146	-.094	.027	.006	-.254
340	147	-.045	.021	.038	-.139
340	148	-.057	.025	.038	-.213
340	149	-.059	.021	.012	-.159
340	150	-.084	.023	.002	-.180
340	151	-.066	.023	.022	-.171
340	152	-.051	.019	.051	-.175
340	153	-.054	.021	.034	-.279
340	154	-.081	.025	.022	-.447
340	155	-.054	.023	.047	-.339
340	156	-.055	.023	.042	-.140
340	157	-.076	.017	-.017	-.150
340	158	-.124	.025	-.053	-.332
340	159	-.092	.022	-.018	-.195
340	160	-.068	.023	.022	-.175
340	161	-.094	.018	-.039	-.183
340	162	-.127	.022	-.059	-.234
340	163	-.093	.021	-.014	-.198
340	164	-.074	.027	.011	-.195
340	165	-.067	.024	.019	-.168
340	166	-.089	.024	-.014	-.218
340	167	-.089	.028	.051	-.201

APPENDIX A -- PRESSURE DATA: CONFIGURATION A: MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
340	201	.036	.086	.450	-.184
340	202	.062	.075	.550	-.129
340	203	.043	.058	.370	-.128
340	204	-.070	.084	.426	-.400
340	205	-.091	.046	.204	-.312
340	206	-.068	.033	.141	-.229
340	207	-.087	.028	.063	-.217
340	208	-.091	.036	.208	-.216
340	209	-.060	.045	.262	-.195
340	210	-.061	.036	.177	-.213
340	211	-.054	.041	.130	-.241
340	212	-.123	.027	.018	-.236
340	213	-.088	.023	-.009	-.283
340	214	-.069	.026	.069	-.164
340	301	-.079	.021	-.017	-.194
340	302	-.150	.028	-.059	-.304
340	303	-.109	.025	-.043	-.276
340	304	-.104	.021	-.035	-.200
340	305	-.105	.019	-.039	-.172
340	306	-.134	.023	-.062	-.223
340	307	-.099	.019	-.038	-.173
340	308	-.065	.023	.018	-.242
340	309	-.099	.018	-.048	-.188
340	310	-.123	.022	-.055	-.227
340	311	-.090	.022	-.009	-.177
340	312	-.105	.022	-.031	-.208
340	313	-.086	.017	-.023	-.152
340	314	-.106	.021	-.030	-.191
340	315	-.077	.020	.009	-.168
340	316	-.063	.023	.011	-.375
340	317	-.042	.016	.016	-.123
340	318	-.075	.016	-.011	-.140
340	319	-.044	.014	.001	-.090
340	320	-.099	.022	-.030	-.200
340	401	-.043	.036	.190	-.205
340	402	-.012	.034	.229	-.132
340	403	-.093	.027	-.008	-.247
340	404	-.061	.024	.003	-.173
340	405	-.058	.021	.013	-.159
340	406	-.048	.018	.016	-.134
350	1	-.067	.038	.115	-.203
350	2	-.100	.022	.048	-.187
350	3	-.103	.021	-.010	-.190
350	4	-.097	.020	-.008	-.168
350	5	-.081	.034	.086	-.212
350	6	-.062	.028	.118	-.169
350	7	-.071	.047	.214	-.271
350	8	-.001	.041	.224	-.127
350	9	-.030	.037	.201	-.214
350	10	-.143	.042	.087	-.300

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
350	11	-.205	.068	.003	-.567
350	12	-.136	.041	.012	-.390
350	13	-.195	.068	.006	-.525
350	14	-.170	.047	.044	-.517
350	15	-.129	.035	-.026	-.309
350	16	-.106	.043	.084	-.401
350	17	-.091	.047	.075	-.445
350	18	-.101	.023	-.026	-.216
350	19	-.062	.028	.118	-.199
350	20	-.045	.033	.129	-.201
350	21	-.072	.025	.028	-.312
350	22	-.073	.021	.016	-.180
350	23	-.097	.029	.028	-.269
350	24	-.106	.032	.006	-.287
350	25	-.042	.037	.146	-.239
350	26	-.100	.030	.028	-.262
350	27	-.081	.024	.019	-.219
350	28	-.061	.024	.037	-.190
350	29	-.064	.021	.019	-.188
350	30	-.079	.019	.003	-.198
350	31	-.058	.028	.082	-.210
350	32	-.023	.033	.176	-.159
350	33	-.058	.032	.066	-.228
350	34	-.086	.019	-.015	-.169
350	35	-.075	.023	.003	-.217
350	36	-.052	.023	.030	-.186
350	37	-.039	.035	.108	-.170
350	38	-.059	.029	.118	-.178
350	39	-.089	.026	.044	-.253
350	40	.001	.054	.334	-.192
350	41	-.067	.025	.037	-.183
350	42	-.083	.022	.007	-.189
350	43	-.078	.021	.008	-.201
350	44	-.059	.022	.030	-.246
350	45	-.043	.027	.086	-.139
350	46	-.081	.019	.001	-.223
350	47	-.092	.028	-.003	-.284
350	48	-.065	.022	.021	-.186
350	49	-.062	.021	.050	-.194
350	50	-.150	.027	-.074	-.268
350	51	-.097	.021	-.020	-.173
350	52	-.108	.025	-.024	-.226
350	53	-.099	.025	-.016	-.216
350	54	-.112	.022	-.012	-.212
350	55	-.098	.028	-.012	-.233
350	56	-.071	.033	.134	-.224
350	57	-.053	.033	.090	-.219
350	101	-.128	.030	-.022	-.366
350	102	-.110	.021	-.037	-.194
350	103	-.084	.030	.055	-.233

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
350	104	-.120	.033	-.010	-.325
350	105	-.112	.020	-.033	-.205
350	106	-.101	.020	-.028	-.176
350	107	-.091	.021	-.010	-.168
350	108	-.091	.023	.006	-.214
350	109	-.105	.034	.053	-.273
350	110	-.140	.037	-.039	-.316
350	111	-.091	.022	-.010	-.208
350	112	-.162	.045	.008	-.385
350	113	-.185	.036	-.076	-.377
350	114	-.103	.023	-.012	-.192
350	115	-.120	.032	-.006	-.258
350	116	-.098	.028	.004	-.230
350	117	-.140	.026	-.063	-.244
350	118	-.194	.055	-.035	-.527
350	119	-.095	.027	-.001	-.215
350	120	-.101	.029	-.009	-.238
350	121	-.090	.022	-.015	-.208
350	122	-.101	.026	.043	-.250
350	123	-.070	.022	.072	-.178
350	124	-.086	.028	.024	-.445
350	125	-.075	.021	-.008	-.199
350	126	-.101	.022	-.030	-.250
350	127	-.067	.021	.015	-.167
350	128	-.075	.025	.044	-.271
350	129	-.057	.016	.019	-.119
350	130	-.088	.025	.082	-.223
350	131	-.081	.023	-.000	-.216
350	132	-.075	.022	-.002	-.185
350	133	-.061	.017	-.003	-.139
350	134	-.152	.041	-.032	-.453
350	135	-.080	.027	.038	-.268
350	136	-.061	.019	.011	-.145
350	137	-.070	.020	.008	-.162
350	138	-.096	.024	.022	-.205
350	139	-.068	.022	.029	-.156
350	140	-.065	.020	-.007	-.134
350	141	-.055	.020	.010	-.179
350	142	-.084	.023	-.003	-.223
350	143	-.058	.019	.006	-.126
350	144	-.071	.027	.036	-.245
350	145	-.046	.021	.050	-.124
350	146	-.096	.022	-.009	-.259
350	147	-.057	.019	.024	-.129
350	148	-.066	.024	.027	-.187
350	149	-.063	.021	.012	-.215
350	150	-.089	.023	-.003	-.203
350	151	-.071	.023	.013	-.203
350	152	-.065	.019	-.004	-.154
350	153	-.058	.022	.057	-.320

APPENDIX A -- PRESSURE DATA: CONFIGURATION A; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
350	154	-.088	.024	.032	-.441
350	155	-.065	.022	.040	-.275
350	156	-.069	.021	.007	-.205
350	157	-.070	.018	-.003	-.157
350	158	-.121	.026	-.032	-.253
350	159	-.092	.022	-.030	-.214
350	160	-.078	.023	.009	-.283
350	161	-.089	.019	-.035	-.248
350	162	-.124	.024	-.053	-.244
350	163	-.093	.024	-.016	-.205
350	164	-.082	.027	.016	-.223
350	165	-.071	.024	.005	-.170
350	166	-.085	.026	-.005	-.228
350	167	-.126	.025	-.027	-.240
350	201	.040	.091	.506	-.216
350	202	.068	.079	.469	-.105
350	203	.052	.065	.348	-.119
350	204	-.104	.068	.250	-.369
350	205	-.103	.044	.216	-.324
350	206	-.089	.029	.054	-.199
350	207	-.110	.037	.005	-.309
350	208	-.097	.036	.132	-.219
350	209	-.074	.036	.137	-.196
350	210	-.082	.031	.105	-.202
350	211	-.085	.037	.157	-.217
350	212	-.137	.035	-.009	-.389
350	213	-.107	.026	-.021	-.266
350	214	-.098	.021	-.016	-.178
350	301	-.082	.021	-.019	-.188
350	302	-.163	.031	-.084	-.378
350	303	-.119	.028	-.043	-.293
350	304	-.108	.023	-.042	-.218
350	305	-.107	.020	-.044	-.215
350	306	-.135	.023	-.064	-.239
350	307	-.103	.020	-.043	-.192
350	308	-.074	.023	.004	-.223
350	309	-.104	.019	-.046	-.186
350	310	-.129	.025	-.053	-.257
350	311	-.102	.027	-.014	-.230
350	312	-.115	.026	-.031	-.251
350	313	-.090	.020	-.017	-.199
350	314	-.108	.024	-.023	-.200
350	315	-.090	.024	-.000	-.196
350	316	-.063	.025	.011	-.253
350	317	-.051	.019	.003	-.131
350	318	-.091	.017	-.031	-.153
350	319	-.057	.016	-.006	-.113
350	320	-.107	.023	-.035	-.203
350	401	-.053	.037	.189	-.269
350	402	-.037	.026	.162	-.195
350	403	-.094	.025	-.011	-.254
350	404	-.059	.022	.037	-.197
350	405	-.064	.021	.022	-.173
350	406	-.057	.017	.011	-.148

APPENDIX A -- PRESSURE DATA: CONFIGURATION B; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
222	10	-.472	.126	-.164	-1.031
222	11	-.473	.096	-.228	-1.013
222	26	-.679	.113	-.378	-1.225
222	32	-.778	.151	-.257	-1.273
222	33	-.841	.137	-.466	-1.383
222	204	-.354	.056	-.183	-.608
222	403	-.286	.286	.454	-1.240
224	10	-.501	.132	-.174	-1.145
224	11	-.483	.096	-.238	-.950
224	26	-.682	.109	-.363	-1.265
224	32	-.761	.138	-.245	-1.336
224	33	-.826	.133	-.493	-1.313
224	204	-.368	.058	-.203	-.836
224	403	-.322	.271	.424	-1.290
226	10	-.516	.148	-.166	-1.140
226	11	-.510	.102	-.262	-.942
226	26	-.691	.109	-.408	-1.538
226	32	-.751	.135	-.190	-1.289
226	33	-.836	.138	-.429	-1.490
226	204	-.372	.063	-.204	-.792
226	403	-.369	.262	.384	-1.102
228	10	-.526	.135	-.175	-1.106
228	11	-.526	.101	-.291	-.996
228	26	-.689	.107	-.323	-1.165
228	32	-.742	.142	-.186	-1.250
228	33	-.812	.135	-.447	-1.357
228	204	-.386	.058	-.233	-.806
228	403	-.387	.262	.545	-1.254
230	10	-.537	.140	-.148	-1.346
230	11	-.548	.111	-.276	-1.074
230	26	-.692	.105	-.438	-1.321
230	32	-.752	.145	-.211	-1.526
230	33	-.799	.133	-.421	-1.382
230	204	-.395	.062	-.227	-.868
230	403	-.440	.269	.380	-1.458
232	10	-.572	.148	-.209	-1.244
232	11	-.576	.108	-.297	-1.056
232	26	-.710	.118	-.388	-1.319
232	32	-.745	.149	-.180	-1.274
232	33	-.809	.149	-.361	-1.389
232	204	-.419	.077	-.227	-1.145
232	403	-.485	.251	.310	-1.436
234	10	-.593	.150	-.217	-1.391
234	11	-.559	.107	-.311	-1.020
234	26	-.694	.111	-.405	-1.168
234	32	-.740	.142	-.299	-1.261
234	33	-.765	.132	-.417	-1.319
234	204	-.426	.076	-.226	-1.065
234	403	-.475	.246	.379	-1.362
236	10	-.602	.145	-.188	-1.249
236	11	-.596	.116	-.322	-1.250
236	26	-.709	.120	-.354	-1.496
236	32	-.716	.135	-.254	-1.479
236	33	-.754	.144	-.352	-1.352
236	204	-.437	.079	-.245	-1.036
236	403	-.497	.237	.333	-1.239
238	10	-.586	.140	-.169	-1.169
238	11	-.613	.109	-.312	-1.125
238	26	-.707	.120	-.398	-1.212
238	32	-.688	.134	-.232	-1.227
238	33	-.745	.142	-.350	-1.350
238	204	-.440	.079	-.258	-1.054
238	403	-.535	.227	.237	-1.285
240	10	-.610	.150	-.192	-1.515
240	11	-.625	.118	-.294	-1.153
240	26	-.707	.113	-.293	-1.422
240	32	-.698	.141	-.263	-1.330
240	33	-.723	.137	-.364	-1.359
240	204	-.468	.102	-.246	-1.199
240	403	-.539	.221	.330	-1.300
242	10	-.619	.141	-.229	-1.136
242	11	-.645	.120	-.331	-1.325
242	26	-.713	.114	-.394	-1.199
242	32	-.673	.132	-.171	-1.263
242	33	-.715	.138	-.360	-1.344
242	204	-.490	.114	-.297	-1.332
242	403	-.563	.210	.206	-1.324
244	10	-.609	.137	-.218	-1.261
244	11	-.647	.117	-.278	-1.223
244	26	-.700	.109	-.376	-1.154
244	32	-.661	.133	-.180	-1.226
244	33	-.677	.128	-.318	-1.152
244	204	-.492	.103	-.249	-1.115
244	403	-.573	.208	.167	-1.271
246	10	-.464	.131	-.140	-1.235
246	11	-.535	.124	-.246	-1.122
246	26	-.542	.121	-.208	-1.050
246	32	-.484	.120	.018	-.996
246	33	-.505	.125	-.206	-1.117
246	204	-.418	.119	-.142	-1.133
246	403	-.441	.178	.155	-1.119
248	10	-.428	.117	-.080	-1.247
248	11	-.524	.120	-.224	-1.074
248	26	-.519	.122	-.117	-1.095
248	32	-.470	.127	-.100	-1.019
248	33	-.477	.123	-.211	-1.098
248	204	-.394	.117	-.129	-1.078
248	403	-.446	.164	.165	-1.272
250	10	-.453	.126	-.113	-1.187
250	11	-.544	.124	-.233	-1.095
250	26	-.530	.115	-.184	-1.315
250	32	-.459	.120	-.110	-1.081
250	33	-.478	.119	-.224	-1.035
250	204	-.434	.141	-.052	-1.324
250	403	-.438	.167	.159	-1.343
252	10	-.445	.136	-.075	-1.255
252	11	-.555	.139	-.232	-1.333
252	26	-.499	.121	-.131	-1.160
252	32	-.420	.114	-.026	-1.003
252	33	-.440	.121	-.171	-1.070
252	204	-.456	.154	-.014	-1.467
252	403	-.428	.151	.300	-1.066
254	10	-.425	.130	-.112	-1.252
254	11	-.586	.150	-.225	-1.396
254	26	-.488	.113	-.156	-.961
254	32	-.416	.114	-.090	-1.044
254	33	-.422	.108	-.182	-1.115
254	204	-.463	.154	.101	-1.328
254	403	-.428	.139	.141	-1.291
256	10	-.424	.131	-.121	-1.191
256	11	-.575	.145	-.202	-1.336
256	26	-.490	.117	-.140	-1.165
256	32	-.419	.116	-.093	-.916
256	33	-.421	.107	-.178	-.957
256	204	-.462	.162	.028	-1.221
256	403	-.446	.144	.081	-1.163
258	10	-.414	.130	-.036	-1.196
258	11	-.543	.126	-.226	-1.173
258	26	-.481	.115	-.167	-.987
258	32	-.398	.112	-.012	-1.018
258	33	-.410	.109	-.163	-1.045
258	204	-.459	.180	.026	-1.283
258	403	-.427	.140	.168	-1.122
260	10	-.434	.135	-.013	-1.133
260	11	-.489	.143	-.101	-1.145
260	26	-.493	.112	-.064	-1.176
260	32	-.388	.108	-.013	-.981
260	33	-.412	.104	-.196	-1.020
260	204	-.391	.168	.107	-1.178
260	403	-.433	.132	.066	-1.003
262	10	-.404	.132	-.071	-1.135
262	11	-.467	.134	-.166	-1.051
262	26	-.469	.121	-.082	-1.014
262	32	-.383	.110	-.084	-.921
262	33	-.389	.103	-.165	-1.004
262	204	-.359	.170	.266	-1.118
262	403	-.436	.137	.024	-1.135
264	10	-.376	.125	.037	-1.188
264	11	-.456	.122	-.118	-1.123
264	26	-.464	.111	.117	-.968

APPENDIX A -- PRESSURE DATA: CONFIGURATION B; MILLION DOLLAR PIER, ATLANTIC CITY

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
264	32	-.367	.111	-.126	-1.094
264	33	-.382	.099	-.142	-1.092

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
264	204	-.343	.167	172	-1.007

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
264	403	-.416	.131	.102	-1.049