WIND-TUNNEL STUDY OF INTERCONTINENTAL HOTEL, SAN DIEGO

by

J. A. Peterka* and J. E. Cermak**

for

Hope Engineers 1475 Sixth Avenue P.O. Box 2488 San Diego, California 92112

Fluid Mechanics and Wind Engineering Program Fluid Dynamics and Diffusion Laboratory Department of Civil Engineering Colorado State University Fort Collins, Colorado 80523

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*Associate Professor **Professor-in-Charge, Fluid Mechanics and Wind Engineering Program

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LIST OF SYMBOLS

Symbol	Definition
U	Local mean velocity
D	Characteristic dimension (building height, width, etc.)
ν, ρ	Kinematic viscosity and density of approach flow
	Reynolds number
E	Mean voltage
A, B, n	Constants
U rms	Root-mean-square of fluctuating velocity
^E rms	Root-mean-square of fluctuating voltage
U_	Reference mean velocity outside the boundary layer
Χ, Υ	Horizontal coordinates
Z	Height above surface
δ	Height of boundary layer
T _u	Turbulence intensity $\frac{U_{rms}}{U_{\infty}}$ or $\frac{U_{rms}}{U}$
C Pmean	Mean pressure coefficient, $\frac{(p-p_{\infty})_{mean}}{0.5 \rho V_{\infty}^2}$
C _p rms	Root-mean-square pressure coefficient, $\frac{((p-p_{\infty})-(p-p_{\infty})_{mean})_{rms}}{0.5 \rho U_{\infty}^{2}}$
C _{pmax}	Peak maximum pressure coefficient, $\frac{(p-p_{\infty})_{max}}{0.5 \rho U_{\infty}^2}$
C _{pmin}	Peak minimum pressure coefficient, $\frac{(p-p_{\infty})_{\min}}{0.5 \rho U_{\infty}^2}$
() _{min}	Minimum value during data record
() _{max}	Maximum value during data record

SymbolDefinitionpFluctuating pressure at a pressure tap on the structure p_{∞} Static pressure in the wind tunnel above the model F_x , F_y Forces in X, Y direction A_R Reference Area CF_χ Force coefficient, X direction, $\frac{F_x}{A_R 0.5\rho U_{\infty}^2}$ CF_γ Force coefficient, Y direction, $\frac{F_y}{A_R 0.5\rho U_{\infty}^2}$

1. INTRODUCTION

1.1 General

A significant characteristic of modern building design is lighter cladding and more flexible frames. These features produce an increased vulnerability of glass and cladding to wind damage and result in larger deflections of the building frame. In addition, increased use of pedestrian plazas at the base of the buildings has brought about a need to consider the effects of wind and gustiness in the design of these areas.

The building geometry itself may increase or decrease wind loading on the structure. Wind forces may be modified by nearby structures which can produce beneficial shielding or adverse increases in loading. Overestimating loads results in uneconomical design; underestimating may result in cladding or window failures. Tall structures have historically produced unpleasant wind and turbulence conditions at their bases. The intensity and frequency of objectionable winds in pedestrian areas is influenced both by the structure shape and by the shape and position of adjacent structures.

Techniques have been developed for wind tunnel modeling of proposed structures which allow the prediction of wind pressures on cladding and windows, overall structural loading, and also wind velocities and gusts in pedestrian areas adjacent to the building. Information on sidewalklevel gustiness allows plaza areas to be protected by design changes before the structure is constructed. Accurate knowledge of the intensity and distribution of the pressures on the structure permits adequate but economical selection of cladding strength to meet selected maximum design winds and overall wind loads for the design of the frame for flexural control. Modeling of the aerodynamic loading on a structure requires special consideration of flow conditions in order to guarantee similitude between model and prototype. A detailed discussion of the similarity requirements and their wind-tunnel implementation can be found in references (1), (2), and (3). In general, the requirements are that the model and prototype be geometrically similar, that the approach mean velocity at the building site have a vertical profile shape similar to the fullscale flow, that the turbulence characteristics of the flows be similar, and that the Reynolds number for the model and prototype be equal.

These criteria are satisfied by constructing a scale model of the structure and its surroundings and performing the wind tests in a wind tunnel specifically designed to model atmospheric boundary-layer flows. Reynolds number similarity requires that the quantity UD/v be similar for model and prototype. Since v, the kinematic viscosity of air, is identical for both, Reynolds numbers cannot be made precisely equal with reasonable wind velocities. To accomplish this the air velocity in the wind tunnel would have to be as large as the model scale factor times the prototype wind velocity, a velocity which would introduce unacceptable compressibility effects. However, for sufficiently high Reynolds numbers (>2x10⁴) the pressure coefficient at any location on the structure will be essentially constant for a large range of Reynolds numbers. Typical values encountered are $10^7 - 10^8$ for the full-scale and $10^5 - 10^6$ for the wind-tunnel model. In this range acceptable flow similarity is achieved without precise Reynolds number equality.

1.2 The Wind-Tunnel Test

The wind-engineering study is performed on a building or building group modeled at scales ranging from 1:150 to 1:400. The building model

is constructed of clear plastic fastened together with screws. The structure is modeled in detail to provide accurate flow patterns in the wind passing over the building surfaces. The building under test is often located in a surrounding where nearby buildings or terrain may provide beneficial shielding or adverse wind loading. To achieve similarity in wind effects the area surrounding the test building is also modeled. A flow visualization study is first made (smoke is used to make the air currents visible) to define overall flow patterns and identify regions where local flow features might cause difficulties in building curtain-wall design or produce pedestrian discomfort.

The test model, equipped with pressure taps (200 to 600 or more), is exposed to an appropriately modeled atmospheric wind in the wind tunnel and the fluctuating pressure at each tap measured electronically. The model, and the modeled area, are rotated 10 or 15 degrees and another set of data recorded for each pressure tap. Normally, 24 or 36 sets of data (360 degrees of turning) are taken; however, when flow visualization or recorded data indicate high pressure regions of small azimuthal extent, data is obtained in smaller azimuthal steps.

Data are recorded, analyzed and processed by an on-line computerized data-acquisition system. Pressure coefficients of several types are calculated by the computer for each reading on each piezometer tap and are printed in tabular form as computer readout. Using wind data applicable to the building site, representative wind velocities are selected for combination with measured pressures on the building model. Integration of test data with wind data results in prediction of peak local wind pressures for design of glass or cladding and may include overall forces and moments on the structure (by floor if desired) for design of

the structural frame. Pressure contours are drawn on the developed building surfaces showing the intensity and distribution of peak wind loads on the building. These results may be used to divide the building into zones where lighter or heavier cladding or glass may be desirable.

Based on the visualization (smoke) tests and on a knowledge of heavy pedestrian use areas, a dozen or more locations may be chosen at the base of the building where wind velocities can be measured to determine the relative comfort or discomfort of pedestrians in plaza areas, near building entrances, near building corners, or on sidewalks. Usually a reference pedestrian position is also tested to determine whether the wind environment in the building area is better or worse than the environment a block or so away in an undisturbed area.

The following pages discuss in greater detail the procedures followed and the equipment and data collecting and processing methods used. In addition, the data presentation format is explained and the implications of the data are discussed.

2. EXPERIMENTAL CONFIGURATION

2.1 Wind Tunnel

Wind-engineering studies are performed in the Fluid Dynamics and Diffusion Laboratory at Colorado State University (Figure 1). Three large wind tunnels are available for wind loading studies depending on the detailed requirements of the study. The wind tunnel used for this investigation is shown in Figure 2. All tunnels have a flexible roof adjustable in height to maintain a zero pressure gradient along the test section. The mean velocity can be adjusted continuously in each tunnel to the maximum velocity available.

2.2 Model

In order to obtain an accurate assessment of local pressures using piezometer taps, models are constructed to the largest scale that does not produce significant blockage in the wind-tunnel test section. The models are constructed of 1/2 in. thick Lucite plastic and fastened together with metal screws. Significant variations in the building surface, such as mullions, are machined into the plastic surface. Piezometer taps (1/16 in. diameter) are drilled normal to the exterior vertical surfaces in rows at several or more elevations between the bottom and top of the building. Similarly, taps are placed in the roof and on any sloping, protruding, or otherwise distinctive features of the building that might need investigation.

Pressure tap locations are chosen so that the entire surface of the building can be investigated for pressure loading and at the same time permit critical examination of areas where experience has shown that maximum wind effects may be expected to occur. Locations of the pressure taps for this study are shown in Figure 3. Dimensions are

given both for full-scale building (in ft) and for model (in in.). The pressure tap numbers are shown adjacent to the taps.

The pressure tests are sometimes made in two stages. In the first stage measurements are made on the initial distribution of pressure taps. If it becomes apparent from the data that the loading on the building is being influenced by some unsuspected geometry of the building or adjacent structures, additional pressure taps are installed in the critical areas. The locations of the taps are selected so that the maximum loading can be detected and the area over which this loading is acting can be defined. Any added taps are also shown in Figure 3.

A circular area 750 to 2000 ft in radius depending on model scale and characteristics of the surrounding buildings and terrain is modeled in detail. Structures within the modeled region are made from styrofoam and cut to the individual building geometries. They are mounted on the turntable in their proper locations. Significant terrain features are included as needed. The model is mounted on a turntable (Figure 2) near the downwind end of the test section. Any buildings or terrain features which do not fit on the turntable are placed on removable pieces which are placed upwind of the turntable for appropriate wind directions. A plan view of the building and its surroundings is shown in Figure 4. The turntable is calibrated to indicate azimuthal orientation to 0.1 degree.

The region upstream from the modeled area is covered with a randomized roughness constructed using various sized cubes placed on the floor of the wind tunnel. Different roughness sizes may be used for different wind directions. Spires are installed at the test-section entrance to provide a thicker boundary layer than would otherwise be

available. The thicker boundary layer permits a somewhat larger scale model than would otherwise be possible. The spires are approximately triangularly shaped pieces of 1/2 in. thick plywood 6 in. wide at the base and 1 in. wide at the top, extending from the floor to the top of the test section. They are placed so that the broad side intercepts the flow. A barrier approximately 8 in. high is placed on the testsection floor downstream of the spires to aid in development of the boundary-layer flow.

The distribution of the roughness cubes and the spires in the roughened area was designed to provide a boundary-layer thickness of approximately 4 ft, a velocity profile power-law exponent similar to that expected to occur in the region approaching the modeled area for each wind direction (a number of wind directions may have the same approach roughness). A photograph of the completed model in the wind tunnel is shown in Figure 5. The wind-tunnel ceiling is adjusted after placement of the model to obtain a zero pressure gradient along the test section.

3. INSTRUMENTATION AND DATA ACQUISITION

3.1 Flow Visualization

Making the air flow visible in the vicinity of the model is helpful (a) in understanding and interpreting mean and fluctuating pressures, (b) in defining zones of separated flow and reattachment and zones of vortex formation where pressure coefficients may be expected to be high and (c) in indicating areas where pedestrian discomfort may be a problem. Titanium tetrachloride smoke is released from sources on and near the model to make the flow lines visible to the eye and to make it possible to obtain motion picture records of the tests. Conclusions obtained from these smoke studies are discussed in Sections 4.1 and 5.1.

3.2 Pressures

Mean and fluctuating pressures are measured at each of the pressure taps on the model structure. Data are obtained for 24 or 36 wind directions, rotating the entire model assembly in a complete circle. Seventysix pieces of 1/16 in. I.D. plastic tubing are used to connect 76 pressure ports at a time to an 80 tap pressure switch mounted inside the model. The switch was designed and fabricated in the Fluid Dynamics and Diffusion Laboratory to minimize the attenuation of pressure fluctuations across the switch. Each of the 76 measurement ports is directed in turn by the switch to one of four pressure transducers mounted close to the switch. The four pressure input taps not used for transmitting building surface pressures are connected to a common tube leading outside the wind tunnel. This arrangement provides both a means of performing in-place calibration of the transducers and, by connecting this tube to a pitot tube mounted inside the wind tunnel, a means of automatically monitoring the tunnel speed. The switch is operated by means of a shaft projecting through

the floor of the wind tunnel. A computer-controlled stepping motor steps the switch into each of the 20 required positions. The computer keeps track of switch position but a digital readout of position is provided at the wind tunnel.

The pressure transducers used are setra differential transducers (Model 237) with a 0.10 psid range. Reference pressures are obtained by connecting the reference sides of the four transducers, using plastic tubing, to the static side of a pitot-static tube mounted in the wind tunnel free stream above the model building. In this way the transducer measures the instantaneous difference between the local pressures on the surface of the building and the static pressure in the free stream above the model.

Output from the pressure transducers is fed to an on-line data acquisition system consisting of a Hewlett-Packard 21 MX computer, disk unit, card reader, printer, Digi-Data digital tape drive and a Preston Scientific analog-to-digital converter. The data are processed immediately into pressure coefficient form as described in Section 4.3 and stored for printout or further analysis.

All four transducers are recorded simultaneously for 16 seconds at a 250 sample per second rate. The results of an experiment to determine the length of record required to obtain stable mean and rms (root-meansquare) pressures and to determine the overall accuracy of the pressure data acquisition system is shown in Figure 6. A typical pressure port record was integrated for a number of different time periods to obtain the data shown. Examination of a large number of pressure taps showed that the overall accuracy for a 16 second period is, in pressure coefficient form, 0.03 for mean pressures, 0.1 for peak pressures, and 0.01 for rms pressures. Pressure coefficients are defined in Section 4.3.

3.3 Velocity

Mean velocity and turbulence intensity profiles are measured upstream of the model to determine that an approach boundary-layer flow appropriate to the site has been established. Tests are made at one wind velocity in the tunnel. This velocity is well above that required to produce Reynolds number similarity between the model and the prototype as discussed in Section 1.1.

In addition, mean velocity and turbulence intensity measurements are made 5 to 7 ft (prototype) above the surface at a dozen or more locations on and near the building for 16 wind directions. The measurement locations are shown on Figure 4. The surface measurements are indicative of the wind environment to which a pedestrian at the measurement location would be subjected. The locations are chosen to determine the degree of pedestrian comfort or discomfort at the building corners where relatively severe conditions frequently are found, near building entrances and on adjacent sidewalks where pedestrian traffic is heavy, and in open plaza areas. In most studies a reference pedestrian position, located about a block away, is also tested. These data are helpful in evaluating the degree of pedestrian comfort or discomfort in the proposed plaza area in terms of the undisturbed environment in the immediate vicinity.

Measurements are made with a single hot-wire anemometer mounted with its axis vertical. The instrumentation used is a Thermo Systems constant temperature anemometer (Model 1050) with a 0.001 in. diameter platinum film sensing element 0.020 in. long. Output is directed to the on-line data acquisition system for analysis.

Calibration of the hot-wire anemometer is performed by comparing output with the pitot-static tube in the wind tunnel. The calibration

data are fit to a variable exponent King's Law relationship of the form

$$E^2 = A + BU^n$$

where E is the hot-wire output voltage, U the velocity and A, B, and n are coefficients selected to fit the data. The above relationship was used to determine the mean velocity at measurement points using the measured mean voltage. The fluctuating velocity in the form $U_{\rm rms}$ (root-mean-square velocity) was obtained from

$$U_{\rm rms} = \frac{2 E E_{\rm rms}}{B n U^{n-1}}$$

where E_{rms} is the root-mean-square voltage output from the anemometer. For interpretation all turbulence measurements for pedestrian winds were divided by the mean velocity outside the boundary-layer U_{∞} . Turbulence intensity in velocity profile measurements used the local mean velocity.

4. **RESULTS**

4.1 Flow Visualization

A film is included as part of this report showing the characteristics of flow about the structure using smoke to make the flow visible. A listing of the contents of the film is shown in Table 1. Several features can be noted from the visualization. As with all large structures, wind approaching the building is deflected down to the plaza level, up over the structure and around the sides. A description of the smoke test results emphasizing flow patterns of concern relative to possible high-wind load areas and pedestrian comfort is given in Section 5.1.

4.2 Velocity

Velocity and turbulence profiles are shown in Figure 7. Profiles were taken upstream from the model which are characteristic of the boundary layer approaching the model and sometimes at the building site with building removed. The boundary-layer thickness, δ , is shown in Figure 7. The corresponding prototype value of δ for this study is also shown in the figure. This value was established as a reasonable height for this study. The mean velocity profile approaching the modeled area has the form

$$\frac{U}{U_m} = \left(\frac{z}{\delta}\right)^n.$$

The exponent n for the approach flow established for this study is shown in Figure 7.

Profiles of longitudinal turbulence intensity in the flow approaching the modeled area are shown in Figure 7. The turbulence intensities are appropriate for the approach mean velocity profile selected. For the velocity profiles, turbulence intensity is defined

as the root-mean-square about the mean of the longitudinal velocity fluctuations divided by the local mean velocity U,

$$Tu = \frac{U}{U}.$$

Velocity data obtained at each of the pedestrian measurement locations shown in Figure 4 are listed in Table 2 as mean velocity U/U_{∞} , turbulence intensity U_{rms}/U_{∞} , and largest effective gust

$$U_{pk} = \frac{U + 3U_{rms}}{U_{\infty}}$$

These data are plotted in polar form in Figure 8. Measurements were taken 5 to 7 ft above the ground surface. A site map is superimposed on the polar plots to aid in visualization of the effects of the nearby structures on the velocity and turbulence magnitudes. An analysis of these wind data is given in Section 5.2.

To enable a quantitative assessment of the wind environment, the wind-tunnel data were combined with wind frequency and direction information obtained at the local airport. Table 3 shows wind frequency by direction and magnitude obtained from summaries published by the National Weather Service. These data, usually obtained at an elevation of about 30-40 ft, were converted to velocities at the reference velocity height for the wind-tunnel measurements and combined with the wind-tunnel data to obtain cumulative probability distributions (percent time a given velocity is exceeded) for wind velocity at each measuring location. The percentage times were summed by wind direction to obtain a percent time exceeded at each measuring position independent of wind direction (but accounting for the fact that the wind blows from different directions with varying frequency). These results are plotted in Figure 9.

Interpretation of Figure 9 is aided by a description of the effects of wind of various magnitudes on people. The earliest quantitative description of wind effects was established by Sir Francis Beaufort in 1806 for use at sea and is still in use today. Several recent investigators have added to the knowledge of wind effects on pedestrians. These investigations along with suggested criteria for acceptance have been summarized by Penwarden and Wise (4) and Melbourne (5). The Beaufort scale (from ref. 4), based on mean velocity only, is reproduced as Table 4 including qualitative descriptions of wind effects. Table 4 suggests that mean wind speeds below 12 mph are of minor concern and that mean speeds above 24 mph are definitely inconvenient. Quantitative criteria for acceptance from reference 5 are superimposed as dashed lines on Figure 9. The peak gust curves shown in Figure 9 are the percent of time during which a short gust of the stated magnitude could occur (say about one of these gusts per hour). Implications of the data plotted in Figure 9 are presented in Section 5.2.

Because some pedestrian wind measuring positions are purposely chosen at sites where the smoke tests showed large velocities of small spacial extent, the general wind environment about the structure may be less severe than one might infer from a strict analysis of Table 2 and Figure 9.

4.3 Pressures

For each of the pressure taps examined at each wind direction, the data record is analyzed to obtain four separate pressure coefficients. The first is the mean pressure coefficient

$$C_{p_{mean}} = \frac{(p - p_{\infty})_{mean}}{0.5 \rho U_{\infty}^2}$$

where the symbols are as defined in the List of Symbols. It represents the mean of the instantaneous pressure difference between the building pressure tap and the static pressure in the wind tunnel above the building model, nondimensionalized by the dynamic pressure

$$0.5 \rho U_{\omega}^2$$

at the reference velocity position. This relationship produces a dimensionless coefficient which indicates that the mean pressure difference between building and ambient wind at a given point on the structure is some fraction less or some fraction greater than the undisturbed wind dynamic pressure near the upper edge of the boundary layer. Using the measured coefficient, prototype mean pressure values for any wind velocity may be calculated.

The magnitude of the fluctuating pressure is obtained by the rms pressure coefficient

$$C_{p_{rms}} = \frac{((p-p_{\infty}) - (p-p_{\infty})_{mean})_{rms}}{0.5 \rho U_{\infty}^{2}}$$

in which the numerator is the root-mean-square of the instantaneous pressure difference about the mean.

If the pressure fluctuations followed a Gaussian probability distribution, no additional data would be required to predict the frequency with which any given pressure level would be observed. However, the pressure fluctuations do not, in general, follow a Gaussian probability distribution so that additional information is required to show the extreme values of pressure expected. The peak maximum and peak minimum pressure coefficients are used to determine these values:

$$C_{p_{\max}} = \frac{(p - p_{\infty})_{\max}}{0.5 \rho U_{\infty}^{2}}$$

$$C_{p_{\min}} = \frac{(p - p_{\omega})_{\min}}{0.5 \rho U_{\omega}^2}$$

The values of $p-p_{\infty}$ which were digitized at 250 samples per second for 16 seconds, representing about one hour of time in the full-scale, are examined individually by the computer to obtain the most positive and most negative values during the 16-second period. These are converted to $C_{p_{max}}$ and $C_{p_{min}}$ by nondimensionalizing with the free stream dynamic pressure.

The four pressure coefficients are calculated by the on-line data acquisition system computer and tabulated along with the approach wind azimuth in degrees from true north. The list of coefficients is included as Appendix A. The pressure tap code numbers used in the appendix are explained in Figure 3.

To determine the largest peak loads acting at any point on the structure for cladding design purposes, the pressure coefficients for all wind directions were searched to obtain, at each pressure tap, the largest peak positive and peak negative pressure coefficients. Table 6 lists the larger values and associated wind directions. Included in Section 5.3 is an analysis of the coefficients of Table 6 including the maximum values obtained and where they occurred on the building.

The pressure coefficients of Table 6 can be converted to full-scale loads by multiplication by a suitable reference pressure selected for the field site. This reference pressure is represented in the equations for pressure coefficients by the $0.5 \rho U_m^2$ denominator. This value is the dynamic pressure associated with an hourly mean wind at the reference velocity measurement position at the edge of the boundary layer. In general, the method of arriving at a design reference pressure for a particular site involves selection of a design wind velocity, translation of the velocity to an hourly mean wind at the reference velocity location and conversion to a reference pressure. Selection of the design velocity can be made from statistical analysis of extreme wind data or selected from wind maps contained in the proposed wind loading code ANSI A58.1 of the American National Standards Institute (6). The calculation of reference pressure for this study is shown in Table 5. The factor used in Table 5 to reduce gust winds to hourly mean winds is given in reference (7).

The reference pressure associated with the design hourly mean velocity at the reference velocity location can be used directly with the peak-pressure coefficients to obtain peak local design wind loads for cladding design. Local, instantaneous peak loads on the full-scale building suitable for cladding design were computed by multiplying the reference pressure of Table 5 by the peak coefficients of Table 6 and are listed as peak pressures in that table. The maximum psf loads given at each tap location are the largest peak positive and peak negative values found in the tests. For ease in visualizing the loads on the structure, contours of equal peak pressures for cladding load shown in Table 6 have been plotted on developed elevation views of the structure,

Figure 10. If a data point which is taken in the basic model configuration is retaken in a resolution configuration, the data are averaged in preparing Figure 10. For control of water infiltration from outside to inside, the largest positive (inward-acting) pressure at each tap location is tabulated in Table 6.

For glass design pressures, a glass load factor is used to account for the different duration between measured peak pressures and the one minute loading commonly used in glass design charts. The design pressure used for glass is normally less than the peak pressures used for cladding design because of the static fatigue property of glass which can withstand higher pressures for short duration loads than for long duration Recent research (8) indicates that the period of application of loads. the peak pressures reported herein is about 5-10 seconds or less. If a glass design is based on these peak-pressure values, then a glass strength associated with this duration load should be used. Because glass design charts are normally based on some alternate load duration -usually one minute -- then some reduction in peak loads should be made. An estimate of a load reduction factor can be obtained from an empirical relation of glass strength as a function of load duration. Current glass selection charts showing glass strength as a function of load duration (9) and older references (10) indicate the following load reduction factors: rof 10 maf 0

	rei 9	rei iu
annealed float	0.80	0.81
heat strengthened	0.94	
tempered	0.97	0.98

Loadings appropriate for glass design can be computed by multiplying the peak-pressure loads of Table 6 by these load factors.

4.4 Forces and Moments

Force coefficients in the horizontal X and Y directions and moment coefficients about the X, Y, and Z axes with the origin at ground level at the base of the building with Z axis vertical may be computed for all wind directions tested by integration of mean pressures on the building. Overall forces and moments acting on the full-scale building due to wind loading which are useful in designing the structural framing of the proposed building may be obtained from use of these coefficients.

Force coefficients were computed for each floor for each wind direction using the equations shown below.

$$CF_{\chi} = \frac{F_{\chi}}{A_{R} 0.5 \rho U_{\infty}^{2}}$$
 $CF_{\gamma} = \frac{F_{\gamma}}{A_{R} 0.5 \rho U_{\infty}^{2}}$

Terms and symbols used in the equations are defined in the List of Symbols and the axes are defined for the building in Figure 3. Force coefficients CF_{χ} and CF_{γ} were computed for the horizontal forces acting along the X and Y axes using the mean pressure coefficient at each pressure tap. A_{R} represents a constant reference area for nondimensionalization of the forces and moments.

The total forces acting on the full-scale building for each floor and wind direction were computed by multiplying the above coefficients by the appropriate full-scale reference area, by the reference pressure of Table 5, and by a gust load factor selected for an appropriate wind gust duration. The gust load factor, shown in Table 5, was selected to increase the loads from an hourly mean load to that of a gust whose duration would be sufficient for its effect to be fully felt by the structure. A table of gust load factors for various gust durations is

incorporated in Table 5 so that force and moment data of Table 7 may be adjusted to a different load duration if desired.

The forces obtained at each floor were used to obtain load, shear, and moment diagrams for the building for each wind direction. The shear diagram, in kips, was obtained by algebraic sum of all forces in each coordinate direction acting above the floor of interest. The load diagram, in psf, was obtained by dividing the shear values by their contributing areas (listed in Table 7). The moment diagram, in 1000 ftkips, was obtained by integration of the shear values so that the moment due to forces acting above the floor level of interest was calculated. The sign of the moment was established by the right-hand rule about an X', Y' axis through the floor of interest. Moments about the Z axis were calculated by considering the displacement of forces in the X and Y directions from the Z axis shown in Figure 3. Eccentricities were computed such that the product of the Y force and X eccentricity minus the product of the X force and Y eccentricity equaled the Z moment. Load, shear, and moment diagrams are shown in Figure 11 for several wind directions.

5. DISCUSSION

5.1 Flow Visualization

Flow patterns identified with smoke showed that the largest pressures on the Intercontinental Hotel building would probably be found near the east and west ends of the building due to flow separation at the vertices at the building ends. Curvature in the separated flow streamlines indicated the possibility of high negative (outward-acting) peak pressures. The presence of the twin structure to the southeast increased curvature in the separated flow streamlines, an indication that higher pressures are likely with the adjacent building in place.

Wind speeds in the vicinity of the Intercontinental Hotel showed that wind speeds at the base of the tower at the west end of the building were larger than those in open areas away from the building. Winds in the opening under the connector between the two towers did not appear to be larger than those in open areas.

5.2 Pedestrian Winds

Pedestrian winds were measured with both towers in place. Figure 4 shows both tower locations and the 21 locations selected for investigation of pedestrian wind comfort. Location 1 was selected as a reference location which should be reasonably undisturbed by presence of the Intercontinental Hotel structures. Table 2 and Figure 8 show that the largest values of mean velocity were measured at locations 13, 18 and 19 with values ranging from 58 to 79 percent of U_{∞} , the mean velocity at the edge of the boundary layer. For comparison, reference location 1 experienced a maximum mean velocity of 50 percent of U_{∞} while an open area such as location 20 experienced a value of 46 percent.

The largest values of fluctuating velocity, $U_{\rm rms}$, were measured at location 17 with values ranging from 21 to 28 percent of U_{∞} . These values are typical of a built-up environment. The largest values of peak gust, represented by the mean plus 3 rms as discussed in Section 4.2, were measured at locations 16, 17 and 18 near and under the small structure near the harbor. These largest peak gusts were measured at several wind directions for each of the three locations.

Velocity data of Table 2 integrated with local wind data listed in Table 3 are shown in Figure 9. Based on the data of this figure, the windiest location for mean winds is predicted to be location 18 which exceeded the criteria for walking comfort 30 percent of the time and the upper limit of acceptability 3 percent of the time. Location 17 was the windiest from the standpoint of peak gusts, exceeding the criteria for walking comfort about 8 percent of the time. Other locations which exceeded the comfort criteria for walking more than 3 percent of the time included 3, 8, 13, 19 and 20. Other locations had more moderate winds.

Wind speeds about the Intercontinental Hotel should be interpreted in light of winds measured at reference location 1 and winds measured in an open area such as location 20. It is likely that wind speeds near the Intercontinental Hotel will not cause significant pedestrian discomfort with the exception of the areas near the small building by the harbor (locations 16, 17, 18 and 19) and possibly in the immediate vicinity of location 13 at the west end of the building. Alterations to the geometry of the small building near locations 16-19 should be considered to reduce wind speeds at those locations. Improvement of the wind environment at location 13 will be more difficult because the

winds result from the mass of the tower structure. Corrective action at location 13 may not be needed, depending on anticipated activities, and should probably be delayed until assessment by users can be evaluated.

5.3 Pressures

Table 6 shows the largest peak pressure coefficients and corresponding loads measured on the building for each pressure tap location. Data identified as Configuration A in Table 6 and Appendix A represent data obtained at all tap locations on the Intercontinental Hotel for 36 wind directions with the proposed east tower in place. Configuration C represents similar data but with the east tower removed. Configuration B represents data obtained at selected taps at 2-degree azimuthal increments near azimuths where large pressure peaks were observed in Configuration A to ensure that the largest peaks were obtained. Configuration D was 2-degree resolution data for Configuration C.

The largest peak pressure coefficient measured on the hotel for Configuration A or C was -3.2 obtained at tap 275 on the south face at the east end of the building with the east tower in place. Flow visualization indicated the possibility of elevated pressures in this region. This pressure coefficient represents, using the 50-year recurrence wind reference pressure of Table 5, a peak cladding pressure of -85 psf, an outward-acting pressure. Figure 10 shows that most of the surface area of the building had pressures in the 30 to 40 psf range.

For wind directions giving the largest peak negative loads near the two ends of the building, peak positive pressures are at or near their peak values on the opposite face of the building just around the corner. Research on other buildings indicates that the peak positive pressure on one face and peak negative pressure on the opposite face just around the

corner are likely to occur simultaneously. Because rooms at the vertices connect both sides of the structure, an open or broken window on one face of the building would cause both the positive and negative pressures to act together on the closed face of the building substantially increasing the load on the curtain wall on the closed side of the room. Under these conditions, the 50-year design load for a single face can be exceeded on the closed side of the room for a wind speed which is substantially smaller than the 50-year wind. Consideration should be given to this possibility for doubling-up of pressures for the end bays where both facades are joined by a single room.

Figure 11 shows load, shear and moment distributions plotted from Table 7 for wind directions where the maximum shear was measured in the X and Y coordinate directions. For maximum loads in the Y direction, a substantial portion of the maximum load in the X direction remained. Torsional moments on the building, shown in Table 7, were of significant magnitude, but did not tend to occur at the same wind directions as the maximum flexural moments.

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FIGURES

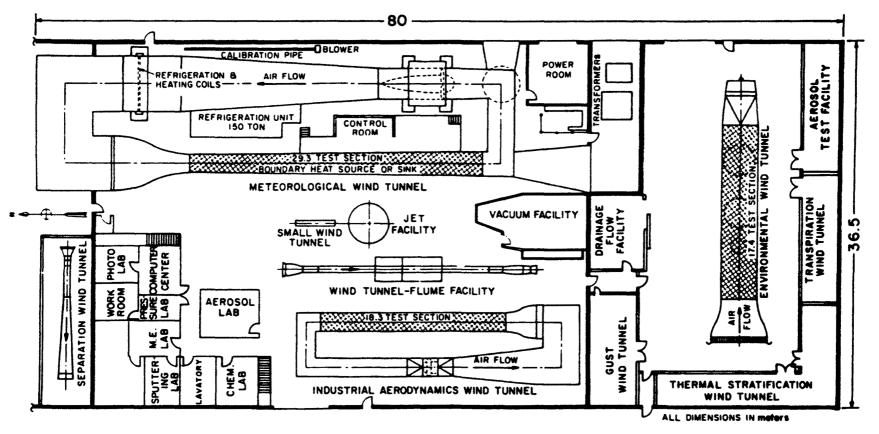
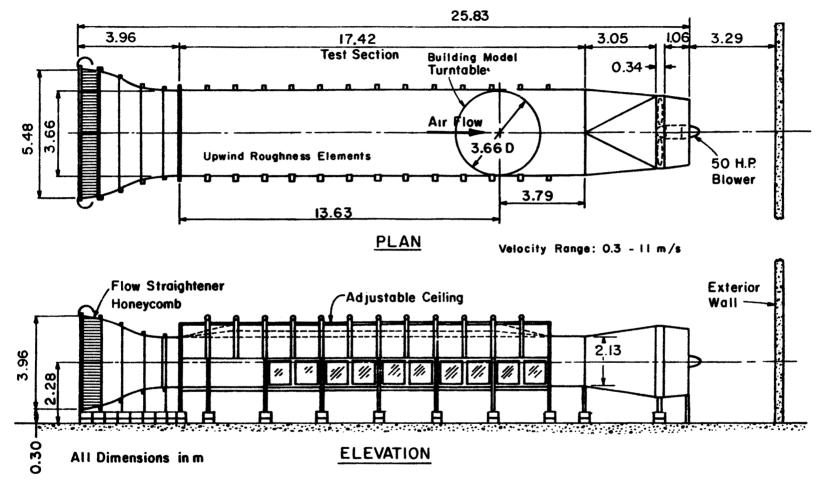
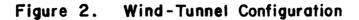


Figure 1. FLUID DYNAMICS AND DIFFUSION LABORATORY COLORADO STATE UNIVERSITY







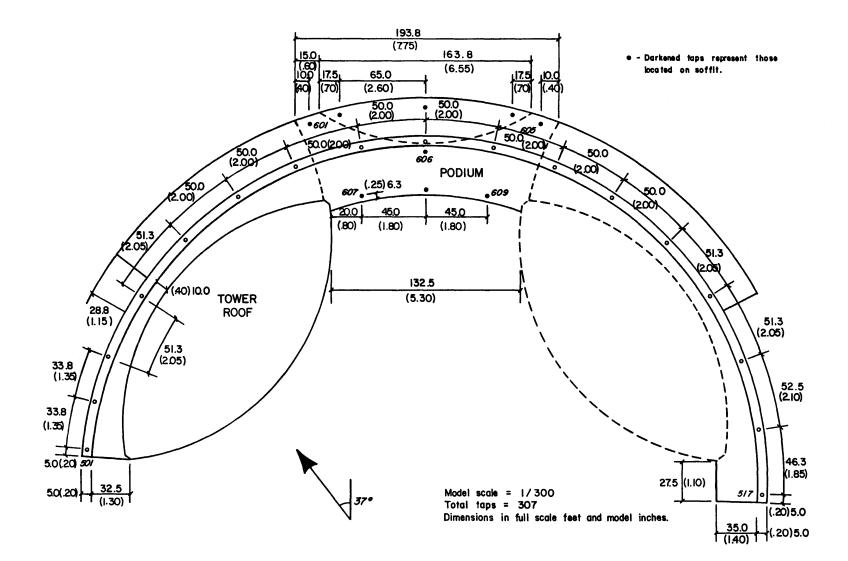


Figure 3a. Pressure Tap Locations

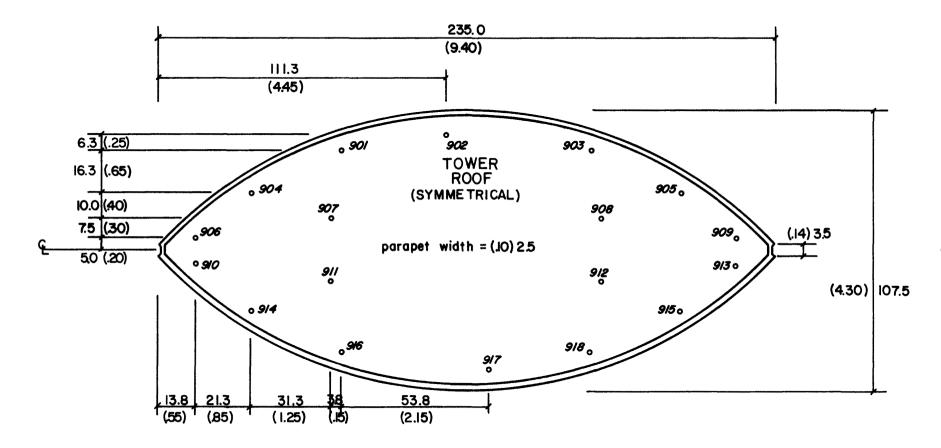


Figure 3b. Pressure Tap Locations

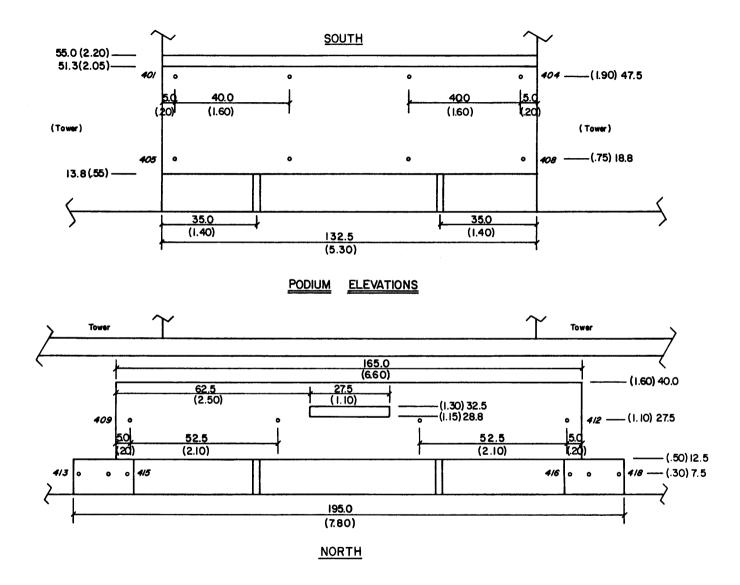
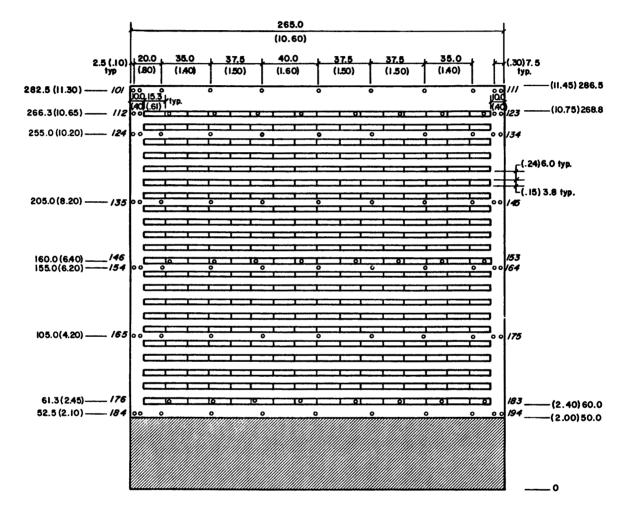
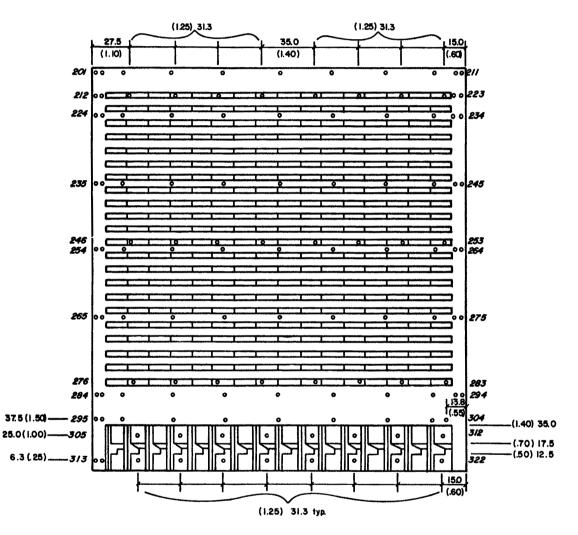


Figure 3c. Pressure Tap Locations



Developed View of North Elevation

Figure 3d. Pressure Tap Locations



Developed View of South Elevation

Figure 3e. Pressure Tap Locations

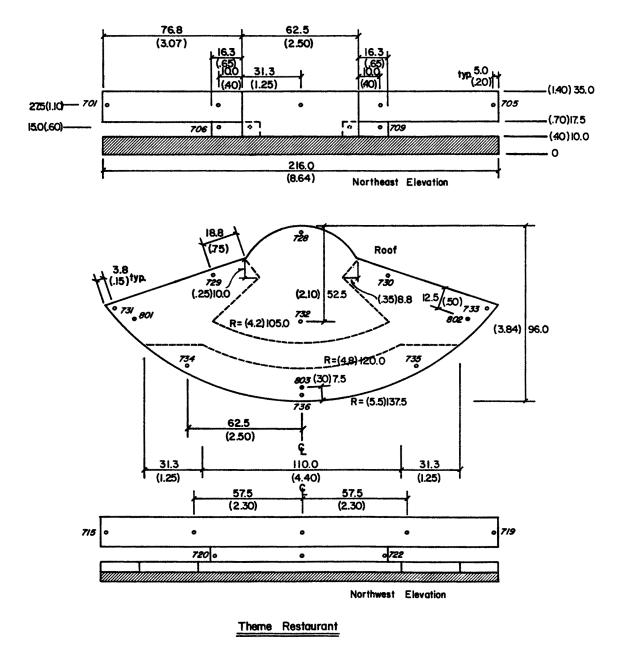


Figure 3f. Pressure Tap Locations

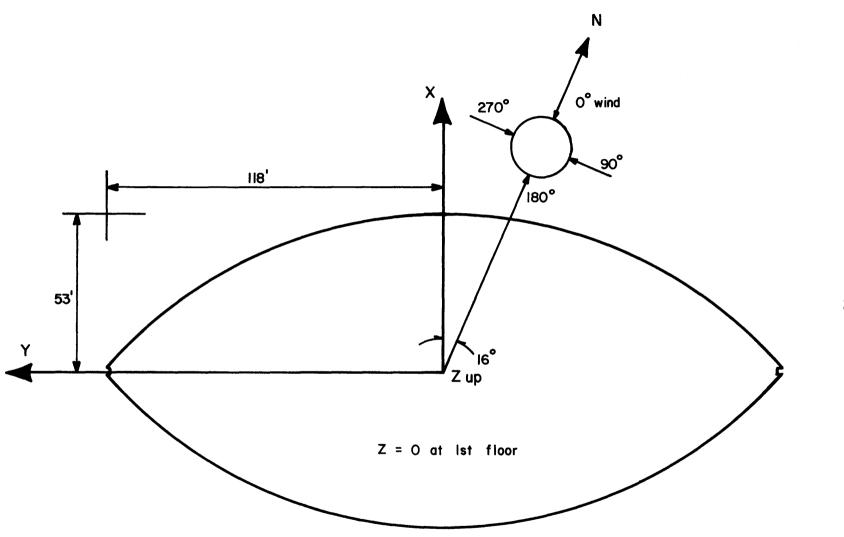
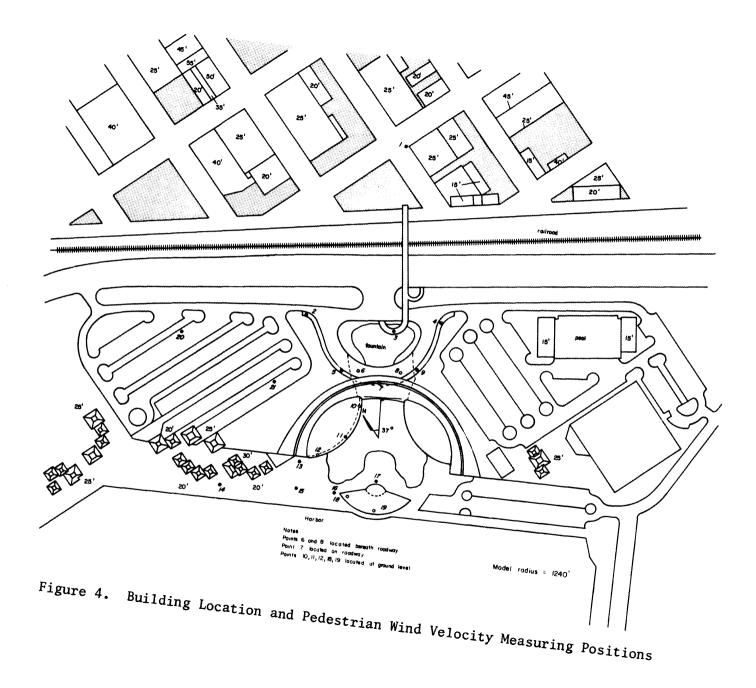


Figure 3g. Force and Moment Coordinate System



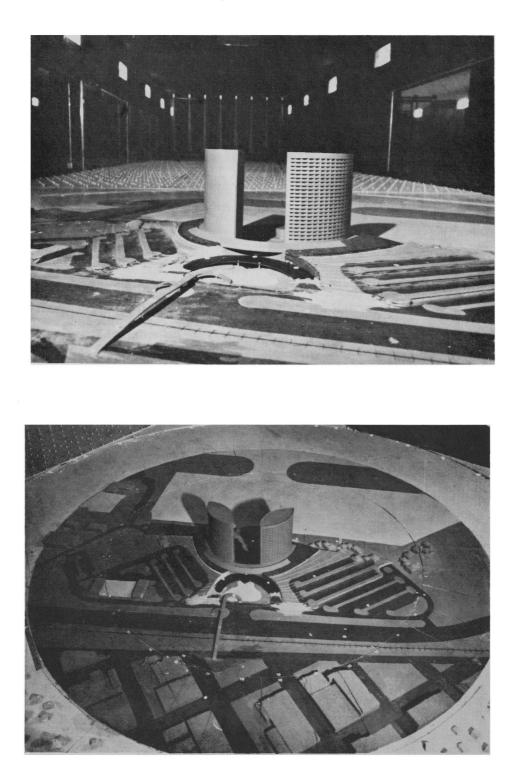
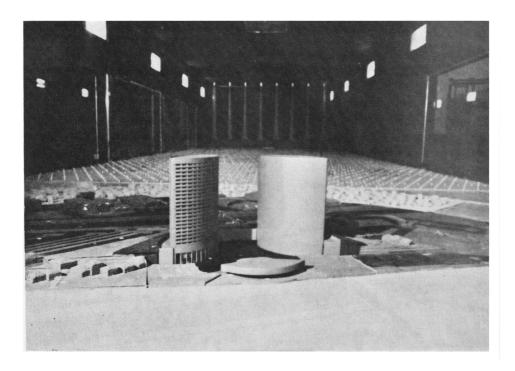


Figure 5. Completed Model in Wind Tunnel



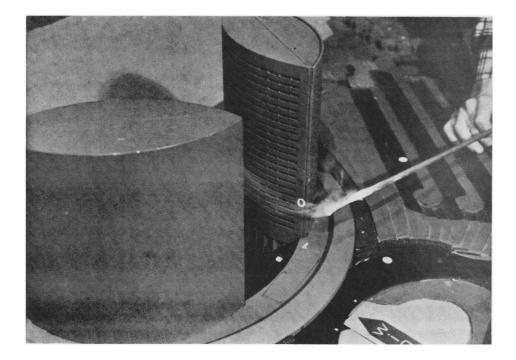


Figure 5. Completed Model in Wind Tunnel

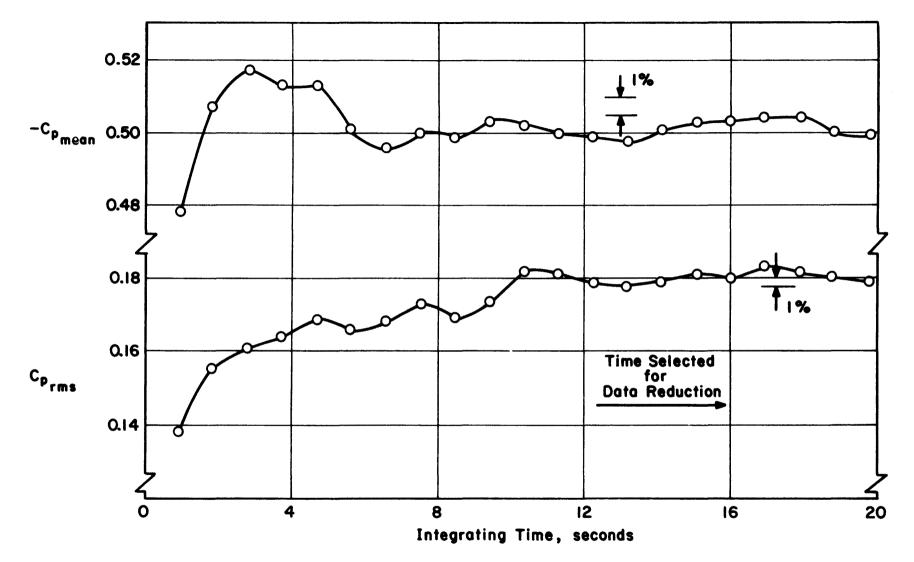


Figure 6. Data Sampling Time Verification

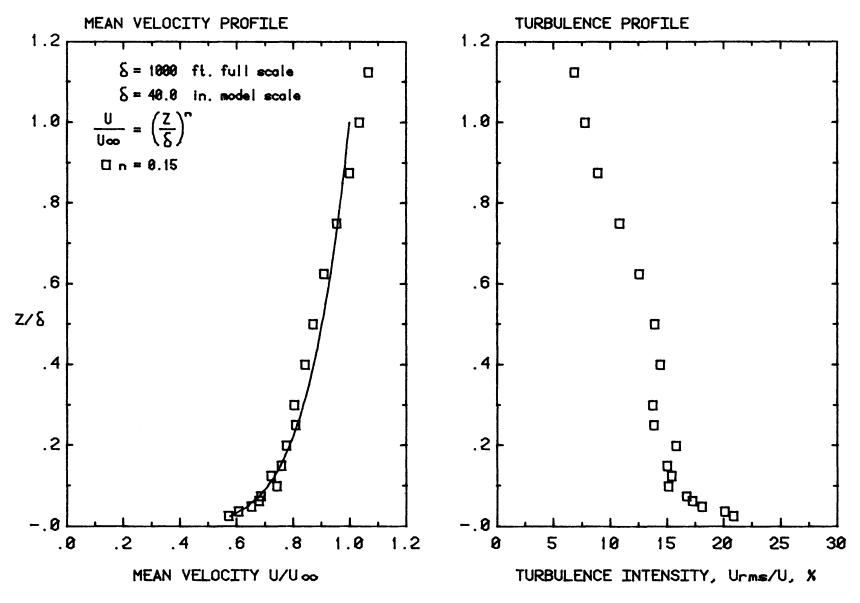
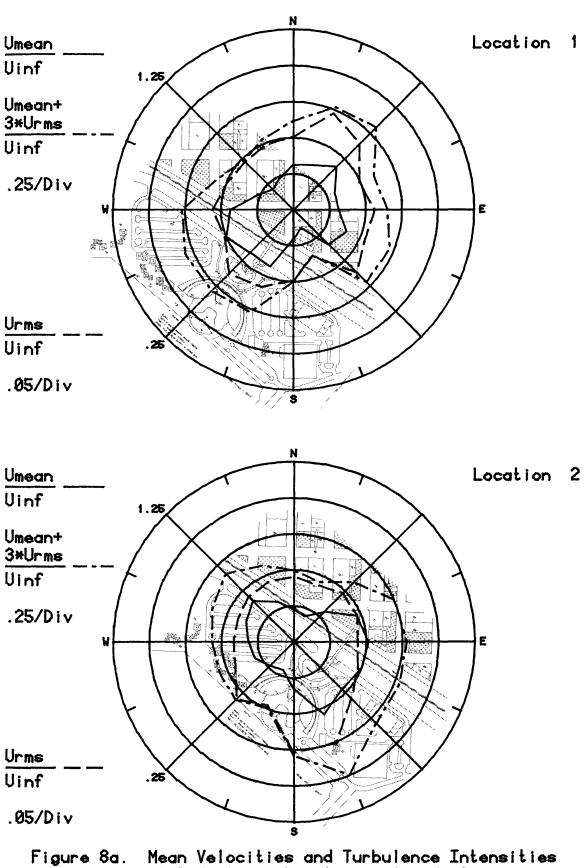
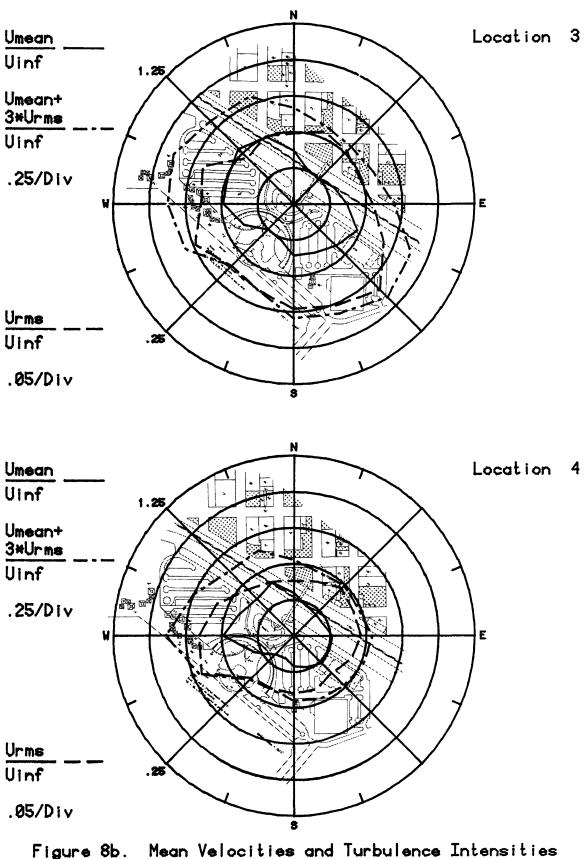


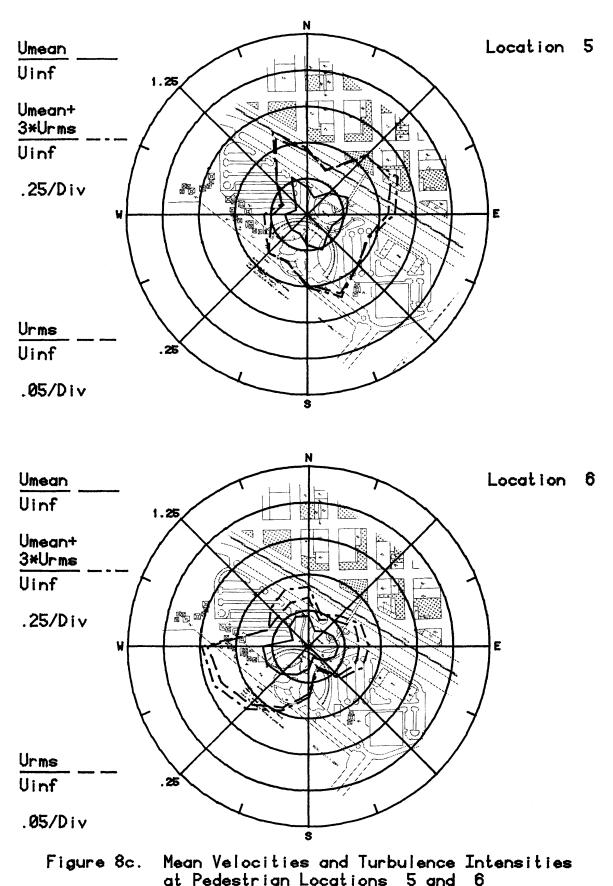
Figure 7. Mean Velocity and Turbulence Profiles Approaching the Model

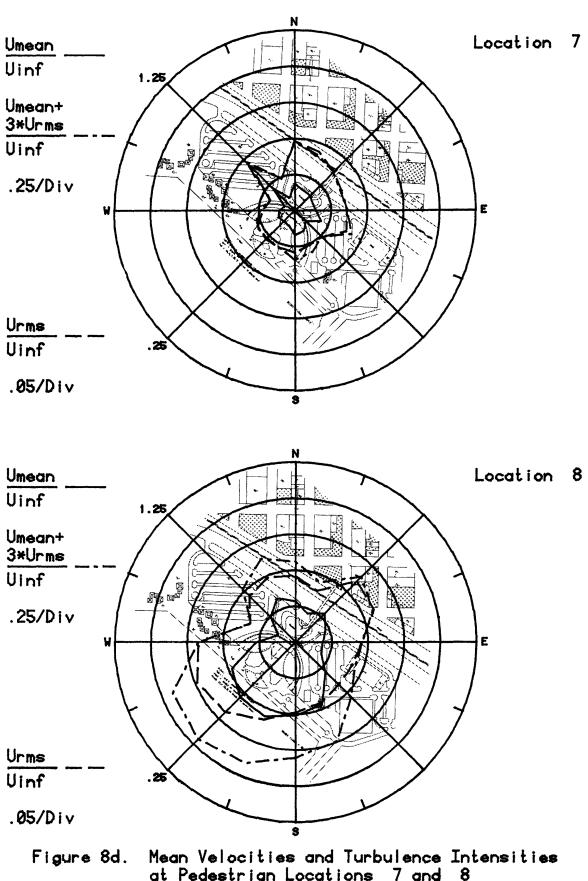


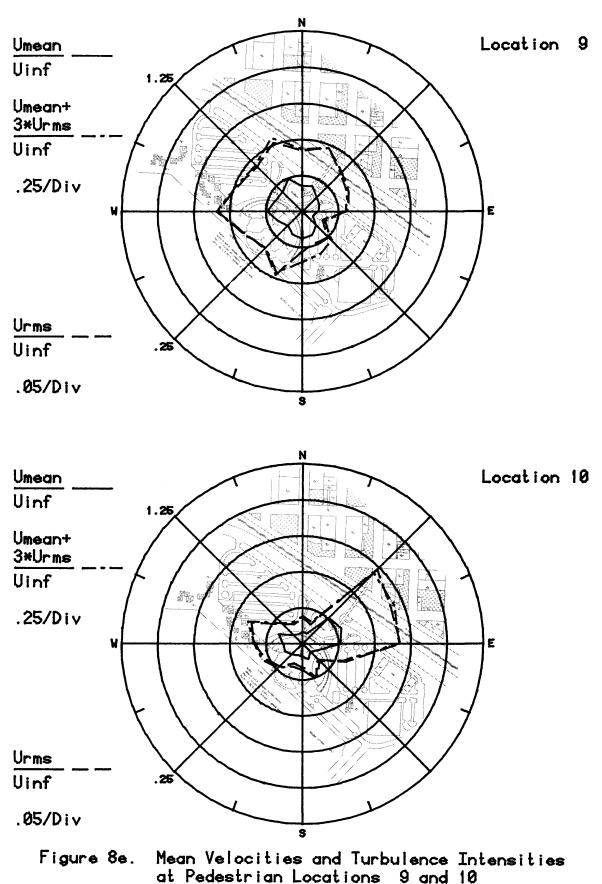
at Pedestrian Locations 1 and 2

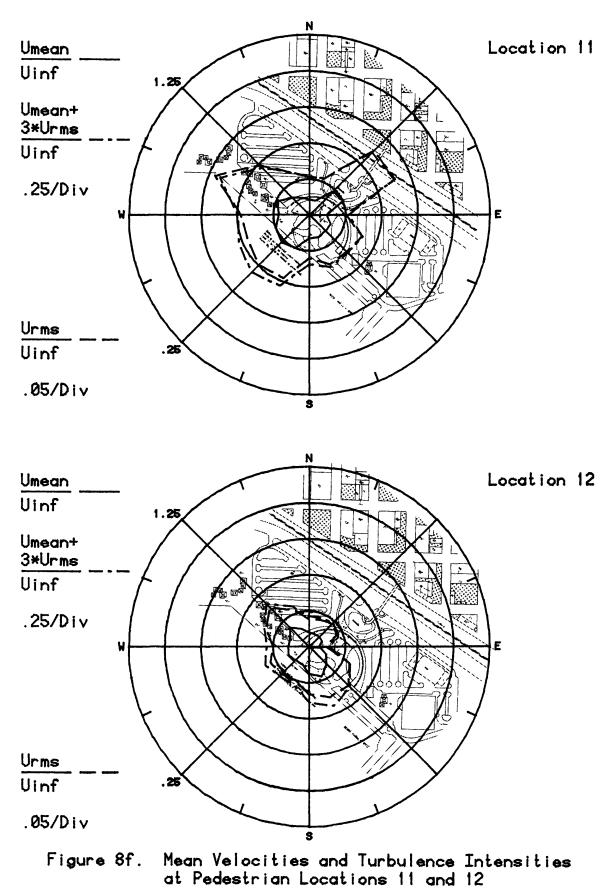


at Pedestrian Locations 3 and 4









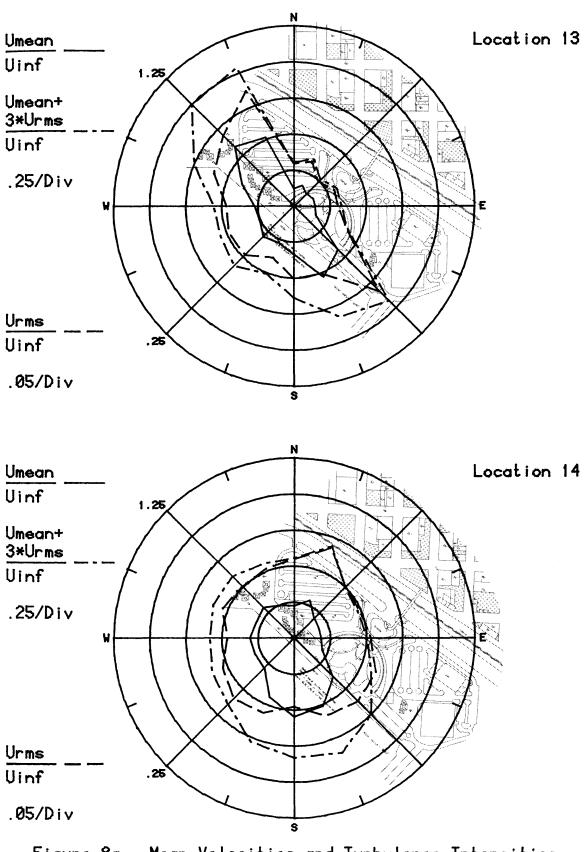
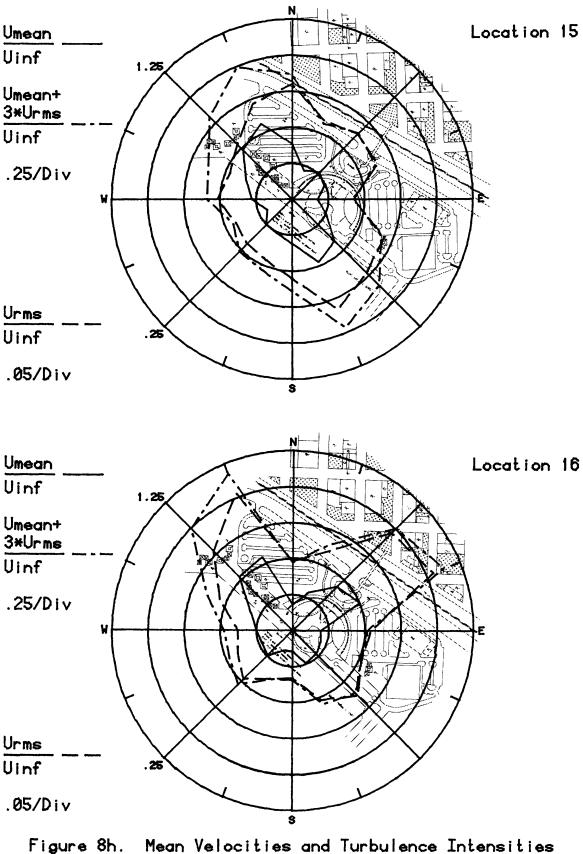
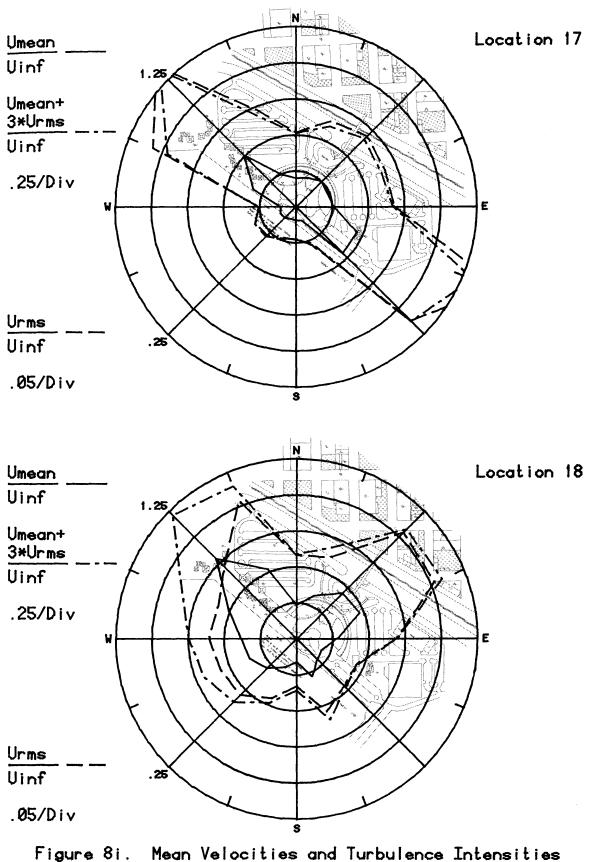


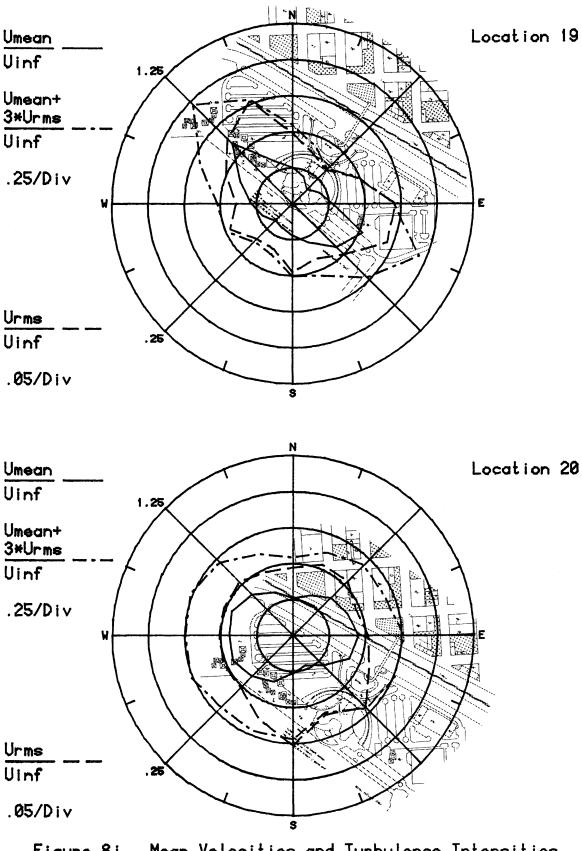
Figure 8g. Mean Velocities and Turbulence Intensities at Pedestrian Locations 13 and 14

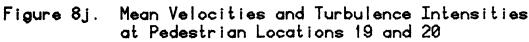


at Pedestrian Locations 15 and 16



at Pedestrian Locations 17 and 18





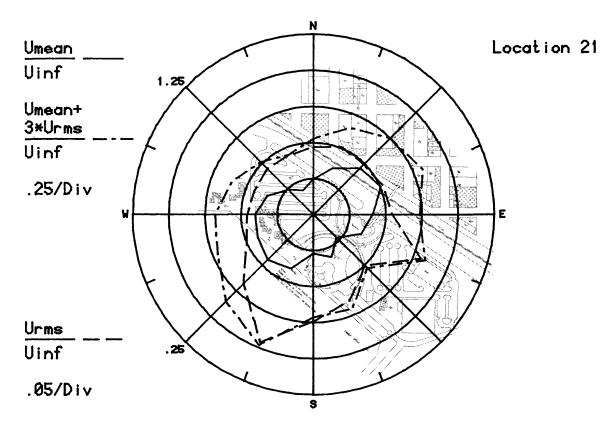


Figure 8k. Mean Velocities and Turbulence Intensities at Pedestrian Location 21

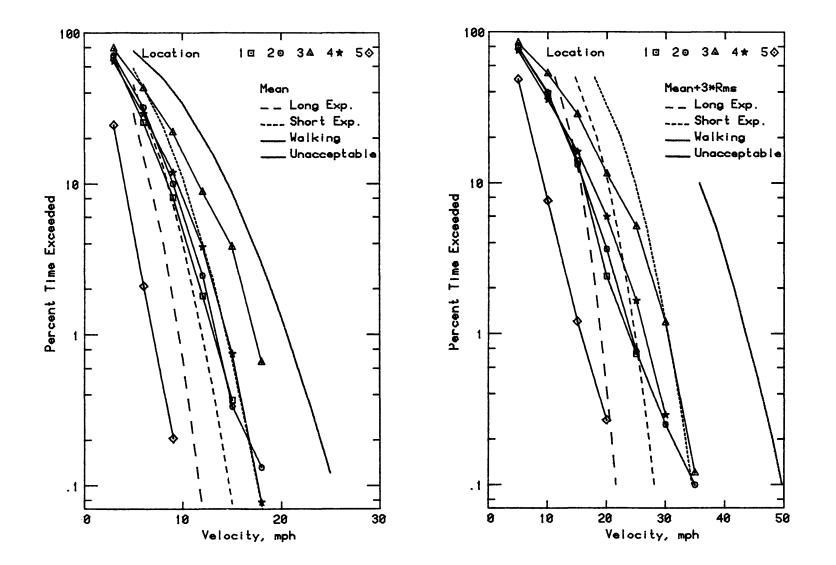


Figure 9a. Wind Velocity Probabilities for Pedestrian Locations

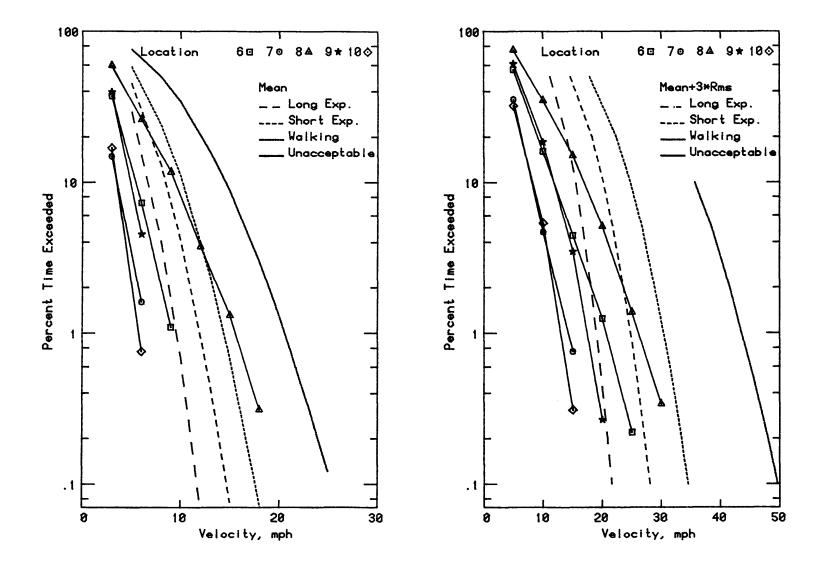


Figure 9b. Wind Velocity Probabilities for Pedestrian Locations

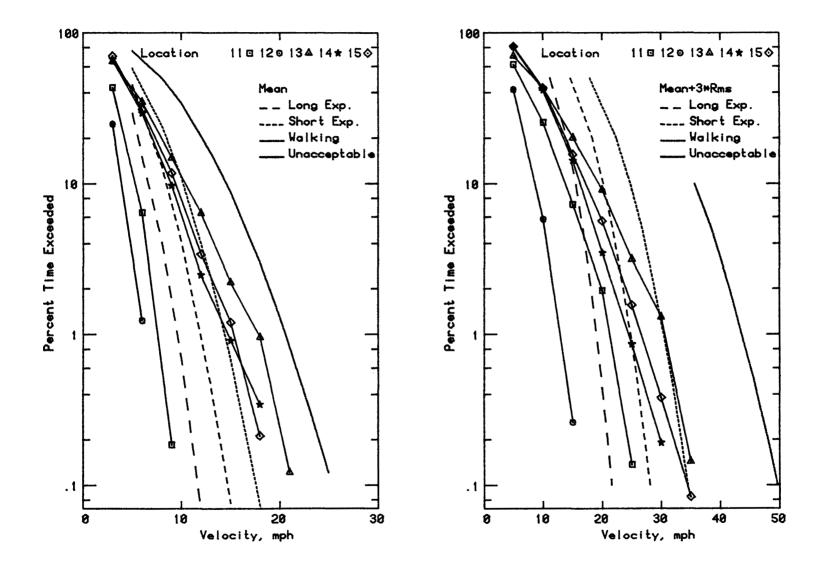


Figure 9c. Wind Velocity Probabilities for Pedestrian Locations

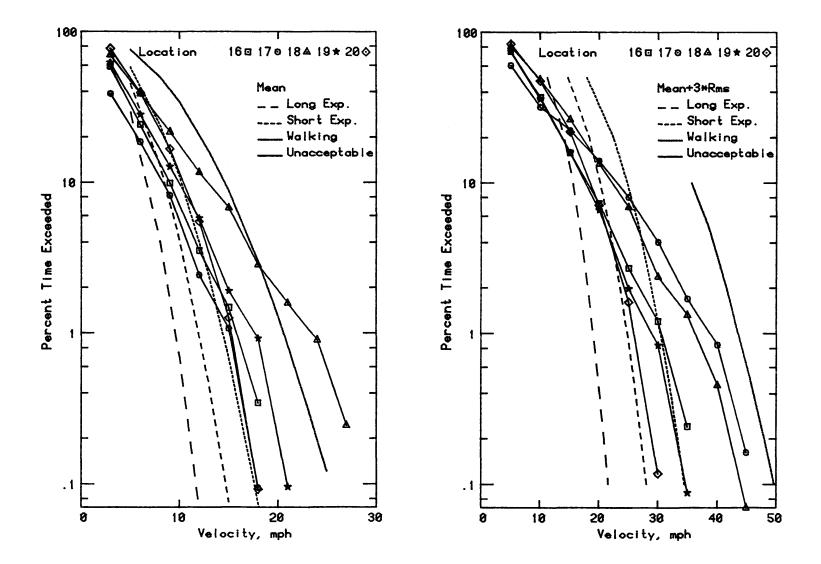


Figure 9d. Wind Velocity Probabilities for Pedestrian Locations

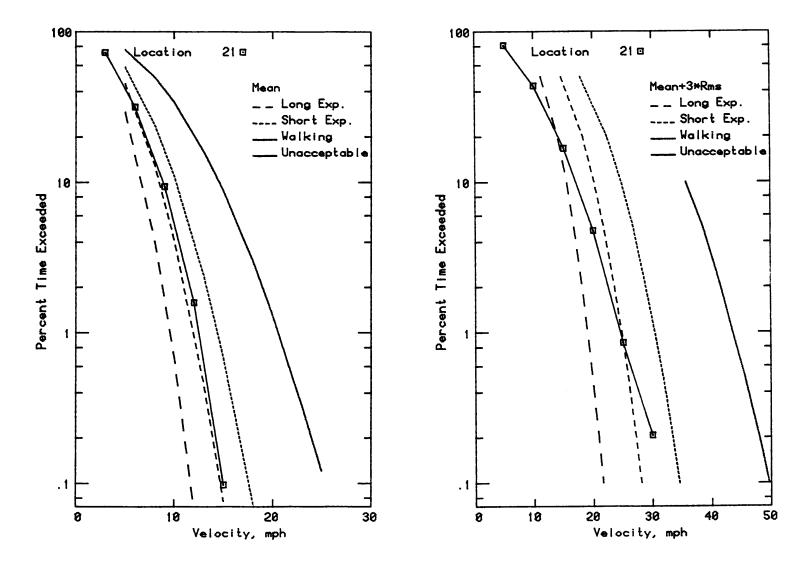


Figure 9e. Wind Velocity Probabilities for Pedestrian Locations

NORTH ELEVATION PEAK NEGATIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

WORST CASE OF EAST TOWER IN / EAST TOWER OUT

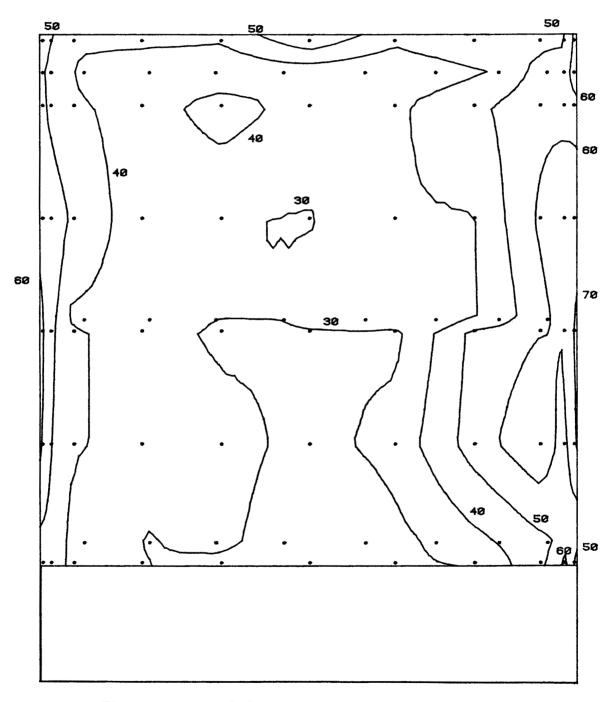


Figure 10a. Peak Pressure Contours on the Búilding for Cladding Loads

SOUTH ELEVATION PEAK NEGATIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

WORST CASE OF EAST TOWER IN / EAST TOWER OUT

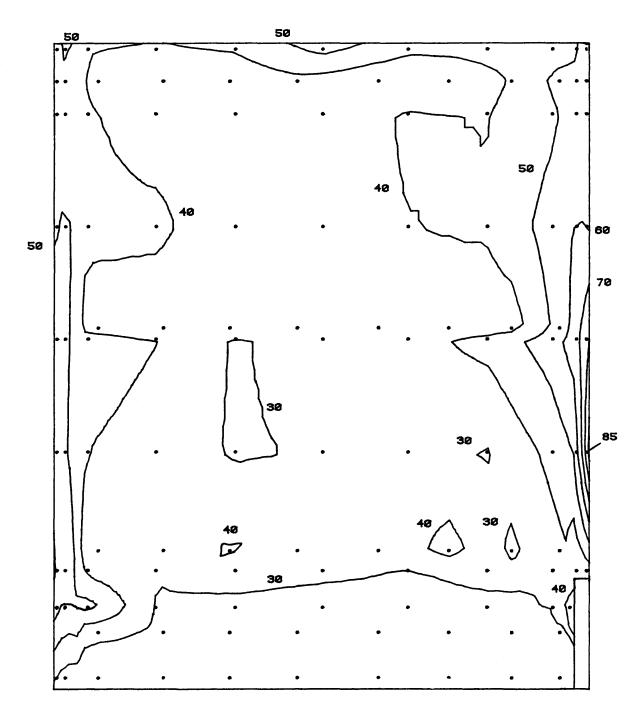


Figure 10b. Peak Pressure Contours on the Building for Cladding Loads

NORTH ELEVATION PEAK POSITIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

WORST CASE OF EAST TOWER IN / EAST TOWER OUT

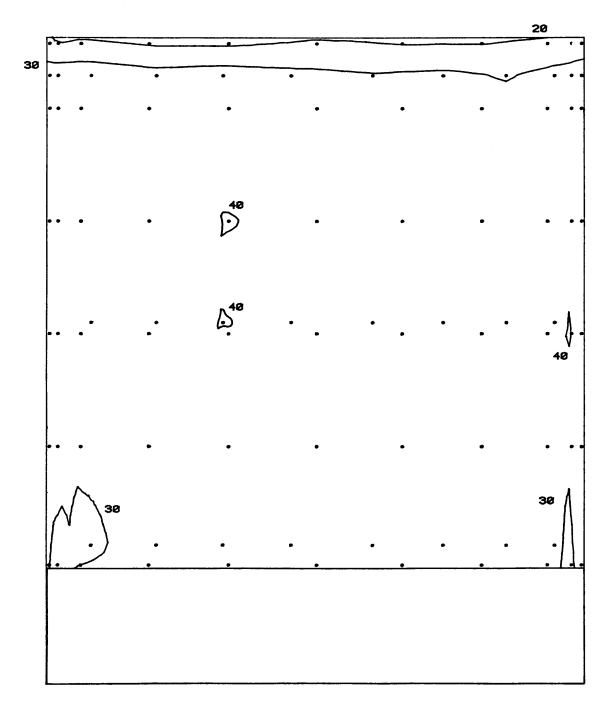


Figure 10c. Peak Pressure Contours on the Building for Cladding Loads

SOUTH ELEVATION PEAK POSITIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

WORST CASE OF EAST TOWER IN / EAST TOWER OUT

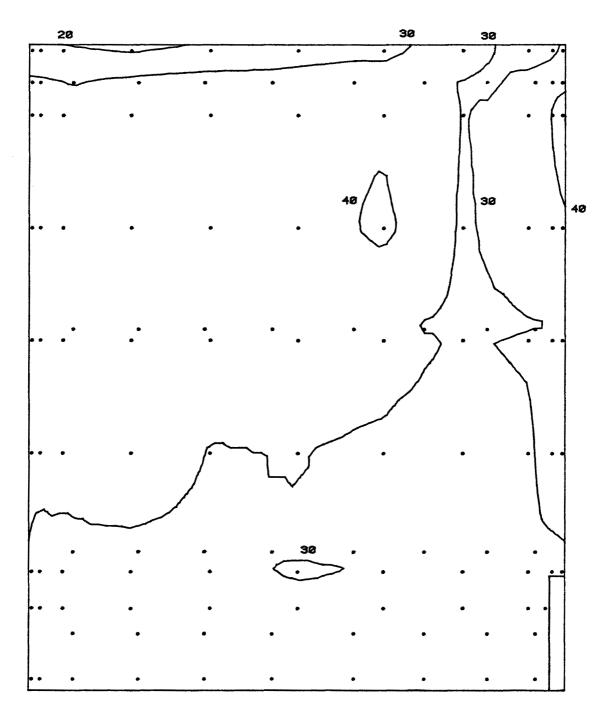


Figure 10d. Peak Pressure Contours on the Building for Cladding Loads

NORTH ELEVATION PEAK NEGATIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

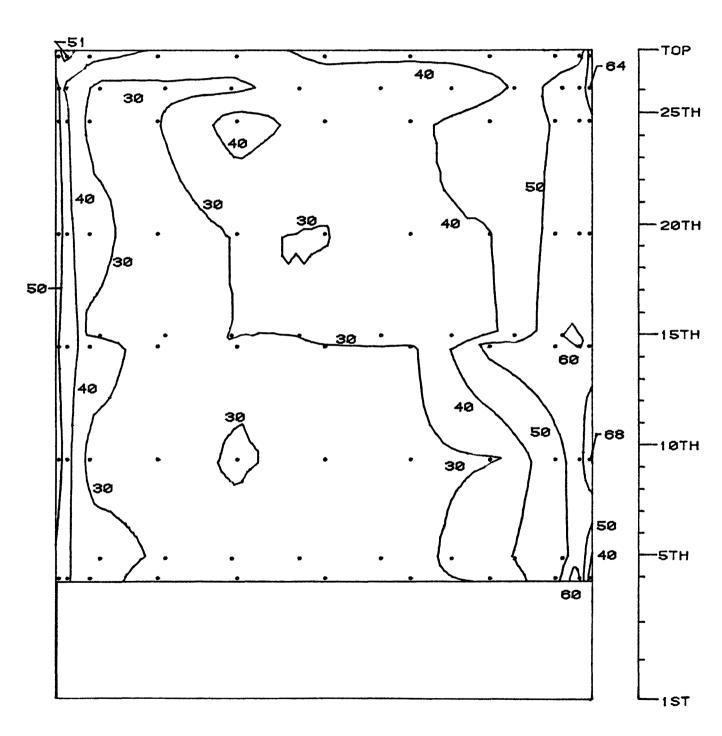


Figure 10e. Peak Pressure Contours on the Building for Cladding Loads

SOUTH ELEVATION PEAK NEGATIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

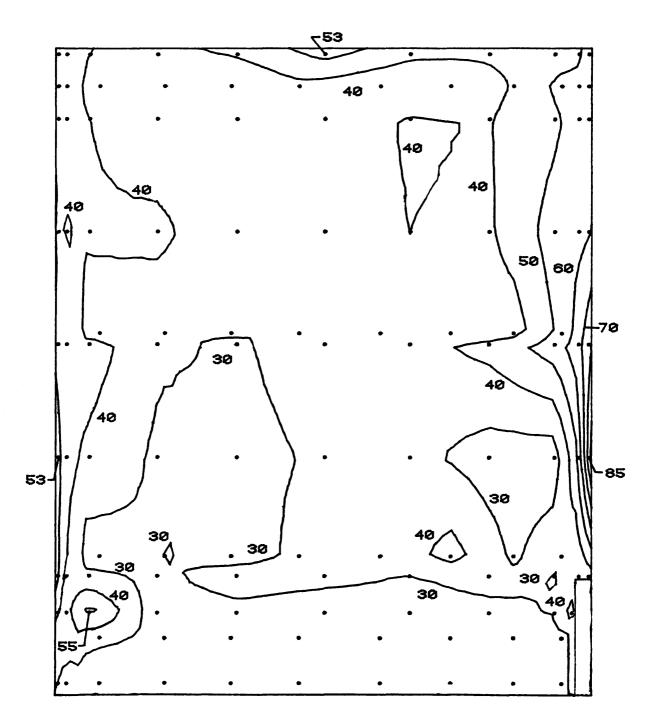


Figure 10f. Peak Pressure Contours on the Building for Cladding Loads

NORTH ELEVATION PEAK POSITIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

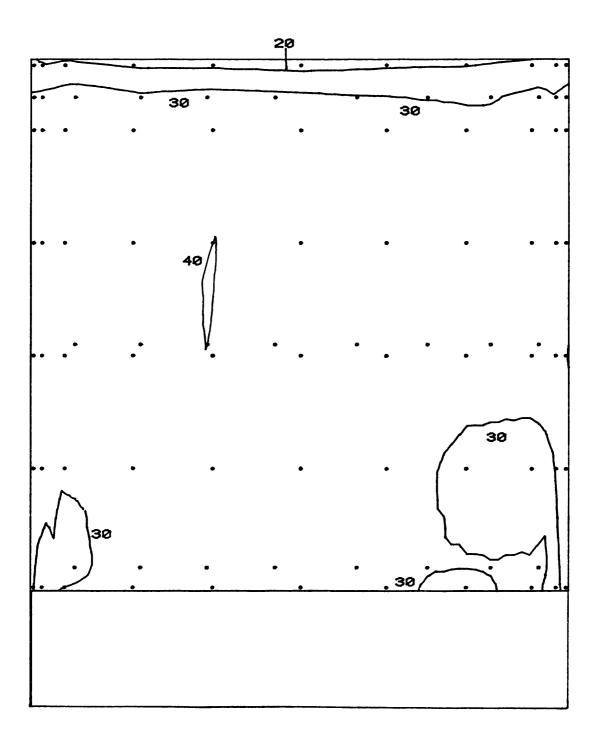


Figure 10g. Peak Pressure Contours on the Building for Cladding Loads

SOUTH ELEVATION PEAK POSITIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF 64

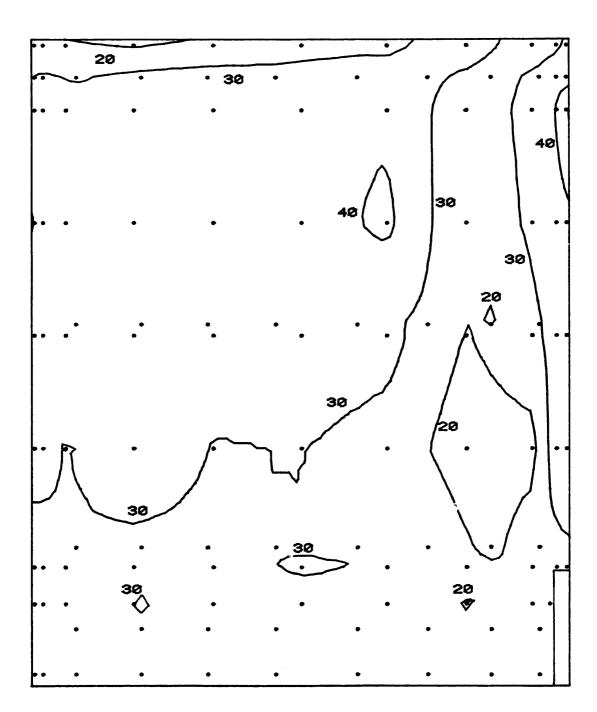


Figure 10h. Peak Pressure Contours on the Building for Cladding Loads

NORTH ELEVATION PEAK NEGATIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

EAST TOWER OUT

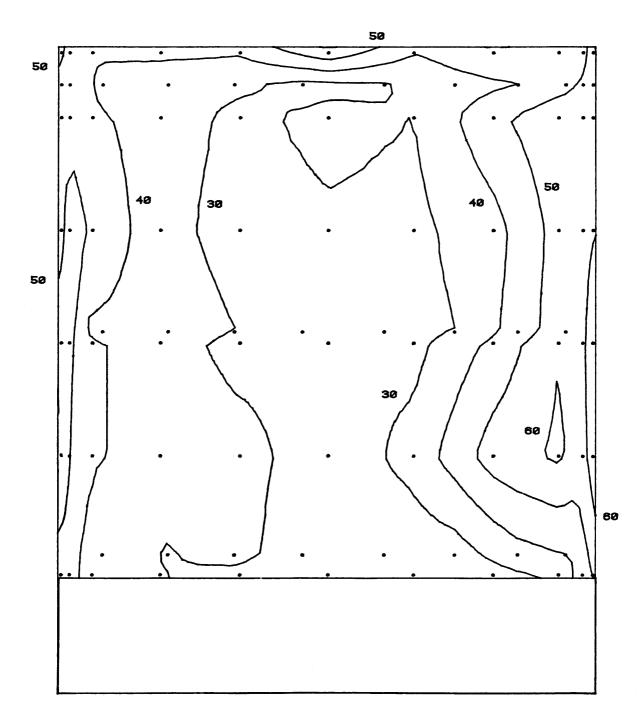


Figure 10i. Peak Pressure Contours on the Building for Cladding Loads

SOUTH ELEVATION PEAK NEGATIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

EAST TOWER OUT

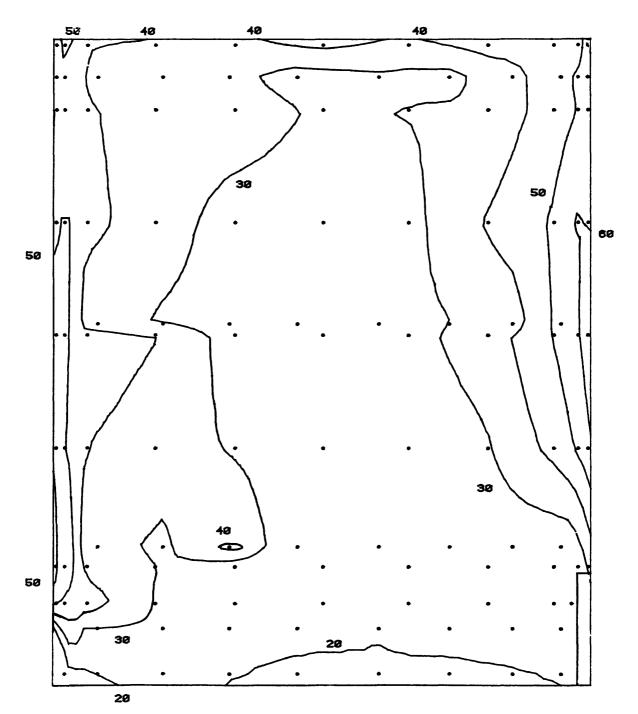


Figure 10j. Peak Pressure Contours on the Building for Cladding Loads

NORTH ELEVATION PEAK POSITIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

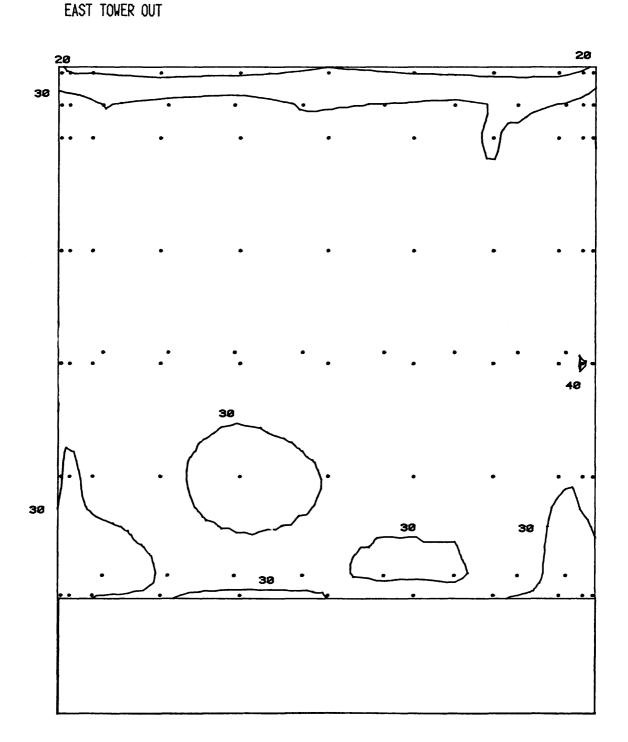


Figure 10k. Peak Pressure Contours on the Building for Cladding Loads

SOUTH ELEVATION PEAK POSITIVE CLADDING LOADS (PSF) FOR 50-YEAR RECURRENCE WIND REFERENCE PRESSURE = 27 PSF

EAST TOWER OUT

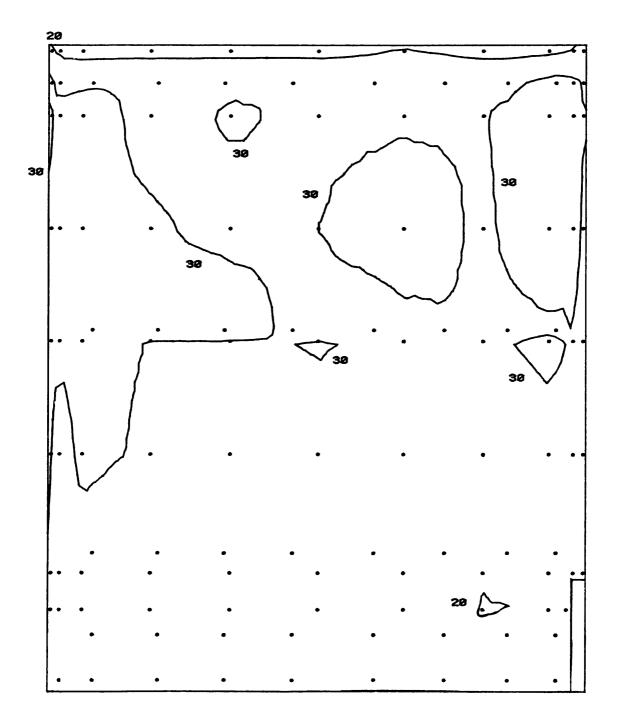


Figure 101. Peak Pressure Contours on the Building for Cladding Loads

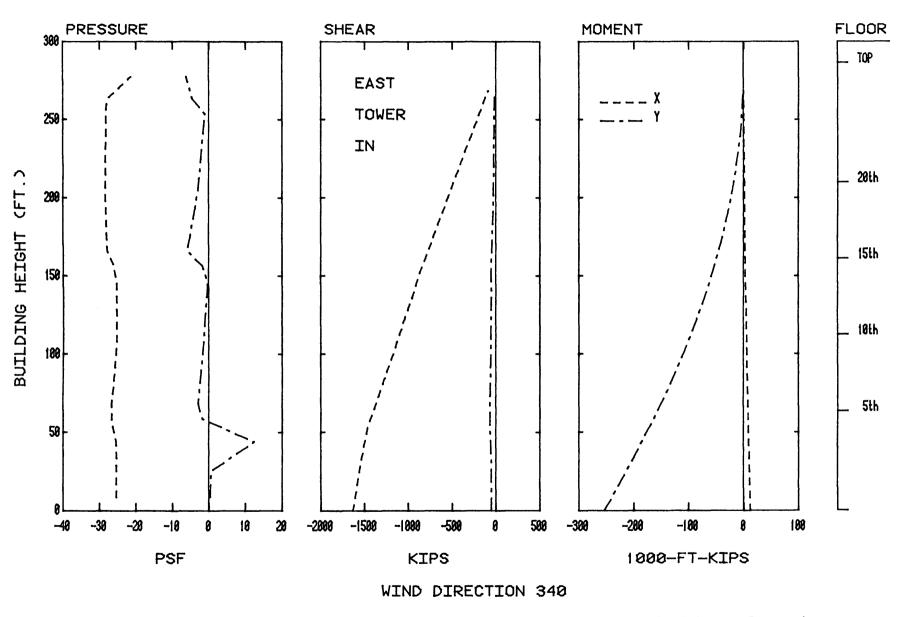


Figure 11. Load, Shear, and Moment Diagrams for Selected Wind Directions

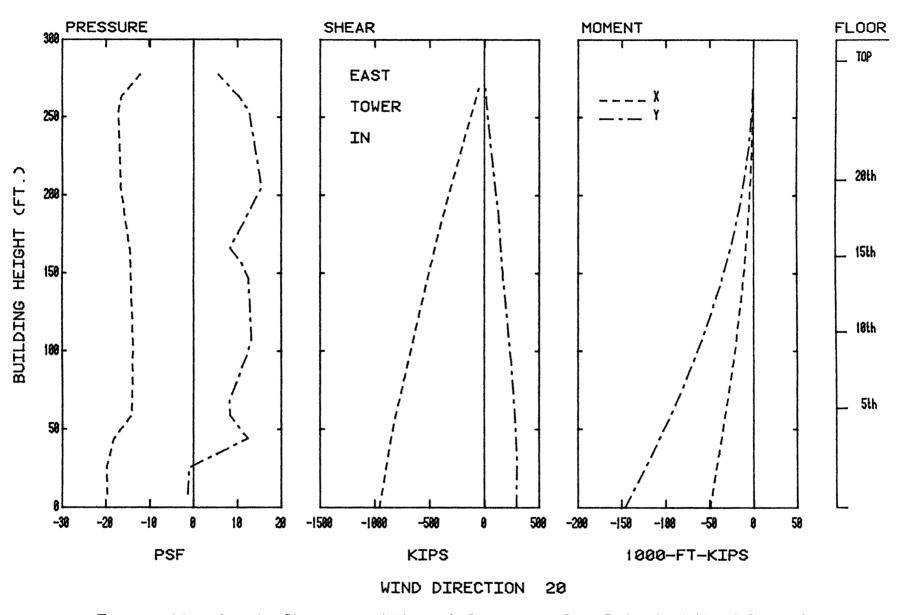
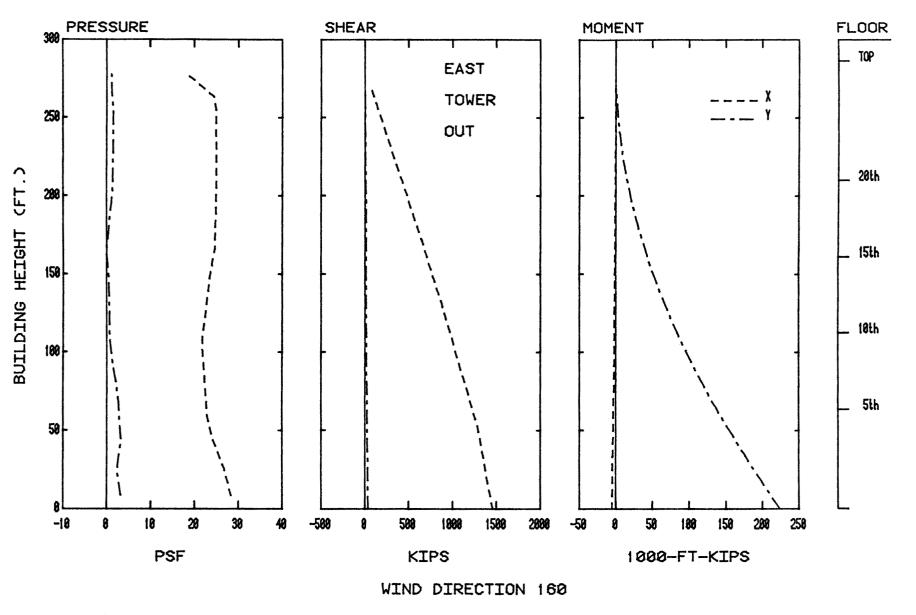
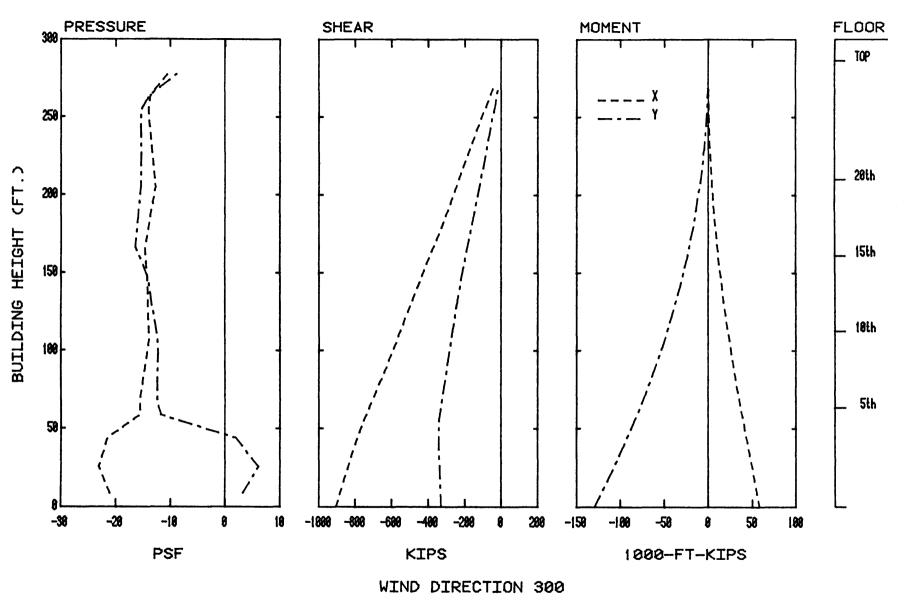


Figure 11. Load, Shear, and Moment Diagrams for Selected Wind Directions









MOTION PICTURE SCENE GUIDE

- 1. Introduction
- 2. Purposes for model testing
- 3. Procedures for conducting tests
- 4. Specific flow visualization scenes for

INTERCONTINENTAL HOTEL

HIGH PRESSURE AREAS

<u>Run</u>	Pressure Tap	<u>Azimuth.</u>
1	275	50
2	275	20
3	909	60

HIGH PEDESTRIAN WIND VELOCITIES

<u>Run</u>	Pedestrian Location	<u>Azimuth.</u>
4	18,13	315

LOCATION 1				LOCATION 2	2		
WIND Azimuth	UNEAN/UINF (PERCENT)	URNS/UINF (Percent)	UMEAN+3+URNS/UINF (PERCENT)	WIND Azimuth	UMEAN/UINF (Percent)	URMS/UINF (Percent)	UMEAN+3+URMS/UINF (PERCENT)
0.00 22.50 45.00 90.00 112.50 135.00 1150.00 2025.00 247.50 247.50 247.50 215.00 247.50 2315.00 315.00	31.1 33.97 31.97 31.97 39.90 34.97 34.90 34.90 34.90 42.12 40.24 543.68 20.12 24.2	1 4 4 0 1 4 4 0 1 4 1 3 . 9 1 1 2 . 9 1 1 0 . 7 1 2 6 9 1 1 2 6 2 1 0 . 2 1	61.4 76.9 80.8 652.0 724.4 50.1 779.8 71.0 77.4 81.0 775.4 58.2 53.5	0.00 22.50 45.00 90.00 112.50 135.00 157.50 205.00 247.50 247.50 247.50 247.50 247.50 247.50 247.50 247.50 247.50 2315.00 315.50	22.5 19.6 47.0 51.4 49.8 49.8 54.0 32.7 23.2 23.2 29.3 315.8 40.0 30.0	9.555852245273499 1155.5273499	49.4 44.7 58.2 75.4 77.9 78.5 80.1 99.7 79.0 2 55.6 56.9 55.6 50.9 55.6 50.9 57.1
LOCATION 3				LOCATION 4	ŀ		
WIND Azimuth	UNEAN/UINF (PERCENT)	URNS/UINF (Percent)	UNEAN+3+URMS/UINF (PERCENT)	WIND Azimuth	UMEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UMEAN+3+URMS/UINF (PERCENT)
0.00 22.50 45.00 90.00 112.50 135.00 135.00 1202.50 2247.50 2247.50 2247.50 2915.00 2915.50 23337.50	1089750679827121 3222341655478940 16855478940 16855478940	90.48 90.48 90.48 90.48 105.48 122.78 122.78 122.78 122.60 14 123.69 14 122.78 10 10 10 10 10 10 10 10 10 10 10 10 10	53 58 58 59 97 87 59 92 95 87 61 87 61 87 61 87 61 87 61 87 10 87 10 87 10 80 10 80 10 80 10 80 10 80 10 80 10 80 10 80 10 10 10 10 10 10 10 10 10 10 10 10 10	0.00 22.50 45.00 90.50 112.50 1135.50 1180.50 202.50 200 200 200 200 200 200 200 200 200 2	29.7 221.37 221.37 226.37 226.37 226.37 226.4 18.1 18.1 18.1 18.1 18.1 18.1 49.5 36.07	623935400928151 7898987887833151 11198	52.5 47.0 49.1 48.4 54.1 51.9 48.3 47.3 45.2 70.6 42.7 70.6 74.9 63.2 64.0

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES San diego intercontinental hotel

LOCATION 5

WIND	UMEAN/UINF	URMS/UINF	UMEAN+3+URMS/UINF	WIND	UNEAN/UINF	URMS/UINF	UMEAN+3+URNS/UINF
Azimuth	(Percent)	(PERCENT)	(PERCENT)	Azimuth	(PERCENT)	(Percent)	(PERCENT)
0.00 22.50 45.00 90.50 112.50 1157.50 1157.50 225.50 22470.50 2470.50 2470.50 2470.50 2470.50 2470.50 25.50	192.04 92.05 92.04 92.05 92.04 92.00	9.67.65 11.1.111 11.1.111 11.1.111 11.1.111 11.1.111 11.1.1111 11.1.1111 11.1.11111 11.1.111111	4356644655709992	6 00 22 50 45 00 90 00 112 500 1137 50 182 500 182 50 225 50 225 50 225 50 225 50 225 50 225 50 225 50 235 50 250 250 250 250 250 250 250 2	21.0 11.6 14.3 20.6 18.7 18.7 25.7 26.9 31.7 21.6 31.7 11.6 22.6	6 4 1 5 7 7 6 5 7 6 9 1 9 1 1 1 3 6 5 6 5 1 1 3 6 5 6 5 6 9 1 5 6 5 5 6 5	41.3 339.3 41.5 339.5 30.8 30.8 30.8 30.8 30.8 30.8 30.9 41.5 30.8 30.9 41.5 30.8 30.8 30.9 41.5 30.8 30.9 41.5 30.9 41.5 30.9 41.5 30.8 30.5 41.5 30.8 30.5 41.5 30.5 41.5 30.8 30.5 41.5 30.5 41.5 30.5 41.5 30.5 41.5 30.8 30.5 41.5 30.5 30.5 30.5 30.5 30.5 30.5 30.5 30

LOCATION	7				LOCATION	6		
WIND Azimuth		UNEAN/UINF (PERCENT)	URNS/UINF (Percent)	UMEAN+3+URMS/UINF (percent)	WIND Azimuth	UNEAN/UINF (PERCENT)	URMS/UINF (Percent)	UMEAN+3*URMS/UINF (PERCENT)
000 245.500 45.500 115.500 115.000 115.000 115.000 227.500 227.500 227.500 2227.500 2227.500 2227.500 2227.500 22227.5000 2227.5000 2227.50000 2227.50000 2227.5000 2227.500000 2227.50000 227		42826533581418604 115561.418604 1165.61.418604	98777755555554768	4 7 1 7 4 4 7 1 4 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6	0.00 22.50 477.50 902.50 11357.50 1802.50 1802.50 2057.50 2045.50 2045.50 2045.50 2045.50 2045.50 2045.50 205.50 2	28.5 221.35 28.43 28.61 28.61 98.19 47.99 47.99 5554.99 24.6 122.6 122.6 123.1 33.1	9.27 11.79 11.79 8.4 9.88 11.67 13.67 13.48 9.88 11.34 13.48 9.89 11.67 13.48 9.89 9.89	55.9 44.6 67.6 46.15 54.5 54.5 74.5 90.7 952.0 67.0 351.8 62.4

LOCATION 9				LOCATION 10	>		
SIND Azimuth	UNEAN/UINF (PERCENT)	URHS/UINF (Percent)	UMEAN+3+URMS/UINF (PERCENT)	WIND Azimuth	UNEAN/UINF (Percent)	URMS/UINF (PERCENT)	UMEAN+3+URMS/UINF (PERCENT)
0.00 22.50 45.50 90.112.50 112.50 1157.50 100222.00 2025.00 2025.00 2027.50 2025.50 2025.50 2025.50 337.50	179.048206 144.8206 1178.8206 1178.85 1178.85 1178.85 1173.85 1187.88 1173.74 1173.85 1189.13 114.8 1172.18 119.13 114.8 1172.18 119.14	897776355553477581 1980 1997781 1980 1980 1980 1980 1980 1980	44332437663242 3773978255529855 1233454855 5529855 12355529855 1255529855 1255529855 1255529855 1255529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 12555529855 125555529855 125555555 125555555 125555555 125555555 1255555555	0.00 22.50 45.00 90.00 112.50 112.50 1157.50 205.00 205.00 205.00 205.00 205.00 205.00 205.50 200 215.50 200 200 200 200 200 200 200 200 200 2	8.6 7.5 25.1 26.3 119 26.3 119 8.5 8.1 123 1.2 7 83 1.2 7 83 1.7 83 1.7 83 1.7 83 1.7 83 1.7 83 1.7 1.7 83 1.7 1.7 83 1.7 83 1.7 1.7 1.7 83 1.7 1.7 7 7 7 7 83 1.7 7 7 87 7 7 7 7 87 7 7 87 7 7 87 7 7 87 87 7 7 87 7 7 87 7 7 87 87 87 7 7 87 87 87 7 7 87 87 7 7 87 87 7 7 87 87 7 7 87 87 7 7 87 87 87 87 7 7 87 7 7 87 7 7 87 7 7 87 7 7 87 87 87 87 87 87 7 87 97 8	3243350020356789 1433650020356789	19.2 16.4 69.9 30.6 9 25.8 18.1 123.1 29.5 30.7 20.0 16.1
LOCATION 11				LOCATION 12	2		
WIND Azimuth	UNEAN/UINF (PERCENT)	URNS/UINF (Percent)	UMEAN+3+URMS/UINF (PERCENT)		UNEAN/UINF (PERCENT)	URMS/UINF (PERCENT)	UNEAN+3+URMS/UINF (PERCENT)
0,50 457,50 457,50 1155,50 1257,50 225,50 235,500 235,5000 235,5000 235,5000 235,5000 235,5000 235,5000 235,5000 235,5000 235,50000 235,50000 235,500000000000000000000000000000000000	11020937846022097 003516578460220507 1105664751472	3569193405825273 11157776999994 195	62061 671. 671. 671. 671. 671. 671. 671. 67	000 22.500 912.500 1137.500 1137.500 125.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 2247.500 225.500 225.500 225.500 225.500 205.5000 205.5000 205.5000 205.5000 205.5000 205.5000 205.5000 205.5000 205.5000 205.5000 205.5000 205.5000 205.50000000000	9.67 9.67 9.67 12.79 62.79 62.79 122.07 122.07 122.07 122.55 14.38 14.55	8051307661480465	21.1 21.6 222.0 13.5 30.0 44.6 28.2 29.1 8 29.4 32.9 33.6 29.4 33.6 29.4 33.6 30.0

LOCATION 13

WIND	UMEAN/UINF	URMS/UINF	UNEAN+3+URMS/UINF	WIND	UNEAN/UINF	URMS/UINF	UMEAN+3+URHS/UINF
Azimuth	(Percent)	(PERCENT)	(PERCENT)	Azimuth	(Percent)	(Percent)	(PERCENT)
0.00 225.00 4670.00 1155.50 11550.50 225.50 11550.50 225.50 200 225.50 200 225.50 200 200 200 200 200 200 200 2	2703749963873.639 111111114533222235 11532446223795.639 11111111153222379578.81	564667607574083 1107799923 1111799923 1117	97542 95542 29542 29542 29533 29533 290 85555555 55454 5555555 55454 2953 2993 895555555 5588 5555555 5588 100 100 100 100 100 100 100 100 100 1	0.00 22.50 45.50 90.500 1135.500 1135.500 125.500 235.500 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.5000 235.50000 235.50000 235.50000 235.50000 235.50000000 235.500000000000000000000000000000000000	28.4 29.2 198.6 198.6 11.4 35.4 4.9 2 2 9.2 1 1 8 0 8 1.1 4 3 2 2 0 8 0 8 0 8 0 8 0 8 0 8 0 8 0 8 0 8	11.0 13.5 9.8 10.2 12.4 11.7 9.2 11.9 11.9 10.7 2 10.7 2 10.7 2 10.4	599.0 599.0 49707.5 575.0 575.0 575.0 8 374.0 580.0 580.0 580.0 580.0 580.0 580.0 580.0 580.0 580.0 580.0 580.0 580.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 590.0 50

LOCATION 15				LOCATION 1	6		
WIND Azimuth	UNEAN/UINF (PERCENT)	URNS/UINF (Percent)	UMEAN+3+URMS/UINF (PERCENT)	WIND Azimuth	UMEAN/UINF (Percent)	URMS/UINF (Percent)	UMEAN+3+URMS/UINF (PERCENT)
0,500 457,000 1157,000 1157,500 1257,500 225,5000 225,5000 225,5000 225,5000 225,5000 225,5000 225,5000 225,	3222375.2099170644 3222375.2099170644 3222312443225884.66 443221234564 456	16.0 1122.8 122.8 134.5 16.1 19.8 80.3 7 5 16.3 19.7 14.3 14.3 14.3 14.3 14.3 14.3 14.3 14.3	37774767615520664 8564226464311. 866422646431. 896535459209. 896535459209.	0.00 22.500 457.050 11357.500 11357.500 11357.500 12025.500 224702.500 24762.500 24762.500 24762.500 24762.500 24762.500 24775.500 23137.500	18 4 28 6 450 1 19 3 20 3 4 0 20 3 4 0 20 4 14 7 22 4 14 7 22 4 14 7 55 3	9.68 11.82 10.93 10.93 10.93 10.93 10.93 10.93 10.93 10.93 10.93 10.95 10.55 10.55 10.55	47.1 64.2 100.5 113.1 51.9 51.6 55.2 34.3 36.6 53.2 36.6 53.2 47.5 64.0 99.4 117.2

LOCATION 17

WIND	UMEAN/UINF	URNS/UINF	UMEAN+3+URMS/UINF	WIND	UNEAN/UINF	URMS/UINF	UMEAN+3*URMS/UINF
Azimuth	(percent)	(Percent)	(Percent)	Azimuth	(Percent)	(PERCENT)	(PERCENT)
0.00 22.50 45.00 90.50 112.50 1157.50 1800.00 2055.50 2055.50 20470.50 2055.50 20470.50 2055.5	2015 2215 223 225 225 226 225 226 225 226 2019 225 226 2019 2019 2019 2019 2019 2019 2019 2019	39937774747810437 22544565164 2264	51.0 66.5 66.6 67.2 122.6 127.0 227.8 27.8 27.8 27.8 27.8 27.8 27.8 27.	0.00 22.50 457.50 902.500 11357.500 1257.500 1257.500 225.000 225.000 22702.500 22702.500 22702.500 2270.500 23337.50	232.5 32.5 47.9 180.9 180.9 122.1 225.3 380.5 380.5 8 50.5 8 22.5 5 22.5 5 22.5 5 22.5 5 22.5 5 22.5 5 22.5 5 22.5 5 22.5 5 5 22.5 5 5 22.5 5 5 5	11 6 12 2 20 6 13 8 9 3 10 9 10 9 11 0 8 9 11 0 3 11 0 11 1 12 1 11 7 12 8	58.6 69.1 107.3 108.9 45.8 45.9 47.8 60.7 35.9 47.9 61.6 67.5 74.5 85.7 121.0 114.5

LOCATION 19				LOCATION 2	•		
WIND Azimuth	UNEAN/UINF (PERCENT)	URMS/UINF (Percent)	UMEAN+3+URMS/UINF (PERCENT)	WIND Azimuth	UMEAN/UINF (Percent)	URMS/UINF (PERCENT)	UNEAN+3+URMS/UINF (PERCENT)
0.00 22.50 45.00 90.50 1125.50 1157.50 1800.50 222.00 2470.50 2470.50 2470.50 2470.50 2470.50 2470.50 2470.50 25.50 2470.50 25.50 2470.50 25.50	2320 5040 5472 5292 5292 5292 527 5292 591 591 591 591 591	9765210358938974 111896697925 1210358938974	54.8 424.0 42.8 794.0 542.7 54.0 574.0 574.0 574.0 578.1 578.1 587.1	0.00 22.50 45.00 90.00 112.50 1157.50 125.00 205.00 205.00 2247.50 2247.50 2247.50 2247.50 2247.50 2247.50 225.50 2247.50 225.50 20.50 20.50 250 250 250 250 250 250 250 250 250 2	26.0 360.2 360.6 451.3 451.4 222.4 264.5 395.1 1 45.3 395.1 1 45.6 34 4 402.3 4 45.3 4 34.4 32.4	9.4 10.67 10.4 11.4 11.4 11.9 152.5 10.24 10.25 10.25 10.35 10.35 10.35 10.35 10.35 10.35 10.35 10.35 10.56	54.2 62.1 69.0 76.4 76.0 78.1 71.8 70.4 76.2 70.4 76.2 76.2 76.3 71.1

TABLE 2--PEDESTRIAN WIND VELOCITIES AND TURBULENCE INTENSITIES

SAN DIEGO INTERCONTINENTAL HOTEL

WIND	UMEAN/UINF	URMS/UINF	UMEAN+3+URMS/UINF
Azimuth	(Percent)	(Percent)	(Percent)
025000 2457.500 4670.500 11357.500 11357.500 11580257.500 200 11580257.500 200 200 200 200 200 200 200 200 200	6745644805575142 44500521770410448 2345452321704448 2345452321704448 245452321704448 245452321704448 245452321704448 2454523217044448 2454523217044448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 2454522170444448 24545221170444448 24545221170444448 24545221170444448 24545221170444448 24545221170444448 24545221170444448 245452211704444448 2454522117044444448 2454522117044444448 24545221170444444448 24545221170444444448 2454522117044444444448244444844484444444444444444	3284911092602708 106.1092602708 111111111119898	56298377961360336 567878520185180014 567185785760336 518014 518518014

* * GREATEST VALUES * *

UMEAN/UINF (PERCENT)

URMS/UINF (PERCENT)

UMEAN+3*RMS/UINF (PERCENT)

LOC	AZ	MEAN	RMS	N+3RMS	LOC	ΑZ	NEAN	RMS	M+3RMS	LOC	AZ	MEAN	RMS	M+3RMS
18	315.0	78.8	14.1	121.0	17	112.5	45.7	27.7	128.8	i 7	315.0	50.7	26.3	129.6
19	315.0	59.3	12.7	97.3	17	315.0	50.7	26.3	129.6	17	112.5	45.7	27.7	128.8
13	315.0	58.3	13.8	99.8	17	135.0	45.3	22.4	112.5	18	315.0	78.8	14.1	121.0
15	337.5	56.4	14.3	99.4	i 7	292.5	31.9	21.4	96.0	16	337.5	55.3	20.6	117.2
8	202.5	55.8	11.6	90.7	16	67.5	50.1	21.0	113.1	18	337.5	52.2	20.8	114.5
16	337.5	55.3	20.6	117.2	i 8	45.0	44.6	20.9	107.3	16	67.5	50.1	21.0	113.1
14	180.0	54.4	9.6	83.0	18	337.5	52.2	20.8	114.5	17	135.0	45.3	22.4	112.5
3	315.0	54.2	9.0	81.3	16	337.5	55.3	20.6	117.2	18	67.5	47.1	20.6	108.9
8	225.0	54.0	13.7	95.2	18	67.5	47.1	20.6	108.9	18	45.0	44.6	20.9	107.3
-	157.5			99.7	16	45.0	42.9	19.2	100.5	13	337.5	51.9	17.3	103.8

PERCENTAGE FREQUENCY OF WIND DIRECTION AND SPEED

	SAN DIE	GO · CALI	FORNIA	(1965-1974)	
SEASON : ANI	NUAL	NO. OF	0ES. = 29216	HT. OF MEAS = 14. FT	
"ELBOITY LE	ELS TN	MPH			
DIRECTION	Ç~ 3	4-7	8-12 13-18	19-24 25 + TOTAL	
NNNEE Sees w Winden Sees w Winden Seuw Winden Tototo	1 200 200 1 100 1 10	0.0 6 (80 10 20 0 00 20 0 00 30 0 00 30 0 00 30 0 00 30 0 00 30 80 20 90 50 50 200 30 80 200 30 50 200 30 30 200 30 30 200 30 30 200 30 30	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	

	Beaufort number	Speed (mph)	Effects
Calm, light air	0, 1	0- 3	Calm, no noticeable wind
Light breeze	2	4- 7	Wind felt on face
Gentle breeze	3	8-12	Wind extends light flag Hair is disturbed Clothing flaps
Moderate breeze	4	13-18	Raises dust, dry soil and loose paper Hair disarranged
Fresh breeze	5	19-24	Force of wind felt on body Drifting snow becomes airborne Limit of agreeable wind on land
Strong breeze	6	25-31	Umbrellas used with difficulty Hair blown straight Difficult to walk steadily Wind noise on ears unpleasant Windborne snow above head height (blizzard)
Near gale	7	32-38	Inconvenience felt when walking
Gale	8	39-46	Generally impedes progress Great difficulty with balance in gusts
Strong gale	9	47-54	People blown over by gusts

SUMMARY OF WIND EFFECTS ON PEOPLE

Note: Table from Reference 4, p. 40.

CALCULATION OF REFERENCE PRESSURE

- 1. Basic wind speed from ANSI A58.1 (Ref. 6): 50-yr fastest mile at 30 ft = 70 mph Mean hourly wind speed = $\frac{70}{1.25}$ = 56.0 mph Mean hourly gradient wind speed = 56.0 $(\frac{1000}{30})^{.17}$ = 101.6 mph Mean hourly wind at ref location U_{∞} = gradient wind Reference pressure = 0.5 ρU_{∞}^{2} = (0.00256) (101.6)² = 26.5 psf Use reference pressure = $\frac{27 \text{ psf}}{27 \text{ psf}}$
- 2. Loads for 100-yr recurrence wind: 100-yr fastest mile at 30 ft = 70 mph (Ref. 6) no change in load.
- Gust load factors to convert hourly mean integrated loads to various gust durations (see Sect. 4.4):

Gust Duration, sec	Gust Load Factor
10-15	$(1.4)^2 = 1.96$
30	$(1.32)^2 = 1.74$
45	$(1.26)^2 = 1.59$

30 sec duration load factor was used in Table 7.

TABLE 6A PEAK LOADS FOR CONFIGURATION A LARGEST VALUES OF GLADDING LOAD

SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN Reference pressure = 27 0 PSF

TAF	AZI- MUTH	PRESS COEFF	NEGATIVE P PEAK PSF	DSITIVE PEAK	TAP	AZ1- Muth	PRESS COEFF	NEGATIVE P PEAK PSF	OSITIVE Peak	TAP	AZI- Nuth	PRESS COEFF	NEGATIVE F PEAK PSF	PEAK
10/74/0707010/04/00/00004/00/00/00/00/00/00/00/00/00	GOGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGGG	4079774940975980801011011111111111111111111111111111	1	1121 2122000000000000000000000000000000	9012345678901234 56789012345678901234567890123412	00000000000000000000000000000000000000	347-99634669372480111111111111111111111111111111111111		362518791002291504260605312175865494331597062219 3643333304423334303213042605051212175865494331597062219	245678901234567890123456789012345678901234567890 2442222222222222222222222222222222222	216000000000000000000000000000000000000	752654588768460872819259148378512748387420013374 435955670568460872819259148378512748387420013374	641996511386648510521583867472393768920856538393 96121148862443072113416102131985699121708469523533 96429965113866485105215844534554344354856952553333 96429965113866485105215844534554343545555353333	64596395747500%70105758744681974%%%1154074139%% 19368457.0019343417.%76643%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%%

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 27.0 PSF

TAP	AZI- Muth	PRESS COEFF	NEGATIVE P PEAK PSF	PEAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE P PEAK PSF	PEAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE PEAK PS	PEAK
19745678901678901678901074567890147456789014745678 55555555555555666666666666666666666	00000000000000000000000000000000000000	406307943707?67091064406561294450061343951919721 3397.66323767.67091064406561294450061343951919721 11111111111222111111111111111111	319822519038721366534421200128439486823579233955 	212333333331233333232321133323222222222	901234567890123456789012123456789012345678123456 9000000000111111111122200000001111111112000000		939145122729621968574900123872739211805286711414 999901622000089019000099895551944177806669776222341 111111111111111111111111111111111	687376755508950202432294704314658736945507293202 6367042713425706221130040110689065256525917469212 6367042713425706221130040110689065256525917469222 63677576755508950202413004011068906566525917469222 63677576755508950202432294704314658736945507293202	712812816969199770385870290011353592332181577127 7555946757873215689885614540256681917860887022680 2321281281696919977038587029001135359238181577127	55555555555566666666667777777777777777	122 2 222 122142678009814214804024423200000000000000000000000000000	324560887893905959581449427451939254450043583447 00821232180679990267431984274519392184675833700288 1111111111111111111222211	956846736643510596393817064654622327969668508685	435474462149446381074242432125722480330315226504

TABLE 6A. PEAK LOADS FOR CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST IOWER IN LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 27.0 PSF

TAP	AZI- Muth	PRESS Coeff		PEAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE I PEAK PSI	PEAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE PEAK PS	POSITIVE PEAK F
803 902 903 903 905 906	230 320 280 40 110 220	49117986 1111659883 111117986	-30.2 -43.3 -42.3 -53.7 -50.7	22.7 12.2 15.2 16.4 14.6 14.9	907 908 910 911 912	230 40 150 210 220	-1.82 -1.68 -2.84 -1.68 -1.68 -1.44	- 49 . 2 - 45 . 4 - 76 . 4 - 56 . 4 - 45 . 3 - 38 . 9	13.7 12.8 16.1 14.2 13.9	913 914 915 916 917 918	70 230 140 350 220 80	-2.59 1.74 2.06 -1.58 1.69 1.40	-69.8 -47.5 -455.8 -42.8 -425.8 -37.8	16.1 12.5 15.9 16.1 21.7 13.3

* * 15 GREATEST PRESSURE MAGNITUDES * *

T P F;	AZI- Muth		NEGATIVE PEAK	PEAK
275	50	-3.15	-85 2	32 4
264	40	-2.86	-77 2	38.0
909	60	-2.84	-76.6	16 1
734	340	-2 78	-75 0	16.2
913	70	-2 59	-69.8	16.1
175	220	-2 51	-67.9	33 2
263	30	-2 47	-66.7	32 9
906	220	-2.36	-63 7	14 9
123	230	2 36	-63 7	33.6
111	220	-2 29	-61 9	24.5
736	90	-2.24	-60 6	15.5
193	220	-2.23	- 60 1	27.2
163	230	-2.22	60.0	33,1
245	40	-2.20	59.5	37,4
153	230	-2 19	59 0	33.1

TABL Larg	E GA. Est va	PEAK I Lues oi	LOADS FOR (F Cladding	CONFIGURATI Load	ON B :	S	AN DIEC	O INTERCO Reference	NTINENTAL Pressure =	HOTEL - 27.0 P	- EAST Sf	CWER	IN	
TAP	AZI- Nuth	PPESS Coeff	NEGATIVE Peak Psi	PFAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE I Peak Psi	PEAK	TAP	AZI- Huth	PRESS COEFF	NEGATIVE PCAK PS	POSITIVE PEAK F
111 123 175 193 263	212 232 224 230 40	-2,47 -2,78 -2,71 -2,58 -2,57	-66.69 -73.3 -69.3	10.4 12.3 7.7 9.2 34.4	264 275 734 701	32 32 392 392	-2.75 -2.35 -2.35 -2.16	- 74 . 3 - 76 . 5 - 63 . 5 - 69 . 4 - 58 . 2	41:7 38:0 16:6 14:8 10:7	904 906 909 913	2260 266 74	-2,22 -1,36 -2,57 -3,20	~59,9 ~52.8 ~69.4 ~36.4	12.0 13.4 8.9 10.1

TABLE 6A. PEAK LOADS FOR CONFIGURATION B : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 27 0 PSF

TAP	AZI- Huth	PRESS COEFF	NEGATIVE PEAK	PEAK	
913	74	-3.20	-86.4	10.i	
275	32	-2 03	-76.5	38.0	
123	232	-2.78	-74.9	12.3	
264	36	-2.75	-74.3	41.7	
175	224	-2.71	-73.3	7.7	
193	230	-2.58	- 69 . 6	9.2	
909	60	-2.57	-69.4	8.9	
736	98	-2.57	-69.4	14.8	
263	40	-2.57	-69.3	34.4	
111	212	-2.47	- 66 . 8	10.4	
734	342	-2.35	-63.5	16.6	

904 26 -2.22 -59.9 12.0

901 22 -2.16 -58.2

906 226 -1.96 -52.8

10.7

13.4

* * 14 GREATEST PRESSURE MAGNITUDES * *

TABLE 68 COMPARISON OF CONFIGURATIONS A AND B : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG B EXCEEDED THAT FOR CONFIG A BY 5 PSF REF. PRESSURE = 27.0 PSF

TAP	AZINUTH	A CONFIG. PSF Load	AZINUTH	B CONFIG PSF LOAD
17936143 1799991	230 220 220 320 320 70	- 63.? - 600.1 - 600.6 - 353.7 - 69.8	232 2230 992 26 74	-73993 -773993 -55993 -5596 -5596 -4299 -5596 -4

TABLE 6A. PEAK LOADS FOR CONFIGURATION C : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSUPS = 27.0 PSF

THP	AZI- Muth	PRESS COEFF	NEGATIVE PEAK P3	PEAK	TAP	821- Nuth	PRESS COEFF	NEGATIVE P PEAK PSF	PEAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE PEAK PSI	PEAK
	COCCOCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC		0417060170027505121606018229755666697570566664	6501949982575867769482457586776748748768419978797978797978 7998819882074667759087546815757777555984-7844825344827 81921-8194998855758677590080755558741994217978444825598	901234567090123456709012345678901234567890-23412 45555555555566666666666777777777888888888	COCCOCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCCC	11111 11111111111111111111111111111111	07074740400790600604080000904004197477777777779495 96041-4440677094005704457465560944457909444577069747 96041-444067709400570445794575609444579009444577069747466 96041-44406770940057044579457605655780060944457706974747777794045	0807	84567890128456789012845676901284567893888884444444428 0000000001111111111111112022222222238888834444444567893 20222222223850128456789012222222385888354444444422	00000000000000000000000000000000000000	148872097072142512353943937398797491327335-68251	7940175072877545631724559046277409385440248819272 435454544554455868422811468025017225547110948647 4354534544554555868422811468025017225547110948647	847580477678551V058577124991873570439240817588884 67770780417999066083299547089940011117049940817588 677707804178990660832995771249918735704392408175884 67770780417804179990660832995771249918735704392408175884 6777078047767855140583771249918735704392408175884 6777078047767853140583771249918735704392408175884 67770780477678785140583771249918735704392408175884 677707804776787851405837712499187357704392408175884 6777078047767878514045837771249918735588 6777078047767858554 67770780477678585 6777078047776785857712499187357857043924084758 677707807707804778858 677707804776878857712499187878558 67770780477787878 6777078047778787878 77707804777878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707807477878 77707878 77707878 77707878 77707878 77707878 77707878 77707878 777077878 77707878 7770778778 777078 777078 77707878 777078 777078 777078 777078 777078 7770778 777078 777078 777078 777078 777078 777078 777078 777078 777078 777078 7770778 7770778 7770778 777078 777078 777078 7770778 7770778 7770778 777078 7770777778 7770778 77707770

TABLE 6A PEAK LOADS FOR CONFIGURATION C : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT LARGEST VALUES OF CLADDING LOAD REFERENCE PRESSURE = 27 0 PSF

TAF	AZJ- MUTH		NEGATIVE	POSITIVE PEAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE P Peak	PEAK	TAP	RZI- Muth	PRESS COEFF	NEGATIVE P PEAK	PEAK
- 555555555555555555555555555555555555	TH 000000000000000000000000000000000000	SF 109301074688691180685900045137704008260835447600 SF 139197501074688691180685900045137704008260835447600 SF 1391975010746886911806859000045137704008260835447600 SF 1391975010746886911806859000045137704008260835447600 SF 1391975010746886911806859000045137704008260835447600 SF 1391975010746886911806859000045137704008260835447600 SF 13919750107468869118008059000045137704008260835447600 SF 139197501074688891180771 SF 139197501074688891180771 SF 1391975010746888911800805900004551377044008828083594476600 SF 139197501074688891180771 SF 1391975010746888911800805900004551377044008828093594476600 SF 139197501071011111111111111111111111111111	9 4 4 4 5 5 5 5 5 5 5 5 5 5 5 5 5	PEAK	90 1254587890112456789012125878901211111111111111111111111111111111111	H 000000000000000000000000000000000000		F P S F F F F F F F F F F F F F	PEAK	55555555555556666666667777777777777777	H 000000000000000000000000000000000000	F 32315623111380085602832119711069332846725363695916 F 60014341016869055602832119711069332846725363695916 F 6001434341016869055602832119711069332846725363695916 F 6001434341011686690556028321197110693332846725586449578 F 60014334101168669055602832111971106933328467285369595816 F 60014334101168669055602832111971106933328467285369595816 F 6001433410116866905560283211111111111111111111111111111111111	F P P P P P P P P P P P P P	P - 2121111112212221111112222123222221111111

TABLE 6A. PEAK LOADS FOR CONFIGURATION C -Largest values of cladding load

SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT Reference pressure = 27.0 PSF

TAP	AZI- Muth	PRESS COEFF	NEGATIVE P PERK PSF	PEAK	THP	AZI- Nuth	PRESS COEFF	NEGATIVE P PEAK PSF	PEAK	TAP	AZI- Huth	PRESS COEFF	NEGATIVE PEAK PS	POSITIVE PEAK F
901 902 903 904 905 906	30 40 290 30 2 90 260	-1.71 -1.88 -1.40 -1.86 -1.55 -2.14	-46 2 -50 8 -37 7 -41 8 -57 6	11 1 86 10,2 12.0 11.2 11.9	907 908 909 910 911 912	290 30 210 210 190	-1.52 -1.308 -2.26 -1.42 -1.51	-41,0 -356,1 -351,0 -38,4 -40,7	9088 1488 1236 1122	913 914 915 916 918	90 220 210 120 220 210	-2.09 -1.47 -1.87 -1.58 -1.60 -1.75	-569.57 -590.57 -423 -4437 -4437	11.82 13.9 11.3 10.6 14.5

* * 15 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI- Muth		NEGATIVE I PEAK PSI	PEAK
164	230	-2.62	-70.6	34.8
173	220	-2.56	-69.2	30.7
144	220	-2.54	-68.5	30.9
719	٥	-2.52	-68.0	26.7
264	40	-2.49	-67.3	29.2
175	220	-2.47	-65.6	31.4
275	40	-2.40	-64.9	29.8
145	230	-2 39	-64.5	34.7
143	230	-2.30	-62.0	35.3
154	100	-2.27	-61.3	33.1
163	220	-2.26	-61.0	42.i
910	210	-2.26	-61.0	12.3
244	50	-2.25	-60.8	32.i
162	220	-2.21	- 59 . 8	30.0
245	40	-2.21	- 53 . 8	29.7

			CONFIGURATION	Ð	;
LARGEST V	ALUES OF	CLADDING	LOAD		

SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT REFERENCE PRESSURE = 27 ¢ PSF

TAP	AZI- Nuth	PRESS COEFF	NEGATIVE F PERK PSF	PERE	TAP	AZI- Huth	PRESS COEFF	NEGATIVE Peak Psi	PEAK	TAP	AZI- Muth	PRESS COEFF	NEGATIVE POS PEAK P PSF -	EAK
143 144 145 154	228 238 238 108	-1.83 -1.80 -2.06 -2.00	-49.3 -50.7 -55.6 -54.1	14.9 19.6 23.4 70.8	163 164 173 175	230 232 230 230	-2.15 -2.33 -2.51 -2.77	-58.0 -62.9 -67.7 -74.8	14.7 15.8 9.0 17.1	264 275 719 910	40 58 4 58	-2,43 -2,37 -2,31 -2,25	-63.9 2 -62.4 2	2.4 8.2 2.1 3.9

 TABLE 6A.
 PEAK LOADS FOR CONFIGURATION D
 SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT

 LARGEST VALUES OF CLADDING LOAD
 REFERENCE PRESSURE = 27.0 PSF

* * 12 GREATEST PRESSURE MAGNITUDES * *

TAP	AZI- NUTH	PRESS COEFF	NEGATIVE P FEAK	PEAK
175	230	-2.77	-74.8	17.1
173	230	-2.51	-67.7	9.0
264	40	-2.43	-65.5	32 4
275	58	-2.37	-63.9	28.2
164	232	-2.33	-62.9	15.8
719	4	-2.31	-62 4	22.1
910	58	-2.25	-60.8	13.9
163	230	-2.15	- 58 . 0	14.7
145	238	-2.06	-55.6	23.4
154	108	-2.00	-54 1	30.8
144	238	-1.38	-50.7	19.6
143	228	-1 83	-49.3	14.9

TABLE 6B. COMPARISON OF CONFIGURATIONS C AND D : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT TAPS WHERE NEGATIVE PEAK LOAD FOR CONFIG. D EXCEEDED THAT FOR CONFIG. C BY 5 PSF REF. PRESSURE = 27.0 PSF

TAP	AZIMUTH	C CONFIG. PSF Load	RZIHUTH	D CONFIG PSF LOAD
175	220	-66.ü	230	-74.8

TABLE 7. BASE Configuration	SHEAR A	AND MOMENT S Reference	UMMARY : Pressure	SAN DIEGO E 27.0	D INTERCONT GUST F	INENTAL HOTEL Actor 1.32	EAST TOWER IN
AZINUTH	SHEAR X	(KIPS) Y	MOMENT (X	(1000-FT-1 Y	(IP\$) E Z	CCEN (FT) X Y	
	455787786218823637561572168455624542 20303832273377626886341906609581559962 205998415188175145145762095815599622 205998415188175145145762077814121824 329764421111128215514576277814121824	3335191051840295252722792693077736124 579591341157415558626481611282451456 1222212211111111111111111111111111111	733164330801643110414066791560170707 3493492710821678 4784297644095651727 244443342 22221 - 12344212332 2444217	30057500009760033325909217017097045040 93686380976003809999935419274611439 21111111111111221 211111111112222		788915145670328145632204707708032198 	

TABLE 7. BASE SHE	AND MONENT SUMMARY :	SAN DIEGO INTERCO	NTINENTAL HOTEL	EAST TOWER OUT
Configuration C	Reference pressur	Re 27.0 gust	Factor 1.32	
AZIMUTH SHI	R (KIPS) HOMENT	(1000-FT-KIPS)	ECCEN (FT)	
X	Y X	Y Z	X Y	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} -194.7 \\ -23.3 \\ -37.3 \\ -37.3 \\ -37.3 \\ -37.4 \\ -551.5 \\ -37.4 \\ -551.5 \\ -355.4 \\ -551.5 \\ -733.4 \\ -555.4 \\ -555.4 \\ -555.4 \\ -768.3 \\ -722.5 \\ -768.3 \\ -733.4 \\ -555.5 \\ -737.4 \\ -122.3 \\ -200.3 \\ -237.8 \\ -555.5 \\ -339.4 \\ -555.5 \\ -5$		

	7. SHEAR TRECTION	AND MOMEN	NT DIAGRI	AMS : Configura	SI TION A	AN DIEGO IN	TERCONT REFE	INENTAL Rence p	HOTEL Ressuri	EAST TO E 27.0 PSF	WER IN	GUST F	ACTOR 1.3	32
FLCOP	HEIGHT	FORCE	(KIPS)	AREA (X	SQ FT)	PFESSURE	(PSF) Y	ECCE	N (FT)	SHEAR X	(KIPS) Y	MONENT	<1000-FT-	-KIFS) Z
15 T	0.00	-46.0	5	2034	876	-22.6	6	φ	- 1	-1362.4	157.3	-23 7	-209.3 -186.5	-36.8 -36.8
2 N D	17 00	-46.0	- 4	2034	876	-22.6	- 4	¢	- 2	-1316.4	157.8	-21.0		
78 D	34 00	- 62 . 1	17 2	2743	1195	-22.7	:4.4	- 5	-17	-1270.4	158.2	-18.3	-164.5	-36.7
4 T H	54.00	-52 7	5.0	2363	1038	-22.9	4.8	- 3	-29	-1208 3	141.0	-15 3	-139.7	-35.5
STH	63.75					-22.8	4.1	-2	-29	-1155 6	136.0	-14.0	-128.2	-34.0
6TH	73.50	- 52 5	4.2	2303	1038					-1103.1	131.8	-12.7	-117.2	-32.4
7TH	03.25	~ 51.5	5.3	2303	1038	-22.4	5.1	- 3	-23	-1051.6	126.5	-11.4	-106.7	-30.9
8TH	93.00	-50.5	6.3	2303	1038	-21.9	6.1	- 4	-29	-1001.1	120.1	-10.2	-96.7	-29.4
9TH	102.75	- 49 . 5	7.4	2303	1038	-21.5	7.1	- 4	-29	-951.6	112.7	-9.1	-87.2	-28.0
10TH	112.50	- 48 .8	8.2	2303	1038	-21.2	7.9	- 5	-29	-902.8	104.6	-9.0	-78.1	-26.5
11TH	122.25	-49.1	8.1	2303	1038	-21.3	7.8	- 5	-29	-853.7	96.5	-70	-69 6	-25.0
		-49.4	Q. Q	2303	1638	-21.4	7.7	- 5	-30	-804.4	88.5	-5.1	-61.5	-23.5
1278	132.00	-49.6	7.9	2303	1038	-21.5	76	- 5	-30	-754.8	80.6	-5 3	-53.9	-22.0
13TH	141.75	-49.9	7.8	2303	1038	-21.7	7.6	- 5	-30			-4 6	-46.8	-20 5
14TH	151.50	-50.4	6.0	2303	1038	-21.9	5.8	- 4	-31	-704.8	72.7			
15TH	161.25	-51.1	2.4	2303	1038	-22.2	23	- 1	-32	-654.5	66.7	-3.9	-40.2	- 18.9
16TH	171.00	-51.3	3.8	2303	1038	-22.3	3.6	- 2	-31	-603.3	64.3	-3.3	-34.0	-17.2
17TH	180.75	-51.5	5.2	2303	1038	-22.4	5.0	- 3	-31	-552 O	60.6	-2.6	-28.4	-15.6
18TH	130.50				1038	-22.5	6.3	- 4	-30	-500.5	55.4	-2.1	-23.3	-14.0
19TH	200.25	-51.7	6.6	2303						-448.8	48.8	-1.6	-18.6	-12.4
20TH	210.00	-51.9	7.9	2303	1038	-22.5	7.6	-5	-30	-396 9	40.9	-1 1	-14.5	-10.8
21ST	219.75	- 52 . 6	7.7	2303	1038	-22.8	7.4	- 4	-29	-344.3	33.2	8	-10.9	- 9.3
2 2 N D	229 50	-53.2	7.5	2303	1038	-23.1	7.2	- 4	-28	-291.1	25.8	5	-7.8	-7.7
23RD	239.25	-53.9	7.2	2303	1638	-23 4	69	- 4	-28	-237 2	18.6	- 3	-5.2	- 6.2
		-54.6	7.0	2303	1038	-23.7	6.7	- 3	-27	-182.6	11 6	- 1	-3.2	-4 7
24TH	249.00	- 55 . 2	6.7	2303	1038	-24.0	6.5	- 3	-27	-127.4	4.8	- 0	-1.7	-3.2
25TH	258.75	- 52 . 2	3.8	2303	103 8	-22.7	3.7	- 2	-26	-12/.4	T . U	. V	4 . •	0.2

TABLE WIND D	7. SHEAR I	AND MOMENT	T DIAGRA	NS : CONFIGURA	ATION A	N DIEGO IN	TERCONT REFE	INENTAL HOTEL - Rence pressure	- EAST TE 27.0 PSF	OVER IN	GUST FA	CTOR 1.3	2
FLOOR	HEIGHT	FORCE ((KIPS)	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT- Y	KIPS) Z
MECH	268.50	-75.2	• •	4252	1917	-17.7	5	-0 -24	-75.2	1.0	- , ¢	7	-1.8
TOP	286.50	- (3.2	1.0	7432 171	****	••••			0.0	0.0	¢.¢	¢.¢	0.0

TABLE Vind D	7 SHEAR IRECTION	AND NONEL	NT DIAGR	ANS : CONFIGURA	TION A	AN DIEGO IN	TERCONT Refe	INENTAL Rence P	HOTEL Ressur	EAST T(E 27.0 PSF	WER IN	GUST I	FACTOR 1.3	32
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (SQ FT>	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	N ON ENT X	(1000-FT- Y	-KIPS) Z
1 S T	0.00	-41.3	4	2034	876	-20.3	4	٥	-0	-1250.5	276.3	- 44 . 3	-193.0	-50.0
2ND	17.00							0	- 2	-1209.2	276.7	- 39 . 6	-172.1	-50.0
3RD	34.00	-41.8	-,4	2034	876	-20.5	4			-1167.4	277.1	- 34 . 9	-151.9	-49.9
4TH	54.00	- 58 . 4	17.9	2743	1195	-21.3	14.9	- 6	-19	-1109.0	259.2	-29.5	-129.2	-48.7
518	63.75	- 45 . 4	8.9	2303	1038	-19.7	8.6	- 8	-41	-1063.6	250.3	-27.0	-118.6	-46.8
		-44.7	8.7	2303	1038	-19.4	8.4	- 8	-42	-1018.9	241.6	-24.6	-108.4	-44.8
6TH	73.50	-45.0	9.8	2303	1038	-19.5	9.5	- 9	-42	-973.9	231.8	-22.3	-98.7	-42.8
7T H	83.25	-45.2	11.0	2303	1038	-19.6	10.5	-10	-41	-928.7	220.9	-20.1	-89.4	-40.9
8T H	93.00	-45.5	12.1	2303	1038	-19.7	11.6	-11	-4i					-38.9
9T H	102.75	- 45.7	12.9	2303	1038	-19.8	12.4	-11	-40	-883.2	208.8	-18.0	-80.6	
1 ¢ T H	112.50	-45.9	12.7	2303	1038	-19.9	12.2	-11	-41	-837.5	195.9	-16.1	-72.2	-36.9
11TH	122.25		12.5	2303	1038	-20.0	12.1	-11	-41	-791.6	183.2	-14.2	-64.3	-34.9
12TH	132.00	-45.0						-11	-42	-745.6	170.7	-12.5	-56.8	-32.9
13TH	141.75	-46.2	12.4	2303	1038	-20.1	11.9			-699.4	158.4	-10.9	-49.7	-30.8
14TH	151.50	- 46 . 4	12.2	2303	1038	-20.1	11.7	-11	-42	-653.0	146.2	-9.4	-43.1	-28.7
	161.25	- 46 . 4	10.4	2303	1038	-20.2	10.0	-10	-44	-606.6	135.7	-8.0	-37.0	-26.5
15TH		-46.7	7.3	2303	1038	-20.3	7.0	- 7	-47	~559.9	128.4	-6.7	-31.3	-24.2
16TH	171.00	- 47.5	9.1	2303	1038	-20.6	8.7	- 9	-46	-512.4	119.4	-5.5	-26.1	-22.0
17TH	180.75	- 48 . 3	10.8	2303	1038	-21.0	10.4	-10	-45			-4.4	-21.3	-19.7
18TH	190.50	- 49 . 1	12.6	2303	1038	-21.3	12.1	-11	-43	-464.2	108.5			
19TH	200.25	-49.9	14.3	2303	1038	-21.6	13.8	-12	-42	-415.1	95.9	-3.4	-17.0	-17.4
20TH	210.00		13.9	2303	1038	-21.7	13.4	-12	-41	-365.2	81.6	-2.6	-13.2	-15.1
21ST	219.75	- 49 . 9								-315.4	67.7	-1.8	-9.9	-12.9
22ND	229.50	- 49 . 9	13.4	2303	1038	-21.7	12.9	-11	-41	-265.5	54.3	-1.2	-7.1	-10.7
23RD	239.25	- 49 . 9	12.9	2303	1038	-21.7	12.5	-10	-40	-215.6	41.4	8	-4.7	-8.6
2478	249.00	- 49 . 9	12.5	2303	1038	-21.7	12.0	-10	-39	-165.7	28.9	4	-2.9	-6.6
		-49.9	12.0	2303	1038	-21.7	11.6	- 9	-38	-115.7	16.9	2	-1.5	-4.5
25TH	258.75	- 48 , 4	8.6	2303	1038	-21.0	8.3	- 7	-38	1 4 W - 1	••••			

TABLE Vind d	7 SHEAR IRECTION	AND MOMENT	T DIAGRA	MS : Configur	ATION A	N DIEGO IN	TERCONT Refei	INENTAL Rence Pr	HOTEL - Essure	- EAST TO 27.0 PSF	DWER IN	GUST FA	CTOR 1.3	2
FLOOR	HEIGHT	FORCE ((KIPS) Y	AREA X	(SQ FT) Y	PRESSURE	(PSF) Y	ECCEN	(FT) Y	SHEAR	(KIPS) Y	NOMENT (X	1000-FT- Y	KIPS) Z
MECH	268.50	-67.3	8.3	4959	1917	-15.8	4 7	- 5	-38	- 67 . 3	8.3	1	6	-2.6
TOP	286.50	- 67.3	0.3	4232	1711	15.5	•.•	•		Ø, Ø	¢.¢	0 , 0	¢.¢	¢.¢

	7. SHEAR IRECTION	AND NOME	NT DIAGR	ANS : CONFIGUR	ATION A	AN DIEGG IN	TERCON Ref	TINENTAL Erence pr	HOTEL	EAST T 27.0 PSF	OVER IN	GUST I	ACTOR 1.	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MONENT X	(1000-FT Y	-KIPS) Z
1 S T	0.00							٨	•	-953.5	297.3	-49.3	-146.0	-50.6
2ND	17.00	-40.0	-1.1	2034		-19.7	-1.3	0	-2	-913.5	298.5	-44.2	-130.1	-50.5
3R D	34.00	-40.4	8	2034		-19.9	9	Ó	- 3	-873.1	299.3	- 39 . 1	-114.9	-50.4
4TH	54.04	-49.7	14.7	2743		-18.1	12.3	- 7	-23	-823.4	284.6	-33 3	-98.0	-49.2
5TH	63.75	- 32 . 8	8.7	2303	1038	-14.2	8.4	-14	-54	-790.6	275.9	-30.6	-90.1	-47.3
6TH	73.50	- 32 . 3	8.5	2303	1038	-14.0	8.2	-15	-55	-758.3	267.4	-27.9	-82.6	-45.4
7TH	83.25	- 32 . 2	9.9	2303	1038	-14.0	9.5	-17	-54	-726.0	257.5	-25.4	-75.3	-43.5
	93.00	- 32 . 1	11.3	2303	1039	-13.9	10.9	-19	-53	-693.9	246.2	-22.9	-68.4	-41.6
8TH		-32.0	12.7	2303	1039	-13.9	12.2	-20	-51	-661.9	233.5	-20.6	-61.8	-39.7
9TH	102.75	- 32 . 0	13.6	2303	1038	-13.9	13.1	-21	-50	-629.9	219.9	-18.4	-55.5	-37.8
1 ¢ T H	112.50	- 32 . 3	13.5	2303	1038	-14.0	13.0	-21	-51				-49.5	-35.8
1178	122.25	- 32 . 6	13.3	2303	1038	-14.1	12.8	-21	-52	-597.6	206.4	-16.3		
12TH	132.00	- 32 . 8	13.2	2303	1038	-14.3	12.7	-21	-53	-565.0	193.0	-14.3	-43.8	-33.8
13TH	141.75	- 33 . 1	13.0	2303	1039	-14.4	12.5	-21	-54	-532.2	179.9	-12.5	-38.5	-31.8
14TH	151.50	- 33 . 2	11.4	2303		-14.4	11.0	-20	-59	-499.1	166.8	-10.8	-33.5	-29.7
15TH	161.25	-33.7	8.7	2303		-14.6	8.4	-17	-65	-465.8	155.4	-9.3	-28.8	-27.5
16TH	171.00			2303		-15.1	10.1	-19	-62	-432.1	146.8	-7.8	-24.4	-25.2
17TH	180.75	-34.9	10.5							-397.2	136.2	-6.4	-20.3	-22.9
18TH	190.50	-36.1	12.4	2303		-15.7	11.9	-20	-58	-361.1	123.8	-5.1	-16.6	-20.5
19TH	200.25	- 37 . 3	14.3	2303		-16.2	13.7		-55	-323.9	109.6	-4.0	-13.3	-18.2
20TH	210.00	- 39 . 4	16.1	2303		-16.7	15.5		-52	-285.5	93.5	-3.0	-10.3	-15.8
21ST	219.75	- 38 . 7	15.5	2303	1038	-16.8	14.9	-20	-51	-246.8	77.9	-2.2	-7.7	-13.5
22ND	229.50	- 38 . 9	14.9	2303	1038	-16.9	14.4	-19	-50	-207.9	63.0	-1.5	-5.5	-11.3
23RD	239.25	- 39 . 1	14.3	2303	1038	-17.0	13.8	-18	-49	-168.8	48.7	9	-3.7	-9.1
		- 39 . 4	13.8	2303	1038	-17.1	13.3	-17	-48	-129.5	34.9	5	-2.2	-7.0
24TH	249.00	-39.6	13.2	2303	1038	-17.2	12.7	-16	-47	-89.9	21.7	3	-1.2	-4.9
25TH	258.75	- 37 . 9	10.7	2303	1038	-16.4	10.3	-14	- 4 9	- 07 / 7	£ £ . (·· . 4	• • 4	.

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	T DIAGRA	MS : CONFIGURAT	SAN Fion a	DIEGO IN	TERCONT REFE	INENTAL HOTEL - Rence pressure	- EAST TI 27.0 PSF	DWER IN	GUST F	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (S X	\$Q FT> Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	HOHENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	-52.0	11.0	4252	1917	-12.2	5 8	-11 -53	- 52 . 0	11.0	1	÷.5	-2.9
TOP	286.50	- J2 . V	11.0	TEJE	1721		•.•		Q . Q	Q.Q	0.0	¢.¢	¢.¢

	7 SHEAR IRECTION	AND NOMEN	IT DIAGR	ANS : Configur:	SI Ation A	AN DIEGG IN	TERCONT REFE	INENTAL Rence P	HOTEL Ressure	EAST TO 27.0 PSF	WER IN	GUST F	ACTOR 1.3	32
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	-KIPS) Z
1ST	0.00			· · · · ·				o	- 5	-790.3	254.5	-43.1	-118.5	-51.5
2ND	17.00	-38.0	-3.9	2034	876	-18.7	-4.4		-	-752.2	258.4	-38.7	-105.3	-51.3
3RD	34.00	-40.4	-3.3	2034	876	-19.8	-3.7	<i>•</i>	- 3	-711.9	261.7	-34.3	-92.9	-51.1
4TH	54.00	-44.7	9.9	2743	1195	-16.3	8.3	-6	-29	-667 2	251.7	- 29 . 1	-79.1	-49.8
5TH	63.75	- 24 . 5	7.4	2303	1039	-10.6	7.1	-20	-65	-642.6	244.4	-26.7	-72.7	-48.0
6TH	73.50	- 25 . 2	7.3	2303	1038	-10.9	7.0	-19	-64	-617.4	237.1	-24.4	-66.6	-46.3
7TH	83.25	- 25 . 4	8.8	2303	1039	-11.0	8.5	-22	-63	-592.1	228.3	-22.1	-60.7	-44.5
8TH	93.00	- 25 . 5	10.3	2303	1038	-11.1	10.0	-25	-62	-566.5	217.9	-19.9	-55.0	-42.7
81 H	102.75	-25.7	11.8	2303	1039	-11.2	11.4	-28	-60	-540.8	206.1	-17.9	-49.6	-40.8
		- 26 . 0	12.9	2 3 0 3	1038	-11.3	12.4	-29	-59	-514.9	193.2	-15.9	-44.5	-38.9
1 ¢ T H	112.50	- 26 . 5	12.5	2303	1038	-11.5	12.0	-29	-61	-488.4	180.7	-14.1	-39.6	-36.9
11TH	122.25	-27.0	12.1	2303	1038	-11.7	11.7	-28	-63	-461.5	168.6	-12.4	-35.0	-34.9
12TH	132.00	- 27 . 4	11.8	2303	1038	-11.9	11.4	-28	-64	-434.0	156.8	-10.8	-30.6	- 32.8
13TH	141.75	- 27 . 9	11.4	2303	1038	-12.1	11.0	-27	-66	-406.1	145.3	-9.3	-26.5	-30.6
14TH	151.50	-28.9	9.6	2303	1038	-12.5	9.3	-23	-69					-28.4
15TH	161.25	-30.2	7.0	2303	1038	-13.1	6.7	-17	-72	-377.2	135.7	-8.0	-22.7	
16TH	171.00	-30.3	9.0	2303	1039	-13.1	8.7	-21	-71	-347.0	128.7	-6.7	-19.2	-26.1
17TH	180.75	-30.3	11.1	2303	1038	-13.2	10.7	-25	-69	-316.7	119.6	-5.5	-15.9	-23.8
18TH	190.50	- 30 . 3	13.1	2303	1039	-13.2	12.6	-29	-67	-286.4	108.6	-4.4	-13.0	-21.4
19TH	200.25	-30.4	15.1	2303	1038	-13.2	14 6	-32	-65	-256.1	95.5	-3.4	-10.3	-19.0
2 O T H	210.00	-30.4	14.3	2303	1038	-13.4	13.8	-30	-64	-225.7	80.3	-2.5	- 8.0	-16.5
21ST	219.75					-13.6	13.0	-27	-63	-194.8	66.1	-1.8	-5.9	-14.1
2 2 N D	229.50	- 31 . 4	13.5	2303	1038					-163.4	52.6	-1.2	-4.2	-11.8
2 3 R D	239.25	-31.9	12.6	2303	1038	-13.8	12.2	-25	-62	-131.5	40.0	8	- 2 . 8	-9.5
24TH	249.00	- 32 . 4	11.8	2303	1038	-14.1	11.4	-22	-61	-99.1	28.2	4	-1.6	-7.3
25TH	258.75	-32.9	11.0	2303	1038	-14.3	10.6	-20	-59	-66.2	17.2	- 2	8	-5.1
		-29.7	8.6	2303	1038	-12.9	8.3	-19	-65					

TABLE WIND D		AND MONEN'	T DINGRI	NS CONFIGUR		N DIEGO INT	REFE	INENTAL HOTEL - Rence pressure	- EAST TO 27.0 PSF	DWER IN	GUST FA	CTOP 1.3	2
FLOOR	HEIGHT	FORCE ((KIPS)	AREA X	(SQ FT) Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR	(KIPS) Y	HOMENT (X	1000-FT- Y	KIPS) Z
MECH	268.50	-36.5	8,6	4252	1917	-8.6	4 5	-18 -79	- 36 . 5	8.6	1	3	-3.0
TOP	296.50	-36.3	Q.Q	7272	1710	-0.0	T .W	10 (7	0.0	0.0	0.0	0.0	0 .0

TABLE Wind (7 SHEAR DIRECTION	AND MONEN	T DIAGR	ANS : Configurs	SA TION A	N DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL	EAST TI 27.0 PSF	OWER IN	GUST F	ACTOR 1.3	32
FLOOR		FORCE	(KIPS)	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	-KIPS) Z
1 S T	0.00						-7.0		0	-693.8	196.1	-34.6	-96.7	-53.3
210	17.00	- 42 . 6	-6.1	2034	876	-20.9		-0		-651.3	202.3	-31.2	-85.3	-53.4
3RD	34.00	-50.3	-6.2	2034	876	-24.8	-7.1	0	- 3	-600.9	208.5	-27.7	-74.6	-53.2
4TH	54.00	- 54 . 8	5.9	2743	1195	-20.0	4.9	- 3	-30	-546.1	202.6	-23.6	-63.2	-51.6
578	63.75	-23.5	5.0	2303	1038	-10.2	4.8	-15	-71	-522.6	197.6	-21.7	-58.0	-49.8
51 H 6 T H	73.50	-24.3	4.7	2303	1038	-10.6	4.5	-13	-69	-498.3	192.9	-19.8	-53.0	-48.1
		-23.9	6.7	2303	1038	-10.4	6.5	-20	-71	-474.4	186.2	-17.9	-48.3	-46.3
7TH	83.25	-23.5	8.8	2303	1038	-10.2	8.5	-27	-72	-450.8	177.4	-16.2	-43.7	-44.3
8TH	93.00	-23.1	10.8	2303	1038	-10.0	10.4	-34	-72	-427.8	166.6	-14.5	-39.5	-42.3
9TH		- 22 . 6	12.2	2303	1038	-9.8	11.7	-39	-72	-405.1	154.4	-12.9	-35.4	-40.2
1 ¢ T H	112.50	-22.0	11.5	2303	1038	-96	11.1	-40	-76	-383.1	142.9	-11.5	-31.6	-38.1
11TH	122.25	-21.4	10.9	2303	1038	-9.3	10.5	-41	-80	-361.7	132.1	-10.1	-27.9	-35.9
12TH	132.00	-20.8	10.2	2303	1038	-9.0	9.8	-41	-94	-340.9	121.9	-8.9	-24.5	-33.7
13TH	141.75	-20:2	9.6	2303	1038	- 8.8	9.2	-42	-89				-21.3	-31.5
14TH	151.50	-21.0	6.2	2303	1038	-9.1	6.0	-29	-97	-320.8	112.3	-7.8		-29.3
15TH	161.25	-24.4	. 9	2303	1038	-10.6	. 9	- 3	-94	-299.8	106.1	~6.7	-18.2	
16TH	171.00	-23.9	4.2	2303	1038	-10.4	4.0	-17	-96	-275.4	105.2	-5.7	-15.4	-27.0
17TH	180.75	-23.4	7.5	2303	1038	-10.1	7.2	-30	-94	-251.6	101.0	-4.6	-12.9	-24.7
18TH	190.50		10.8	2303	1038	-9.9	10.4	-42	-89	-228.2	93.5	-3.7	-10.5	-22.2
19TH	200.25	-22.9			1038	-9.7	13.5	-52	-82	-205.3	82.7	-2.8	- 8.4	-19.7
2 O T H	210.00	- 22 . 4	14.0	2303		-10.2	12.5	-45	-81	-182.9	68.7	-2.1	-6.5	-17.2
215T	219.75	-23.6	13.0	2303	1038					-159.3	55.7	-1.5	-4.9	-14.7
2 2 N D	229.50	-24.7	11.9	2303	1038	-10.7	11.4	-38	-80	-134.6	43.9	-1.¢	-3.4	-12.2
23RD	239.25	- 25 . 9	10.8	2303	1038	-11.2	10.4	-32	-77	-108.7	33.1	6	-2.2	-9.9
2411	249.00	-27.0	9.7	2303	1038	-11.7	9.3	-27	-75	-81.7	23.4	4	-1.3	-7.6
2578	258.75	- 29 . 2	8.6	2303	1038	-12.2	8.3	-22	-72	- 53 . 5	14.8	2	7	-5.4
2318	230.13	- 25 . 2	7.5	2303	1038	-10.9	7.2	-24	-80					

TABLE Vind D	7. SHEAR IRECTION	AND NOMEN 40	IT DIAGR	ANS : Configura	SAI Tion a	I DIEGO IN'	TERCONT REFE	INENTAL HOTEL - Rence pressure	- EAST TO 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT> Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	-29.4		4252	1917	-6.7	7 0	-27 -106	-28.4	7.3	1	3	-3.2
TOP	286.50	-28.4	(, 3	4232	1716	- 5.7	3.8	-27 -106	\$.\$	Q .Q	Ģ.Ģ	Q . Q	Q.Q

TABLE Vind D	7 SHEAR IRECTION	AND NOME	IT DIAGRI	AMS : Configurf		AN DIEGO IN	TERCONT Refe	INENTAL HOTEL Rence pressure	EAST T 27.0 PSF	OWER IN	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	PRE-SSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	MOMENT X	(1009-FT) Y	-KIPS) Z
IST	6.6G		_	- · - ·			-	A A	-608.3	216.9	- 39 . 4	-83.5	-44.5
2ND	17.00	-45.6	3	2034	876	-22.4	- 3	0 -4	-562.7	217.1	-35.7	-73.6	-44.3
3RD	34,00	-52.4	-2.1	2034	876	-25.8	-2.4	0 -6	-510.3	219.3	-32 0	-64.4	-44.0
4TH	54.00	-58.7	3.6	2743	1195	-21.4	3.0	-1 -24	-451.6	215.7	-27.7	-54.8	-42.6
STH	63.75	-14.8	3.1	2303	1038	- 6, 4	3.0	-23 -109	-436 8	212.6	-25.6	-50.5	-40.9
6TH	73.50	-15.0	2.6	2303	1038	-6.5	25	-19 -111	-421.8	210.0	-23.5	-46.3	-39.2
7TH	83.25	-15.9	5.0	2303	1038	-6 9	4.8	-30 -96	-405.8	205.0	-21 5	-42.3	-37.5
		-16.9	7.4	2303	1038	-7.3	7.1	-36 -92	-389.0	197.6	-19 5	-38.4	-35.8
8TH	93.00	-17.8	9.8	2303	1038	-7.7	9.4	-39 -71	-371 2	187.8	-17 7	-34.7	-34.2
9TH	102.75	-18.5	11.5	2303	1038	-8.0	11.1	-39 -63	-352.7	176.3	-15.9	-31.2	-32.6
1 Q T H	112.50	-18.9	11.3	2303	1038	- 8.2	10.9	-39 -64	-333.8	165.0	-14.2	-27 8	-30.9
11TH	122.25	-19.2	11.2	2303	1038	-83	10.8	-38 -65			-12 7	-24.7	-29.2
12TH	132 00	-19.5	11.0	2303	1038	-8.5	10.6	-37 -66	-314.6	153.8			-27.5
13TH	141.75	-19.9	10.9	2303	1038	-8.6	10.5	-27 -67	-295.1	142.7	-11 2	-21.7	
14TH	151.50	-19.0	7.1	2303	1038	-8.2	6.9	-32 -84	-275.2	131.9	-9.9	-18.9	-25.8
15TH	161.25	-16.4	1	2303	1038	-7.1	1	1 - 124	-256.3	124.7	-8 6	-16.3	-24.0
16TH	171.00	-17.5	3.5	2303	1038	-7.6	3.3	-22 -112	-239.9	124.9	-7.4	-13.9	-21.9
17TH	180.75	-18.5	7 1	2303	1038	-8.0	6.8	-37 -96	-222.4	121.4	-6.2	-11.6	-19.9
18TH	190.50			2303	1038	-8.5	10.2	-44 -80	-203.9	114.3	-5.1	-9.6	-17.9
19TH	200.25	-19.5	10.6				13.7	-46 -67	-184.4	103.7	-4.0	-7.7	-15.8
20TH	210.00	- 20 . 5	14.2	2303	1038	-8.9			-163 8	89.5	-3.1	-6.0	-13.8
215T	219.75	-21.2	13.8	2303	1038	-9.2	13.2	-43 -66	-142 7	75.8	-2 3	-4.5	-11.8
22ND	229.50	-21.8	13.3	2303	1638	-9.5	12 8	-40 -66	-120 9	62.4	-1.6	-3.2	-9.8
23RD	239.25	- 22 . 4	12.9	2303	1038	-9.7	12.4	-38 -65	-98 4	49.5	-1.0	-2.1	-7.9
24TH	249.00	-23.1	12.5	2303	1038	-10.0	12.0	-35 -64	-75 3	37.0	- 6	-1.3	-6.0
25TH	258.75	-23 7	12.1	2303	1038	-10.3	11.6	-32 -64	-51.6	25.0	3	7	-4.1
2018	200.10	-22.2	10.7	2303	1038	-9.7	10.3	-29 -60					

TABLE Wind D		AND MOMEI 50	NT DIAGR	AMS : Configurati	SAN On a	DIEGO IN	FERCONT 1 Refer	INENTAL HOTEL Rence pressure 2	- EAST TI 27.0 PSF	OVER IN	GUST (FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ X	FT) Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	- 29 . 4	14 7	4252 19	917	<i>.</i>	- -		-29.4	14.3	1	3	-2.4
TOP	286.50	- 27.4	14.3	4232 1	-17	-6.9	<i>c</i> .3	-33 -67	¢,¢	Q.Q	Q.Q	Q.Q	Q . Q

	7 SHEAR IRECTION	AND NOMEN	T DIAGR	ANS : Configurat		AN DIEGO II	NTERCONT Refe	INENTAL HOTEL Rence pressure	EAST TO 27.0 PSF	DVER IN	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (S X	Q FT) Y	PRESSURI X	E (PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	M OM ENT X	(1000-FT Y	-KIPS) Z
1 S T	¢ , ¢ ¢	-42.7	4.5	2034	876	-21.0	5.1	-1 -12	-443.7	234.1	-42.3	-58.8	-28.8
2ND	17.00		4.5	2034	876				-401.0	229.6	-38.4	-51.6	-28.2
3R D	34.00	- 47.3				-23.2	1.9	-0 -9	-353.8	227.9	-34.5	-45.2	-27.8
4 T H	54.00	-52.5	1.6		1195	-19.1	1.3	-1 -17	-301.3	226.4	-29.9	-38.6	-26.9
5TH	63.75	-5.6	2.5		1038	-2.4	2.4	-90 -201	-295.7	223.9	-27.8	-35.7	-25.6
€TH	73.50	-6.4	2.0		1039	-2.8	1.9	-60 -197	-289.3	221.9	-25.6	-32.9	-24.2
7TH	83.25	-8.3	4.6		1038	-3.6	4.4	-67 -121	-281.0	217.3	-23.4	-30.1	-22.9
8T H	93.00	-10.1	7.2		1038	-4.4	6.9	-57 -80	-270.9	210.2	-21.4	-27.4	-21.7
9T H	102.75	-11.9	9.8		1038	-5.2	9.4	-47 -57	-259.0	200.4	-19.4	-24.8	-20.5
10TH	112.50	-13.3	11.6		1038	- 5 . 8	11.2	-40 -46	-245.7	188.8	-17.5	-22.3	-19.5
11TH	122.25	-13.6	11.4		1038	-5.9	11.0	-37 -45	-232.2	177.5	-15.7	-20.0	-18.4
12TH	132.00	-13.8	11.2		1038	-6.0	10.7	-35 -44	-218.4	166.3	-14.0	-17.8	-17.4
13TH	141.75	-14.1	10.9		1038	-6.1	10.5	-33 -43	-204.3	155.4	-12.4	-15.8	-16.5
14TH	151.50	-14.3	10.7	2303	1038	-6.2	10.3	-31 -42	-190.0	144.6	-11.0	-13.8	-15.6
15TH	161.25	-12.2	7.4	2303	1038	-5.3	7.1	-37 -61	-177.7	137.3	-9.6	-12.0	-14.5
16TH	171.00	-7.3	1.2	2303	1039	-3.2	1.1	-28 -174	-170.4	136.1	-8.3	-10.3	-13.2
17TH	180.75	-9.1	4.5	2303	1039	-3.9	4.3	-56 -113	-161.4	131.6	-7.9	-8.7	-12.0
1874	190.50	-10.8	7.8	2303	1038	-4.7	75	-55 -76	-150.5	123.8	-5.7	-7.2	-10.7
19TH	200.25	-12.6	11.2	2303	1038	-5.5	10.7	-48 -55	-137.9	112.6	-4.6	-5.8	-9.5
2011	210.00	-14.4	14.4	2303	1038	-6.2	13.9	-42 -42	-123 6	98.2	-3 5	-4.5	-8.3
21ST	219.75	-15.3	14.1	2303	1038	-6.6	13.6	-39 -42	-108.3	84.1	-2.6	-3.4	-7.1
2280	229.50	-16.2	13.8	2303	1039	-7.0	13.2	-36 -43	-92.1	70.3	-1.9	-2.4	-5.9
23RD	239.25	-17.1	13.4	2303	1038	-7.4	12.9	-34 -43	-75.0				
		-18.0	13.1	2303	1038	-7.8	12.6	-31 -43		56.9	-1.3	-1.6	-4.7
24TH	249.00	-18.9	12.7	2303	1038	- 8.2	12.3	-29 -43	-57.0	43.9	8	-1.0	-3.5
25TH	258.75	-16.1	12.6	2303	1038	-7.0	12.2	-27 -34	-38.1	31.1	- 4	5	-2.4

TABLE Wind D	7 SHEAR IRECTION	AND MONEN	T DIAGRI	AMS : Configuration	SAN Na	DIEGO IN	TERCONT REFE	INENTAL H Rence pre	IO T E L ES SUR E	EAST TE 27.0 PSF	DWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ U	FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	HOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	-22.0	18.5	4252 19:	17	-5,2	97	-33 -	. 7 9	-22.0	18.5	2	2	-1.5
TOP	286.50	~ 22 . V	10.3	7232 17		- 5 . 2				Q.Q	Q.Q	Ø., Ø.	0.Q	¢.¢

TABLE Wind D	7. SHEAR	AND NOMEN	IT DIAGRA	NS : Configura		AN DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL	EAST TO 27.0 PSF	WER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	P RE SSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00							- 3	-14	-212 8	149.2	-27.3	-26.6	-7.6
2ND	17.00	-29.1	6.4	2034	876	-14.3	7.4			-183.7	142.8	-24.8	-23.2	-7.i
3R D	34.00	-30.0	3.2	2034	876	-14.8	3.7	-1	-11	-153.7	139.6	-22.4	-20.3	-6.8
4TH	54.00	-40.9	-2.2	2743	1195	-14.9	-1.8	1	-11	-112.7	141.7	-196	-17.7	-6.3
STH	63.75	2.2	. 7	2303	1038	. 9	.7	-89	259	-114.9	141.0	-18.2	-16.5	-5.7
6T H	73.50	2.1	. ¢	2303	1038	. 9	. 0	-4	306	-117.0	141.0	-16.8	-15.4	-5.1
778	83.25	. 6	1.9	2303	1038	. 2	1.8	-257	77	-117 5	139.1	-15.4	-14.3	-4.6
8TH	93.00	-1.0	3.7	2303	1038	4	3.6	-104	-27	-116.6	135.4	-14.1	-13.1	-4.1
9TH	102.75	-2.5	5.6	2303	1038	- i . i	5.4	-45	-20	-114.1	129.8	-12.8	-12.0	-3.8
1078	112.50	-3.8	6.9	2303	1038	-1.6	6.7	-23	-13	-110.3	122.8	-11.6	-10.9	-3.6
1178	122.25	-4.5	E.9	2303	10 38	-1.9	6.7	-17	-11	-105.8	115.9	-10.4	-9.9	-3.5
1278	132.00	-5.2	6.9	2303	1038	-2.3	6.6	-11	- 8	-100.7	109.0	-9 3	- 8.8	-3.3
	141.75	-5.9	6.9	2303	1038	-2.6	6.6	- 6	- 5	-94.8	102.2	-8.3	-7.9	-3.3
1378		-6.6	6.9	2303	1038	-2.9	6.6	- 2	- 2	-89.2	95.3	-7.3	-7.0	-3.3
14TH	151.50	-4.5	4.9	2303	1038	-2.0	4 7	-11	-10	-83.6	90.4	-6.4	-6.2	-3.2
15TH	161.25	. 9	1.0	2303	1038	. 4	1.0	-205	189	-84.6	89.4	-5.5	-5.3	-2.8
16TH	171.00	-1.4	3.0	2303	1038	6	2.9	-95	-46	-83.1	86.4	-4.7	-4.5	-2.4
1778	180.75	-3.8	5.0	2303	1039	-1.7	4.8	-40	-31			-3.9	-3.7	-2.1
1874	190.50	-6.2	6.9	2303	1039	-2.7	6.7	-22	-20	-79.3	81.4			-1.8
19TH	200.25	-8.6	8.9	2303	1038	-3.7	8.5	-14	-14	-73.1	74.5	-3.1	-3.0	
20TH	210.00	-8.7	8.8	2303	1038	-3.8	8.5	-14	-14	-64 5	65.6	-2.4	-2.3	-1.6
21ST	219.75	-8.9	8.8	2303	1038	-38	8.4	-14	-15	- 55 . 8	56.8	-1.8	-1.7	-1.3
2 2 N D	229.50	-9.0	8.7	2303	1038	-3.9	8.4	-15	-15	-46.9	48.0	-1.3	-1.2	-1,1
2 3 R D	239.25	-9.1	8.7	2303	1038	-4.0	8.3	-15	-16	- 37 . 9	39.3	9	8	8
24TH	249.00		- · ·	2303	1038	-4.0	8 3	-15	-16	- 28 . 8	30.7	5	5	5
25TH	258.75	-9.3	8.6				8.6	-1	-1	-19.5	22.0	3	3	- , 3
		-7.4	8.9	2303	1038	-3.2	0.9	-1	-1					

TABLE VIND D	7 SHEAR IRECTION	AND MONES	NT DIAGR	ANS : SAN Configuration a	DIEGO IN	REFEI	INENTAL H Rence pre	OTEL - SSURE	EAST T 27.0 PSF	OVER IN	GUST F	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN *	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-1 Y	KIPS) Z
MECH	268.50	-12.2	47.4	4252 1917	-2.9	<u> </u>	-10	. 0	-12.2	13.1	1	1	2
TOP	286.50	-12.2	13.1	4232 1918	-2.7	0.0	-10		Q.Q	0 .0	Ŷ.Ŷ	¢.¢	\$.\$

	7. SHEAR	AND NONEI	NT DIAGR	ANS : Configure	STION A	AN DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL Ressuri	EAST TE 27.0 PSF	OWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA C	SQ FT>	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR	(KIPS) Y	MOMENT X	(1000-FT-) Y	KIPS) Z
1 S T	0.00								- 1 6	-152.6	-11.5	1.0	-19.6	. 8
2ND	17.00	- 22 . 2	6.3	2034	876	-10.9	7.2	-5	-16	-130.4	-17.8	. 8	-17.2	1.1
SRD	34.00	-22.1	3.0	2034	876	-10.9	3.5	- 3	-21	-108.3	-20.8	. 4	-15.2	1.6
4TH	54.00	-29.9	-5.0	2743	1195	-10.9	-4.2	2	-11	-78.4	-15.8	. 1	-13.3	1.9
	63.75	3.1	-3.6	2303	1039	1.4	-3.5	49	42	- 81 . 5	-12.2	- 1	-12.5	2.3
STH		2.8	-4.7	2303	1039	1.2	-4.5	51	30	-84.2	-7.5	2	-11.7	2.6
6TH	73.50	1.2	-3.6	2303	1038	. 5	-3.4	55	19	- 85 . 5	-4.0	2	-10.9	2.8
7T H	83.25	3	-2.4	2303	1038	i	-2.3	46	- 5	- 85.2	-1.6	3	-10.1	2.9
8T M	93.00	-1.8	-1.3	2303	1038	8	-1.2	2	- 2	-83.4	3	3	-9.3	2.9
9TH	102.75	-3.0	3	2303	1039	-1.3	3	- 3	26			3	-8.5	2.8
10TH	112.50	-3.4	0	2303	1038	-1.5	0	- 0	35	-80.4	. 0		-7.7	2.7
11TH	122.25	-3.8	. 3	2303	1039	-1.7	. 3	4	40	-76.9	. 0	3		
12TH	132.00	-4.2	. 7	2303	1038	-1.9	.7	7	44	-73.1	3	3	-7.0	2.6
13TH	141.75	-4.6	1.0	2303	1038	-2.0	1.0	11	47	-68.9	-1.0	3	-6.3	2.4
14TH	151.50			2303	1038	-1.2	0	-1	60	-64.3	-2.0	3	- 5.6	2.1
15TH	161.25	-2.8	0					12	8	-61.5	-2.0	3	-5.0	2.0
16TH	171.00	1.9	-3.1	2303	1038	. 8	-3.0			-63.5	1.1	3	-4.4	2.0
17TH	180.75	. 1	-2.3	2303	1038	. 1	-2.2	-1	-0	-63.6	3.4	3	-3.8	2.0
1878	190.50	-1.6	-1.4	2303	1038	7	-1.3	-17	20	-62.0	4.8	2	-3.2	2.0
1978	200.25	-3.4	5	2303	1038	-1.5	5	- 5	31	- 58 . 5	5.3	2	-2.6	1.9
		-5.2	. 3	2303	1038	-2.3	. 3	2	31	-53.3	5.0	1	-2.0	1.7
20TH	210.00	-5.9	. 5	2303	1038	-2.5	. 5	2	29	-47.5	4.5	1	-1.5	1.5
215T	219.75	-6.5	. 7	2303	1038	-2.8	. 7	3	26	-41.0	3.8	1	-1.1	1.4
22ND	229.50	-7.1	. 9	2303	1038	-3.1	. 9	3	24		2.9	Q	7	1.2
2 3 R D	239.25	-7.8	1.1	2303	1038	-3.4	1.1	3	23	-33.8			5	1.0
24TH	249.00	-8.4	1.3	2303	1038	-3.7	1.3	3	21	-26.0	1.0	0	_	
25TH	258.75	-6.3	1.2	2303	1038	-2.7	1.1	11	61	-17.6	. 5	. ¢	2	. 8
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TABLE VIND D	7 SHEAR IPECTION	AND NOMEN	T DIAGRI	CONFIGUE	CATION A SA	N DIEGO IN	REFE	INENTAL Rence pr	HOTEL - Essure	- EAST TO 27.0 PSF	DWER IN	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	-11.3	- 7	4989	2 1917	-2.7	- 4	- 2	77	-11.3	7	. ¢	1	. 4
TOP	286.50	-11.3	- .,	4634		- Z , F		- 2	31	0 .0	Ø. Ø	\$.\$	0 .0	\$.\$

TABLE WIND D	7 SHEAR IRECTION	AND HONE	NT DIAGR	ANS : CONFIGUR	ATION A	AN DIEGO IN	TERCONT	INENTAL Rence p	RESSURE	EAST T 27.0 PSF	QWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA	(SQ FT) Y	P RE SSURE X	(PSF) Y	ECCE	(PT) Y	SHE AR X	(KIPS) Y	NONENT (X	(1000-FT-1 Y	KIPS) Z
1 S T	¢.00			0474	0.74	-10.8	7.4	-4	-12	-113.2	-119.1	20.8	~10.9	3.7
2ND	17.00	-22.1	6.5	2034	876					-91.1	-125.7	18.7	-9.2	4.0
3RD	34.00	-21.6	3.9	2034	876	-10.6	4.5	-4	-24	-69.5	-129.6	16 6	-7.8	4.6
4TH	54.00	-30.5	-3.2	2743	1195	-11.1	-2.7	1	-11	-39.0	-126.4	14.0	-6.7	4.9
STH	63.75	-1.1	-5.0	2303	1039	5	-4.8	39	-9	- 37 . 9	-121.4	12.8	-6.3	5.1
6TH	73.50	1	-6.7	2303	1038	1	-6.4	29	-1	-37.7	-114.8	11.7	-6.0	5.3
718	83.25	2	-6.5	2303	1038	1	-6.2	11	- 0	-37.6	-108.3	10.6	-5.6	5.4
8TH	93.04	3	-6.3	2303	1038	1	-6.0	- 8	¢	-37.3	-102.0	9.5	-5.2	5.3
9TH	102.75	3	-6.1	2303	1038	1	-5.9	-29	2	-37.4	-95.9	8.6	-4.9	5.1
1078	112.50	5	-5.8	2303	1038	2	-5.6	-46	4	-36.5	-90.1	7.7	-4.5	4.9
11TH	122.25	- 8	-5.4	2303	1038	3	-5.2	-51	7	-35.7	-84.7	6.8	-4.2	4.6
1278	132.00	-1.1	-4.9	2303	1038	5	-4.7	-57	13	-34.6	-79 8	6 .¢	-3.8	4.3
13TH	141.75	-1.4	-4.4	2303	1038	6	-4.3	-63	20	-33.2	-75.4	5.3	-3.5	4.0
1478	151.50	-1.7	-4.0	2303	1038	7	-3.8	-58	29	-31.5	-71.4	4.5	-3.2	3.7
1578	161.37	4	-4.3	2303	1038	2	-4.1	-60	6	-31.1	-67.1	3.9	-2.9	3.4
		2.8	-6.0	2303	1039	1.2	-5.8	-14	- 6	-33.9	-61.1	3.2	-2.6	3.3
16TH	171.00	1.4	-6.0	2303	1038	. 6	-5.8	-24	- 5	-35.2	-55.1	2.7	-2.2	3.2
17TH	180.75	1	-6.0	2303	1038	0	-5.8	-33	¢		-49.1	2.2	-1.9	3.0
18TH	190.50	-1.5	-6.0	2303	1039	7	-5.8	-39	10	-35.2			-1.5	2.7
19TH	200.25	-3.0	-5.9	2303	1038	-1.3	-5.7	-40	20	-33.6	-43.1	1.7		
20TH	210.00	-3.3	-5.6	2303	1038	-1.4	-5.4	-37	21	-30.7	-37.1	1.3	-1.2	2.4
21ST	219.75	-3.6	-5.4	2303	1038	-1.5	-5.2	-35	23	-27.4	-31.5	1.0	9	2.1
22N D	229.50	-3.9	-5.1	2303	1038	-1.7	-4.9	-32	24	-23 8	-26.1	. 7	7	1.9
2 3 R D	239.25	-4.2	-4.8	2303	1038	-1.8	-4.6	-29	25	-20.0	-21.1	. 5	5	1.6
24TH	249.00	-4.5	-4.5	2303	1038	-1.9	-4.3	-25	25	-15.8	-16.3	. 3	3	1.4
25TH	258.75	-3.2	-4.0	2303	1038	-1.4	-3.8	-71	58	-11.4	-11.9	. 2	2	1.2
			•••											

TABLE WIND D	7 SHEAR IRECTION	AND MONEN	T DIAGRI	ANS : Configuration (SAN DIEGO IN A	TERCONT REFE	INENTAL HO Rence Pres	SURE	27 0 PSF	OWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	> PRESSURE X	(PSF) Y	ECCEN (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	-9.1	-7.9	4252 1917	-1.9	- 4 - 1	-42 4		-8.1	-7.9	. 1	1	. 7
TOP	286.50	-9.1	-7.9	7636 1717	-1.7		~76 7	-	Q .Q	0.0	\$.\$	¥.\$	¢.¢

TAELE Wind D	7 SHEAR	AND MONEL	NT DIAGR	ANS : Configura	TION A	AN DIEGO IN	TERCONT Refe	INENTAL Rence p	HOTEL	EAST T 27.0 PSF	OWER IN	GUST FA	CTOR 1.32	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT-K Y	KIPS) Z
1 S T	0.00		• •	0.474	876	-11.5	5.8	- 0	-1	-83.1	-157.8	28.9	-3.7	6.4
2ND	17.00	-23.5	5.1	2034						- 59 . 6	-162.9	25.3	-2.5	6.5
3RD	34.00	- 23 . 8	3.5	2034	876	-11.7	4.0	-2	-14	- 35 . 8	-166.4	22.5	-1.7	6.8
4TH	54.00	-29.6	-2.0	2743	1195	-10.8	-1.7	0	- 2	-6.2	-164.4	19.2	-1.2	6.9
STH	63.75	9	-5.0	2303	1038	4	-4.9	12	- 2	-5.3	-159.4	17.6	-1.2	6.9
6TH	73.50	2	-6.4	2303	1038	1	-6.2	12	- 0	-5.1	-153.0	16.1	-1.1	7.0
718	83.25	3	-6.8	2303	1039	1	-6.5	- 5	¢	-4.8	-146.2	14.6	-1.1	7.0
STH	93.00	5	-7.1	2303	1039	2	-6.9	-19	1	-4.3	-139.1	13.2	-1.0	6.8
9TH	102.75	6	-7.5	2303	1038	3	-7.2	-32	3	-3.7	-131.6	11.9	-1.0	6.6
1078	112.50	7	-7.6	2303	1038	3	-7.4	-42	4	-3.0	-124.0	10.7	-1.0	6.3
	122.25	7	-7.3	2303	1038	3	-7.0	-47	5	-2.3	-116.7	9.5	- 9	5.9
11TH		7	-6.9	2303	1038	3	-6.7	-52	6	-1.6	-109.8	8.4	- 9	5.5
1278	132.00	8	-6.6	2303	1038	3	- 6.3	-58	7	8	-103.2	7.4	- 9	5.2
13TH	141.75	8	-6.2	2303	1039	4	-6.0	-64	8		-97.0	6.4	- 9	4.8
14TH	151.50	. 7	-5.9	2303	1038	. 3	-5.7	-59	- 7	. ¢				
15TH	161.25	4.2	-6.4	2303	1038	1.8	-6.1	-21	-14	7	-91.1	5.5	9	4.4
16TH	171.00	3.i	-6.9	2303	1038	1.4	-6.7	-28	-13	-4.9	-84.8	4.6	9	4.2
17TH	180.75	2.1	-7.5	2303	1038	. 9	-7.2	-35	-10	-8.1	-77.9	3.8	8	4.¢
1 8T H	190.50	1.0	-8.0	2303	1038	. 4	-7.7	-40	- 5	-10.2	-70.4	3.1	7	3.7
19TH	200.25	0	-8.6	2303	1038	0	-8.3	-43	0	-11.2	-62.3	2.4	6	3.4
20TH	210.00			2303	1038	2	-7.9	-43	2	-11.1	-53.7	1.9	5	3.0
21ST	219.75	4	-8.3						4	-10.7	-45.5	1.4	4	2.6
2 2 N D	229.50	8	-7.9	2303	1038	4	-7.6	-43		-9.9	-37.6	1.¢	3	2.3
2 3 R D	239.25	-1.2	-7.6	2303	1038	5	-7.3	-42	7	-8.6	-30.0	. 7	2	2.0
24TH	249.00	-1.6	-7.2	2303	1038	7	-7.0	-41	9	-7.9	~22.8	. 4	1	1.7
25TH	258.75	-2.0	-6.9	2303	1038	9	-6.6	-40	12	-5.0	-15.9	. 2	i	1.4
		8	-6.1	2303	1038	3	-5.9	-78	10					

TABLE WIND D	7. SHEAR IRECTION	AND NONE	NT DIAGR	ANS : SAN Configuration a	DIEGO IN	TERCONT REFE	INENTAL HOT Rence press	EL EAST T URE 27.0 PSF	OWER IN	GUST F	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) V	ECCEN (F X Y	T) SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50			4252 1917	-1.0		-76 33	-4.2	-9.8	. 1	¢	. 9
TOP	286.50	-4.2	-9.8	4232 1718	-1.0	-J.1	~ 10 - 34	¢,¢	0 .0	\$ _ \$	¢.¢	¢.¢

TÁBLE Wind d	7 SHEAR IRECTION	AND HOMEI	NT DIAGRI	AMS : Configura	TION A	N DIEGO IN	TERCONT REFE	INENTAL Rence p	HOTEL Ressure	EAST T(27.0 PSF	JWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT>	PRESSURE X	(PSF) Y	ECCE X	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT : X	(1000-FT-I Y	KIPS) Z
1 S T	0.00	-29.3	-3.4	2034	876	-14.4	-3.9	- 0	1	-187.8	-137.4	22.1	-18.6	3.0
2ND	17.00		-3.1	2034	876	-16.2	-3.6	1	- 6	-158.5	-134.0	19.8	-15.6	3.0
3R D	34.00	- 32 . 9				-12.1	-2.3	1	-10	-125.5 *	-130.8	17 5	-13.2	3.1
4TH	54.00	- 33.2	-2.8	2743	1195			-2	2	-92.3	-128.1	14.9	-11.0	3.5
STH	63.75	-5.i	-4.8	2303	1039	-2.2	-4.7			- 87 . 3	-123.3	13.7	-10.2	3.5
6 T H	73.50	-4.7	-5.5	2303	1038	-2.1	-5.3	-1	0	-82.5	-117.8	12.5	-9.3	3.4
7T H	83.25	-4.4	-5.5	2303	-1038	-1.9	-5.3	- 5	4	-78.1	-112.2	11.4	-86	3.4
етн	93.00	-4.1	-5.6	2303	1039	-1.8	-5.4	- 9	7	-74.0	-106.7	10.3	-7.8	3.3
9T H	102.75	-3.8	-5.6	2303	1038	-1.7	-5.4	-14	10	-70.1	-101.1	9.3	-7.1	3.2
1 Q T H	112.50	-3.6	-5.6	2303	1038	-1.6	-5.3	-19	12	-66.6	-95.5	8.4	-6.4	3.1
11TH	122.25	-3.5	-5.4	2303	1038	-1.5	-5.2	-23	15	-63.0	-90.1	7.5	-5.8	2.9
		-3.4	-5.2	2303	1038	-1.5	-5.0	-27	18	- 59 . 6	-85.0	6.6	-5.2	2.7
1278	132.00	-3.4	-5.0	2303	1038	-1.5	- 4 . 8	-3 i	21	-56.2	-79.9	5.8	-4 6	2.5
13TH	141.75	-3.3	-4.8	2303	1038	-1.4	-4.7	-36	24			5.1	-4.1	2.2
14TH	151.50	-2.6	-4.8	2303	1039	-1.1	-4.6	-32	17	-52.9	-75.1			
15TH	161.25	-1.4	-5.2	2303	1038	6	-5.0	- 2	0	-50.3	-70.3	4.3	-3.6	2.0
16TH	171.00	-2.1	-5.3	2303	1038	9	-5.1	- 6	2	-48.9	-65.2	3.7	-3.1	2.0
17TH	180.75	-2.8	-5.5	2303	1039	-1.2	-5.3	- 9	4	-46.9	-59.8	3.1	-2.7	2.0
18TH	190.50	-3.5	-5.7	2303	1038	-1.5	-5.5	-11	7	-44.1	-54.3	2.5	-2.2	1.9
19TH	200.25	-4.2	-5.9	2303	1038	-1.8	-5.7	-13	9	-40.6	-48.6	2.0	-1.8	1.8
20TH	210.00					-1.9	-5.6	-13	9	-36.4	-42.7	1.6	-1.4	1.7
21ST	219.75	-4.3	~5.8	2303	1038					-32.0	-36.9	1.2	-1.1	1.6
2 2 N D	229.50	-4.4	- 5.8	2303	1039	-1.9	-5.6	-13	10	-27.6	-31.1	. 9	8	1.5
23RD	239.25	-4.5	-5.7	2303	1038	-2.0	-5.5	-13	11	-23.0	-25.4	. 6	6	1.4
24TH	249.00	-4.7	-5.7	2303	1038	-2.0	-5.5	-14	11	-18.4	-19.7	. 4	4	1.2
25TH	258.75	-4.8	-5.6	2303	1038	-2.1	-5.4	-14	12	-13.6	-14.1	. 2	2	1.1
e o i A	244.44	-3.9	-5.2	2303	1038	-1.7	-5.0	-35	26					

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	IT DÍAGRI	ANS : SAN Configuration a	DIEGO IN	TERCONT REFE	INENTAL HO Rence pres	TEL SURE	EAST TO 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (X	FT) Y	SHEAR	(KIPS) Y	NONENT X	(1000-FT-) Y	(IPS) Z
MECH	268.50	-9.7	-8.9	4252 1917	-2.3	-4.7	-41 4	5	-9.7	-8.9	. 1	1	. 8
TOP	286.50	-3.6	- 5.7	7232 1711	- 2. 3	~ ~ . 4	71 7	-	Q .Q	0 .0	Q,Q	\$.\$	¢.¢

TABLE Wind D	7 SHEAR	AND HOMENT	DIAGRAMS CO	: NFIGURA	SAN Tion a	DIEGO IN	TERCONT	NENTAL Rence P	HOTEL	EAST TE 27.0 PSF	OWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE (KIPS) Y	APEA (X	SQ FT) Y	P PESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00						-6.9	2	- 5	-117.8	-147.0	21.6	-10.8	-3.8
ZND	17.00	-15.6	-6.0	2034	876	-7.7			-	-102.2	-141.0	19.2	-8.9	-3.7
380	34.00	-19.3	-6.4	2034	876	-9.5	-7.3	3	-9	- 82 . 9	-134.6	16.9	-7.3	-3.5
	54.00	-19.6	-6.0	2743	1195	-6.8	-5.0	9	-28	-64.2	-128.6	14.2	-5.9	-2.9
4TH		-3.7	-6.1	2303	1039	-1.6	-5.8	9	-5	-60.5	-122.6	13.0	-5.3	-2.8
STH	63.75	-4.1	-6.3	2303	1039	-18	-6.0	7	- 5	-56.5	-116.3	11.8	-4.7	-2.8
6TH	73.50	-3.7	-6.2	2303	1038	-1.6	-6.0	12	- 7	-52.8	-110.0	10.7	-4.2	-2.7
7TH	83.25	-3.2	-6.2	2303	1039	-1.4	-5.9	17	- 9	-49.6	-103.9	9.7	-3.7	-2.6
8TH	93.00	-2.8	-6.1	2303	1038	-1.2	-5.9	23	-11	-46.7	-97.8	8.7	-3.2	-2.4
9TH	102.75	-2.6	-6.0	2303	1038	-1.1	- 5 . 8	27	-12		-91.8	7.8	-2.8	-2.2
1¢TH	112.50	-2.7	-5.6	2303	1038	-1.2	-5.4	26	-13	-44.2		6.9	-2.3	-2.0
11TH	122.25	-2.9	-5.2	2303	1038	-12	-5.0	25	-14	-41.4	-86.2			
12TH	132.00	-3.0	-4.9	2303	1038	-1.3	-4.7	24	-15	- 38 . 6	-81.0	6.1	-1.9	-1.8
1 3 T H	141.75		-4.5	2303	1038	-1.4	-4.3	23	-16	-35.5	-76.1	5.3	-1.6	-1.7
14TH	151.50	-3.2					-4.5	24	-19	- 32 . 4	-71.6	4.6	-1.3	-1.5
15TH	161.25	-3.6	-4.7	2303	1038	-1.6				-28.8	-67.0	3.9	-1.0	-1.3
16TH	171.00	-4.3	-6.0	2303	1038	-1.9	-5.8	30	-21	-24.5	-61.0	3.3	7	-1.1
1718	180.75	-4.2	~5.9	2303	1038	-1.8	-5.7	30	-22	-20.3	-55.1	2.7	- .5	8
1878	190.50	-4.1	-5.8	2303	1039	-1.8	-5.6	31	-22	-16.2	-49.3	2.2	3	5
		-3.9	-5.7	2303	1038	-1.7	-5.5	31	-22	-12.3	-43.6	1.8	2	3
19TH	200.25	-3.8	-5.6	2303	1039	-1.6	-5.4	32	-22	-8.5	-38.1	1.4	1	¢
20TH	210.00	-3.3	-5.4	2303	1038	-1.4	-5.2	29	-17	-5 3	-32.6	1.0	, ¢	. 2
21ST	219.75	-2.7	-5.3	2303	1038	-1.2	-5.1	25	-13	-2.5	-27.3	. 7	. 0	. 4
2 2 N D	229.50	-2.2	-5.2	2303	1038	-1.0	-5.0	20	- 9		-22.2	. 5	. 1	. 5
2 3 R D	239.25	-1.7	-5.0	2303	1038	7	- 4 . 8	14	- 5	- 3		. 3	. 1	. 6
24TH	249.00	-1.2	-4.9	2303	1038	5	-4.7	7	- 2	1.4	-17.2			. 6
25TH	258.75	. 9	-4.4	2303	1038	. 4	-4.2	-23	- 4	2.6	-12.3	. 2	. 0	. 0
			* . *											

TABLE WING D	7 SHEAR IRECTION	AND HOMEN	T DIAGR	ANS : Configurati	SAN On a	DIEGO IN	REFEI	INENTAL H Rence pre	O T E L S S U R E	EAST T 27.0 PSF	OVER IN	GUST !	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS)	AREA (SQ X	FT>	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
NECH	268.50	1.7	-7.9	4252 1	917	. 4	- 4 1	-62 -	+ 7	1.7	-7.9	. 1	. 0	. 5
TOP	286.50	1.7	- 2.7	4232 1	711	. •	- 4 . 1	-92 -		¢.¢	0.0	¢.¢	Q.Q	\$.\$

TABLE 4THD D	7 SHEAR	AND MONEN	T DIAGR	ANS : Configura	SAN TION A	DIEGO IN	TERCONT REFE	INENTAL Rence Pi	HOTEL -	- EAST T 27.0 PSF	OVER IN	GUST FA	CTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (X	SQ FT>	PRESSURE	(PSF) Y	ECCEI	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT-1 Y	(IPS) Z
1ST	0.00		·							236.2	-115.2	16.4	41.6	3.5
210	17.00	6.4	-4.7	2034	876	3.2	-5.4	- 8	-12	229.7	-110.5	14.5	37.6	3.4
		2.8	-5.5	2034	875	1.4	-6.3	10	5	226 . 9	-105.0	12.7	33.7	3.4
380	34.00	5.0	-7.0	2743	1195	1.8	-5.8	13	9	221.9	-98.0	10.7	29.2	3.6
4TH	54.00	8.8	-4.5	2303	1039	3.8	-4.3	- 2	- 5	213.1	-93.6	9.7	27.1	3.5
STH	63.75	8.1	-4.6	2303	1038	3.5	-4.4	-4	- 8	205.0	-89.4	8.8	25.1	3.4
6TH	73.50	7.7	-4.7	2303	1038	3.4	-4.5	- 4	- 7	197.3	-84.3	8.0	23.1	3.4
7TH	83.25	7.4	-4.8	2303	1038	3.2	-4.6	- 4	- 6	189.9	-79.5	7.2	21.2	3.3
8TH	93.00	7.0	-4 9	2303	1039	3.0	-4.8	-4	- 5		-74.5	6.4	19.4	3.2
9T H	102.75	6.8	-5.0	2303	1038	3.0	-4.8	- 3	- 5	182.9			17.7	3.2
1 Q T H	112.50	7.2	-4.7	2303	1038	3.1	-4.5	- 4	- 6	176.1	-69.6	5.7		3.1
11TH	122.25	7.6	-4.4	2303	1039	3.3	-4.2	-4	- 7	168.9	-64.9	5.1	16.0	
12TH	132.00			2303	1038	3.5	-3.9	-4	- 8	161.3	-60.5	4.5	14.4	3.1
13TH	141.75	8.0	-4.1	2303	1038	3.6	-3.7	-4	- 9	153.4	-56.4	3.9	12.8	3.0
14TH	151.50	8.3	-3.8			3.7	-3.5	-4	-9	145.0	-52.6	3.4	11.4	2.9
15TH	161.25	8.4	-3.7	2303	1038				- 5	136.6	-49.0	2.9	10.0	2.8
16TH	171.00	7.8	-3.9	2303	1038	3.4	-3.8	- 2	-	128.8	-45.¢	2.4	8.7	2.8
1778	180.75	7.7	-4.0	2303	1038	3.4	-3.9	- 2	-5	121.0	-41.0	2.0	7.5	2.7
1878	190.50	7.7	-4.1	2303	1039	3.3	-4.0	- 2	- 5	113.4	-36.9	1.6	6.4	2.7
19TH	200.25	7.6	-4.2	2303	1038	3.3	-4.0	- 2	- 4	105.8	-32.7	1.3	5.3	2.6
		7.5	-4.3	2303	1039	3.3	-4.1	- 2	- 4	98.3	-28.4	1.0	4.3	2.6
20TH	210.00	8.4	-4.2	2303	1038	3.6	-4.1	- 5	-10	89.9	-24.2	.7	3.4	2.5
21ST	219.75	9.3	-4.2	2303	1038	4.0	-4.0	- 6	-14	80.6	-20.1	. 5	2.6	2.3
22ND	229.50	10.2	-4.1	2303	1039	4.4	-4.0	- 7	-18	70.4	-15.9	. 3	1.8	2.1
23RD	239.25	11.1	-4.1	2303	1038	4.6	-3.9	- 8	-22	59.3	-11.8	. 2	1.2	1.8
24TH	249.00	12.0	-4.0	2303	1038	5.2	-3.9	- 8	-25				.7	1.5
25TH	258.75	16.0	-3.1	2303	1038	7.0	-3.0	- 5	-26	47.3	-7.8	. 1		2 · · · ·

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN 130	T CIAGR	ANS : Configuration	SAN DIEGO IN A	TERCONT REFE	INENTAL HOTEL Rence pressure :	- EAST TI 27.0 PSF	OVER IN	GUST (FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT X Y	> PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHE AR X	(KIPS) Y	HOMENT X	(1000-FT-) Y	KIPS) Z
NECH	268.50	31.3	-4.6	4252 1917	7 4	-2.4	-5 -34	31.3	-4.6	. Q	. 3	1.1
TOP	286.50	31.3		4232 1717	8 . 4	-2.4	-3 -34	¢,¢	0.0	¢,¢	Q .Q	\$.\$

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN	IT DIAGR	AMS : Configura	TION A	AN DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL	EAST TO 27.0 PSF	WER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA (X	SQ FT>	PRESSURE X	(PSF) Y	ECCE X	N (FT) Y	SHEAR X	(KIPS) Y	MONENT	(1000-FT- Y	KIPS) Z
1 S T	0.00							- 0	-18	852.3	-55.9	7.3	130.3	23.6
2ND	17.00	36.3	4	2034	876	17.8	4			816.0	-55.5	6.3	116.1	22.9
BRD	34.00	33.4	-1.2	2034	876	16.4	-1.4	-0	-10	782.6	-54.2	5.4	102.5	22.6
4TH	54.00	40.4	-8.2	2743	1195	14.7	-6.8	-5	-25	742.2	-46.1	4.4	87.3	21.5
STH	63.75	32.0	9	2303	1038	13.9	8	-1	-22	710.2	-45.2	3.9	80.2	20.8
6TH	73.50	31.1	4	2303	1038	13.5	4	- 0	-24	679.1	-44.8	3.5	73.4	20.1
7TH	83.25	30.1	-1.5	2303	1039	13.1	-1.5	- 1	-26	649.0	-43.3	3.1	66.9	19.3
8TH	93.00	29.2	-2.6	2303	1038	12.7	-2.5	- 2	-27	619.9	-40.7	2.7	60.8	18.5
97 H	102.75	28.2	-3.7	2303	1038	12.2	-3.6	- 4	-29	591.7	-37.0	2.3	54.8	17.7
1078	112.50	27.8	-4.4	2303	1038	12.1	-4.3	- 5	-30	563.9	-32.5	1.9	49.2	16.8
11TH	122.25	29.7	-4.1	2 30 3	1038	12.5	-4.0	-4	-30	535.2	-28.4	1.7	43.9	16.0
1278	132.00	29.7	-3.8	2303	1039	12.9	-3.7	- 4	-29	505.5	-24.6	1.4	38.8	15.1
13TH	141.75	30.6	-3.5	2303	1038	13.3	-3.3	- 3	-29	474.9	-21.2	1.2	34.0	14.2
		31.6	-3.2	2303	1038	13.7	-3.0	- 3	-29	443.3	-18.0	1.0	29.5	13.2
14TH	151.50	32.7	-1.8	2303	1038	14.2	-1.8	- 2	-27	410.6	-16.2	. 8	25.4	12.3
15TH	161.25	33 .1	. 4	2303	1038	14.4	. 4	٥	-24	377.5	-16.5	. 7	21.5	11.5
1678	171.00	32.7	5	2303	1038	14.2	4	- 0	-25	344.7	-16.1	.5	18.0	10.7
17TH	180.75	32.3	-1.3	2303	1038	14.0	-1.3	- i	-27	312.4	-14.8	.3	14.8	9.8
1878	190.50	31.9	-2.1	2303	1038	13.9	-2.1	- 2	-28	280.5	-12.6	2	11.9	8.9
19TH	200.25	31.5	-3.0	2303	1038	13.7	-2.8	- 3	-29			. 1	9.3	8.0
20TH	210.00	31.9	-2.8	2303	1038	13.8	-2.7	- 3	-30	249.0	-9.7			7.0
21ST	219.75	32.2	-2.6	2303	1038	14.0	-2.5	- 3	-31	217.1	-6.9	. ¢	7.1	
22ND	229.50	32.6	-2.4	2303	1038	14.1	-2.3	- 2	-32	184.9	-4.3	0	5.1	6.0
23RD	239.25	32.9	-2.3	2303	1038	14.3	-2.2	- 2	-33	152.3	-1.9	- 1	3,5	5.0
24TH	249.00	33.2	-2.1	2303	1038	14.4	-2.0	- 2	-34	119.4	. 4	1	2.1	3.9
25TH	258.75	35.3	9	2303	1038	15.3	9	- 1	-31	86.2	2.5	1	1.1	2.8

TABLE Wind D	7. SHEAR IRECTION	AND NONEN	T DIAGR	ANS : Configur:	SAI Ation a	I DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TO	OVER IN	GUST FA	ACTOR 1.32	
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA ((SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT-K Y	IPS) Z
MECH	268.50	50.9	7 4	4252	1917	12.0	1 8	2 -33	56.9	3.4	- , ¢	. 5	1.7
TOP	286.50	30.7	3.4	4232	1711			2 00	Ø. Ø	Ø.Ø	¢,¢	¢.¢	¢ .¢

TABLE Wind D	7 SHEAR IRECTION	AND MOMEI 150	NT DIAGR	AMS : Configure	SA TION A	N DIEGO IN	ITERCONT Refe	INENTAL Rence f	HOTEL	EAST TO 27.0 PSF	VER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	P RE SS U RE X	(PSF) Y	ECCE	H (FT) Y	SHEAR X	(KIPS) Y	MOMENT	(1000-FT- Y	KIPS) Z
1 S T	0.00							2	-20	1216.0	57.5	-9.1	183.3	38.3
2ND	17.00	53.5	5.5	2034	876	26.3	6.2	2		1162.5	52.0	-8.2	163.1	37.3
3R D	34.00	53.6	3.9	2034	876	26.3	4.4	1	-14	1108.9	48.1	-7.4	143.7	36.5
4TH	54.00	58.4	-4.6	2743	1195	21.3	-3.8	- 3	-33	1050 6	52.7	-6.3	122.2	34.6
STH	63.75	43.7	5.5	2303	1038	19.0	5.3	3	-27	1006.9	47.2	-5.9	112.1	33.4
6T H	73.50	43.2	6.2	2303	1038	18.7	6.0	4	-29	963.7	41.0	-5.4	102.5	32.1
7TH	83.25	42.5	4.2	2303	1038	18.4	4.0	3	-31	921.3	36.8	-5.0	93.3	30.8
8TH	93.00	41.7	2.1	2303	1038	18.1	2.0	2	-33	879.5	34.7	-4.7	84.5	29.5
9TH		41.0	. 1	2303	1038	17.8	. 1	0	-34	838.5	34.6	-4.4	76.2	28.1
	102.75	40.8	-1.3	2303	1038	17.7	-1.3	- 1	-35	797.7	35.9	-4.0	68.2	26.6
1078	112.50	41.9	-1.1	2303	1038	18.2	-1.0	- 1	-35	755.7	37.0	-3.7	60.6	25.1
11TH	122.25	43 .1	- 8	2303	1038	18.7	8	- 1	-35	712.7	37.8	-3.3	53.5	23.6
1278	132.00	44.2	5	2303	1038	19.2	5	-0	-35				46.7	22.1
13TH	141.75	45.3	3	2303	1038	-19.7	2	- 0	-34	668.5	38.3	-2.9		
14TH	151.50	47.0	2.1	2303	1038	20.4	2.0	1	-33	623.2	38.6	-2.6	40.4	20.5
15TH	161.25	48.5	6.8	2303	1038	21.1	6.5	4	-29	576.2	36.4	-2.2	34.6	19.0
16TH	171.00	47.9	5.2	2303	1038	20.8	5.0	3	-31	527.7	29.7	-1.9	29.2	17.6
17TH	180.75	47.4	3.7	2303	1038	20.6	3.5	2	-32	479.8	24.4	-1.6	24.3	16.1
18TH	190.50	46.8	2.1	2303	1038	20.3	2.0	2	-33	432.4	20.8	-1.4	19.8	14.6
19TH	200.25			2303	1038	20.1	. 6	0	-35	385.7	18.6	-1.2	15.9	13.0
20TH	210.00	46.2	. 6				. 7		-35	339.5	18.1	-1. ¢	12.3	11.4
21ST	219.75	46.2	. 7	2303	1038	20.0		1		293.3	17.4	8	9.2	9.8
2 2 H D	229.50	46.1	. 8	2303	1038	20.0	.7	1	-35	247.1	16.6	7	6.6	8.2
238D	239.25	46.1	. 9	2303	1039	20.0	. 8	1	-35	201.0	15.8	- 5	4.4	6.6
24TH	249.00	46.1	. 9	2303	1038	20.0	. 9	1	-35	154.9	14.8	- 4	2.7	4.9
2514	258.75	46.1	1.0	2303	1038	20.0	1.0	1	-35	108.9	13.8	2	1.4	3.3
N N 1 1		46.4	2.4	2303	1038	20.2	2.3	2	-32					

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN 150	NT DIAGRA	NS : SAN Configuration a	DIEGO IN	TERCONT I Refei	INENTAL HOTEL Rence pressure 2	EAST TO 7.0 PSF	WER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS)	MONENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	62.4		4252 1917	14.7	5 3	5 -28	62.4	11.4	1	. 6	1.8
TOP	286.50	52.4	11.4	4232 1916	14.6	3.7	J ~26	0.0	0.0	¢,¢	9.0	Q .Q

TABLE Wind D	7 SHEAR IRECTION	AND NOMEN	IT DIAGRA	MS : Configurs	STION A	AN DIEGO IN	TERCONT REFE	INENTAL Rence f	HOTEL	EAST TO 27.0 PSF	WER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00			0.67.4	876	30.0	3.1	1	-16	1318.3	4.2	. 1	198.2	31.4
2ND	17.00	61.0	2.7	2034				0	-18	1257.2	1.5	. 2	176.3	30.5
3R D	34.00	58.8	. 9	2034	876	28.9	1.1			1198.4	. 6	. 2	155.4	29.9
4TH	54.00	64.2	-7.3	2743	1195	23.4	-6.1	- 3	-25	1134.2	7.9	. 3	132.1	28.3
5T H	63.75	46.4	5.1	2303	1038	20.2	5.0	2	-21	1087 8	2.8	. 3	121.2	27.3
6T H	73.50	46.0	5.9	2303	1038	20.0	5.7	3	-23	1041.7	-3.2	. 3	110.9	26.2
718	83.25	45.5	3.8	2303	1038	19.7	36	2	-24	996.2	-7.0	. 3	100.9	25.1
8T H	93.00	45.0	1.6	2303	1038	19.5	1.6	1	-25	951.3	-8.6	. 2	91.4	23.9
9TH	102.75	44.4	6	2303	1038	19.3	5	- 0	-26	906.8	-8.0	. 1	82.4	22.8
1078	112.50	44.4	-2.1	2303	1038	19.3	-2.0	- 1	-26	862.5	-5.9	, ¢	73.7	21.6
11TH	122.25	45.5	-2.1	2303	1038	19.6	-2.0	- 1	-26	816.9	-3.8	- 0	65.6	20.4
		46.7	-2.1	2303	1038	20.3	-2.0	- 1	-26	770.2	-1.7	- 0	57.8	19.2
1278	132.00	47.9	-2.1	2303	1038	20.8	-2.0	- 1	-26	722.4	. 4	0	50.5	18.0
13TH	141.75	49.0	-2.0	2303	1038	21.3	-2.0	- 1	-26				43.7	16.7
14TH	151.50	50.6	. 1	2303	1038	22.0	. 1	0	-25	673.3	2.4	0		
1 5 T H	161.25	51.9	4.7	2303	1039	22.5	4.5	2	-24	622.7	2.3	- 0	37.4	15.4
16TH	171.00	51.5	2.9	2303	1038	22.4	2.8	1	-24	570.8	-2.4	- , ¢	31.6	14.2
17TH	180.75	51.1	1.2	2303	1038	22.2	1.1	1	-25	519.3	-5.3	¢	26.3	12.9
18TH	190.50	50.6	6	2303	1038	22.0	6	- 0	-25	468.2	-6.4	1	21.5	11.6
19TH	200.25	50.2	-2.3	2303	1038	21.8	-2.2	- 1	-26	417.6	- 5 . 8	- 2	17.2	10.3
20TH	210.00					21.8	-2.1	- 1	-26	367.5	-3.5	- 2	13.3	9.0
215T	219.75	50.1	-2.2	2303	1038					317.3	-1.3	2	10.0	7.7
2 2 N D	229.50	50.1	-2.1	2303	1038	21.7	-2.0	-1	-26	267.3	. 7	2	7.1	6.4
23RD	239.25	50.0	-2.0	2303	1038	21.7	-1.9	-1	-26	217.3	2.7	- 2	4.8	5.1
24TH	249.00	50.0	-1.9	2303	1038	21.7	-1.8	- 1	-26	167.3	4.6	2	2.9	3.8
25TH	258.75	49.9	-1.7	2303	1038	21.7	-1.7	- 1	-27	117.4	6.3	1	1.5	2.4
		49.1	6	2303	1038	21.3	6	- 0	-24					

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	IT DIAGRA	NS : SAN Configuration a	DIEGO INT	REFE	INENTAL HOTEL	- EAST TO 27.0 PSF	WER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR	(KIPS) Y	NOMENT	(1000-FT-1 Y	(IPS) Z
MECH	268.50	68.3	()	4252 1917	16.1	7 6	2 -18	68.3	6.9	1	. 6	1.3
TOP	286.50	65.3	8.7	4232 1717	10.1	3.8	2 -10	0 .0	Q. Q	Q.Q	0.0	Q.Q

	7. SHEAR IRECTION	AND MONEL	NT DIAGR	AMS : CONFIGUR		AN DIEGO IN	TERCONT Refe	INENTAL Rence P	HOTEL Ressure	EAST T E 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00		_					- 0	-12	1338 7	-83.5	14.0	198.5	19.5
2ND	17.00	66.0	5	2034	876	32.5	6	-0		1272.7	-83.0	12.6	176.3	18.8
3RD	34.00	60.4	-2.2	2034	876	29.7	-2.5	-0	- 6	1212.3	-80.8	11.2	155.2	18.4
4TH	54.00	69.1	-11.0	2743	1195	25.2	-9.2	- 2	-14	1143.2	-69.8	9.7	131.7	17.4
5TH	63.75	46.7	2.2	2303	1038	20.3	2.1	1	-14	1096.5	-72.0	9.0	120.8	16.8
6TH	73.54	46.2	2.7	2303	1038	20.1	2.6	1	-15	1050.2	-74.7	8.3	110.3	16.1
		46.4	. 8	2303	1038	20.2	. 7	Ó	-15	1003.8	-75.4	7.6	100.3	15.4
7TH	83.25	46.6	-1.2	2303	1038	20.2	-1.1	- 0	-15	957.2	-74.3	6.9	90.7	14.7
8TH	93.00	46.8	-3.1	2303	1038	20.3	-3.0	- 1	-15	910.4	-71.2	6.2	81.6	13.9
9T H	102.75	47.2	-4.5	2303	1038	20.5	-4.3	- 1	-15	863.2	-66.7	5.5	73.0	13.2
1 Q T H	112.50	49.1	-4.4	2303	1038	20.9	-4.3	- 1	-15				64.8	12.5
11TH	122.25	49.1	-4.4	2303	1038	21.3	-4.2	- 1	-16	815.1	-62.2	4.9		
12TH	132.00	50.0	-4.3	2303	1038	21.7	-4.2	- 1	-16	766.9	-57.9	4.3	57.1	11.7
13TH	141.75	51.0	-4.3	2303	1038	22.1	-4.1	- 1	-17	716.0	-53.5	3.7	49.8	10.9
14TH	151.50		-3.1	2303	1038	22.4	-3.0	-1	-16	664.9	-49.2	3.2	43.1	10.0
15TH	161.25	51.5					9	-0	-15	613.4	-46.1	2.8	36.9	9.2
16TH	171.00	50.6	9	2303	1038	22.0			_	562.9	-45.2	2.3	31.2	8.4
17TH	180.75	50.4	-2.1	2303	1038	21.9	-2.0	-1	-15	512.5	-43.1	1.9	25.9	7.7
18TH	190.50	50.2	-3.3	2303	1039	21.8	-3.2	- 1	-16	462.3	-39.9	1.5	21.2	6.9
19TH	200.25	50.0	-4.5	2303	1038	21.7	-4.3	- 1	-16	412.3	-35.4	1.1	16.9	6.0
		49.8	-5.7	2303	1038	21.6	-5.5	- 2	-17	362.5	-29.7	. 8	13.1	5.2
20TH	210.00	49.7	-5.5	2303	1038	21.6	-5.3	- 2	-17	312.8	-24.2	. 5	9.8	4.4
21ST	219.75	49.6	-5.4	2303	1038	21.5	-5.2	- 2	-16	263.2	-18.7	. 3	7.0	3.6
2 2 N D	229.50	49.5	-5.3	2303	1038	21.5	-5.1	- 2	-16			. 2	4.7	2.7
2 3 R D	239.25	49.4	-5.2	2303	1038	21.5	-5.0	- 2	-16	213.7	-13.4			1.9
24TH	249.00	49.3	-5.1	2303	1038	21.4	-4.9	- 2	-16	164.3	-8.3	. 1	2.8	
2 5 T H	258.75	48.3	-4.0	2303	1038	21.0	-3.9	- 1	-14	115.0	-3.2	. Q	1.5	1.1
		TU . U	·• · •	2000				-						

TABLE Wikd d	7 SHEAR IRECTION	AND MONENT	E DIAGRA	NS : CONFIGURA	SAI FION A	N DIEGO INT	EPCONT REFE	INENTAL Rence pri	HOTEL . FSSURF	EAST TO 27.0 PSF	WER IN	GUST F	ACTOR 1.33	2
FLOGR	HEIGHT	FORCE (X	KIPS) Y	AREA (D FT)	P P F S S U R F X	(PSF) Y	ECCEN X	(FT)	SHFAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	(IPS)
NECH	268.50	66.6	٥	4252	1917	15.7	4	¢	- 7	66.6	. 8	0	. 6	. 4
TOP	286.50	58.5	. 5	7252	171(•		Q . Q	Q .Q	¢.¢	0.0	Q .Q

TABLE Wind D	7 SHEAR	AND MONEI	NT DIAGR	ANS : CONFIGURI	STION A	AN DIEGO IN	TERCONT	INE'NTAL Rence pr	HOTEL	EAST TI 27.0 PSF	DWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA S X	SØ FT) Y	PRFSSURE X	(PSF) Y	ECCEN X	4 (FT) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT-1 Y	(195) 2
157	0.00							- 0	- 8	1353.5	-163.2	27 4	199.9	8.2
2ND	17.00	64.5	-3.1	2034	876	31.7	-36		_	1289.0	-160.0	24.7	177.4	7.7
3R D	34.00	58.3	-4.8	2034	876	28.6	-5.4	-0	- 3	1230.7	-155.3	22 ¢	158.0	7.5
4TH	54.00	71.0	-13.2	2743	1195		-11.1	- 2	-9	1159.7	-142.0	19.0	132.1	6.8
5TH	63.75	49.7	. 6	2303	1038	21.1	. 5	0	- 8	1111.0	-142.6	17.6	121.0	6.4
61 H	73.50	49.2	. 8	2303	1038	20.9	. 9	0	-9	1062.8	-143.4	16.2	110.4	6.0
7TH	83.25	48.5	-1.1	2303	1038	21.0	-1.1	- 0	- 8	1014.4	-142.3	14.8	100.3	5.6
8T H	93.00	49.7	-3.1	2303	1038	21.1	-3.0	- 0	- 8	965.7	-139.2	13.5	90.6	5.2
91H	102.75	49.0	-5.0	2303	1038	21.3	-4.8	- 1	- 7	916.7	-134.1	12.1	81.5	4.9
10TH	112.50	49.4	-6.5	2303	1039	21.4	-6.3	- 1	- 6	867.4	-127.6	10.9	72.8	4.5
11TH	122.25	50.1	-6.7	2303	10 39	21.7	-6.5	- 1	-7	817.3	-120.9	9.6	64.6	4.2
		50.8	-6.9	2303	1038	22.0	-6.7	- 1	-7	766.5	-114.0	8.5	56.8	3.8
1218	132.00	51.5	-7.1	2303	1038	22.4	-6.9	- 1	-7	715.0	-196.9	7.4	49.6	3.5
1318	141.75	52.2	-7.3	2 3 0 3	1038	22.7	-7.1	- 1	- 7	662.8	-99.5	6.4	42.9	3.1
1418	151.50	51.9	-7.1	2303	1038	22.5	-6.8	- 1	- 6	610.9	-92.4	5.5	36.7	2.8
15)H	161.25	49.4	-6.2	2303	1038	21.5	-6.0	- 1	-4	561.4	-86.2	4.6	31.0	2.6
16TH	171.00	49.7	-6.7	2303	1038	21.6	-6.5	- 1	- 5	511.8	-79 5	3.8	25.7	2.3
17TH	180.75	49 9	-7.3	2303	1038	21.6	-7.0	- 1	- 5			3.1	21.0	2.1
18TH	190.50	50.1	-7.8	2303	1038	21.7	-7.5	- 1	- 6	461.9	-72.2	2.4	16.7	1.8
1 9 T H	200.25	50.3	-8.3	2303	1038	21.8	-8.0	- 1	- 7	411.9	-64.4			1.4
2 O T H	210.00	50.2	-8.5	2303	1038	21.8	-8.2	- 1	- 6	361.6	-56.1	1.8	13.0	
21ST	219.75	50.1	-8.6	2303	1038	21.7	-8.3	- 1	- 6	311.4	-47.6	1.3	9.7	1.1
2 2 N D	229.50	50.0	-8.7	2303	1038	21.7	-8.4	- 1	- 6	261.3	-39.0	. 9	6.9	. 8
23RD	239.25	49.9	-8.9	2303	1038	21.7	-8 5	- 1	- 6	211.3	-30.3	. 5	4.6	. 4
241H	249.00			2303	1038	21.6	-8.7	- 1	- 6	161.4	-21.4	. 3	2.8	. 1
251 H	258.75	49.8 47.0	-9.0 -7.7	2303	1038	20.4	-7.4	- 1	- 3	111.5	-12.5	. 1	1.4	2

TABLE WIND D	7 SHEAP IRECTION	AND MONEN	NT DIAGR	ANS : SAN Configuration a	DIEGO IN	REFE	INENTAL HOTEL Rence pressure 2	EAST TO	WER IN	GUST F	ACTOR 1.32	!
FLOOR	HEIGHT	F DR C E X	(KIPS) Y	AREA (SQ FT) X Y	PRF SSURE X	(PSF) Y	ECCEN (FT) X Y	SHE AR X	(KIPS) Y	NONENT X	(1000-FT-K Y	(IPS) Z
NECH	268.59	64.5	-4.7	4252 1917	15.2	-2.5	6 5	64.5	-4.7	. Q	. 6	3
TOP	286.50	99.J	- 4.7	4152 1911	13.1		• •	¢ .¢	¢.¢	¢.¢	Q.Q	0 .0

TABLE VIND	7 SHEAR DIRECTION	AND MOMEN	NT DIAGRA	MS : Configuri	SAN TION A	DIEGO IN	ITERCONT REFE	INENTAL Rence pr	HOTEL ESSURE	EAST T 27.0 PSF	OVER IN	GUST P	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	APER (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHE AR X	(K1PS) Y	NOMENT X	(1000-F1- Y	KIPS) Z
157	0.00					74 8		•		1314 6	-223.7	38.1	192.0	-3.7
2ND	17.00	64.0	-4.7	2034	876	31.5	-5.4	-0	-4	1250.6	-218.9	34.4	170.2	-4.0
3R D	34.00	56.0	-6.2	2034	876	27.5	-7.1	-0	-0	1194.6	-212.7	30.7	149.4	-4.0
47H	54.00	72.1	-14.8	2743	1195	26.3	-12 4	-1	- 3	1122 4	-197.9	26.6	126.3	-4.2
5TH	63.75	49.1	~.5	2303	1038	21.3	5	- 0	- 2	1073.4	-197.4	24.6	115.6	-4.3
6T H	73.50	48.3	3	2303	1038	21.0	3	- 0	- 3	1025.1	-197.1	22.7	105.3	-4.5
71H	83.25	48.4	-2.3	2303	1038	21.0	-2.2	- 0	- 2	976.6	-194.8	20.8	95.6	-4.5
81H	93.00	48.6	-4.2	2303	1038	21.1	-4.0	- 0	- 0	928.0	-190.6	18.9	86.3	-4.6
		48.?	-6.2	2303	1038	21.2	-5.9	٥	1	879.3	-184.5	17.1	77.5	-4.5
97H		49.0	-7.7	2303	1038	21.3	-7.4	¢	2	830.3	-176.8	15.3	69.1	-4.5
1078		49.5	-8.0	2303	1038	21.5	-7.7	¢	2	780.8	-168.8	13.7	61.3	-4.4
1174		50.1	-8.4	2303	1038	21.7	- 8.1	0	2		-160.4	12.1	53.9	-4.3
12TH	132.00	50.6	-8.8	2303	1038	22.0	-8.4	¢	2	730.8				-4.2
1 3 T H	141.75	51.1	-9.1	2303	1038	22.2	- 8.8	Ó	2	680.2	-151.6	10.5	47.0	
14TH	151.50	49.9	-9.6	2303	1038	21.7	-9.3	i	3	629.1	-142.5	9.1	49.7	-4.1
15TH	161.25	46.0	-10.4	2303	1038	20.0	-10.0	1	5	579.1	-132.6	7.8	34.8	-3.9
16TH	171.00	46.5	-10.7	2303	1038	20.2	-10.3	1	5	533.2	-122.4	6.5	29.3	-3.7
17TH	180.75	47.1	-11.1	2303	1038		-10.7	1	4	486.6	-111.7	5.4	24.4	-3.4
1 8T H	190.50	47.6	-11.4	2303	1038	20.7	-11.0	- 1	4	439.5	-100.7	4.3	19.9	-3.2
1 9 T H	200.25				1038		-11.3	1	۰ ۲	391.9	-89.3	3.4	15.8	-3.0
20TH	210.00	48.2	-11.7	2303				1	4	343.7	-77.5	2.6	12.2	-2.8
2 I S T	219.75	48.2	-11.6	2303	1038	20.9	-11.2			295.5	-65.9	1.9	9.1	-2.6
2 2 N D	229.50	48.1	-11.6	2303	1038	20.9	-11.1	1	5	247.4	-54.3	1.3	6.5	-2.3
2 3 R D	239.25	48.1		2303	1038		-11.1	1	5	199.3	-42.8	. 8	4.3	-2.1
2418	249.00	48.0	-11.4	2303	1038	20.9	-11.0	1	6	151.3	-31.4	. 5	2.6	-i.8
25TH	258.75	48.0	-11.3	2303	1038	20.8	-10.9	1	6	103.3	-20.1	. 2	1.3	-1.5
14 W 1 11	****	43.6	-10.7	2303	1038	18.9	-10.3	2	8					

TABLE WIND D	7 SHEAR IRECTION	AND NOMEN	NT DIAGRI	AMS : SAN Configuration a	DIEGO IN	REFE	INENTAL HOTEL Rence pressure i	EAST TO 27.9 PSF	DVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHE AR X	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
NECH	268.50	59.7	-9.4	4252 1917	14.0		3 18	59.7	-9.4	. 1	. 5	-1.1
TOP	286.50	39.7	~ 7. 4	4232 1918	14.0		3 10	¢.¢	Q.Q	¢.¢	0 .0	0 .0

TABLE Wind I	7 SHEAR DIRECTION	AND MOMEN	IT DIAGR	AMS : Configuri		AN DIEGO IN	TERCONT Refe	INENTAL Rence pr	HOTEL	EAST TO 27.0 PSF	OWER IN	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FURCE	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MONENT X	(1000-FT- Y	-KIPS) Z
1 S T	0.00						= 0	-0	-0	1241.1	-260.2	44.4	179.9	-16.1
2ND	17.00	60.4	-5.1	2034	876	29.7	-5.9		-	1180.7	-255.1	40.0	159.3	-16.1
3R D	34.00	51.4	-7.2	2034	876	25.2	-8.3	1	5	1129.4	-247.8	35.8	139.7	-15.9
4TH	54.00	69.2	-15.5	2743	1195		-13.0	1	4	1060.2	-232.3	31.0	117.8	-15.6
5TH	63.75	46.6	9	2303	1938	20.2	9	¢	5	1013.6	-231.4	28.7	107.6	-15.4
6T H	73.50	45.7	-1.1	2303	1039	19.6	-1.0	0	5	967.9	-230.3	26.4	98.0	-15.2
718	83.25	46.6	-3.1	2303	1038	20.2	-3.0	¢	7	921.4	-227.2	24.2	88.8	-14.9
8TH	93.00	47.5	-5.2	2303	1039	20.6	-5.Ú	1	8	873.9	-222.0	22.0	80.0	-14.4
9TH	102.75	48.4	-7.2	2303	1038	21.0	-7.0	1	10	825.5	-214.7	19.9	71.7	-14.0
10TH		49.0	-8.8	2303	1038	21.3	-8.5	2	11	776.5	-205.9	17.8	63.9	-13.4
_	122.25	48.9	-9.2	2303	1039	21.2	- 8 . 9	2	11	727.6	-196.7	15.9	56.6	-12.8
1178		48.8	-9.6	2303	1038	21.2	-9.2	2	12	678.9	-187.1	14.0	49.7	-12.2
1278	132.00	48.7	-10.0	2303	1038	21.1	-9.6	2	12	630.2	-177.1	12.2	43.4	-11.6
13TH	141.75	48.6	-10.3	2303	1038	21.1	-10.0	3	12	581.6	-166.8	10.6	37.5	-11.0
14TH	151.50	46.4	-11.4	2303	1038	20.2	-11.0	3	13	535.2	-155.4	9.0	32.0	-10.4
15TH	161.25	41.7	-13.3	2303	1038	18.1	-12.8	5	15			7.5	27.0	-9.7
16TH	171.00	42.8	-13.3	2303	1038	18.6	-12.8	5	15	493.5	-142.1			-9.0
1718	180.75	43.8	-13.2	2303	1038	19.0	-12.8	5	15	450.7	-128.8	6.2	22.4	
18TH	190 50	44.9	-13.2	2303	1038	19.5	-12.7	5	15	406.9	-115.6	5.0	18.2	-8.3
19TH	200.25	45.9	-13.2	2303	1038	19.9	-12.7	4	16	362.0	-102.4	4.0	14.5	-7.6
2 O T H	210.00	45.4	-13.2	2303	1038		-12.7	5	16	316.1	-89 2	3.0	11.2	-6.8
21ST	219.75	45.0	-13.1	2303	1038		-12.6	5	17	270.7	-76.0	2.2	8.3	-6.0
2 2 N D	229.50			2303	1038		-12.6	5	17	225.7	-62.9	1.5	5.9	-5.2
2 3 R D	239.25	44.5	-13.1				-12.6	5	17	181.3	-49.8	1.0	3.9	-4.4
24TH	249.00	44.0	-13.1	2303	1038			5	18	137.3	-36.8	. 6	2.3	-3.5
25TH	258.75	43.5	-13.0	2303	1038		-12.5			93.8	-23.7	. 3	1.2	-2.7
		39.6	-12.2	2303	1038	17.2	-11.8	6	20					

TABLE WIND D	7 SHEAR IRECTION	AND MOMENT DIAGRA	NS 1 SAN Configuration a	DIEGO INT	REFE	INENTAL HOTEL Rence pressure 2	EAST TO 7.0 PSF	WER IN	GUST FI	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE X	(PSF) Y	ECCEN (FT)	SHEAR X	(KIPS) Y	NONENT X	(1000-FT-1 Y	(IPS) Z
MECH	268.50	54.2 -11.5	4252 1917	12.7	-6.0	7 32	54.2	-11.5	. 1	. 5	-1.8
TOP	286.50	34.2 411.3	7636 1918	6 Ga - 4			0.0	¢ .¢	¢.¢	Q.Q	¢ .¢

TABLE Vind (7 SHEAR Direction	AND NONE	NT DIAGR	AMS : CONFIGUR	S Ation a	AN DIEGG IN	TERCONT REFE	INENTAL Rence pr	HOTEL	EAST T 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHE AR X	(KIPS) Y	NONENT X	(1000-FT) Y	-KIPS) Z
1 S T	0.00						- /			1239.5	-248.2	42 0	180.2	-28.8
2ND	17.00	55.8	-6.7	2034	876	27.4	-7.5	1	6	1183.7	-241.5	37.9	159.6	-28.5
3RD	34.00	46.7	-7.7	2034	876	23.0	- 8.8	1	7	1137.0	-233.7	33.8	139.9	-28.2
4TH	54.00	66.0	-15.7	2743			-13 1	2	9	1071.0	-218.1	29.3	117.8	-27.5
571	63.75	47.5	. 1	2303	1038	20.6	. 1	- 0	12	1023.5	-218.1	27.2	107.6	-26.9
6TH	73.50	46.4	1	2303	1038	20.1	1	¢	13	977.1	-218.0	25.1	97.8	-26.3
7TH	83.25	47.5	-2.2	2303	1038	20.6	-2.1	1	15	929.6	-215.8	23.0	88.5	-25.6
5TH	93.00	49.6	-4.3	2303	1038	21.1	-4.1	2	17	881.0	-211.5	20.9	79.7	-24.8
	102.75	49.7	-6 4	2303	1038	21.6	-6.1	2	19	831.3	-295.1	19.8	71.4	-23.8
9TH 16TH	112.50	50.5	-8.0	2303	1038	21.9	-7.7	3	21	780.8	-197.1	16.9	63.5	-22.7
1078		50.5	-8.5	2303	1038	21.9	- 8 . 2	4	21	730.3	-188.6	15.0	56.1	-21.6
11TH	122.25	50.4	-9.0	2303	1038	21 9	-8.7	4	21	679.9	-179.5	13.2	49.3	-20.6
1278	132.00	50.4	-9.5	2 30 3	1039	21 9	-9.2	.4	21	629.5	-170.0	11.5	42.9	-19.4
13TH	141.75	50.4	-10.0	2303	1038	21.9	-9.7	4	21	579.1	-160.0	9.9	37.0	-18.3
14TH	151.50	47.7	-11.2	2303	1038	20.7	-10.8	5	22	531.4	-148.7	8.4	31.6	-17.2
15TH	161.25	41.3	-13.3	2303	1038	17.9	-12.8	7	22	490.1	-135.5	7.0	26.6	-16.2
16TH	171.00	42.6	-13.2	2303	1038	18.5	-12.7	7	24		-122.3	5.7	22.0	-15.1
17TH	180.75	43.9	-13.1	2303	1038	19.1	-12.6	7	25	447 5			17.9	-13.9
18TH	190.50	45.2	-12.9	2303	1038	19.6	-12.5	7	26	403.6	-109.3	4.6	14.2	-12.7
19TH	200.25	46.4	-12.8	2303	1038	20.1	-12.4	8	27	358.4	-96.3	3.6		
20TH	210.00	45.7	-12.8	2303	1038	19.9	-12.3	8	28	312.0	-83.5	2.7	10.9	-11.3
215T	219.75	45.0		2303			-12.2	8	29	266.3	-70.7	2.0	8.1	-9.9
2 2 N D	229.50	44.4	-12.6	2303	1038		-12.2	8	30	221.3	-58.0	1.4	5.7	-8.5
2 3 R D	239.25				1038		-12.1	9	30	176.9	-45.4	. 9	3.8	-7.1
24TH	249.00	43.7	-12.5	2303			-12.0	9	31	133.3	-32.8	. 5	2.2	-5.7
25TH	258.75	43.0	-12.5	2303				-	35	90.3	-29.4	. 2	1.2	-4.2
		38.9	-11.8	2303	1038	16.9	-11.4	11	50					

TABLE WIND D	7 SHEAR IRECTION	AND NOMES	T DIAGR	ANS : CONFIGURAT	SAN Fion a	DIEGO IN	TERCONT REFE	INENTAL HO Rence fres	TEL - Sure	27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (S X	SQ FT> Y	PRESSURE X	(PSF) Y	ECCEN C	FT) Y	SHE AR X	(KIPS) Y	NOMENT	(1000-FT- Y	KIPS) Z
NECH	268.50	51.3	-8.5	4252	1917	12.1	-4 4	9 5	2	51.3	-8.5	. 1	. 5	-2.8
TOP	286.50	51.3	-6.3	4232	1711		··· • • •	7 3	-	¢ .¢	Q.Q	0 0	0 .0	Q.Q

TABLE Wind D	7 SHEAR IRECTION	AND NOMEI 220	NT DIAGR	AMS : CONFIGUR	ATION A	AN DIEGO IN	ITERCONT Refe	INENTAL Rence pi	HOTEL Ressure	EAST T 27.0 PSF	OWER IN	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA X	(SQ FT) Y	P RE SS U RE X	(PSF) Y	ECCEI X	N (FT) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT Y	-KIPS) Z
1 S T	0.00		<i>.</i> .	0474	876	AC 1	-6.9	1	9	1370.7	-180.7	29.6	203.1	-41.3
2N D	17.00	53.0	-6.0	2034		26.1			-	1317.7	-174.7	26.6	180.3	-40.8
3RD	34.00	42.8	-7.0	2034	876	21.0	-8.0	2	9	1274.9	-167.7	23.7	158.2	-40.4
4TH	54.00	65 9	-15.8	2743	1195		-133	3	12	1208 9	-151.8	20.5	133.4	-39.6
5TH	63.75	53.3	1.9	2303	1038	23.2	1.8	- 1	15	1155.6	-153.7	19.0	121.9	-38.8
6T H	73.50	51.9	1.6	2303	1038	22.5	1.5	- 0	15	1103.7	-155.3	17.5	110.8	-38.0
7TH	83.25	52.9	6	2303	1038	23.0	6	¢	18	1050.8	-154.6	16.0	100.3	-37.0
8TH	93.00	52.9	-2.9	2303	1038	23.4	-2.8	1	21	996.9	-151.8	14.5	90.4	-35.9
9TH	102.75	54.9	-5.1	2303	1038	23.8	-4.9	2	23	942.0	-146.7	13.0	80.9	-34.6
1078	112.50	55.8	-6.7	2303	1038	24.2	-6.5	3	25	886.2	-140.0	11.6	72.0	-33.2
11TH	122.25	56.3	-6.8	2303	1038	24.4	-6.5	3	26	829.9	-133.2	10.3	63.6	-31.7
1274	132.00	56.7	- 6 . 8	2303	1038	24.6	-6.6	3	27	773.2	-126.4	9.0	55.8	-30.2
		57.2	-6.9	2303	1038	24.8	-6.6	3	28				48.5	-28.6
13TH	141.75	57.7	-6.9	2303	1038	25.0	-6.6	3	28	716.0	-119.5	7.9		
14TH	151.50	54.6	-7.7	2303	1038	23.7	-7.5	4	29	658.3	-112.6	6.7	41.8	-26.9
15TH	161.25	46.5	-9.8	2303	1038	20.2	-9.4	7	32	603 7	-104.9	5.7	35.7	-25.3
16TH	171.00	48.2	-9.7	2303	1038	20.9	-9.3	7	33	557.2	-95.1	4.7	30.0	-23.8
17TH	180.75	49.8	-9.6	2303	1038	21.6	-9.2	7	35	509.0	-85.5	3.8	24.8	-22.1
18TH	190.50	51.4	-9.4	2303	1038	22.3	-9.1	7	37	459.3	-75.9	3.0	20.1	-20.3
19TH	200.25	53.0	-9.3	2303	1038	23.0	-9.0	7	38	407.8	-66.4	2.3	15.9	-18.3
2 O T H	210.00	52.5	-9.3	2303	1039	22.6	-9.0	7	38	354.8	-57.1	1.7	12.2	-16.3
215T	219.75									302.3	-47.8	1.2	9.0	-14.2
2 2 N D	229.50	52.0	-9.4	2303	1038	22.6	-9.0	7	39	250.3	-38.4	. 8	6.3	-12.1
238 D	239.25	51.6	-9.4	2303	1038	22.4	-9.0	7	39	198.7	-29.1	. 5	4.1	-10.0
24TH	249.00	51.1	-9.4	2303	1038	22.2	-9.0	7	40	147.6	-19.7	. 2	2.4	-7.9
25TH	258.75	50.6	-9.4	2303	1038	22.0	-9.0	8	41	97.1	-10.3	. 1	1.2	-5.8
		44 5	- 8.5	2303	1038	19.3	- 8 . 1	9	46	· · · •				

TABLE VIND D	7 SHEAR IRECTION	AND MOMEN 220	NT DIAGRA	NS : CONFIGUR	ATION A SA	N DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TO 7.0 PSF	GWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y		(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	KIPS) Z
NECH	268.50	52.6	-1.9	4959	1917	12.4	-10	2 69	52.6	-1.9	. •	. 5	-3.6
TOP	286.50	32.6	-1.7	4232		• • • •			¢.¢	Q.Q	¢.¢	¢.¢	¢.¢

TABLE Wind D	7 SHEAR IRECTION	AND MOMEI 230	NT DIAGR	ANS : Configur:	ATION A	AN DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL Essure	EAST T E 27.0 PSF	OVER IN	GUST F	ACTOR 1 3	32
FLOOR	HEIGHT	FORCE	(KIPS)	AREA :	(SQ FT)	P RE SS URE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MONENT : X	(1000-FT- Y	-KIPS) Z
1 S T	¢.¢¢	5 4 0	-6.7	2034	876	25.2	-7.6	2	12	1366.2	-114.9	17.6	205.7	-46.7
2 N D	17.00	51.2					- 6 2	2	12	1315 1	-108.2	15.7	182.9	-46.1
3RD	34.00	39.2	-7.2	2034	876	19.3			14	1275.8	-101.1	13.9	160.8	-45.6
4TH	54.00	61.6	-16.0	2743	1195		-13.4	4		1214.3	-85.1	12.0	135.9	-44.7
STH	63.75	53.8	3.1	2303	1039	23.4	3.0	-1	17	1160.5	-88.2	11.2	124.4	-43.7
6 T H	73.50	52.2	3.1	2303	1030	22.7	3.0	-1	18	1108.2	-91.3	10.3	113.3	-42.8
7TH	83.25	52.8	1.0	2303	1039	22.9	1.0	- 0	22	1055.5	-92.4	9.4	102.8	-41.6
8TH	93.00	53.3	-1.1	2303	1038	23.1	-1.0	Ó	25	1002.2	-91.3	8.5	92.7	-40.3
9TH	102.75	53.8	-3.2	2303	1038	23.3	-3.1	2	28	948.4	-88.1	7.7	83.2	-38.8
1078	112.50	54.2	-4.7	2303	1038	23.6	-4.5	3	30	894.2	-83.5	6.8	74.2	-37.1
1178	122.25	54.6	-4.5	2303	1038	23.7	-4.3	3	31	839.6	-79.0	6,0	65.8	-35.4
1278	132.00	55.0	-4.3	2303	1038	23.9	-4.2	3	32	784.6	-74.6	5.3	57.9	-33.6
		55.3	-4.2	2303	1038	24.0	-4.0	3	34	729.3	-70.5	4.6	50.5	-31.8
13TH	141.75	55.7	-4.0	2303	1038	24.2	-3.8	2	35	673.6	-66.5	3.9	43.6	-29.8
14TH	151.50	53.3	-4.5	2303	1039	23.1	-4.3	3	36	620.3	-62.0	3.3	37.3	-27.9
15TH	161.25	47.1	-6.2	2303	1038	20.4	-5.9	5	39			2.7	31.5	-26.0
16TH	171.00	48.7	-5.9	2303	1038	21.1	-5.7	5	41	573.2	-55.8		26.2	-24.0
17TH	180.75	54.3	-5.7	2303	1038	21.8	-5.4	5	42	524.5	-49.9	2.2		
18TH	190.50	51.9	-5.4	2303	1039	22.5	-5.2	4	43	474.3	-44.3	1.7	21.3	-21.8
19TH	200.25	53.4	-5.2	2303	1038	23.2	-5.0	4	44	422.4	-38.9	1.3	16.9	-19.6
2 0 T H	210.00	52.8	-5.4	2303	1038	22.9	-5.2	4	44	368.9	-33.7	1.0	13.1	-17.2
215T	219.75			2303	1039	22.7	-5.4	5	44	316 1	-28.3	. 7	9.7	-14.9
2 2 N D	229.50	52.2	-5.6				-5.6	5	44	263.8	-22.7	. 4	6.9	-12.5
2 3 R D	239.25	51.6	-5.8	2303	1038	22.4		-		212 2	-16.9	. 2	4.6	-10.2
24TH	249.00	51.0	-6.0	2303	1038	22.1	-5.8	5	44	161.2	-10.9	. 1	2.8	-8.0
25TH	258.75	50.4	-6.3	2303	1038	21.9	-6.0	5	44	110.8	-4.6	, ¢	1.4	-5.7
		46.3	-5.5	2303	1038	20.1	-5.3	6	47					

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	T DIAGRA	NS : CONFIGURA	TION A SA	N DIEGO IN	REFE	INENTAL I Rence pri	10 T E L ESSURE	EAST TO 27.0 PSF	DWER IN	GUST F	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT> Y	P RE SSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	64.5	٥	4252	1017	15.2	. 5	- 1	54	64.5	. 9	0	. 6	-3.5
TOP	286.50	67.3	. 7	4232	1211		. 🗸	•	•••	¢.¢	0 .0	¢,¢	0 .0	\$.\$

TABLE Wind D	7 SHEAR	AND MONEN	T DIAGR	AMS : Configura	SI TION A	AN DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL	EAST T 27.0 PSF	OWER IN	GUST F	ACTOR 1.3	12
FLOOR	HEIGHT		(KIPS)	AREA (X	SQ FT)	PRESSURE	(PSF) Y	ECCEN X	(FT)	SHEAR	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00				0.77	00 7	-6.7	2	14	1120.1	-166.2	26.7	164.8	-42.9
2ND	17.00	46.1	~5.9	2034	876	22.7			16	1074.0	-160.2	23.9	146.2	-422
3RD	34.00	35.8	~7.0	2034	876	17.6	-8.0	3		1039.3	-153.3	21.3	128.2	-41.7
4TH	54.00	53.7	-15.3	2743	1195	19.6	-12.8	5	17	984.5	-137.9	18.4	108.0	-40.6
STH	63.75	47.1	1.4	2303	1038	20.4	1.4	-1	17	937.4	-139.4	17.0	98.6	-39.9
6TH	73.50	45.4	1.4	2303	1038	19.7	1.3	-1	18	892.0	-140.8	15.6	89.7	-39.0
7TH	83.25	45.2	9	2303	1038	19.6	9	¢	22	846.8	-139.8	14.3	81.2	-38.0
8TH	93.00	45.0	-3.2	2303	1038	19.5	-3.1	2	26	801.8	-136.6	12.9	73.2	-36.9
	102.75	44.8	-5.5	2303	1038	19.5	-5.3	4	30	757.0	-131.1	11.6	65.6	-35.5
9TH		44.8	-7.2	2303	1038	19.4	- 5.9	5	33	712.2	-123.9	10.4	58.4	-34.0
1078	112.50	45.2	-7.1	2303	1038	19.6	- 6 . 8	5	35	667.9	-116.8	9.2	51.7	-32.4
11TH	122.25	45.6	-7.0	2303	1038	19.8	-6.7	6	36	621.4	-109.8	8.1	45.4	-30.7
1278	132.00	46.0	-6.9	2303	1039	20.0	-6.6	6	38	575.4	-102.9	7.1	39.6	-28.9
13TH	141.75	46.4	-6.8	2303	1038	20.2	-6.5	6	39	528.9	-96.2	6.1	34.2	-27.0
14TH	151.50	43.9	-6.8	2303	1038	19.1	-6.5	6	42		-89.4	5.2	29.3	-25.1
15TH	161.25	37.0	-7.2	2303	1038	16.1	-6.9	9	46	485.0			24.7	-23.3
16TH	171.00	38.1	-7.3	2303	1038	16.5	-7.0	9	48	448.1	-82.2	4.3		
17TH	180.75	39.2	-7.3	2303	1038	17.0	-7.1	9	50	410.0	-74.9	3.6	20.5	-21.4
18TH	190.50	40.2	-7.4	2303	1038	17.5	-7.1	10	52	370.8	-67.6	2.9	16.7	-19.4
1 9T H	200.25		-7.5	2303	1038	17.9	-7.2	10	54	330.6	-60.2	2.3	13.3	-17.2
20TH	210.00	41.3			1038	17.8	-7.4	10	53	289.3	-52.7	1.7	10.3	-14.9
21ST	219.75	41.0	-7.7	2303			-7.6	10	51	248.3	-45.0	1.2	7.7	-12.7
2 2 N D	229.50	40.7	-7.9	2303	1038	17.7				207.6	-37.1	. 8	5.5	-10.5
23RD	239.25	40.3	-8.1	2303	1038	17.5	-7.8	10	50	167.3	-29.0	. 5	3.6	-8.4
24TH	249.00	40.0	-8.3	2303	1038	17.4	-8.0	10	49	127.2	-20.7	. 3	2.2	-6.4
25TH	258.75	39.7	-8.6	2303	1038	17.2	-8.2	10	48	87.5	-12.1	. 1	1.1	-4.4
LUIN	244.44	35.8	-8.4	2303	1038	15.5	- 8 . 1	11	48					

TABLE WIND D	7 SHEAR IRECTION	AND NOMEN	T DIAGRI	ANS : SAN Configuration a	DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TO	DWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (SQ FT) X Y	P P E S S U R E X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	MONENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	51.7	-3.7	4252 1917	12.2	-19	4 49	51 7	-3.7	. ¢	. 5	-2.6
TOP	286.50	51.7	-3.7	4232 1711	12.2	~ 4		Q .Q	Q .Q	0.0	Q.Q	0 .0

TABLE Wind D	7 SHEAR IRECTION	AND MONES	NT DIAGR	ANS : Configura	SI TION A	AN DIEGO IM	ITERCONT REFE	INENTAL Rence pr	HOTEL Ressure	EAST T 27.0 PSF	OVER IN	GUST FA	CTOR 1.3	32
FLOOR	HEIGHT		(KIPS)	AREA (X	SQ FT>	PRESSURE	(PSF) Y	ECCEN	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT (X	1000-FT- Y	-KIPS) Z
1 S T	0.00						- .			679.6	-213.6	34.9	91 1	-29.9
ZND	17.00	36.0	-4.4	2034	876	17.7	-5.0	2	14	643.6	-209.2	31.3	79.9	-29.4
3RD	34.00	28.3	-4.6	2034	876	13.9	-5.3	2	12	615.3	-204.5	27.8	69.2	-29.0
4TH	54.00	42.2	-13.9	2743	1195	15.4	-11.6	5	15	573.1	-190.6	23.8	57.3	-28.3
578	63.75	33.3	-1.3	2303	1039	14.5	-1.2	¢	10	539.8	-189.3	22.0	51.9	-28.0
	73.50	31.5	-1.0	2303	1038	13.7	-1.0	¢	12	508.3	-188.3	20.1	46.7	-27.6
6TH		31.1	-3.4	2303	1038	13.5	-3.2	2	19	477.2	-185.0	18.3	41.9	-27.0
7TH	83.25	30.8	-5.7	2303	1039	13.4	~5.5	5	25	446.5	-179.2	16.6	37.4	-26.2
STH	93.00	30.4	-8.i	2303	1039	13.2	-7.8	8	31	416.0	-171.2	14.8	33.2	-25.2
9T H	102.75	30.1	-9.8	2303	1038	13.1	-9.4	11	35	385.9	-161.4	13.2	29.3	-24.0
1 O T H	112.50	30.0	-9.8	2303	1038	13.0	-9.4	12	37	355.9	-151.6	11.7	25.7	-22.8
11TH	122.25	29.9	-9.8	2303	1038	13.0	-9.4	13	38	326.4	-141.8	10.3	22.4	-21.5
12TH	132.00	29.8	-9.8	2303	1038	12.9	-9.4	13	40			8.9	19.4	-20.2
13TH	141.75	29.6	-9.8	2303	1038	12.9	-9.5	14	41	296.3	-132.0		16.6	-18.8
14TH	151.50	26.1	-9.5	2303	1038	11.3	-9.1	16	44	266.6	-122.2	7.7		-17.5
15TH	161.25	17.7	-8.8	2303	1038	7.7	-8.5	25	51	240.6	-112.7	6.5	14.1	
16TH	171.00	18.8	-9.0	2303	1038	8. i	-8.7	26	55	222.9	-103.9	5.5	11.9	-16.4
17TH	180.75		-9.3	2303	1038	8.6	-8.9	27	58	204.1	-94.9	4.5	9.8	-15.1
18TH	190.50	19.8				9.1	-9.2	28	62	184.3	-85.6	3.6	7.9	-13.7
19TH	200.25	20.9	-9.5	2303	1038			29	64	163.5	-76.1	2.9	6.2	-12.2
20TH	210.00	21.9	-9.8	2303	1038	9.5	-9.4		62	141.6	-66.3	2.2	4.7	-10.5
215T	219.75	21.7	-9.9	2303	1038	9.4	-9.5	28		119.9	-56.4	1.6	3.4	-8.8
22ND	229.50	21.5	-10.1	2303	1038	9.3	-9.7	28	60	98.4	-46.4	1.1	2.4	-7.3
23RD	239.25	21.3	-10.2	2303	1038	9.2	-9.8	28	58	77.1	-36.2	. 7	1.5	-5.7
2411	249.00	21.1	-10.3	2303	1038	9.2	-10.0	27	56	56.0	-25.8	. 4	. 9	-4.3
25TH	258.75	20.9	-10.5	2303	1038	9.1	-10.1	27	54	35.1	-15.4	. 2	. 4	-2.9
2018	230.(3	16.1	-9.9	2303	1038	7.0	-9.6	34	54					

TABLE UIND D	7 SHEAR IRECTION	AND NOME	T DIAGR	ANS : SAN Configuration a	DIEGO INT	REFE	INENTAL HOTEL - Rence pressure	- EAST TO 27.0 PSF	WER IN	GUST FA	ACTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAP X	(KIPS) Y	NOMENT (X	1000-FT-1 Y	(IPS) Z
NECH	268.50	1.0 .	-5.4	4252 1917	4.5	-28	23 80	19.0	-5.4	, ¢	. 2	-1.6
TOP	286.50	19.0	-9.4	4232 1717	· · ·			Q.Q	¢.¢	¢.¢	V.V	¢.¢

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN	NT DIAGR	AMS : Configura	SAI TION A	N DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL	EAST T 27 0 PSF	OWER IN	GUST FA	CTOR 1.3	2
FLOOR	HEIGHT		(FIPS)	AREA (X	SQ FT) Y	PRESSURI	E (PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT- Y	KIPS) Z
157	0.00								_	175.8	-212.9	34.1	97	-7.5
200	17.00	25.8	9	2034	876	12.7	-1.1	0	8	150.0	-211.9	30.5	6.9	-7.2
		26.9	-1.4	2034	876	10.3	-1.6	¢	7	129.1	-210.5	26.9	4.6	-7.1
3RD	34.00	24.8	-10.1	2743	1195	9.1	-8.5	2	4	104.3	-200.4	22.8	2.2	-7.0
4TH	54.00	15.6	-4.8	2303	1038	6.8	-4.6	- 8	-25	88.7	-195.6	20.9	1.3	-7.4
STH	63.75	13.7	-4.5	2303	1038	6.0	-4.3	- 7	-22	74.9	-191.1	19.0	. 5	-7.7
6T H	73.50	13.0	-6.2	2303	1039	5.6	-6.0	-4	- 9	61.9	-184.9	17.1	2	-7.9
7TH	83.25	12.2	-8.0	2303	1038	5.3	-7.7	2	3	49.8	-176.9	15.4	7	-7.8
8TH	93.00	11.4	-9.7	2303	1038	5.0	-9.4	10	12	38.3	-167.1	13.7	-1.2	-7.6
9TH	102.75	10.7	-11.0	2303	1038	4.7	-10.6	18	17	27.6	-156.2	12.1	-1.5	-7.2
10TH	112.50	10.3	-10.9	2303	1038	4,5	-10.5	19	18	17.3	-145.3	10.7	-1.7	-6.8
11TH	122.25	9.9	-10.8	2303	1038	4.3	-10.4	20	18	7.3	-134.5	9.3	-1.8	-6.4
12TH	132.00	9.5	-10.6	2303	1038	4.1	-10.2	21	19	-2.2	-123.9	8.0	-1.8	-6.0
13TH	141.75	9.1	-10.5	2303	1038	4.0	-10.1	22	19		-113.4	6.9	-1.8	-5.6
14TH	151.50	5.9	-10.0	2303	1038	2.6	-9.6	25	15	-11.3		5.8	-1.6	-5.3
15TH	161.25	-1.3	-8.9	2303	1039	6	-8.6	22	- 3	-17.2	-103.4		-1.5	-5.1
16TH	171.00	9	-8.9	2303	1038	4	-8.5	33	- 3	-15.9	-94.5	4,9	-1.3	-4.8
17TH	180.75	6	-8.9	2303	1038	3	-8.5	44	- 3	-15.0	-85.6	4.0		
18TH	190.50			2303	1038	1	-8.5	55	- 1	-14.4	-76.7	3.2	-1.2	-4.4
19TH	200.25	2	-8.8	2303	1038	. 1	-8.5	66	1	-14.2	-67.9	2.5	-1.0	-3.9
20TH	210 00	. 1	-8.8			. 0	-8.7	62	0	-14.3	-59.1	1.9	9	-3.3
21ST	219.75	. 1	-9.0	2303	1038		-8.9	58	- 0	-14.4	-50.1	1.3	8	-2.8
2 2 N D	229.50	0	-9.2	2303	1038	-,0			- 0	-14.4	-40.9	. 9	6	-2.2
2380	239.25	1	-9.4	2303	1038	0	-9.0	54		-14.3	-31.5	. 5	-,5	-1.7
2418	249.00	- 1	-9.6	2303	1038	1	-9.2	50	-1	-14.2	-21.9	. 3	3	-1.3
25TH	258.75	2	-9.8	2303	1038	1	-9.4	47	-1	-14.0	-12.2	. 1	2	8
2010	200.00	-3.7	-8.8	2303	1038	-1.6	-8.5	30	-13					

TABLE WIND D	7 SHEAR IRECTION	AND NOMEN 260	IT DIAGRA	MS : SAN Configuration a	DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure :	EAST TO 27.0 PSF	WER IN	GUST F	ACTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT-K Y	(IPS) Z
MECH	268.50	-10.3	-3.4	4252 1917	-2.4	- 1 9	14 -43	-10.3	-3.4	. 0	1	~.5
TOP	286.50	-10.3	-3.4	4232 1717	-2.4	-1.0	14 45	¢.¢	Q.Q	Ø., Ø	Q.Q	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	IT DIAGRI	NS 3 Configura	SF TION A	N DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL	EAST T 27.0 PSF	OWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA (X	SQ FT> Y	PRESSURE	(PSF) Y	ECCE	H (FT) Y	SHEAR X	(KIPS) Y	MOMENT	(1000-FT- Y	KIPS) Z
1 S T	0.00							-0	2	-288.4	-128.3	20.5	-62.0	23.1
2ND	17.00	14.9	4.0	2034	876	7.3	4.5			-303.3	-132.4	18.3	-57.0	23.1
380	34.00	12.2	3.5	2034	876	6.0	4.0	4	-13	-315.5	-135.8	16.0	-51.8	22.9
4TH	54.00	5.8	-4.0	2743	1195	2.1	-3.3	-62	-90	-321.3	-131.9	13.3	-45.4	22.2
STH	63.75	-2.1	-5.7	2303	1039	9	-5.5	-171	64	-319.2	-126.2	12.1	-42.3	21.1
6TH	73.54	-3.5	~5.5	2303	1039	-1.5	-5.3	-134	87	-315.6	-120.7	10.9	-39.2	20.0
718	83.25	-5.0	-6.1	2303	1038	-2.2	-5.8	-97	80	-310.6	-114.6	9.7	-36.1	19.0
8TH	93.00	-6.4	-6.6	2303	1038	-2.8	-6.4	-72	70	-304.3	-108.0	8.6	-33.1	18.1
9TH	102.75	-7.8	-7.2	2303	1038	-3.4	-6.9	-55	60	-296.5	-100.7	7.6	-30.2	17.2
1018	112.50	-9.0	-7.6	2303	1039	-3.9	-7.3	-45	54	-287.4	-93.2	6.7	-27.3	16.4
1178	122.25	-9.8	-7.3	2303	1038	-4.2	-7.1	-43	57	-277.7	-85.8	5.8	-24.6	15.5
1278	132.00	-10.5	-7.1	2303	1038	-4.6	-6.9	-41	60	-267.2	-78.7	5.¢	-21.9	14.6
1378	141.75	-11.2	-6.9	2303	1038	-4.9	-6.7	-39	63	-255.9	-71.8	4.2	-19.4	13.6
		-12.0	-6.7	2303	1038	-5.2	-6.4	-36	65	-244.0	-65.1	3.6	-16.9	12.6
14TH	151.50	-13.3	-6.5	2303	1038	- 5.8	-6.3	-31	63	-230.6	-58.6	3.0	-14.6	11.6
15TH	161.25	-15.8	-6.4	2303	1038	-6.9	-6.1	-22	54	-214.8	-52.2	2.4	-12.5	10.6
1678	171.00	-16.6	-6.0	2303	1038	-7.2	-5.8	-19	52	-198.2	-46.2	2.0	-10.4	9.6
1778	180.75	-17.4	-5.7	2303	1038	-7.5	-5.5	-16	50	-180.8	-40.6	1.5	-8.6	8.6
18TH	190.50	-18.1	-5.3	2303	1038	-7.9	-5.1	-14	48	-162.7	-35.2	1.2	-6.9	7.7
19TH	200.25	-18.9	-5.0	2303	1038	- 8.2	-4.8	-12	46	-162.7	-30.3	. 8	-5.4	6.8
20TH	210.00	-19.7	-5.1	2303	1038	-8.i	-4.9	-13	46			. 6	-4.1	5.8
21ST	219.75	-18.6	-5.2	2303	1038	- 8.1	-5.0	-13	47	-125.1	-25.2		-3.0	4.9
2 2 N D	229.50	-18.5	-5.3	2303	1038	-8.0	-5.i	-13	47	-106.5	-20.0	. 4		
2 3 R D	239.25	-18.4	-5.4	2303	1038	-8.0	-5.2	-14	47	-88.0	-14.8	. 2	-2.0	4.¢
24TH	249.00	-18.2	-5.5	2303	1038	-7.9	-5.3	-14	47	-69.6	-9.4	. 1	-1.3	3.0
25TH	258.75	-19.8	-5.1	2303	1038	-8.6	-4.9	-11	44	-51.3	-4.0	, Q	7	2.1

	7. SHEAR IRECTION	AND MONEN 270	T DIAGRA	NS : SAN Configuration a	DIEGO INT	ERCONT: Refei	INENTAL HOTEL Rence pressure 2	- EAST TO 27.0 PSF	OVER IN	GUST FA	CTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT-K Y	(IPS) Z
MECH	268.50	-31.5	1 3	4252 1917	-7 4	6	1 37	-31.5	1.2	0	3	1.2
TOP	286.50	-31.3	1.4	4232 1711	(. 4		0.0	0.0	0.0	0.0	0.0

TABLE	7 SHEAR IRECTION	AND MONES	T DIAGR	AMS : Configura	SI TION A	N DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL Ressure	EAST TO 27 0 PSF	DWER IN	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y		SQ FT>	PRESSURE	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1ST	0.00									-611.5	-52.0	9.6	-107.9	49.4
210	17.00	4.6	9.3	2034	876	2.3	10.6	17	- 9	-616.1	-61.3	8.6	-97.4	49.2
		4.9	8.2	2034	876	2.4	9.4	29	-17	-620.9	-69.5	7.5	-86.9	48.9
3R D	34.00	-12.6	2.5	2743	1195	-4.6	2.1	21	109	-608.3	-72.0	6.1	-74.6	47.5
4TH	54.00	-15.1	-5.5	2303	1038	-6.5	-5.3	-30	84	-593.3	-66.5	5.4	-68.8	46.1
STH	63.75	-16.2	-5.4	2303	1038	-7.0	-5.2	-27	80	-577.1	-61.1	4.8	-63.1	44.6
6TH	73.50	-19.0	-4.9	2303	1038	- 8.2	-4.7	-20	77	-558.1	-56.2	4.2	-57.5	43.1
7 T H	83.25	-21.7	-4.4	2303	1038	-9.4	-4.2	-15	74	-536.4	-51.8	3.7	-52.2	41.4
8T H	93.00	-24.5	-3.9	2303	10 38	-10.6	-3.7	-11	71	-511.9	-47.9	3.2	-47.1	39.6
9T H	102.75	- 26 . 6	-3.4	2303	1039	-11.5	-3.3	- 9	70	-485.3	-44.5	2.8	-42.2	37.7
1 Q T H	112.50	-26.6	-3.2	2303	1038	-11.6	-3.1	- 9	73	-458.7	-41.3	2.3	-37.6	35.7
11TH	122.25	- 26 . 7	-3.0	2303	1038	-11.6	-2.9	- 8	76	-431.9	-38.3	2.0	-33.3	33.7
12TH	132.00	-26.8	-2.7	2303	1038	-11.6	-2.6	- 8	79			1.6	-29.2	31.5
1 3 T H	141.75	-26.9	-2.5	2303	1038	-11.7	-2.4	- 8	82	-405.2	-35.6		-25.4	29.3
14TH	151.50	- 25 . 6	-3.4	2303	1038	-11.1	-3.2	-11	82	-378.3	-33.1	1.3		27.2
15TH	161.25	-23.3	-5.7	2303	1038	-10.1	-5.5	-18	74	-352.7	-29.7	1.0	-21.8	
16TH	171.00	-23.3	-4.8	2303	1038	-10.9	-4.7	-14	75	-329.4	-24.1	. 7	-18.5	25.3
17TH	180.75			2303	1038	-11.8	-3.9	-11	74	-304.2	-19.2	. 5	-15.4	23.4
18TH	190.50	-27.1	-4.0			-12.6	-3.1	- 8	74	-277.1	-15.2	. 3	-12.6	21.3
19TH	200.25	-29.0	-3.2	2303	1038		-2.3	- 6	74	-248.1	-12.0	. 2	-10.0	19.1
20TH	210.00	- 30.9	-2.4	2303	1038	-13.4			74	-217.2	-9.6	. 1	-7.7	16.9
21ST	219.75	-30.6	-2.4	2303	1038	-13.3	-2.3	- 6		-186.6	-7.2	Q	-5.8	14.6
22ND	229.50	- 30 . 4	-2.5	2303	1038	-13.2	-2.4	- 6	75	-156.2	-4.7	1	-4.1	12.3
23RD	239.25	- 30 . 2	-2.5	2303	1038	-13.1	-2.4	-6	75	-126.0	-2.2	1	-2.7	10.0
24TH	249.00	- 30 . 0	-2.6	2303	1038	-13.0	-2.5	- 6	76	-96.1	. 3	1	-1.6	7.7
		- 29 . 7	-2.6	2303	1038	-12.9	-2.5	- 7	77	-66.3	2.9	1	9	5.4
25TH	258.75	- 28 . 2	-2.5	2303	1038	-12.2	-2.4	-7	78					

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	NT DIAGRA	NS : SAN Configuration a	DIEGO IN	TERCONT REFE	INENTAL HO Rence pres	SURE	27.0 PSF	DWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN C	FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-1 Y	KIPS) Z
NECH	268.50	- 38 . 2		4252 1917	-9.0	28	12 8	12	- 38 . 2	5.4	¢	3	3.2
TOP	286.50	-38.2	J. 4	7232 1911	···· 2. V	a W		-	Q.Q	0 .0	¢,¢	Q . Q	¢.¢

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN	T DIAGR	AMS : Configura	SI TION A	AN DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL	EAST T 27 0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT>	PRESSURE X	(PSF) Y	ECCEN X	(FT)	SHEAR X	(KIPS) Y	NONENT	(1000-FT- Y	KIPS) Z
1 S T	0.00					. .	10.3	5	12	-845.5	-127.7	25.0	-134.7	50.2
2ND	17.00	-19.5	9.0	2034	876	-9.6			11	-826.9	-136.7	22.7	-120.5	49.9
3RD	34.00	-17.9	8.9	2034	876	-8.8	10.1	5		-808.1	-145.6	20.3	-106.6	49.6
4TH	54.00	-38.3	6.3	2743	1195	-13.9	5.3	6	38	-769.8	-151.9	17.3	-90.9	48.1
578	63.75	- 27 . 5	-6.5	2303	1038	-12.0	-6.3	-12	51	-742.3	-145.4	15.9	-83.5	46.7
6TH	73.50	- 27.1	-7.3	2303	1038	-11.8	-7.0	-14	51	-715.2	-138.1	14.5	-76.4	45.2
		-28.8	-6.8	2303	1038	-12.5	-6.6	-13	53	-686.3	-131.3	13.2	-69.6	43.6
7TH	83.25	- 30 . 5	-6.3	2303	1038	-13.3	-6.1	-11	55	-655.8	-124.9	11.9	-63.0	41.8
8TH	93.00	- 32 . 2	-5.9	2303	1038	-14.0	-5.6	-10	56	-623.6	-119.1	10.8	-56.8	40.0
9TH	102.75	- 33 . 4	-5.5	2303	1038	-14.5	-5.2	- 9	58	-590.1	-113.6	9.6	-50.9	38.0
1 0 T H	112.50	- 33 . 3	-5.3	2303	1038	-14.5	-5.1	- 9	60	-556.8	-108.4	8.5	-45.3	35.9
11TH	122.25	-33.2	-5.1	2303	1038	-14.4	-4.9	- 9	62	-523.7	-103.3	7.5	-40.0	33.8
12TH	132.00	-33.0	-4.9	2303	1038	-14.3	-4.7	- 9	64	-490.6	-98.5	6.5	-35.1	31.6
13TH	141.75	- 32 . 9	-4.7	2303	1038	-14.3	-4.5	- 9	66	-457.7	-93.8	5.6	-35.4	29.4
14TH	151.50	-31.9	-5.9	2303	1038	-13.8	-5.7	-12	66		-87.9	4.7	-26.1	27.2
15TH	161.25	-30.4	-9.5	2303	1039	-13.2	-9.1	-18	58	-425.9		3.9	-22.1	25.3
16TH	171.00	-31.9	-8.9	2303	1038	-13.8	-86	-17	59	-395.5	-78.4			23.3
17TH	180.75	- 33 . 4	-8.4	2303	1038	-14.5	-8.1	-15	59	-363.6	-69.5	3.2	-18.4	
18TH	190.50	-34.9	-7.9	2303	1038	-15.2	-7.6	-13	59	-330.2	-61.0	2.5	-15.0	21.2
19TH	200.25	-34.9	-7.4	2303	1038	-15.8	-7.1	-12	60	-295.3	-53.1	2.¢	-12.0	19.0
20TH	210.00			2303	1038	-15.7	-6.9	-12	60	-258.9	-45.7	1.5	-9.3	16.7
21ST	219.75	-36.2	-7.2				-6.8	-12	60	-222.7	-38.5	1.1	-6.9	14.5
22ND	229.50	-35.9	-7.0	2303	1038	-15.6				-186.8	-31.5	. 7	-4.9	12.2
2 3 R D	239 25	- 35 . 7	-6.8	2303	1038	-15.5	-6.6	-11	60	-151.1	-24.6	. 5	-3.3	10.0
24TH	249.00	- 35 . 5	-6.6	2303	1038	-15.4	-6.4	-11	60	-115.6	-18.0	. 3	-2.0	7.8
25TH	258.75	- 35 . 3	-6.4	2303	1038	-15.3	-6.2	-11	60	- 80 . 3	-11.6	. 1	-1.0	5.6
6. U I H		-33,4	-7.2	2303	1039	-14.5	-6.9	-13	63					

TABLE Wind D	7 SHEAR IRECTION	AND MONEN	IT DIAGR	ANS : Configurat	SA Ion a	N DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL	EAST TI 27.0 PSF	DVER IN	GUST FA	CTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (S X	Q FT>	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR	(KIPS) Y	NOMENT (X	1000-FT-1	KIPS) Z
NECH	268.50	- 47 6	-4.4	4252	1617	-11.0	-23	-7	72	-47.0	-4.4	. •	4	3.4
TOP	286.50	-47.9		TEVE	1714	••••	4 4 · · •4	•	••	0.0	0.0	0.0	Ó.Ô	0.0

TABLE Wind D	7 SHEAR	AND HOME	NT DIAGR	AMS : Configuri	SA TION A	N DIEGO IN	TERCONT Refe	INENTAL Rence Pri	HO T E L E S S U R I	EAST T E 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MONENT X	(1000-FT- Y	KIPS) Z
1 S T	6.00			.			7 0	2	10	-1015.0	-248.7	46.1	-156.0	43.4
2ND	17.00	-37.0	7.0	2034	876	-18.2	7.9			-978.0	-255.7	41.8	-139.1	43.0
380	34.00	- 34 . 9	6.6	2034	876	-17.1	7.6	2	8	-943.1	-262.3	37.4	-122.7	42.7
4TH	54.00	-51.7	5.7	2743	1195	-18.9	4.8	2	21	-891.4	-268.1	32.1	-104.4	41.6
578	63.75	-36.i	-8.7	2303	1038	-15.7	-8.3	- 9	38	-855.3	-259.4	29.6	-95.9	40.2
	73.50	- 35 . 8	-10.0	2303	1038	-15.5	-9.6	-11	38	-819.5	-249.4	27.1	-87.7	38.7
6TH		- 36 . 3	-10.1	2303	1038	-15.7	-9.7	-11	39	-783.3	-239.3	24.7	-79.9	37.2
7TH	83.25	-36.7	-10.2	2303	1038	-16.0	-9.8	-11	41	-746.5	-229.1	22.4	-72.4	35.6
8TH	93.00	- 37 . 2	-10.3	2303	1038	-16.2	-10.0	-12	43	-709.3	-218.8	20.2	-65.3	33.8
9T H	102.75	- 37 . 4	-10.4	2303	1038	-16.3	-10.0	-12	44	-671.8	-208.4	18.2	-58.6	32.1
1 ¢ T H	112.50	-36.9	-10.1	2303	1038	-16.0	-9.8	-13	46	-634.9	-198.3	16.2	-52.2	30.3
1 1 T H	122.25	-36.3	-9.9	2303	1038	-15.8	-9.5	-13	47		-108.3	14.3	-46.2	28.4
12TH	132.00	-35.8	-9.7	2303	1038	-15.5	-9.3	-13	49	-598.6		12.5	-40.6	26.5
13TH	141.75	- 35 . 2	-9.5	2303	1038	-15.3	-9.1	-14	51	-562.8	-178.7			24.6
14TH	151.50	- 35 . 5		2303	1038	-15.4	-10.2	-15	50	-527.5	-169.2	10.8	-35.3	
15TH	161.25	- 37 . 7		2303	1038		-13.5	-16	44	-492.1	-158.6	9.2	-30.3	22.7
16TH	171.00	-39.3	-13.9	2303	1039		-13.4	-16	43	-454.3	-144.6	7.7	-25.7	20.8
17TH	180.75			2303	1039		-13.3	-15	43	-416.1	-130.7	6.4	-21.4	18.9
18TH	190.50	- 38 . 8	-13.8				-13.2	-15	43	-377.3	-116.9	5.2	-17.6	17.0
19TH	200.25	- 39 . 3	-13.7	2303	1038					-338.0	-103.2	4.1	-14.1	15.2
20TH	210.00	- 39 . 9	-13.6	2303	1038		-13.1	-14	42	-298.1	-89.6	3.2	-11.0	13.3
2157	219.75	- 39 . 9	-13.2	2303	1038		-12.7	-14	42	-258.3	-76.4	2.4	-8.3	11.4
22ND	229.50	- 39 . 9	-12.8	2303	1038	-17.3	-12.3	-13	41	-218.4	-63.6	1.7	-5.9	9.6
		- 39 . 9	-12.4	2303	1038	-17.3	-11.9	-13	41	-178.4	-51.3	1.1	-4.0	7.8
23RD	239.25	- 39 . 9	-11.9	2303	1038	-17.3	-11.5	-12	40	-138.5	-39.3	. 7	-2.5	6.1
24TH	249.00	- 39 . 9	-11.5	2303	1038	-17.3	-11.1	-i i	40	- 98 . 6	-27.8	. 3	-1.3	4.3
25TH	258.75	- 39 . 6	-12.5	2303	1038	-17.2	-12.1	-12	39					

TABLE Wind D	7 SHEAR IRECTION	AND NOMENT DIAGRA	INS : SAN Configuration a	DIEGO INT	REFE	INENTAL HOTEL Rence pressure 2	EAST TO	WER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	(IPS) Z
NECH	268.50	-59.0 -15.3	4252 1917	-13.9	-8.0	-11 42	-59.0	-15.3	. 1	5	2.6
TOP	286.50	-39.0 -13.3	4232 1717	-13.7	-0.0	-11 -12	Q.Q	0 .0	Q.Q	\$.\$	\$.\$

TABLE Wind D	7 SHEAR IRECTION	AND NOMEN	NT DIAGRI	ANS : Configura	SAI TION A	N DIEGO IN	TERCONT	INENTAL RENCE PR	HOTEL Essure	EAST T 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1ST	0.00				0.74	07 0	5.3	1	8	-1329.2	-250.3	45.7	-201.4	31.6
2ND	17.00	- 54 . 8	4.6	2034	876	-26.9				-1274.4	-255.0	41.4	-179.2	31.2
3RD	34.00	-53.1	4.2	2034	876	-26.1	4.8	0	6	-1221.3	-259.2	37.0	-158.0	30.9
4TH	54.00	-70.4	7.9	2743	1195	-25.7	6.6	1	7	-1151.0	-267.1	31.8	-134.3	30.3
	63.75	- 48 . 5	-9.4	2303	1039	-21.0	-9.1	- 4	20	-1102.5	-257.7	29.2	-123.3	29.3
5TH		- 47.7	-10.8	2303	1038	-20.7	-10.4	- 5	21	-1054.8	-246.8	26.8	-112.8	28.3
6TH	73.50	-47.5	-10.8	2303	1039	-20.6	-10.4	- 5	23	-1007.2	-236.1	24.4	-102.8	27.1
7TH	83.25	- 47 . 4	-10.7	2303	1038	-20.6	-10.3	- 5	24	-959.9	-225.4	22.2	-93.2	25.9
8T H	93.00	-47.2	-10.7	2303	1038	-20.5	-10.3	- 6	26	-912.7	-214.7	20.0	-84.0	24.7
9TH	102.75	-47.0	-10.5	2303	1038	-20.4	-10.1	- 6	27		-204.1	18.0	-75.4	23.3
1 O T H	112.50	-46.7	-10.1	2303	1038	-20.3	-9.7	- 6	28	-865.7			-67.2	22.0
11TH	122.25	-46.3	-9.6	2303	1038	-20.1	-9.3	- 6	28	-819.0	-194.1	16.0		
12TH	132.00	-46.0	-9.1	2303	1039	-20.0	-8.8	- 6	29	-772.7	-184.5	14.2	-59.4	20.6
13TH	141.75	-45.6	-8.7	2303	1038	-19.8	-8.4	- 6	30	-726.7	-175.3	12.4	-52.1	19.2
14TH	151.50				_	-20.2	-9.6	- 6	29	-681.1	-166.6	10.8	-45.2	17.8
15TH	161.25	-46.6	-10.0	2303	1038				27	-634.5	-156.7	9.2	-38.8	16.4
16TH	171.00	- 50 . 0	-14.2	2303	1038		-13.7	- 8		-584.5	-142.5	7.7	-32.9	15.0
1718	180.75	- 50.3	-13.9	2303	1038		-13 4	-7	26	-534.2	-128.6	6.4	-27.4	13.5
1878	190.50	- 50 . 6	-13.7	2303	1038		-13.2	-7	26	-483.6	-114.9	5.2	-22.4	12.1
1978	200.25	-50.9	-13.5	2303	1038	-22.1	-13.0	- 7	25	-432.7	-101.4	4.2	-18.9	10.7
		-51.2	-13,2	2303	1038	-22.2	-12.8	- 6	25	-381.5	-88.1	3.2	-14.0	9.4
20TH	210.00	-51.2	-12.7	2303	1038	-22.2	-12.2	- 6	24	-330.3	-75.5	2.4	-10.5	8.1
21ST	219.75	-51.2	-12.1	2303	1038	-22.2	-11.6	- 6	24	-279.1	-63.4	1.8	-7.6	6.8
22ND	229.50	-51.2	-11.5	2303	1038	-22.2	-11.1	- 5	23		-51.9	1.2	-5.1	5.5
2 3 R D	239.25	-51.2		2303	1038	-22.2	-10.5	- 5	23	-228.0			-3.1	4.3
24TH	249.00	-51.1	-10.4	2303	1038	-22.2	-10.0	-4	22	-176.8	-40.9	. 8		
25TH	258.75	-50.8	-12.2	2303	1039	-22.1	-11.7	-5	23	-125.7	-30.6	. 4	-1.7	3.2

TABLE Wind D	7 SHEAR IRECTION	AND MONENT DIAGR	NS : SAN Configuration a	DIEGO IN	TERCONT REFE	INENTAL HOTEL - Rence pressure	- EAST TO 27 0 PSF	DWER IN	GUST F	ACTOR 1.32	Z
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE X	(PSF) Y	ECCEN (FT)	SHEAR X	(KIPS) Y	MONENT	(1000-FT-#	(IPS) Z
MECH	268.50	-74.9 -18.4	4252 1917	-17.6	-9.6	-6 25	-74.9	-18.4	. 2	7	1.9
TOP	286.50	-74.7 -16.4	4232 1711	-17.0			\$.\$	Ø.Ø	¢ .¢	0 .0	¢.¢

TABLE Wind D	7 SHEAR IRECTION	AND MONEN	T DIAGR	AMS : Configuri	SAI	OIEGO I	NTERCONT Refe	INENTAL Rence pr	HOTEL Essure	EAST T 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS)	AREA (SQ FT>	PRESSURI	E (PSF) Y	ECCENX	(FT)	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
1ST	0.00							•	-	-1519.4	-218.6	41.0	-231.5	18.2
2 N D	17.00	- 57 . 4	2.5	2034	876	-28.2	2.9	0	7	-1462.0	-221.2	37.2	-206.1	17.8
3RD	34.00	- 55 . 8	2.9	2034	876	-27.5	3.3	0	5	-1406.2	-224.0	33.5	-181.8	17.5
4TH	54.00	-73.3	10.6	2743	1195	-26.7	8.9	0	1	-1332.9	-234.6	28.9	-154.4	17.4
5TH	63.75	- 56 . 4	-8.0	2303	1038	-24.5	-7.7	- 1	9	-1276.5	-226.6	26.6	-141.6	16.9
	73.50	-56.3	-9.4	2303	1038	-24.4	-9.1	- 2	9	-1220.2	-217.2	24.5	-129.5	16.4
6TH		- 55 . 8	-9.2	2303	1038	-24.2	- 8 . 8	- 2	10	-1164.4	-208.0	22.4	-117.8	15.8
718	83.25	- 55 . 4	-8.9	2303	1038	-24.1	- 8 . 6	- 2	11	-1109.0	-199.1	20.4	-106.8	15.1
8TH	93.00	- 55 . 0	-8.7	2303	1038	-23.9	-8.4	- 2	13	-1054.0	-190.4	18.5	-96.2	14.4
9T H	102.75	- 54 . 6	- 8.4	2303	1038	-23.7	- 8 . 1	- 2	14	-999.4	-182.0	16.7	-86.2	13.7
1 0 T H	112.50	- 54 . 3	-7.9	2303	1038	-23.6	-7.6	- 2	14	-945.1	-174.1	15.0	-76.7	12.9
11TH	122.25	-54.0	-7.4	2303	1039	-23.5	-7.1	- 2	14			13.3	-67.8	12.1
12TH	132.00	- 53 . 8	-6.9	2303	1038	-23.3	-6.6	- 2	15	-891.1	-166.7			11.3
13TH	141.75	-53.5	-6.4	2303	1039	-23.2	-6.1	- 2	15	-837.3	-159.9	11.7	-59.4	
14TH	151.50	- 55 . 3	-8.0	2303	1038	-24.0	-7.7	- 2	15	-783.8	-153.5	10.2	-51.4	10.5
15TH	161.25			2303	1038	-26.2	-12.8	- 3	13	-728.5	-145.5	8.7	-44.1	9.7
16TH	171.00	-60.4	-13.3			-26.0	-12.5	- 3	13	-668.1	-132.2	7.4	-37.3	8.8
17TH	180.75	- 59 . 9	-12.9	2303	1038				13	-608.3	-119.3	6.1	-31.0	8.0
18TH	190.50	- 59.3	-12.6	2303	1038	-25.7	-12.1	- 3		-549.0	-106.7	5.0	-25.4	7.2
1978	200.25	- 58 . 8	-12.2	2303	1038	-25.5	-11.8	- 3	13	-490.2	-94.5	4.1	-20.3	6.3
2014	210.00	- 58 . 2	-11.9	2303	1038	-25.3	-11.5	- 3	13	-432.0	-82.6	3.2	-15.8	5.5
21ST	219.75	- 58 . 2	-11.3	2303	1038	-25.2	-10.9	- 3	13	-373.8	-71.3	2.4	-11.9	4.8
		-58.i	-10.6	2303	1038	-25.2	-10.2	- 2	13	-315.7	-60.7	1.8	-8.6	4.0
22ND	229.50	- 58. ¢	-10.0	2303	1038	-25.2	-9.6	- 2	12	-257.7	-50.6	1.3	-5.8	3.3
2 3 R D	239.25	- 57.9	-9.4	2303	1038	-25.1	-9.0	- 2	12	-199.8	-41.2	. 8	-3.5	2.6
24TH	249.00	- 57.8	-8.8	2303	1038	-25.i	-8.4	- 2	i i		-32.5	. 4	-1.9	1.9
25TH	258.75	- 57.9	-11.8	2303	1038	-25.i	-11.3	- 2	12	-142.0		. 4	• • •	• · ·

TABLE WIND D	7 SHEAR IRECTION	AND MONENT DIAGRA	NS : SAN Configuration a	I DIEGO INTERCONTI Refer	NENTAL HOTEL - Ence pressure	- EAST TO 27 0 PSF	WER IN	GUST FA	CTOR 1.32	Ł
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE (PSF)	ECCEN (FT) X Y	SHEAR	(KIPS) Y	HOMENT (X	1000-FT-K Y	IPS) Z
MECH	268.50	-84.1 -20.7	4252 1917	-19.8 -10.8	-3 14	-84.1	-20.7	. 2	8	1.2
TOP	286.50	-64.1 -24.6	4232 1718	-17.0 -10.0	-3 14	0 .0	0 .0	0 .0	0.0	0. 0

TABLE	7 SHEAR IRECTION	AND NOMEN	T DIAGR	ANS : Configura	SA TION A	N DIEGO IN	TERCONT Refei	INENTAL Rence pr	HOTEL	EAST T E 27.0 PSF	OWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS)		SQ FT)	PRESSURE	(PSF) Y	ECCEN	с с т э	SHEAR X	(KIPS) Y	MONENT	(1000-FT-) Y	KIPS) Z
1 S T	0.00			2034	876	-26.7	1.6	Ó	6	-1580.5	-141.1	27.7	-244.0	1.6
2ND	17.00	-54.3	1.4				1.7	0	3	-1526.2	-142.5	25.3	-217.6	1.3
3R D	34.00	-53.7	1.4	2034	876	-26.4			-5	-1472.5	-144.0	22.9	-192.1	1.1
4TH	54.00	-70.9	12.8	2743	1195	-25.9	10.7	-1	-3	-1401.5	-156.8	19.9	-163.4	1.5
STH	63.75	-58.7	-5.0	2303	1039	-25.5	-4.8	0	-	-1342.8	-151.8	18.4	-150.0	1.7
6TH	73.50	- 58 . 7	-6.4	2303	1038	-25.5	-6.1	0	-2	-1284.1	-145.5	16.9	-137.2	1.8
7TH	83.25	-58.0	-6.0	2303	1039	-25.2	-5.8	¢	-1	-1226.1	-139.4	15.5	-124.9	1.9
STH	93.00	- 57 . 3	-5.7	2303	1038	-24.9	-5.4	٥	-0	-1168.8	-133.8	14.2	-113.3	1.9
	102.75	- 56 . 6	~5.3	2303	1038	-24.6	-5.1	- 0	¢	-1112.2	-128.5	12.9	-102.1	1.9
9TH		- 56 . 1	-4.9	2303	1039	-24.3	-4.8	-0	1	-1056.2	-123.6	11.7	-91.6	1.8
1078	112.50	- 56 . 1	-4.6	2303	1038	-24.3	-4.4	-0	1	-1000.1	-119.0	10.5	-81.5	1.7
11TH	122.25	- 56 . 1	-4.3	2303	1038	-24.3	-4.1	- 0	2	-944.0	-114.7	9.4	-72.1	1.6
12TH	132.00	- 56 . 1	-3.9	2303	1038	-24.4	-3.8	- 0	2	-887.9	-110.8	8.3	-63.1	1.5
13TH	141.75	- 56 . 1	-3.6	2303	1038	-24.4	-3.5	- 0	2	-831.8	-107.2	7.2	-54.7	1.4
14TH	151.50	-58.1	-5.3	2303	1038	-25.2	-5.i	-0	3	-773.8	-101.9	6.2	-46.9	1.2
15TH	161.25	-63.1	-10.0	2303	1038	-27.4	-9.7	- 0	3			5.3	-39.7	1.1
16TH	171.00	-62.8	-9.4	2303	1039	-27.3	-9.1	-0	2	-710.7	-91.9			.9
17TH	180.75	-62.5	-8.8	2303	1038	-27.1	-8.5	-0	2	-647.9	~82.5	4.4	-33.1	
18TH	190.50	-62.3	-8.2	2303	1038	-27.0	-7.9	-0	1	-585.4	-73.7	3.6	-27.0	. 8
19TH	200.25		-7.6	2303	1038	-26.9	-7.3	-0	1	-523.1	-65.5	3.0	-21.6	. 7
20TH	210.00	-62.0				-27.0	-6.9	-0	1	-461.1	-57.9	2.4	-16.8	. 7
215T	219.75	-62.1	-7.2	2303	1038			-0	. 1	-399.0	-50.7	1.8	-12.7	. 6
22ND	229.50	-62.2	-6.8	2303	1038	-27.0	-6.6			-336.8	-43.9	1.4	-9.1	. 6
23RD	239.25	-62.3	-6.4	2303	1038	-27.0	-6.2	-0	0	-274.6	-37.4	1.0	-6.1	. 6
24TH	249.00	- 62 . 4	-6.0	2303	1039	-27.1	- 5 . 8	-0	¢	-212.2	-31.4	. 6	-3.7	. 5
	258.75	- 62 . 5	-5.7	2303	1038	-27.1	-5.5	- 0	0	-149.7	-25.7	. 4	-2.0	. 5
25TH	230.(3	-61.7	- 8.8	2303	1038	-26.8	-8.4	- 0	2					

TABLE WIND D	7 SHEAR IRECTION	AND MOMENT DIAGRA	NS : SAN Configuration a	DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TO	DWER IN	GUST FF	ACTOR 1.32	2
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT)	SHEAR X	(KIPS) Y	NOMENT (X	1000-FT-8 Y	(1P\$) Z
MECH	268.50	-89.0 -17.0	4252 1917	-20.7	- 9 9	-1 5	- 88 . 9	-17.0	. 2	8	. 4
TOP	286.50	-85.0 -17.0	7232 1916	-24.4			¢.¢	Q.Q	0 , 0	0.0	¢ .¢

	7 SHEAR IRECTION		IT DIAGR	AMS : Configur:	SI TION A	N DIEGO IN	TERCONT Refe	INENTAL Rence Pi	HO TEL Ressure	27.0 PSF	OVER IN	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT>	PRESSURE X	(PSF) Y	ECCEI	N (FT) Y	SHEAR X	(KIPS) Y	MONENT X	(1000-FT- Y	-KIPS) Z
1 S T	0.00	_	_					0	3	-1629.4	-51.2	12.0	-253.4	-14.1
2ND	17.00	-51.4	. 3	2034	876	-25.3	. 4			-1578.0	-51.5	11.1	-226.1	-14.3
3RD	34.00	-51.5	. 6	2034	876	-25.3	.7	٥ -	1	-1526.6	-52.1	10.2	-199.7	-14.3
4TH	54.00	-69.8	14.8	2743	1195	-25.5	12.3	- 3	-12	-1456.7	-66.8	9.0	-169.9	-13.4
STH	63.75	-61.5	-1.9	2303	1038	-26.7	-1.8	Ó	-12	-1395.2	-65.0	8.4	-156.0	-12.7
6TH	73.50	-61.3	-3.0	2303	1038	-26.6	-2.9	1	-12	-1333.9	-61.9	7.8	-142.7	-11.9
7TH	83.25	-60.4	-2.6	2303	1038	-26.2	-2.5	Ó	-11	-1273.5	-59.3	7.2	-129.9	-11.3
8TH	93.60	- 59 . 5	-2.2	2303	1039	-25.8	-2.2	¢	-11	-1214.0	-57.1	6.6	-117.8	-10.6
		- 58 . 6	-1.8	2303	1038	-25.5	-1.8	¢	-10	-1155.4	-55.2	6.1	-106.3	-10.0
9TH	102.75	- 59 . 0	-1.5	2303	1039	-25.2	-1.4	0	-10	-1097.4	-53.8	5.5	-95.3	-9.5
10TH	112.50	- 58 . 1	-1.2	2303	1039	-25.2	-1 .1	٥	- 9	-1039.4	-52.6	5.0	-84.9	-8.9
11TH	122.25	- 58 . 1	9	2303	1038	-25.2	9	٥	- 9	-981.2	-51.7	4.5	-75.0	-8.4
12TH	132.00	- 59 . 2	6	2303	1039	-25.3	6	0	- 9	-923.0	-51.1	4.0	-65.7	-7.9
13TH	141.75	- 58 . 3	3	2303	1038	-25 3	3	¢	- 8	-864.7	-50.8	3.5	-57.0	-7.4
14TH	151.50	- 59 . 9	-1.8	2303	1038	-26.0	-1.8	¢	- 8					-6.9
15TH	161.25	-64.3	-6.1	2303	1038	-27.9	-5.8	1	- 8	-804.8	-49.0	3.0	-48.9	
16TH	171.00	-64.5	-5.3	2303	1038	-28.0	-5.1	1	- 8	-740.5	-42.9	2.6	-41.4	-6.4
17TH	180.75	-64.8	-4.6	2303	1038	-28.1	-4.4	1	- 9	-676.0	-37.6	2.2	-34.4	-5.9
18TH	190.50	-65.0	-3.8	2303	1038	-28.2	-3.7	1	- 9	-611.2	-33.1	1.8	-28.2	-5.3
19TH	200.25	-65.3	-3.0	2303	1038	-28.3	-2.9	0	-9	-546.2	-29.3	1.5	-22.5	-4.7
20TH	210.00		-2.7	2303	1038	-28.3	-2.6	0	-9	-480.9	-26.2	1.3	-17.5	-4.1
215T	219.75	-65.2				-28.3	-2.2	ů ů	-9	-415.7	-23.6	1.0	-13.2	-3.5
22ND	229.50	-65.2	-2.3	2303	1038			-		-350.5	-21.3	. 8	-9.4	-2.8
2 3 R D	239.25	-65.1	-1.9	2303	1038	-28.3	-1.8	0	-10	-285.4	-19.4	. 6	-6.3	-2.2
24TH	249.00	-65.1	-1.5	2303	1038	-28.3	-1.5	0	-10	-220.3	-17.9	. 4	-3.9	-1.6
25TH	258.75	-65.0	-1.1	2303	1038	-28.2	-1.1	0	-10	-155.2	-16.7	. 2	-2.0	-1.0
		-64.1	-4.8	2303	1038	-27.8	-4.6	i	- 8					

TABLE Wind D	7 SHEAR IRECTION	AND MOMENT DIAGRA	NS : SAN Configuration a	DIEGO INT	REFE	LNENTAL HOTEL Rence pressure 2	EAST TO 27.0 PSF	GWER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	-91.1 -11.9	4252 1917	-21.4	-6.2	1 - 5	-91.1	-11.9	. 1	8	5
TOP	286.50	-91.1 -11.9	4232 1717	-21.4	-0.2	1 - 5	Q .Q	Q.Q	¢.¢	0 .0	0 .0

TABLE Wind D	7 SHEAR	AND MOMEN	T DIAGR	AMS : Configura	SAI TION A	N DIEGO IN	TERCONT REFE	INENTAL Rence Pr	HOTEL	EAST TO 27.0 PSF	OWER IN	GUST F	ACTOR 1.3	32
FLOOR	HEIGHT	F BR C E X	(KIPS) Y	AREA (X	SQ FT> Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	-KIPS) Z
15 T	0.00							•		-1542.2	63.4	-7.7	-239.6	-27.7
210	17.00	-46.1	-1.0	2034	876	-22.7	-1.2	-0	1	-1496.1	64.4	-6.6	-213.8	-27.7
3R D	34.00	- 47 . 6	7	2034	876	-23.4	8	0	-1	-1448.5	65.1	~5.5	-188.8	-27.7
4TH	54.00	-64.8	15.5	2743	1195	-23.6	13.0		-17	-1383.7	49.6	-4.4	-160.4	-26.5
STH	63.75	-57.i	1.7	2303	1038	-24.8	1.7		-21	-1326.6	47.9	-3.9	-147.2	-25.3
6TH	73.50	- 57.2	1.1	2303	1038	-24.8	1.1		-21	-1269.3	46.7	-3.4	-134.6	-24.1
7TH	83.25	-57.2	1.9	2303	1038	-24.8	1.8	- 1	-20	-1212.1	44.9	-3.0	-122.5	-23.0
		- 57.1	2.6	2303	1038	-24.8	2.5	-1	-20	-1155.0	42.3	-2.6	-110.9	-21.8
8TH	93.00	- 57 . 1	3.4	2303	1038	-24.8	3.2	- 1	-19	-1097.9	38.9	-2.2	-100.0	-20.7
9TH	102.75	-57.0	4.0	2303	1039	-24.7	3.8	- 1	-19	-1040.9	34.9	-1.8	-89.5	-19.6
10TH	112.50	- 56 . 8	4.3	2303	1039	-24.7	4.1	- 1	-19	-984.1	39.7	-1.5	-79.7	-18.5
11TH	122.25	- 56 . 6	4.6	2303	1038	-24.6	4.4	- 2	-19	-927.5	26.1	-1.2	-70.3	-17.5
1278	132.00	- 56 . 4	4.9	2303	1038	-24.5	4.7	- 2	-19	-871.0	21.2	-1.0	-61.6	-16.4
13TH	141.75	- 56 . 2	5.2	2303	1038	-24.4	5.0	- 2	-19		16.0	8	-53.4	-15.3
14TH	151.50	- 57.7	3.5	2303	1038	-25.1	3.4	- 1	-19	-814.8			-45.7	-14.2
15TH	161.25	-62.1	-1.2	2303	1038	-27.0	-1.1	٥	-19	-757.1	12.5	7		-13.0
16TH	171.00	-61.9	3	2303	1038	-26.9	3	Ó	-19	-695.0	13.7	5	-38.6	
17TH	180.75	-61.8	. 5	2303	1038	-26.8	. 5	- 0	-20	-633.0	14.0	4	-32.1	-11.9
1 8T H	190.50	-61.7	1.4	2303	1038	-26.8	1.4	- 0	-20	-571.2	13.4	3	-26.3	-10.6
19TH	200.25	-61.5	2.3	2303	1038	-26.7	2.2	- 1	-20	-509.5	12.0	1	-21.0	-9.4
20TH	210.00		2.5	2303	1038	-26.6	2.4	-1	-20	-448.0	9.8	0	-16.3	-8.2
21ST	219.75	-61.2				-26.4	2.7		-20	-386.8	7.2	. 1	-12.3	-7.0
2 2 N D	229.50	-60.9	2.8	2303	1039					-326.0	4.4	. 1	- 8.8	-5.8
23RD	239.25	- 60.5	3.1	2303	1038	-26.3	3.0		-19	-265.4	1.4	. 1	-5.9	-4.6
24TH	249.00	-60.2	3.3	2303	1038	-26.1	3.2		-19	-205.3	-2.0	. 1	-3.6	-3.4
25TH	258.75	- 59 . 8	3.6	2303	1038	-26.0	3.5		-19	-145.4	-5.6	. 1	-1.9	-2.3
		-59.6	1	2303	1038	-25.9	1	0	-17					

TABLE WIND D	7 SHEAR	AND MOMENT DIA	GRANS : SAN Configuration a	DIEGG IN	TERCONT REFE	INENTAL HOTEL - Rence pressure	- EAST TO 27.0 PSF	OVER IN	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE (KIPS X Y) AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	-85.8 -5.	4 4252 1917	-20.2	-2.8	1 -14	- 85 . 8	-5.4		8	
TOP	286.50	-53.0 -3.	7 7252 1711				¢ .¢	¢.¢	¢ ¢	¢.¢	¢.¢

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	IT DIAGR	ANS : Configura		N DIEGO IN	TERCONT REFE	INENTAL Rence pi	HOTEL Ressure	EAST T 27.0 PSF	OWER OUT	GUST F	FACTOR 1.3	32
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (SQ FT>	PRESSURE	(PSF)	ECCE	N (FT)	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	-KIPS) Z
1ST	0.00									-1260.8	173.2	-30.0	-194.7	-23.3
210	17.00	-41.7	-5.7	2034	876	-20.5	-6.5	¢	- 4	-1219.0	179.0	-27.0	-173.6	-23.3
		-40.4	-3.2	2034	876	-19.9	-3.7	- 0	2	-1178.6	182.2	-23.9	-153.2	-23.4
380	34.00	-60.0	. 4	2743	1195	-21.9	. 3	- ¢	-4	-1118.6	181.8	-20.3	-130.3	-23.2
4TH	54.00	-49.2	8.6	2303	1038	-21.3	8.3	- 3	-18	-1069.5	173.2	-19.6	-119.6	-22.3
5TH	63.75	-47.9	9.0	2303	1038	-29.8	8.7	-4	-19	-1021.5	164.2	-16.9	-109.4	-21.3
6TH	73.50	-46.8	8.6	2303	1038	-20.3	8.3	-4	-20	-974.7	155.6	-15.4	-99.7	-20.4
7TH	83.25	-45.7	8.2	2303	1038	-19.8	7.9	- 4	-20		147.4	-13.9	-90.4	-19.4
8T H	93.00	-44.6	7.9	2303	1038	-19.3	7.6	-4	-21	-929.0		-12.5	-81.5	-18.5
9T H	102.75	-43.9	7.5	2303	1038	-19.0	7.2	-4	-22	-984.5	139.5			-17.5
10TH	112.50	-44.3	7.3	2303	1038	-19.2	7.1	-4	-22	~840.6	132.0	-11.2	-73.1	
11TH	122.25		7.1	2303	1038	-19.4	6.9	-4	-22	-796.4	124.7	-9.9	-65.2	-16.5
12TH	132.00	-44.6			1038	-19.6	6.7	- 3	-22	-751.7	117.6	-8.7	-57.6	-15.4
13TH	141.75	-45:0	6.9	2303			6.5	- 3	-23	-706.7	110.7	-7.6	~50.5	-14.4
14TH	151.50	-45.4	6.7	2303	1038	-19.7				-661.2	103.9	-6.6	-43.8	-13.4
15TH	161.25	-46.1	7.4	2303	1038	-20.0	7.1	-4	-23	-615.2	96.6	-5.6	-37.6	-12.3
1678	171.00	- 47 . 3	9.3	2303	1038	-20.5	8.9	- 5	-23	-567.9	87.3	-4.7	-31.8	-11.1
	180.75	-47.9	8.9	2303	1038	-20.8	8.6	-4	-22	-520.0	78.4	-3.9	-26.5	-10.0
1778		- 48 . 6	8.5	2303	1038	-21 .1	8.2	-4	-21	-471.4	69.9	-3.2	-21.7	-9.0
1878	190.50	-49.2	8.1	2303	1038	-21.4	7.8	- 3	-20	-422.2	61.9	-2.5	-17.3	-8.0
19TH	200.25	-49.9	7.7	2303	1038	-21.7	7.4	- 3	-19	-372.3	54.2	-2.0	-13.5	-7.0
20TH	210.00	-50.3	7.6	2303	1038	-21.8	7.3	- 3	-18	-322.1	46.6	-1.5	-10.1	-6.1
21ST	219.75	-50.7	7.5	2303	1038	-22.4	7.2	- 3	-18	-271.4	39.2	-1.0	-7.2	-5.i
2 2 N D	229.50	-51.0	7.4	2303	1038	-22.2	7.1	- 3	-18			7	-4.8	-4.2
2 3 R D	239.25	-51.4	7.3	2303	1038	-22.3	7.0	- 3	-18	-220.4	31.8			-3.3
24TH	249.00	-51.8	7.2	2303	1038	-22.5	6.9	- 2	-18	-168.9	24.5	4	-2.9	
2 5 T H	258.75			2303	1038	-21.5	6.9	- 3	-19	-117.1	17.3	2	-1.5	-2.3
		-49.6	7.2	2000	1430	6. L · V		•	••					

TABLE WIND D	7 SNEAR IRECTION	AND NONE	NT DIAGR	ANS : SAN Configuration C	DIEGO IN	TERCONT : REFEI	INENTAL HOTEL - Rence pressure	- EAST TO 27.0 PSF	DVER OUT		ACTOR 1.3	
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	{1000-FT- Y	KIPS) Z
NECH	268.50	-67.5	10.1	4252 1917	-15.9	5.3	-3 -20	-67.5	10.1	1		-1.4
TOP	286.50	~\$ {.3	10.1	7646 1714				Q.Q	Q.Q	Q.Q	Q.Q	Q.Q

TABLE Wind D	7 SHEAR IRECTION	AND NOMEN	IT DIAGR	ANS : Configure	TION C	AN DIEGO IN	TERCONT Refe	INENTAL Pence Pi	HOTEL	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	32
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (X	SQ FT>	PRESSURE X	(PSF) Y	ECCEN	(FT) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	-KIPS) Z
1 S T	0.00			• • • • ·			= 0		3	-1151.1	265.2	-46.5	-177.3	-32.6
2ND	17.00	- 42 . 4	-5.0	2034	876	-20.8	-5.8	-0		-1108.7	270.2	-41.9	-158.1	-32.7
3RD	34.00	-42.8	-3.i	2034	876	-21.1	-3.6	-0	2	-1065.8	273.3	- 37 . 3	-139.6	-32.8
4TH	54.00	-55.7	1.2	2743	1195	-20.3	1.0	-0	~5	-1010.1	272.1	-31.8	-118.9	-32.5
578	63.75	-42.1	11.0	2303	1038	-18.3	10.6	- 7	-26	-968.1	261.1	- 29 . 2	-109.2	-31.3
6TH	73.50	-41.4	11.2	2303	1038	-18.0	10.8	- 7	-27	-926.7	249.9	-26.8	-100.0	-30.1
7TH	83.25	-40 4	10.9	2303	1038	-17.5	10.5	- 7	-28	-886.3	239.0	-24.4	-91.1	-28.9
8TH	93.00	- 39 . 4	10.5	2303	1038	-17.1	10.1	- 8	-29	-846.9	228.5	-22.1	-82.7	-27.7
9TH	102.75	- 38 . 5	10.2	2303	1038	-16.7	9.8	- 8	-30	-808.4	218.4	-19.9	-74.6	-26.5
1078	112.50	- 39 . 0	10.0	2303	1038	-16.5	9.6	- 8	-31	-770.4	208.4	-17.8	-66.9	-25.2
11TH	122.25	-39.0	10.3	2303	1039	-16.9	9.9	- 8	-31	-731.4	198.1	-15.8	-59.6	-23.9
1278	132.00	- 39 . 9	10.6	2303	1038	-17.3	10.2	- 8	-31	-691.5	187.5	-14.0	-52.7	-22.6
	141.75	- 40 . 9	10.9	2303	1039	-17.8	10.5	- 8	-31	-650.6	176.7	-12.2	-46.1	-21.2
13TH	151.50	-41.9	11.2	2303	1038	-18.2	10.7	- 8	-31	-608.7	165.5	-10.5	-49.0	-19.8
14TH		-42.9	12.2	2303	1038	-18.6	11.7	- 9	-32	-565.8	153.3	-9.0	-34.3	-18.4
15TH	161.25	-44.1	14.0	2303	1038	-19.1	13.5	-10	-33	-521.7	139.4	-7.5	-29.0	-16.8
1678	171.00	-44.8	13.6	2303	1038	-19.4	13.1	-10	-32	-476.9	125.8	-6.2	-24.1	-15.2
1778	180.75	- 45.5	13.2	2303	1039	-19.7	12.7	- 9	-31	-431.4	112.6	-5.1	-19.7	-13.6
1878	190.50	-46.2	12.8	2303	1039	-20.0	12.3	- 8	-30	-385.3	99.8	-4.1	-15.7	-12.1
19TH	200.25	-46.8	12.4	2303	1038	-20.3	12.0	- 8	-30	-338.4	87.4	-3.1	-12.2	-10.6
20TH	210.00	-46.8	i2.3	2303	1039	-20.3	11.8	- 8	-29		75.1	-2.3	-9.1	-9.2
21ST	219.75	-46.7	12.1	2303	1038	-20.3	11.7	- 8	-29	-291.6			-6.5	-7.7
2 2 N D	229.50	-46.7	12.0	2303	1038	-20.3	11.5	- 7	-29	-244.9	62.9	-1.7		-6.3
2 3 R D	239.25	-46.6	11.8	2303	1038	-20.2	11.4	- 7	-29	-198.2	51.0	-1.1	-4.3	
2 4 T H	249.00	-46.6	11.7	2303	1038	-20.2	11.3	- 7	-28	-151.6	39.1	7	-2.6	-4.9
25TH	258.75	- 44 5	11.4	2303	1038	-19.3	11.0	- 8	-29	-105.1	27.4	4	-1.4	-3.5

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	IT DIAGRI	AMS : Configuratio	N C SAN	DIEGO IN	TERCONT REFE	INENTAL HOTEL	EAST TI	DVER OUT	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ X		PRESSURE		ECCEN (FT) X Y	SHEAR X	(KIPS) Y	N DN E N T X	(1000-FT- Y	KIPS) Z
MECH	268.50	-60.6	16.0	4252 19	17	-14.3	8.4	-8 -32	- 60 . 6	16.0	1	5	-2.1
TOP	286.50	- 60.8	18.9	7232 17	74	-14.3	O. 1	-0 -32	Q.Q	Q.Q	0.0	¢.¢	Q.Q

TABLE WIND D	7 SHEAR	AND NOME	NT DIAGR	ANS : Configur	ATION C	AN DIEGO IN	TERCONT REFEI	INENTAL Rence p	HOTEL	EAST TO 27.0 PSF	WER OUT	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCE X	N (FT) Y	SHEAR X	(KIPS) Y	NOHENT X	(1000-FT) Y	-KIPS) Z
1 S T	0.00							ò	- 1	-912.5	281.1	-50 0	-139.5	-37.6
2ND	17.00	- 39 . 1	-6.7	2034	876	-19.2	-7.6			-873.4	287.7	-45.2	-124.3	-37.5
3RD	34.00	-40.4	-4.9	2034	876	-19.8	~5.6	0	- 2	-833.0	292.6	-40.3	-109.8	-37.4
4TH	54.00	-50.2	3	2743	1195	-18.3	2	0	-10	-782.8	292.9	-34.4	-93.6	-36.9
5TH	63.75	-31.4	10.7	2303	1038	-13.6	10.3	-13	-38	-751.5	282.2	-31.6	-86.2	-35.6
6T H	73.50	- 30 . 2	11.2	2303	1038	-13.1	10.8	-15	-40	-721.3	270.9	-28.9	-79.0	-34.2
711	83.25	-29.7	11.2	2303	1039	-12.9	10.8	-16	-41	-691.6	259.7	- 26 . 3	-72.1	-32.8
ETH	93.00	- 29.3	11.3	2303	1038	-12.7	10.9	-16	-43	-662.3	248.4	-23.8	-65.5	-31.4
9TH	102.75	- 29 . 8	11.3	2303	1038	-i2.5	10.9	-17	-44	-633.5	237.1	-21.5	-59.2	-29.9
		- 29 . 8	11.4	2303	1038	-12.5	11.0	-18	-45	-604.7	225.7	-19.2	-53.1	-28.4
1078	112.50	-29.8	11.7	2303	1038	-12.9	11.2	-17	-44	-574.9	214.1	-17.1	-47.4	-26.9
11TH	122.25	- 30 . 8	11.9	2303	1038	-13.4	11.5	-17	-43	-544.1	202.2	-15.1	-41.9	-25.4
12TH	132.00	- 31 . 8	12.2	2303	1038	-13.8	11.7	-16	-43		190.0	-13.1	-36.8	-23.8
1 3 T H	141.75	- 32 . 8	12.4	2303	1038	-14.3	12.0	-16	-42	-512.3			-31.9	-22.3
14TH	151.50	- 33 . 4	13.1	2303	1038	-14.5	12.6	-17	-42	-479.4	177.5	-11.3		-20.6
15TH	161.25	-33.0	14.2	2303	1038	-14.3	13.7	-19	-44	-446.1	164.4	-9.7	-27.4	
16TH	171.00	- 33 . 8	14.0	2303	1038	-14.7	13.5	-18	-43	-413.0	150.2	-8.1	-23.2	-18.9
17TH	180.75	- 34 . 6	13.8	2303		-15.0	13.3	-17	-42	-379.2	136.2	-6.8	-19.4	-17.2
18TH	190.50	- 35 . 4	13.6	2303		~15.4	13.1	-15	-41	-344.6	122.4	-5.5	-15.9	-15.5
19TH	200.25	-36.2	13.5	2303	1038	-15.7	13.0	-15	-40	~309.3	198.7	-4.4	-12.7	-13.9
2 ¢ T H	210.00			2303		-15.9	12.9	-14	-40	-273.1	95.2	-3.4	-9.8	-12.2
21ST	219.75	-36.7	13.4						-39	-236.4	81.8	-2.5	-7.3	-10.6
2 2 N D	229.50	- 37 . 3	13.4	2303		-16.2	12.9	-14		-199.1	68.4	-1.8	-5.2	-8.9
2 3 R D	239.25	- 37 . 9	13.4	2303	1038	-16.4	12.9	-14	-39	-161.2	55.0	-1.2	-3.5	-7.3
24TH	249.00	- 38 . 4	13.3	2303	1038	-16.7	12.8	-13	-38	-122.8	41.7	7	-2.1	-5.6
25TH	258.75	- 39 . 0	i3.3	2303	1038	-16.9	12.8	-13	-38	- 83 . 8	28.4	4	-1.1	-4.¢
****		- 35 . 9	12.5	2303	1038	-15.6	12.1	-14	-39					

TABLE WIND D	7 SHEAR IRECTION	AND NONES	IT DIAGR	ANS : Configura	TION C	DIEGO IN	TERCONT : Refei	INENTAL HOTEL Rence pressure :	EAST TO 27.0 PSF	DWER OUT	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE		ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NONENT X	<1000-FT- Y	KIPS) Z
MECH	268.50		1	4252	1917	-11.3	8.3	-15 -45	-48.0	15.9	1	4	-2.4
TOP	286.50	-48.0	15.9	4232	1211		0.3	-17 -47	Q.Q	Q.Q	¢,¢	9.Q	Q.Q

TABLE Vind D	7 SHEAR IRECTION	AND HOMEN	T DIAGR	ANS : Configure	SAI	N DIEGO IN	TERCONT REFE	INENTAL Rence Pr	HOTEL	EAST T 27.0 PSF	OVER OUT	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT> Y	P RESSURE X	(PSF) Y	ECCEN	I (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT) Y	-KIPS) Z
1 S T	0.00					4.0.0				-792.0	264.7	- 47.6	-119.4	-48.6
2ND	17.00	-39.i	-8.5	2034	876	-19.2	-9.7	1	-4	-752.9	273.2	-43.0	-106.2	-48.4
3RD	34.00	- 40 . 3	-6.9	2034	876	-19.8	-7.9	1	-6	-712.7	280.1	-38.3	-93.8	-48.2
4TH	54.00	- 48 . 4	-2.4	2743	1195	-17.6	-2.0	1	-17	-664.3	282.5	-32.7	-80.0	-47.4
STH	63.75	-24.7	10.7	2303	1038	-10.7	10.3		-51	-639.5	271.8	-30.0	-73.7	-45.9
GTH	73.50	-23.9	11.2	2303	1038	-10.4	10.8	-25	-52	-615.6	260.6	-27.4	-67.5	-44.3
718	83.25	-23.8	11.1	2303	1038	-10.3	10.7	-26	-55	~591.8	249.4	-24.9	-61.6	-42.8
8T H	93.00	-23.8	11.1	2303	1038	-10.3	10.7	-26	-57	-568.1	238.4	-22.5	-56.0	-41.1
9T H	102.75	-23.7	11.0	2303	1039	-10.3	10.5	-27	-59	-544.4	227.4	- 20 . 2	-50.6	- 39.4
		-23.9	11.0	2303	1038	-10.4	10.6	-28	-61	-520.4	216.3	-18.1	-45.4	- 37.7
10TH	112.50	- 25 . 1	11.2	2303	1038	-10.9	10.8	-27	-61	-495.3	205.1	-16.0	-40.4	-35.8
11TH	122.25	- 26 . 3	11.5	2303	1038	-11.4	11.1	-27	-61					-33.9
12TH	132.00	-27.5	11.7	2303	1038	-12.0	11.3	-26	-61	-468.9	193.6	-14.1	-35.7	
1 3 T H	141.75	-28.7	11.9	2303	1038	-12.5	11.5	-26	-62	-441.4	181.9	-12.3	-31.3	-31.9
14TH	151.50	-29.1	12.8	2303	1038	-12.6	12.3	-27	-62	-412.7	170.0	-10.5	-27.1	-29.8
15TH	161.25	-28.1	14.3	2303	1038	-12.2	13.7	-32	-63	-383.6	157.2	-8.9	-23.2	-27.7
16TH	171.00	- 29.2	14.1	2303	1038	-12.7	13.6		-62	-355.5	142.9	-7.5	-19.6	-25.4
17TH	180.75	-30.3	13.9	2303	1038	-13.2	13.4		-61	-326.2	128.9	-6.2	-16.3	-23.2
18TH	190.50					-13.6	13.2		-50	-295.9	115.0	-5.0	-13.3	-21.0
19TH	200.25	-31.4	13.7	2303	1038					-264.5	101.3	-3.9	-10.6	-18.7
2 Q T H	210.00	- 32 . 5	13.5	2303	1038	-14.1	13.0		-59	-231.9	87.8	-3.0	- 8.1	-16.5
21ST	219.75	- 32 . 7	13.2	2303	1038	-14.2	12.8		-59	-199.2	74.6	-2.2	-6.0	-14.2
2 2 N D	229.50	- 32 . 9	13.0	2303	1038	-14.3	12.5	-23		-166.3	61.6	-1.5	-4.2	-12.0
2380	239.25	-33.1	12.8	2303	1038	-14.4	12.3		-59	-133.3	48.8	-1.0	-2.8	-9.8
2411	249.00	-33.2	12.5	2303	1038	-14.4	12.0	-22	-58	-100.1	36.3	6	-1.6	-7.5
25TH	258.75	-33.4	12.3	2303	1038	~14.5	11.8	-21	-5B	-66.7	24.0	- 3	8	-5.3
2010	200.00	- 29 . 8	11.6	2303	1038	-12.9	11.2	-24	-62					

TABLE Wind D		AND MONEI 30	NT DIAGR	AMS : Configuration	SAN C	I DIEGG IN	TERCONT Refe	INENTAL HOTE Rence pressu	L EAST T Re 27.0 PSF	GVER OUT	GUST	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ I X Y	7 7) 7	PRESSURE	(PSF) Y	ECCEN (FT X Y) SHEAR X	(KIPS) Y	NOMENT X	{1000-FT- Y	KIPS) Z
MECH	268.50	-36.8		4050 404	-				-36.8	12.4	1	3	-3.2
TOP	286.50	- 39.8	12.4	4252 191	. 7	-8.7	£.5	-26 -78	Ģ.Ģ	¢.¢	0.0	Ç.Ç	Q.Q

	7 SHEAR	AND MONEL	NT DIAGR	AMS : Configurí	STION C	AN DIEGO II	NTERCONT : Refei	INENTAL Rence f	HOTEL Pressure	- EAST TO 27 0 PSF	WER OUT	GUST F	ACTOR 1.3	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT)	PRESSURI	E (PSF) Y	ECCE	EN (FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00	/			876	-18.7	-11.5	2	-6	-645.4	160.8	-29.2	-94.6	-54.7
2ND	17.00	-38.1	-10.1	2034					-10	-697.3	170.9	-26.3	-83.9	-54.5
3R D	34.00	-40.8	- 8.8	2034	876	-20.1	-10.0	2	-	-566.4	179.7	-23.4	-73.9	-54.0
4 T H	54.00	- 48 . 0	-4.1	2743	1195	-17.5	-3.4	2	-19	-518.5	183.8	-19.7	-63.1	-53.1
5T H	63.75	-17.4	9.2	2303	1038	-7.6	8.9	-37	-69	-501.1	174.6	-18.0	-58.1	-51.6
6TH	73.50	-16.5	9.5	2303	1038	-7.2	9.1	-42	-74	-484.6	165.1	-16.3	-53.3	-49.9
7TH	83.25	-17.3	9.1	2303	1038	-7.5	8.8	-41	-77	-467.3	156.0	-14.8	-48.7	-48.2
8TH	93.00	-18.0	8.8	2303	1038	-7.8	8.4	-39	-81	-449.3	147.3	-13.3	-44.2	-46.4
97 H	102.75	-19.7	8.4	2303	1038	- 8.1	8.1	-37	-94	-430.5	138.8	-11.9	-39.9	-44.6
		- 19 . 5	8.1	2303	1038	~8.5	7.8	-36	-86	-411.0	130.7	-10.6	-35.8	-42.6
10TH	112.50	-20.5	7.9	2303	1038	-8.9	7.6	-34	-87	-390.5	122.8	-9.3	-31.9	-40.5
11TH	122.25	-21.4	7.7	2303	1038	-9.3	7.4	-32	-88	-369.1	115.1	-8.2	-28.2	-38.4
12TH	132.00	- 22 . 4	7.5	2303	1038	-9.7	7.3	-30	-89	-346.8	107.6	-7.1	-24.7	-36.2
13TH		-23.3	7.3	2303	1038	-10.1	7.i	-28	-90	-323.4	100.2	-6.1	-21.4	-33.9
14TH		- 22 . 9	7.7	2303	1038	-9.9	7.4	-32	-95		92.5	-5.1	-18.4	-31.4
1 5 T H	161.25	-20.4	8.9	2303	1038	-8.9	8.6	-45	-103	-300.6	83.6	-4.3	-15.6	-28.9
16TH	171.00	-21.8	8.6	2303	1038	-9.5	8.3	-40	-100	-280.2				-26.4
17TH	180.75	-23.1	8.3	2303	1038	-10.0	8.0	-35	-97	-258.4	75.0	-3.5	-12.9	-23.9
1 8 T H	190.50	-24.5	8.1	2303	1038	-10.6	7.8	-31	-94	-235.3	66.6	-2.8	-10.5	
1 9 T H	200.25	-25.9	7.8	2303	1038	-11.2	7.5	-27	-91	-210.8	58.6	-2.2	-8.4	-21.3
20TH	210.00	-26.1	7.7	2303	1038	-11.3	7.5	-27	-90	-184.9	50.8	-1.7	-6.4	-18.8
21ST	219.75		7.7	2303	1038	-11.5	7.4	-26	-89	-158.8	43.1	-1.2	-4.8	-16.2
2 2 N D	229.50	-26.4			1038	-11.6	7.4	-25	-88	-132.4	35.4	- 8	-3.3	-13.7
2 3 R D	239.25	-26.6	7.7	2303	-			-25	-87	~105.8	27.7	5	-2.2	-11.1
24TH	249.00	-26.9	7.6	2303	1038	-11.7	7.4			-78.9	20.1	3	-1.3	- 8.6
25TH	258.75	- 27 . 2	7.6	2303	1038	-11.8	7.3	-24	-86	-51.7	12.5	1	6	-6.1
		-23.9	6.9	2303	1038	-10.4	6.7	-27	-94					

TABLE Wind D	7 SHEAR IRECTION	AND NONEL 40	IT DIAGRA	ANS : SAN Configuration C	DIEGO IN		INENTAL HOTEL - Rence pressure		OWER OUT	GUST I	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE		ECCEN (FT)	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
NECH	268.50	-27.8	5.6	4252 1917	-6.5	2.9	-25 -125	- 27 . 8	5.6	0	2	-3.6
TOP	286.50	-21.6	3.6	4232 1717	-6.3	2.7	-23 -123	0.0	0.0	0.0	ð. Ó	0.0

WIND D	IRECTION	50	•	CONFIGURA				ENCE PRESSURE					
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (X	SQ FT>	PRESSURE	E (PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	MONENT	(1000-FT- Y	-KIPS) Z
1 S T	0.00		•			. – –			-506.2	94.0	-20.1	-68.3	-51.9
210	17.00	-36.3	-11.8	2034	876	-17.8	-13.4	4 -11	-469.9	105.8	-18.4	-60.0	-51.4
3RD	34.00	-42.0	-10.3	2034	875	-20.7	-11.8	3 -14	-427.9	116.1	-16.5	-52.4	-50.8
4TH	54.00	-52.2	-6.8	2743	1195	-19.0	-5.7	3 -22	-375.7	123.0	-14.1	-44.3	-49.6
		-14.5	6.1	2303	1038	-6.3	5.9	-37 -88	-361.2	116.8	-12.9	-40.7	-48.1
5TH	63.75	-13.5	6.1	2303	1038	-5.8	5.8	-43 -96	-347.7	110.8	-11.8	-37.3	-46.6
6TH	73.50	-14.2	5.7	2303	1038	-6.2	5.5	-40 -101	-333 5	105.1	-10.7	-33.9	-44.9
7TH	83.25	-14.9	5.3	2303	1038	-6.5	5.1	-37 -104	-318.6	99.8	-9.8	-30.8	-43.2
8T H	93.00	-15.6	4.9	2303	1038	-6.8	4.8	-34 -108	-303.0	94.8	-8.8	-27.7	-41.3
9T H	102.75	-16.2	4.7	2303	1038	-7.0	4.5	-32 -111	-286.8	90.2	-7.9	-24.9	-39.4
1 Q T H	112.50	-16.2	4.7	2303	1038	-7.0	4.5	-33 -114	-270.6	85.5	-7.0	-22.1	- 37.4
11TH	122.25	-16.2	4.7	2303	1038	-7.0	4.5	-34 -118	-254.5	80.8	-6.2	-19.6	-35.3
12TH	132.00	-16.2	4.7	2303	1038	-7.0	4.6	-36 -121		76.0	-5.5	-17.2	-33.2
13TH	141.75	-16.2	4.8	2303	1038	-7.0	4.6	-37 -125	-238.3			-14.9	-31.0
14TH	151.50	-15.3	4.7	2303	1038	-6.7	4.5	-41 -135	-222.1	71.2	-4.8		-28.7
15TH	161.25	-13.7	4.5	2303	1038	-5.9	4.4	-50 -152	-206.8	66.6	-4.1	-12.8	
16TH	171.00	-14.6	4.8	2303	1038	-6.3	4.6	-47 -143	-193.1	62.0	-3.5	-10.9	-26.4
17TH	180.75	-15.6	5.1	2303	1038	-6.8	4.9	-44 -136	-178.5	57.3	-2.9	-9.1	-24.1
18TH	190.50	-16.5	5.3	2303	1038	-7.2	5.1	-42 -129	-162.9	52.2	-2.3	-7.4	-21.8
19TH	200.25			2303	1038	-7.6	5.4	-39 -123	-146.4	46.9	-1.9	-5.9	-19.4
20TH	210.00	-17.4	5.6			-7.7	5.5	-39 -120	-129.0	41.3	-1.4	-4.6	-17.0
2 1 S T	219.75	-17.7	5.7	2303	1038			-39 -117	-111.3	35.6	-1.¢	-3.4	-14.7
2 2 N D	229.50	-17.9	5.9	2303	1038	-7.8	5.7		-93.4	29.7	7	-2.4	-12.4
2 3 R D	239.25	-18.2	6.0	2303	1038	-7.9	5.8	-38 -115	-75.2	23.7	~ . 5	-1.6	-10.1
2478	249.00	-18 5	6.2	2303	1038	-8.0	5.9	-37 -112	-56.7	17.5	~ 3	9	-7.8
25TH	258.75	-18.7	6.3	2303	1038	-8.1	6.1	-37 -110	- 38 0	11.2	1	5	-5.5
LUIN	200.00	-17.2	5.8	2303	1038	-7.5	5.6	-39 -116					

TABLE Vind D		AND NOMES	T DIAGR	ANS : Configur:		OIEGO IN		INENTAL HOTEL - Rence pressure			GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y		(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	-20.9	5.4	4252	1917	-4.9	2.8	70 147	-20.9	5.4	¢	2	-3.2
TOP	286.50	-20.7	J.4	4232	171(-4.7	2.6	-38 -146	Q.Q	Q.Q	Q.Q	2.0	Q.Q

TABLE	7 SHEAR IRECTION	AND NOMEN	T DIAGRA	MS : Configura	SI TION C	N DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	32
FLOOR	HEIGHT		(KIPS)	AREA (PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT : X	(1090-FT- Y	-KIPS) Z
1 Ş T	0,00								-308.1	110.9	-23.5	-35.8	-35.9
210	17.00	-29.3	-8.0	2034	876	-14.4	-9.1	2 - 9	-278.8	118.9	-21 5	-30.8	-35.6
		- 39 . 0	-8.1	2034	876	-18.7	-9.2	3 -13	-240.8	127.0	-19.4	-26.4	-35.1
3RD	34.00	- 46 . 4	-5.3	2743	1195	-16.9	-4.4	2 -20	-194.3	132.3	-16.8	-22.1	-34.1
4TH	54.00	-8.6	4.7	2303	1038	-3.7	4.5	-56 -103	-185.7	127.6	-15.6	-20.2	-33.0
5T H	63.75	-7.6	4.6	2303	1038	-3.3	4.5	-69 -114	-178.1	123.0	-14.4	-18.4	-31.8
6 T H	73.50	-8.0	4.6	2303	1038	-3.5	4.4	-67 -117	-170.1	118.4	-13.2	-16.7	-30.5
7TH	83.25	-8.4	4.6	2303	1038	-3.6	4.4	-65 -120	-161.7	113.8	-12.0	-15.1	-29.2
8T H	93.00	-9.8	4.5	2303	1038	-3.8	4.3	-53 -123		109.3	-11.0	-13.6	-27.9
9T H	102.75	-9.1	4.5	2303	1038	-3.9	4.4	-63 -126	-152.9		-9.9	-12.1	-26.4
1 ¢ T H	112.50	-9.0	4.7	2303	1038	-3.9	4.5	-67 -127	-143.9	104.8			-25.0
11TH	122.25	-8.9	4.9	2303	1038	-3.8	4.7	-71 -128	-134.9	100.0	-8.9	-10.8	-23.5
12TH	132.00	-8.8	5.1	2303	1038	-3.8	4.9	-74 -129	-126.0	95.2	-8.0	-9.5	
13TH	141.75		5.2	2303	1038	-3.8	5.i	-78 -130	-117.3	90.1	-7.1	- 8.3	-22.0
14TH	151.50	-8.7			1038	-3.3	4.5	-90 -147	-108.6	84.8	-6.2	-7.2	-20.5
15TH	161.25	-7.7	4.7	2303			4.J 3.2	-115 -200	-100.9	8¢.1	-5.4	-6.2	-18.9
16TH	171.00	-5.8	3.4	2303	1038	-2.5			- 95 . 1	76.8	-4.6	-5.2	-17.4
1778	180.75	-6.6	4.2	2303	1038	-2.9	4.0	-107 -169	- 88 . 5	72.6	-3.9	-4.3	-15.8
1878	190.50	-7.3	5.0	2303	1038	-3.2	4.8	-100 -146	-81 2	67.6	-3.2	-3.5	-14.2
1978	200.25	-8.1	5.8	2303	1038	-3.5	5.6	-93 -129	-73.1	61.8	-2.6	- 2 . 8	-12.7
-		-8.8	6.6	2303	1038	-3.8	6.4	-86 -115	-64.3	55.2	-2.0	-2.1	-11.1
2 ¢ T H	210.00	-9.2	6.9	2303	1038	-4.0	6.7	-81 -109	-55.1	48.3	-1.5	-1.5	-9.5
2157	219.75	-9.7	7.2	2303	1038	-4.2	6.9	-77 -103	-45.4	41.1	-1.1	-1.0	-7.9
2 2 N D	229.50	-10.1	7.5	2303	1038	-4.4	7.2	-73 -98	-35.3	33.6	7	6	-6.4
2 3 R D	239.25	-10.5	7.8	2303	1038	-4.6	7.5	-69 -93	-24.8	25.8	- 4	- 3	-4.9
24TH	249.00	-10.9	8.1	2303	1038	-4.8	7.8	-65 -89		17.7	- 2	1	-3.4
25TH	258.75	-7.9	7.9	2303	1038	-3.4	7.6	-86 -86	-13.8	L (. (. 2		

TABLE Wind D		AND NONEI 60	AT DIAGR	ANS ; Configura		N DIEGO IN	TERCONT Refe	INENTAL HOTEL - Rence pressure	- EAST TO 27.0 PSF	WER OUT	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	-5.9	9.8	4252	1917	-1.4	4 1	-152 -92	-5.9	9.8	1	1	-2.0
TOP	286.50	-3.7	7.6	4232	1214	-1.4	4 .1		0.0	0.0	0.0	9.0	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND MONEI	T DIAGR	ANS : Configura	TION C	AN DIEGO IN	TERCONT Refe	INENTAL Rence P	HOTEL	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT (X	1000-FT- Y	KIPS) Z
1 S T	0.00									-130.4	127.6	-24.5	-7.4	-13.0
2ND	17.00	-25.8	-2.8	2034	876	-12.7	-3.2	0	-4	-104.7	130.4	- 22 . 3	-5.4	-12.9
380	34.00	- 33 . 9	-3.2	2034	876	-16.7	-3.6	1	- 7	-70.7	133.5	-20.1	-3.9	-12.6
4TH	54.00	- 36 . 6	8	2743	1195	-13.3	7	¢	-12	-34.1	134.4	-17.4	-2.8	-12.2
	63.75	-2.3	3.5	2303	1038	-1.0	3.4	-121	-78	-31.8	130.8	-16.1	-2.5	-11.6
5TH		-1.7	3.6	2303	1038	8	3.5	-134	-64	-30.1	127.2	-14.9	-2.2	-11.0
6TH	73.50	-2.3	4.1	2303	1038	-1.0	3.9	-114	-64	-27.8	123.2	-13.7	-1.9	-10.4
7TH	83.25	-2.8	4.5	2303	1038	-1.2	4.3	-99	-62	-25.0	118.7	-12.5	-1.7	-9.7
8T H	93.00	-3.4	5.0	2303	1038	- i . 5	4.8	-87	-60	-21.6	113.7	-11.3	-1.4	-9.1
9TH	102.75	-3.6	5.3	2303	1038	-1.6	5.i	-82	-57	-17.9	108.4	-10.3	-1.2	-8.5
1 O T H	112.50	-3.1	5.3	2303	1038	-1.3	5.1	-89	-51			-9.2	-1.1	-7.8
11TH	122.25	-2.5	5.3	2303	1038	- i . i	5.1	-94	-44	-14.9	103.1		9	-7.2
12TH	132.00	-1.9	5.4	2303	1038	8	5.2	-99	-36	-12.4	97.8	-8.2		
13TH	141.75	-1.4	5.4	2303	1038	6	5.2	-103	-26	-10.4	92.4	-7.3	8	-6.6
14TH	151.50	2	4.6	2303	1038	i	4.4	-114	- 6	-9.1	87.0	-6.4	7	-6.0
15TH	161.25		3.1	2303	1038	. 5	3.0	-117	43	-8.8	82.4	-5.6	7	-5.5
16TH	171.00	1.1		2303	1038	. 3	3.9	-106	16	-10.0	79.3	-4.8	6	-5.1
17TH	180.75	. 6	4.0				4.8	-93	2	-10.6	75.3	-4.1	~.5	-4.7
18TH	190.50	. 1	4.9	2303	1039	. 0		-83	- 6	-10.7	70.4	-3.4	4	-4.2
19TH	200.25	4	5.9	2303	1038	2	5.7			-10.3	64.5	-2.7	3	-3.7
20TH	210.00	- 9	6.8	2303	1038	4	6.6	-74	-10	-9.3	57.7	-2.1	~ . 2	-3.2
21ST	219.75	-1.4	7.2	2303	1038	b	6.9	-68	-13	-7.9	50.5	-1.6	1	-2.7
22ND	229.50	-1.9	7.5	2303	1038	8	7.2	-62	-16	-6.0	43.0	-1.1	~.¢	-2.2
22RD 23RD	229.30	-2.4	7.9	2303	1038	-1.0	7.6	-56	-17	-3.7	35.1	7	. 0	-1.7
		-2.9	8.2	2303	1038	-1.2	7.9	-51	-18	8	26.9	4	. 1	-1.3
24TH	249.00	-3.3	8.6	2303	1038	-1.5	8.3	-47	-18	2.5	18.3	2	. 1	8
25TH	258.75	4	8.3	2303	1038	2	8.0	-40	- 2	2.0				

TABLE WIND D	7 SHEAR IRECTION	AND NOMEN	NT DIAGR	AMS : Configur:		I DIEGO IN	TERCONT Refei	INENTAL Rence pr	HOTEL - Essure	- EAST T 27.0 PSF	OWER OUT	GUST I	FACTOR 1.3	12
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA : X	(SQ FT) Y	PRESSURE X		ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NDNENT X	(1000-FT- Y	KIPS) Z
HECH	268.50		14.4	4959	1917	7	5.2	-42	12	2.9	10.0	1	. 0	5
TOP	286.50	2.9	10.0	4232	1717	. (J. 2		• -	¢.¢	Q.Q	Q.Q	Q .Q	0.0

TABLE Wind D	7 SHEAR IRECTION	AND MOME	NT DIAGR	ANS : Configur:	ATION C	AN DIEGO IN	TERCONT Refe	INENTAL Rence p	HOTEL - Ressure	- EAST TO 27.0 PSF	DWER OUT	GUST FI	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS)	AREA X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT : X	1000-FT- Y	KIPS) Z
1 S T	0.00	_						-		15.5	164.4	-27.6	12.9	13.0
210	17.00	-20.2	5.5	2034	876	-9.9	6.3	3	11	35.7	158.9	-24.8	12.5	12.7
3RD	34.00	-24.9	3.8	2034	876	-12.2	4.3	1	6	60.6	155.1	- 22 . 1	11.7	12.6
4TH	54.00	- 26 . 2	5.3	2743	1195	-9.5	4.4	2	9	86.8	149.8	-19.1	10.2	12.3
578	63.75	3.8	3.2	2303	1038	1.6	3.1	13	-15	83.0	146.6	-17.7	9.4	12.2
6TH	73.50	4.1	3.3	2303	1038	1.8	3.2	20	-24	78.9	143.3	-16.2	8.6	12.1
		3.9	4.2	2303	1038	1.7	4.1	25	-24	75.0	139.1	-14.9	7.8	11.9
7TH	83.25	3.7	5.2	2303	1038	1.6	5.0	30	-22	71.3	133.9	-13.5	7.1	11.6
8TH	93.00	3.6	6.1	2303	1038	i.5	5.9	33	-19	67.7	127.8	-12.3	6.4	11.4
9T H	102.75	3.4	6.7	2303	1038	1.5	6.5	36	-18	64.3	121.1	-11.0	5.8	11.1
1 ¢ T H	112.50	3.2	6.7	2303	1038	1.4	6.4	43	-20	61.2	114.4	-9.9	5.2	10.7
11TH	122.25	2.9	6.6	2303	1038	1.3	6.3	50	-22	58.2	107.9	-8.8	4.6	10.3
12TH	132.00	2.7	6.5	2303	1038	i.2	6.2	58	-24	55.5	101.4	-7.8	4.Q	9.9
1.3TH	141.75	2.5	6.4	2303	1038	1.1	6.2	66	-26	53.0	95.0	-6.8	3.5	9.4
14TH	151.50	3.1	5.7	2303	1038	1.4	5.5	80	-44			-5.9	3.0	8.8
15TH	161.25	5.0	4.4	2303	1038	2.2	4.3	76	-86	49.9	89.3		2.5	8.0
16TH	171.00	4.6	5.1	2303	1038	2.0	4.9	78	-71	44.9	84.9	-5.1		
17TH	180.75	4.3	5.8	2303	1038	1.9	5.6	78	-58	40.3	79.8	~4.3	2.1	7.3
18TH	190.50	4.0	6.5	2303		1.7	6.3	75	-46	36.4	74.0	-3.5	1.8	6.6
19TH	200.25			2303	1038	1.6	6.9	71	-36	32.0	67.5	~2.8	1.4	5.9
20TH	210.00	3.7	7.2	2303	1038	1.5	7.2	71	-33	28.3	60.3	-2.2	1.1	5.3
21ST	219.75	3.5	7.5				7.6	70	-30	24.8	52.8	-1.7	. 9	4.6
2 2 N D	229.50	3.3	7.8	2303		1.4				21.5	44.9	-1.2	. 7	4.0
23RD	239.25	3 .1	8.2	2303	1038	1.4	7.9	69	-27	18.3	36.7	8	. 5	3.3
24TH	249.00	2.9	8.5	2303	_	1.3	8.2	69	-24	15.4	28.3	5	. 3	2.7
25TH	258.75	2.8	8.8	2303	1038	1.2	8.5	68	-21	12.6	19.4	2	. 2	2.0
Evin		5.8	8.7	2303	1038	2.5	8.4	62	-42					

TABLE Wind D		AND HOMEI 80	T DIAGR	ANS : Configur		N DIEGO IN	TERCONTI Refei	INENTAL HOT Rence press	TEL EAST T Sure 27.0 PSF	OVER OUT	GUST	FACTOR 1.32	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA X	(SQ FT) Y	PRESSURE X		ECCEN (F		(KIPS) Y	NOMENT X	(1000-FT-8 Y	KIPS) Z
MECH	268.50	()		1050	1017	1.6	5.6	83 -52	6.8	10.7	1	. 1	1.2
TOP	286.50	6.8	10.7	4232	1917	1.6	J.8	63 -34	¢.¢	0.0	Q.Q	0.0	Q.Q

TABLE Wind D	7 SHEAR	AND MOMEN	T DIAGR	AMS : CONFIGURA	SAN TION C	DIEGO IN	TERCONI Refe	INENTAL Rence P	HOTEL Ressure	EAST TI 27.0 PSF	DWER OUT	GUST F#	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT> Y	PRESSURE X	(PSF) Y	ECCE	N (FT)	SHEAR X	(KIPS) Y	HOMENT (X	1000-FT- Y	KIPS) Z
1 S T	0.00					= 0		7.0	7.0	204.1	179.7	-26.1	40.2	36.8
2ND	17.00	-10.6	13.1	2034	876	-5.2	15.0	39	32	214.7	166.5	-23.2	36.7	36.0
3RD	34.00	-14.5	11.1	2034	876	-7.1	12.6	28	36	229.2	155.5	-20.4	32.9	35.1
4TH	54,00	-14.4	12.4	2743	1195	-5.3	10.4	40	46	243.6	143.1	-17.4	28.2	34.0
518	63.75	8.7	4.6	2 3 0 3	1038	3.8	4.4	38	-73	234.9	138.5	-16.1	25.8	33.2
		9.2	4.5	2303	1038	4.0	4.3	39	-80	225.7	134.0	-14.7	23.6	32.3
6TH	73.50	9.3	5.0	2303	1038	4.0	4.8	4 4	-82	216.4	129.0	-13.5	21.4	31.3
7TH	83.25	9.4	5.4	2303	1038	4.1	5.2	48	-83	207.0	123.6	-12.2	19.4	30.2
8T H	93.00	9.5	5.9	2303	1038	4.1	5.7	52	-83	197.5	117.7	-11.1	17.4	29.1
9T H	102.75	9.7	6.2	2303	1038	4.2	6.0	55	-85			-9.9	15.5	28.0
1 ¢TH	112.50	10.0	6.0	2303	1038	4.3	5.8	55	-91	187.8	111.5			26.7
11TH	122.25	10.3	5.8	2303	1038	4.5	5.6	54	-97	177.9	105.5	-8.9	13.7	
12TH	132.00	10.6	5.6	2303	1038	4.6	5.4	54	-102	167.6	99.7	-7.9	12.1	25.4
13TH	141.75	11.0	5.4	2303	1038	4.8	5.2	53	- 108	156.9	94.1	-6.9	10.5	24.0
14TH	151.50	11.2	5.6	2303	1038	4.9	5.4		-113	146.0	88.8	-6.0	9.0	22.6
1 5 T H	161.25			2303	1038	4.9	6.3		-113	134.8	83.2	-5.2	7.6	21.0
16TH	171.00	11.3	6.6							123.5	76.6	-4.4	6.4	19.3
17TH	180.75	11.7	6.4	2303	1038	5.1	6.1		-114	111.7	70.2	-3.7	5.2	17.6
18TH	190.50	12.1	6.1	2303	1038	5.3	5.9		-114	99.6	64.1	-3.1	4.2	15.8
19TH	200.25	12.5	5.9	2303	1038	5.4	5.7		-113	87.1	58.2	-2.5	3.3	14.1
20TH	210.00	12.9	5.7	2303	1038	5.6	5.5	50	-113	74.2	52.4	-1.9	2.5	12.4
2157	219.75	12.2	6.2	2303	1038	5.3	6.0	57	-111	62.1	46.2	-1.4	1.8	10.7
		11.4	6.7	2303	1038	5.0	6.5	64	-108	50.6	39.5	-1.0	1.3	9.0
22ND	229.50	10.7	7.2	2 3 0 3	1038	4.7	7.0	70	-104	39.9	32.3	7	. 8	7.4
23RD	239.25	10.0	7.7	2303	1038	4.3	7.4	77	-100	29.9	24.5	4	. 5	5.8
24TH	249.00	9.3	8.2	2303	1038	4.0	7.9	83	-94			2	. 3	4.2
25TH	258.75	9.6	7.8	2303	1038	4.2	7.5	82	- 101	20.7	16.3	6		7.6

TABLE Wind D	7 SHEAR IRECTION		IT DIAGRI	AMS : SAN Configuration C	DIEGO IN	TERCONT I Refer	INENTAL HOTEL Rence pressure 2	- EAST TI 27.0 PSF	DVER OUT	GUST Fr	ACTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	HOMENT (X	(1000-FT-K Y	(IPS) Z
MECH	268.50			4252 1917	2.6		114 -148	11.1	8.5	1	. 1	2.6
TOP	286.50	11.1	8.5	4232 1711	2.0	•.•	114 - 140	0.0	Q .Q	Q.Q	\$.0	Q.Q

TABLE WIND D	7. SHEAR	AND MOMEN	NT DIAGR	ANS : Configur	ATION C	N DIEGO IN	TERCONT Refe	INENTAL Rence !	L HOTEL Pressure	EAST TI 27.0 PSF	DWER OUT	GUST Ff	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA X	(SQ FT) Y	P RE SSURE X	(PSF) Y	ECCI	EN (FT) Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT- Y	KIPS) Z
1 S T	0.00					Å	21.5	76	٥	402.0	197.5	-25.9	70.3	54.8
2ND	17.00	1	18.8	2034		0				402.1	178.7	-22.7	63.4	53.4
3R D	34.00	-3.1	17.0	2034		-1.5	19.4	85	16	405.2	161.6	-19.8	56.6	51.9
4TH	54.00	7	17.0	2743		3	14.2	112	5	405.9	144.6	-16.7	48.5	50.0
5TH	63.75	15.4	6.1	2303		6.7	5.8	30	-77	390.5	138.6	-15.3	44.6	48.6
6TH	73.50	15.6	6.0	2303		6.6	5.8	32		375.0	132.6	-14.0	40.9	47.1
7TH	83.25	15.6	5.8	2303	1038	6.8	5.6	33	-90	359.4	126.8	-12.7	37.3	45.5
8TH	93.00	15.5	5.6	2303	1038	6.7	5.4	35	-97	343.9	121.2	-11.5	33.8	43.8
9TH	102.75	15.5	5.3	2303	1038	6.7	5.1	36	-104	328.3	115.9	-10.4	30.6	42.0
10TH	112.50	15.6	5.2	2303	1039	6.8	5.0	36	-109	312.7	110.7	-9.3	27.4	40.1
		15.9	5.2	2303	1038	6.9	5.0	37	-111	296.8	105.5	-8.2	24.5	38.2
1178	122.25	16.2	5.3	2303	1038	7.1	5.1	37	-113	280.6	100.2	-7.2	21.7	36.1
1278	132.00	16.6	5.3	2303	1038	7.2	5.1	37	-115	264.0	94.8	-6.3	19.0	34.0
13TH	141.75	16.9	5.4	2303	1038	7.3	5.2	37	-117	247.1	89.5	-5.4	18.5	31.9
14TH	151.50	17.0	6.8	2303	1038	7.4	6.6	46	-114	230.1	82.6	-4.5	14.2	29.6
15TH	161.25	16.9	9.8	2303	1038	7.3	9.5	60	-103	213.2	72.8	-3.8	12.0	27.3
16TH	171.00	17.4	8.8	2303	1038	7.5	8.4	55	- 108	195.9	64.0	-3.1	10.0	24.9
17TH	180.75	17.8	7.7	2303	1038	7.7	7.4	49	-113		56.3	-2.5	8.2	22.5
18TH	190.50	18.2	6.6	2303	1038	7.9	6.4	42	-117	178.1			6.6	20.1
19TH	200.25	18.7	5.6	2303	1038	8.1	5.4	36	-119	159.8	49.7	-2.0		17.7
20TH	210.00	18.9	5.8	2303	1038	8.2	5.6	36	-116	141.2	44.1	-1.5	5.1	
215T	219.75	19.2	6.1	2303		8.3	5.9	36	-113	122.2	38.3	-1.1	3.8	15.3
22ND	229.50	19.2	6.3	2303		8.4	6.1	36	-110	103.1	32.2	8	2.7	12.9
2 3 R D	239.25			2303		8.5	6.4		-108	83.6	25.9	5	1.8	10.5
24TH	249.00	19.7	6.6			8.6	6.6		-105	64.0	19.3	3	1.1	8.2
25TH	258.75	19.9	6.9	2303						44.0	12.5	1	. 6	5.8
		19.8	6.5	2303	1038	8.6	6.3	30	-106					

TABLE WIND D			T DIAGR	ANS : SAU Configuration C	N DIEGO IN	TERCONT: Refei	INENTAL HOTEL Rence pressure :	- EAST TO 27.0 PSF	WER OUT	GUST F	ACTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	(IPS) Z
MECH	268.50	24.2	5 0	4252 1917	57	7 1	33 - 136	24.2	5.9	1	. 2	3.5
TOP	286.50	24.2	J.7	4232 1717	J. 1	3.1	22 -130	¢,¢	Q.Q	Q.Q	Q.Q	Q.Q

TABLE VIND D	7 SHEAR F	ND MOMEN 10	T DIAGRA	NS : Configura	TION C	N DIEGO IN	REFER	ENCEF	RESSURE	27.0 PSF			ACTOR 1.3	
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (X	SQ FT>	PRESSURE	(PSF) Y	ECCE X	EN (FT) Y	SHEAR X	(KIPS) Y	MOHENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00									681.5	229.4	- 32 . 8	112.0	57.3
210	17.00	11.6	19.8	2034	876	5.7	22.6	62		669.9	209.6	-29.1	100.5	55.7
380	34.00	9.5	17.3	2034	876	4.7	19.8	71	-39	660.4	192.3	-25.6	89.2	54.1
4TH	54.00	12.9	17.3	2743	1195	4.7	14.5	78	-58	647.5	175.0	-22.0	76.1	52.0
		24.3	6.0	2303	1038	10.5	5.7	14	-58	623.3	169.0	-20.3	69.9	50.5
STH	63.75	24.7	6.0	2303	1038	10.7	5.8	15	-62	598.6	163.0	-18.7	64.0	48.9
6TH	73.50	25.5	5.4	2303	1038	11.1	5.2	14	-66	573.1	157.6	-17.1	58.3	47.1
7 T H	83.25	26.2	4.9	2303	1038	11.4	4.7	13	-69	546.9	152.7	-15.6	52.8	45.2
8 T H	93.00	26.9	4.3	2303	1038	11.7	4.2	12	-73	520.0	148.4	-14.1	47.6	43.2
9 T H	102.75	27.4	4.1	2303	1038	11.9	3.9	11	-75	492.6	144.4	-12.7	42.7	41.1
1 Q T H	112.50	27.2	4.7	2303	1038	11.8	4.5	i 3	-77		139.7	-11.3	38.0	39.0
11TH	122.25	27 1	5.3	2303	1038	11.7	5.i	15	-79	465.4				36.8
12TH	132.00	26.9	5.9	2303	1038	11.7	5.7	18	-80	438.3	134.4	-10.0	33.6	34.5
13TH	141.75	26.7	6.5	2303	1038	11.6	6.3	20	-81	411.4	128.5	-8.7	29.4	
14TH	151.50	26.7	8.4	2303	1038	11.6	8.1	25	-90	384.7	122.0	-7.5	25.6	32.2
15TH	161.25		11.5	2303	1038	11.9	11.1	31	-73	358.0	113.7	-6.3	21.9	29.9
16TH	171.00	27.4			1038	12.0	10.5	29	-74	330.5	102.1	-5.3	18.6	27.5
17TH	189.75	27.7	10.9	2303				28	-75	302.8	91.2	-4.3	15.5	25.1
18TH	190.50	29.1	10.3	2303	1038	12.2	9.9			274.7	80.9	-3.5	12.7	22.7
19TH	200.25	28.4	9.7	2303	1038	12.3	9.3	26	-77	246.3	71.3	-2.8	10.1	20.3
2011	210.00	28.7	9.1	2303	1038	12.5	8.7	24	-77	217.6	62.2	-2.1	7.9	17.8
21ST	219.75	29.1	9.1	2303	1038	12.6	8.8	24	-76	188.6	53.1	-1.5	5.9	15.4
		29.5	9.1	2303	1039	12.8	8.8	23	-74	159.1	44.0	-1.1	4.2	13.0
22ND	229.50	29.8	9.2	2303	1038	13.0	8.8	22	-73	129.3	34.8	7	2.8	10.6
23RD	239.25	30.2	9.2	2303	1038	13.1	8.9	22	-72	99.0	25.6	- 4	1.7	8.3
2 4 T H	249.00	30.6	9.2	2303	1038	13.3	8.9	21	-70	68.4	16.4	- 2	9	5.9
2 5 T H	258.75	29.8	8.6	2303	1038	12.9	8.3	21	-72	00 4	10.7	. 6		

TABLE Wind D	7 SHEAR IRECTION	AN D N ONER 110	ET DIAGR	AMS : S Configuration C	AN DIEGO IN	TERCONT	INENTAL HOTEL Rence pressure a	EAST T	OWER OUT	GUST	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	N DN E NT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	38.7	7 0	4252 1917	9.1		18 -89	38.7	7.8	1	. 3	3.6
TOP	286.50	-30.((.0	4232 1717	7.1	4.1	10 -07	Q.Q	Q.Q	Q.Q	0.0	¢.¢

		120		CONFIGURA			REFE	RENCE P	RESSURE	27.0 PSF		GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	P RE SS U RE X	(PSF) Y	ECCE X	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	¢.¢¢						21.2	40	-43	904.9	280.4	-43.9	146.1	46.7
2ND	17.00	19.5	18.5	2034	876	9.6				885.4	261.9	-39.3	130.9	45.1
3RD	34.00	17.2	15.9	2034	876	8.4	18.2	43	-47	868.3	245.9	~35.0	115.9	43.6
4TH	54.00	23.6	15.8	2743	1195	8.6	13.2	36	-53	844.7	230.2	-30.2	98.8	41.8
5TH	63.75	32.2	5.9	2303	1038	14.0	5.7	7	-38	812.5	224.3	-28.0	90.7	40.5
6ТН	73.50	32.9	5.9	2303	1038	14.3	5.7	7	-41	779.5	218.4	-25.8	83.0	39.1
7TH	83.25	33.7	5.7	2303	1038	14.6	5.5	7	-42	745.8	212.7	-23.7	75.5	37.7
		34 . 5	5.5	2303	1038	15.0	5.3	7	-44	711.3	207.2	-21.7	68.4	36.1
8TH	93.00	35.3	5.3	2303	1038	15.3	5.1	7	-46	676.0	202.0	-19.7	61.7	34.4
9TH	102.75	35.8	5.4	2303	1038	15.5	5.2	7	-47	640.2	196.6	-17.7	55.3	32.7
1 ¢ T H	112.50	35.4	6.2	2303	1038	15.4	6.0	8	-48			-15.9	49.2	31.0
1 1 T H	122.25	35.1	7.1	2303	1038	15.2	6.9	10	-49	604.7	190.4			29.2
12TH	132.00	34.7	8.0	2303	1038	15.1	7.7	11	-50	569.7	183.2	-14.0	43.5	
13TH	141.75	34.3	8.9	2303	1038	14.9	8.6	13	-50	535.0	175.2	-12.3	38.1	27.4
14TH	151.50	35.0	10.8	2303	1038	15.2	10.4	15	-49	500.7	166.3	-10.6	33.0	25.5
1 5 T H	161.25	37.5	13.6	2303	1038	16.3	13.1	16	-45	465.7	155.5	-9.0	28.3	23.7
16TH	171.00			2303	1038	16.3	12.9	16	-45	428.2	142.0	-7.6	24.0	21.8
17TH	180.75	37.6	13.4				12.7	16	-45	390.6	128.6	-6.3	20.0	19.9
18TH	190.50	37.6	13.2	2303	1038	16.3				353.1	115.3	-5.1	16.3	17.9
19TH	200.25	37.6	13.0	2303	1038	16.3	12.6	16	-46	315.5	102.3	-4.0	13.1	16.0
2 ¢ T H	210.00	37.6	12.9	2303	1038	16.3	12.4	16	-46	277.9	89.4	-3.1	10.2	14.1
21ST	219.75	37.5	12.9	2303	1038	16.3	12.4	16	-45	240.4	76.6	-2.3	7.7	12.2
22ND	229.50	37.4	12.9	2303	1038	16.2	12.4	15	-45	203.0	63.7	-1.6	5.5	10.3
23RD	239.25	37.3	12.9	2303	1038	16.2	12.4	15	-44	165.8	50.8	-1.0	3.7	8.4
		37.2	12.9	2303	1038	16.1	12.4	15	-44	128.6	37.9	6	2.3	6.6
24TH	249.00	37.0	12.9	2303	1038	16.1	12.4	i 5	-43	91.5	25.1	3	1.2	4.8
25TH	258.75	37.4	11.9	2303	1038	16.2	11.5	14	-45	7 L - G	24.1	. 0		

TABLE Wind D	7 SHEAR IRECTION	AND NOMEN	NT DIAGR	ANS : Configuri		DIEGO IN		INENTAL HOTEL Rence pressure			GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHE AR X	(KIPS) Y	HONENT Ķ	(1000-FT- Y	KIPS) Z
MECH	268.50	54.1	13.2	4252	1917	12.7	6.9	13 -52	54.1	13.2	1	. 5	3.0
TOP	286.50	34.1	13.4	4432	171/	12.6	•.7	13 -32	Q.Q	Q.Q	Q.Q	0.0	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	T DIAGRA	NS : Configura	TION C	N DIEGO IN	TERCONTI Refer	NENTAL Ence P	HOTEL	EAST TO 27.0 PSF	WER OUT	GUST F	ACTOR 1.3	2
FLOOR		FORCE	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCE X	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0. 00						19.5	20	-37	1088.1	276.1	-44.1	173.9	38.0
210	17.00	31.5	17.1	2034	876	15.5				1056.5	259.0	- 39 . 5	154.8	36.4
3RD	34.00	29.1	14.3	2034	876	13.8	16.4	20	-39	1028.5	244.7	-35.3	137.1	35.1
4TH	54.00	34.3	14.3	2743	1195	12.5	12.0		-39	994.1	230.4	-30.5	116.9	33.5
578	63.75	39.7	6.1	2303	1038	16.8	5.9	4	-26	955.5	224.3	-28.3	107.4	32.5
		39.3	5.9	2303	1038	17.1	5.7	4	-27	916.2	218.3	-26.1	98.2	31.4
6TH	73.50	39.4	5.7	2303	1038	17.1	5.5	4	-29	876.8	212.7	-24.0	89.5	30.2
7TH	83.25	39.5	5.4	2303	1038	17.2	5.2	4	-31	837.3	207.3	-22.0	81.1	29.0
8T H	93.00	39.6	5.1	2303	1038	17.2	4.9	4	-32	797.6	202.2	-20.0	73.2	27.7
9T H	102.75	39.8	5.2	2303	1038	17.3	5.0	4	-33	757.8	197.1	-18.0	65.6	26.4
1 ¢ T H	112.50	40.3	6.2	2303	1038	17.5	6.0	5	-33	717.5	190.9	-16.1	58.4	25.0
11TH	122.25	40.7	7.2	2303	1038	17.7	6.9	6	-34			-14.3	51.6	23.6
12TH	132.00	41.2	8.2	2303	1038	17.9	7.9	7	-33	676.8	183.7			22.1
13TH	141.75	41.6	9.3	2303	1038	18.1	8.9	7	-33	635.6	175.4	-12.6	45.2	
14TH	151.50	42.7	10.8	2303	1038	18.5	10.4	8	-33	594.0	166.2	-10.9	33.2	20.7
15TH	161.25		12.6	2303	1038	19.3	12.2		-31	551.3	155.3	-9.3	33.6	19.2
16TH	171.00	44.4			1038	19.2	12.2	9	-32	507.0	142.7	-7.9	28.5	17.7
17TH	180.75	44.3	12.6	2303			12.1	9	-32	462.6	130.1	-6.E	23.7	16.2
18TH	190.50	44.3	12.6	2303	1038	19.2				418.3	117.5	-5.3	19.4	14.7
19TH	200.25	44.2	12.6	2303	1038	19.2	12.1	9	-32	374.1	104.9	-4.3	15.6	13.1
20TH	210.00	44.1	12.5	2303	1038	19.2	12.1	9	-32	330.0	92.4	-3.3	12.1	11.6
215T	219.75	44.1	12.6	2303	1038	19.2	12.2	9	-32	285.9	79.7	-2.5	9.1	10.1
		44.1	12.8	2303	1038	19.2	12.3	9	-32	241.7	67.0	-1.7	6.6	8.5
22ND	229.50	44.1	12.9	2303	1038	19.1	12.4	9	-32	197.6	54.1	-1.2	4.4	7.0
23RD	239.25	44.1	13.0	2303	1038	19.1	12.5	10	-32	153.5	41.1	7	2.7	5.4
24TH	249.00	44.1	13.1	2303	1038	19.1	12.6	10	-32	109.5	28.0	4	1.4	3.9
25TH	258.75	44.5	12.3	2303	1038	19.3	11.8	9	-32	142.0				

TABLE WIND D	7 SHEAR I	AND MONEN 130	T DIAGR	AMS : CONFIGURA		DIEGG IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TO 7.0 PSF	OVER OUT	GUST FA	CTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE X		ECCEN (FT) X Y	SHEAR X	(KIPS) Y	HONENT (X	1000-FT-K Y	(IPS) Z
MECH	268.50	65.0	15.7	4252	1917	15.3	8.2	8 -34	65.0	15.7	1	. 6	2.3
TOP	286.50	63.V	13.7	4232	1717	13.3	.	5 -34	Q.Q	Q.Q	Q .Q	Q.Q	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND MONEI	NT DIAGR	ANS ; CONFIGURI	SP ATION C	N DIEGO IN	TERCONT Refe	INENTAL Rence Pi	HOTEL Ressure	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA 4	(SQ FT) Y	PRESSURE	(PSF) Y	ECCEN	N (FT) Y	SHE AR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
15T	0.00			- · - ·				•		1272.1	222.7	-35.4	199.9	27.3
2ND	17.00	43.4	12.8	2034	876	21.3	14.6	9	-29	1228.7	209.9	-31.8	178.6	25.9
JRD	34.00	40.0	10.9	2034	876	19.7	12.4	8	-28	1188.7	199.1	-28.3	158.1	24.7
4TH	54.00	49.1	11.8	2743	1195	17.9	9.8	6	-26	1139.6	187.3	-24.4	134.8	23.3
		44.8	5.5	2303	1038	19.5	5.3	2	-17	1094.8	181.8	-22.6	123.9	22.6
STH	63.75	45.1	5.6	2303	1038	19.6	5.4	2	-17	1049.7	176.2	-20.9	113.4	21.8
6T H	73.50	44.7	5.4	2303	1038	19.4	5.2	2	-18	1004.9	170.8	-19.2	103.4	21.0
7TH	83.25	44.4	5.3	2303	1038	19.3	5.1	2	-19			-17.5	93.8	20.1
8T H	93.00	44.1	5. i	2303	1038	19.1	4.9	2	-20	960.5	165.5			19.2
9T H	102.75	44.1	5.1	2303	1038	19.1	4.9	2	-21	916.4	160.5	-15.9	84.7	
1 ¢ T H	112.50	45.0	5.6	2303	1038	19.5	5.4	3	-21	872.3	155.4	-14.4	76.0	18.3
11TH	122.25	45.8	6.1	2303	1038	19.9	5.9	3	-21	827.4	149.8	-12.9	67.7	17.3
12TH	132.00			2303	1038	20.3	6.4	3	-21	781.6	143.6	-11.5	59.8	16.3
13TH	141.75	46.7	6.7					3	-20	734.9	136.9	-10.1	52.5	15.4
14TH	151.50	47.6	7.2	2303	1038	20.7	6.9			687.3	129.7	-8.8	45.5	14.4
1 5 T H	161.25	48.2	7.8	2303	1038	20.9	7.5	3	-19	639.1	122.0	-7.6	39.1	13.4
1678	171.00	48.7	8.3	2303	1038	21.1	8.0	3	-17	590.4	113.7	-6.4	33.1	12.6
1718	180.75	49.8	8.8	2303	1038	21.6	8.4	3	-18	540.6	104.9	-5.4	27.5	11.6
		50.9	9.2	2303	1038	22.1	8.9	3	-19	489.7	95.7	-4.4	22.5	10.6
18TH	190.50	51.9	9.7	2303	1038	22.6	9.4	4	-20	437.8	86.0	-3.5	18.0	9.6
19TH	200.25	53.0	10.2	2303	1038	23.0	9.8	4	-21	384.8	75.8	-2.7	14.0	8.4
20TH	210.00	52.7	10.3	2303	1038	22.9	9.9	4	-21			-2.0	10.5	7.3
21\$T	219.75	52.5	10.4	2303	1038	22.8	10.0	4	-21	332.0	65.5			6.2
22ND	229.50	52.2	10.5	2303	1038	22.7	10.1	4	-21	279.5	55.1	-1.5	7.5	
2 3 R D	239.25	51.9	10.5	2303	1038	22.6	10.1	4	-21	227.3	44.7	-1.0	5.0	5.1
24TH	249.00	51.7	10.5	2303	1038	22.4	10.2	4	-21	175.4	34.1	6	3.1	3.9
2 5 T H	258.75					21.6	9.5	4	-21	123.7	23.5	3	1.6	2.8
		49.8	9.9	2303	1038	21.0	7.3	4	÷.					

	TABLE 7 SHEAR AND MOMENT DIAGRAMS : SAN DIEGO INTERCONTINENTAL HOTEL EAST TOWER OUT Wind direction 140 configuration c reference pressure 27.0 PSF												2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT> Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT-) Y	(IPS) Z
MECH	268.50	73.9	13.6	4252	1917	17.4	7 1	4 -23	73.9	13.6	1	. 7	1.7
TOP	286.50	(3.7	13.0	7232	171(4 . L	4 -23	Q.Q	0 .0	Q.Q	Q.Q	Q.Q

	7 SHEAR IRECTION		NT DIAGR	AMS : Configuri	SA ATION C	N DIEGG IN	TERCONT Refe	INENTAL Rence pi	HOTEL Ressure	EAST TE 27.0 PSF	BWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEI X	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00							3	-20	1363.1	140.2	-21.2	211.1	16.4
2ND	17.00	52.6	8.2	2034	876	25.9	9.4			1310.5	132.0	-18.9	188.4	15.3
380	34.00	49.0	6.9	2034	876	24.1	7.9	2	-17	1261.5	125.1	-16.7	166.5	14.5
4TH	54,00	59.8	8.5	2743	1195	21.8	7.1	2	-17	1201.6	116.5	-14.3	141.9	13.4
578	63.75	48.0	4.7	2303	1038	20.8	4.6	1	-10	1153.6	111.8	-13.2	130.4	12.9
6TH	73.50	47.5	4.7	2303	1038	20.6	4.6	1	-10	1106.1	107.0	-12.1	119.4	12.5
		47.1	4.5	2303	1038	20.4	4.3	1	-10	1059.0	102.6	-11.1	108.8	12.0
7TH	83.25	46.7	4.2	2303	1038	20.3	4.0	1	-11	1012.3	98.4	-10.1	98.7	11.5
8TH	93.00	46.2	3.9	2303	1038	20.1	3.8	1	-11	966.1	94.5	-9.2	89.1	10.9
9T H	102.75	46.2	3.7	2303	1038	20.0	3.6	1	-11	919.9	90.8	-8.3	79.9	10.4
1 0 T H	112.50	47.1	3.9	2303	1038	20.5	3.7	i	-11	872.8	86.9	-7.4	71.1	9.9
11TH	122.25	48.1	4.0	2303	1038	20.9	3.9	i	-11			-6.6	62.9	9.3
12TH	132.00	49.1	4.1	2303	1038	21.3	4.0	1	- i i	824.7	82.9			8.8
13TH	141.75	50.0	4.3	2303	1038	21.7	4.1	1	-11	775.6	78.8	-5.8	55.1	
14TH	151.50	51.7	4.6	2303	1038	22.5	4.4	1	-11	725.6	74.5	-5.1	47.7	8.2
15TH	161.25	54.1	5.2	2303	1038	23.5	5.0	1	-10	673.9	69.9	-4.4	40.9	7.7
16TH	171.00	54.3	5.3	2303	1038	23.6	5.1	1	-10	619.8	64.7	-3.7	34.6	7.1
17TH	180.75	54.5	5.3	2303	1038	23.6	5.1	1	-11	565.5	59.4	-3.1	28.8	6.6
18TH	190.50			2303	1038	23.7	5.2	1	-11	511.1	54.1	-2.5	23.6	6.0
19TH	200.25	54.6	5.4				5.3			456.5	48.7	-2.0	18.9	5.4
20TH	210.00	54.7	5.5	2303	1038	23.8		1	-11	401.7	43.2	-1.6	14.7	4.7
21ST	219.75	54.5	5.6	2303	1038	23.7	5.4	1	-11	347.2	37.6	-1.2	11.0	4.1
22ND	229.50	54.3	5.7	2303	1038	23.6	5.5	1	-12	293.0	31.9	9	7.9	3.5
23RD	239.25	54.0	5.8	2303	1038	23.5	5.6	1	-12	238.9	26.2	6	5.3	2.8
2478	249.00	53.8	5.9	2303	1038	23.4	5.7	1	-12	185.1	20.3	4	3.3	2.2
		53.6	6.0	2303	1038	23.3	5.7	1	-12	131.5	14.3	2	1.7	1.6
25TH	258.75	54.3	5.8	2303	1038	23.6	5.6	1	-11					

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN	T DIAGR	ANS : SAI Configuration C	I DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	- EAST TI 27.0 PSF	DVER OUT	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE X		ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	77.2	8.5	4252 1917	18.2		1 -12	77.2	8.5	1	.7	1.0
TOP	286.50	<i></i>	0.7	4232 1711	10.2	•••	1 -12	0.Q	Q.Q	0.0	ə. o	Q.Q

TABLE VIND D	7 SHEAR IRECTION	AND MONEL	NT DIAGR	ANS : Configuri	SA Ation C	N DIEGO IN	TERCONT REFE	INENTAL Rence pi	HOTEL RESSURE	EAST TO 27.0 PSF	WER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA ((SQ FT) Y	P RE SSURE X	(PSF) Y	ECCEI	N (FT) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT-1 Y	KIPS) Z
1ST	0.00					.				1460.3	37.9	-5.0	223.9	3.5
2ND	17.00	57.7	2.8	2034	876	28.4	3.2	0	-10	1402.6	35.2	-4.4	199.5	2.9
380	34.00	54.5	2.0	2034	876	26.8	2.3	Ó	-7	1348.1	33.1	-3.8	176.2	2.5
4TH	54.00	66.4	3.9	2743	1195	24.2	3.3	¢	-7	1281.7	29.2	-3.2	149.9	2.1
5TH	63.75	52.7	2.9	2303	1038	22.9	2.8	¢	- 3	1229.0	26.3	-2.9	137.6	1.9
		52.3	2.7	2303	1038	22.7	2.6	0	- 2	1176.7	23.5	-2.7	125.9	1.8
6TH	73.50	51.6	2.2	2303	1038	22.4	2.1	¢	- 2	1125.1	21.3	-2.4	114.7	1.7
7TH	83.25	51.0	1.7	2303	1038	22.1	1.6	0	-2	1074.2	19.6	-2.2	104.0	1.6
8T H	93.00	50.3	1.2	2303	1038	21.8	1.1	٥	- 2		18.5	-2.1	93.7	1.5
9T H	102.75	50.i	. 8	2303	1038	21.7	.7	¢	- 1	1023.9			84.0	1.4
1 ¢ T H	112.50	5 i.1	.7	2303	1038	22.2	.7	¢	- 1	973.8	17.7	-1.9		
11TH	122.25	52.1	. 6	2303	1038	22.6	. 6	0	- 1	922.7	17.0	-1.7	74.7	1.4
12TH	132.00	53.0	. 6	2303	1038	23.0	. 5	٥	-1	870.7	16.4	-1.6	66.0	1.3
13TH	141.75	54.0	. 5	2303	1038	23.5	.5	0	-1	817.6	15.8	-1.4	57.8	1.3
14TH	151.50			2303	1038	24.0	.2	0	-0	763.6	15.3	-1.2	50.1	1.2
1 5 T H	161.25	55.4	. 3				.0	-0	-0	708.2	15.1	-1.1	42.9	1.2
16TH	171.00	56.9	0	2303	1038	24.7				651.4	15.1	9	36.3	1.2
17TH	180.75	57.0	. 4	2303	1038	24.8	.4	0	-1	594.3	14.7	- . 8	30.2	1.2
1878	190.50	57.2	. 7	2303	1038	24.8	.7	0	- 1	537.1	14.0	7	24.7	1.1
19TH	200 25	57.4	1.1	2303	1038	24.9	1.1	¢	-1	479.7	12.9	5	19.7	1.0
		57.8	1.5	2303	1038	25.0	1.4	Ó	- 2	422.1	11.4	4	15.3	. 9
2 Q T H	210.00	57.5	1.5	2303	1038	25.0	1.5	0	- 2	364.6	9.9	3	11.5	. 8
21\$T	219.75	57.5	1.5	2303	1038	25.0	1.5	0	- 2	307.1	8.3	2	8.2	. 7
22ND	229.50	57.5	1.6	2303	1038	25.0	1.5	0	- 2	249.6	6.8	1	5.5	. 5
2 3 R D	239.25	57.4	1.6	2303	1038	24.9	1.5	0	- 2				3.3	. 4
24TH	249.00	57.4	1.6	2303	1038	24.9	1.6	0	- 2	192.2	5.2	1		. 3
25TH	258.75	56.2	1.3	2303	1038	24.4	1.3	0	- 2	134.7	3.5	Q	1.7	. 4
			•••	• •										

TABLE WIND D	7 SHEAR IRECTION		NT DIAGR	AMS : Configura	TION C	N DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL Essure	EAST TO 27.0 PSF	DWER OUT	GUST	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X		SHEAR X	(KIPS) Y	NONENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	78.5		4050	1017	4 0 E		4		78 5	2.2	0	. 7	. 2
TOP	286.50	78 .0	2.2	4252	1917	18.5	1.1	0	-2	Q .Q	0.0	Q . Q	0.0	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND NONEI	NT DIAGR	ANS : CONFIGURI	SAN RTION C	DIEGO II	NTERCONT REFE	INENTAL I Rence pri	HOTEL ESSURE	EAST T 27.0 PSF	OVER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	(SQ F1) Y	PRESSURI X	E (PSF) Y	ECCEN X	(FD) Y	SHE AR X	(KIPS) Y	NGMENT S X	(1000-FT- Y	K148) Z
157	0.00									1440.9	-65.1	11.6	217.3	-9.6
2ND	17.00	58.6	-1.7	2034	876	28.8	-2.0	-0	-1	1382.2	-63.4	10.5	193.3	-9.6
3RD	34.00	55.1	-2.2	2034	876	27.1	-2.5	¢	1	1327.1	-61.3	9.4	170.3	-9.5
4TH	54.00	68.6	-1.7	2743	1195	25.0	-1.4	Ŷ	2	1258.5	-59.5	8.2	144.4	-9.4
		54.8	. 6	2303	1038	23.8	. 6	- ¢	4	1203.7	-60.1	7.6	132.4	-9.2
5T H	63.75	54.1	. 3	2303	1038	23.5	. 3	- 0	5	1149.7	-60.5	7.0	120.9	-8.9
67 H	73.50	53.3	3	2303	1038	23.2	3	¢	6	1096.3	-60.2	6.4	110.0	-8.6
7T H	83.25	52.6	9	2303	1038	22.8	9	¢	6	1043.8	-59.3	5.9	99.6	-8.3
8T H	93.00	51.8	-1.5	2303	1038	22.5	-1.4	٥	7	991.9	-57.8	5.3	89.6	-7.9
9T H	102.75	51.4	-2.0	2303	1038	22.3	-1.9	0	8			4.7	80.2	-7.5
1 QT H	112.50	51.9	-2.3	2303	1038	22.5	-2.2	٥	8	940.5	-55.8			
11TH	122.25	52.4	-2.5	2303	1038	22.7	-2.4	0	8	888.7	-53.5	4.2	71.3	-7.1
12TH	132.00	52.9	-2.8	2303	1038	23.0	-2.7	٥	8	836.3	-51.0	3.7	62.9	-6.7
13TH	141.75	53.4	-3.0	2303	1038	23.2	-2.9	ð	8	783.4	-48.2	3.2	55.0	-6.2
14TH	151.50			2303		23.5	-3.5	1	9	730.1	-45.2	2.7	47.6	-5.8
15TH	161.25	54.2	-3.6				-4.2	1	9	675.9	-41.6	2.3	40.8	-5.3
16TH	171.00	55.1	-4.3	2303	1038	23.9				620.8	-37.2	1.9	34.4	-4.8
17TH	180.75	55.1	-4.1	2303	1038	23.9	-3.9	1	9	565.7	-33.1	1.6	28.6	-4.3
1878	190.50	55.0	-3.9	2303	1038	23.9	-3.7	1	9	510.7	-29.3	1.3	23.4	-3.8
1918	200.25	55.0	-3.6	2303	1038	23.9	-3.5	1	8	455.7	-25.7	1.0	18.7	-3.4
2018	210.00	55.0	-3.4	2303	1038	23.9	-3.2	0	8	400.7	-22.3	. 8	14.5	-2.9
		54.9	-3.3	2303	1038	23.8	-3.2	Ó	8	345.9	-19.0	. 6	10.9	-2.5
2157	219.75	54.8	-3.2	2303	1039	23.8	-3.1	0	7	291.1	-15.9	. 4	7.8	-2.1
22ND	229.50	54.7	-3.1	2303	1038	23.7	-3.0	¢	7	236.5	-12.7	.3	5.2	-1.7
23RD	239.25	54.6	-3.0	2303	1038	23.7	-2.9	٥	7	181.9	-9.7	.2	3.2	-1.3
24TH	249.00	54.5	-2.9	2303	1038	23.6	-2.8	0	7			. 1	1.6	-1.0
25TH	258.75	53.4	-3.0	2303	1038	23.2	-2.9	o	7	127.4	~6.8	. 1	1.9	- L . V

TABLE VIND D	7 SHEAR IRECTION	AND NOMES	NT DIAGR	AMS : SAN Configuration C	DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TO 7.0 PSF	OVER OUT	GUST F	ACTOR 1.3	?
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRE SSURE X	(PSF) Y	ECCEN (FT) X Y	SHE AR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	(TPS) Z
NECH	268.50	74.0	-3.8	4252 1917	17.4	. 2. 4	0 8	74.0	-3.8	. 0	. 7	6
TOP	286.50	24.V	-3.5	4232 1917	17.4	-2 0	v o	0 .0	0 .0	0.0	¥.0	0 .0

TABLE WIND D	7 SHEAR IRECTION	AND NONEI 180	NT DIAGRI	ANS : Configura	TION C	AN DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	32
FLOOR	HEIGHT		(KIPS) Y	AREA (X	SØ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHE AR X	(KIPS) Y	NOMENT	(1000-FT- Y	·KIPS) Z
1 S T	0.00							•		1378.3	-143.8	24.7	206.2	-20.1
SHD	17.00	59.4	-5.2	2034	876	29.2	-6.0	¢	4	1318.9	-138.6	22.3	183.3	-19.9
3RD	34.00	55.0	-5.3	2034	876	27.1	-6.0	1	6	1263.8	-133.3	19.9	161.3	-19.5
4TH	54.00	66.7	-4.4	2743	1195	24.3	-3.7	¢	7	1197.1	-129.0	17.3	136.7	-19.1
	63.75	51.8	5	2303	1038	22.5	5	ò	è	1145.3	-128.4	16.1	125.3	-18.6
5TH		51.6	-1.0	2303	1038	22.4	-1.0	0	11	1093.7	-127.4	14.8	114.4	-18.1
6TH	73.50	51.0	-1.8	2303	1038	22.2	-1.9	0	12	1042.7	-125.6	13.6	103.9	-17.4
7TH	83.25	50.4	-2.6	2303	1038	21.9	-2.5	1	14	992.2	-123.0	12.4	94.0	-16.7
8T H	93.00	49.8	-3.5	2303	1038	21.6	-3.3	1	15	942.4	-119.5	11.2	84.6	-16.0
9T H	102.75	49.5	-4.2	2303	1038	21.5	-4.0	1	16	892.9	-115.3	10.0	75.6	-15.1
1 ¢ T H	112.50	49.9	-4.7	2303	1038	21.7	-4.5	2	17	843 0	-110.6	8.9	67.2	-14.3
11TH	122.25	50.3	-5,2	2303	1038	21.8	-5.0	2	17	792.7	-105.5	7.9	59.2	-13.5
12TH	132.00	50.6	-5.7	2303	1038	22.0	~5.5	2	17	742.1	-99.8	6.9	51.7	-12.6
13TH	141.75	51.0	-6.1	2303	1038	22.1	-5.9	2	17			5.9	44.7	-11.7
14TH	151.50	51.5	-7.0	2303	1038	22.4	-6.8	2	18	691.1	-93.7		38.3	-10.8
15TH	161.25	52.1		2303	1038	22.6	-7.8	3	18	639.6	-86.6	5.1		-9.8
16TH	171.00	52.4		2303	1038	22.7	-7.5	3	18	587.5	-78.5	4.3	32.3	
17TH	180.75	52.7		2303	1038	22.9	-7.2	2	17	535 2	-70.7	3.5	26.8	-8.9
18TH	190.50	53.0		2303	1038	23.0	-6.9	2	16	482.5	-63.3	2.9	21.8	-8.0
19TH	200.25			2303	1038	23.1	-6.6	2	16	429.5	-56.1	2.3	17.4	-7.1
2 O T H	210.00	53.3			1038	22.9	-6.6	- 2	16	376.3	-49.2	1.8	13.5	-6.2
215T	219.75	52.8		2303			~6.5	2	16	323.4	-42.4	1.3	10.1	-5.4
2 2 N D	229.50	52.4		2303	1038	22.8		2	16	271.0	-35.7	1.0	7.2	-4.5
2 3 R D	239.25	52.0	-6.7	2303	1038	22.6	-5.4			219.0	-29.0	. 6	4.8	-3.7
2418	249.00	51.6		2303	1038	22.4	-6.4	2	16	167.5	-22.4	. 4	2.9	-2.9
25TH	258.75	51.2	-6.5	2303	1038	22.2	-6.3	2	16	116.3	-15.8	. 2	1.5	-2.0
2018	200.10	49.0	-6.6	2303	1039	21.3	-6.3	2	17					

TABLE VIND (7 SHEAR DIRECTION	AND HONEN 180	IT DIAGRI	ANS : Configuration	SAN C	DJEGO IN	TERCONT REFE	TINENTAL Rence Pr	HOTEL	27.0 PSF	OWER OUT	GUST !	FACTOR 1.3	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SR F X Y	7.)	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	67.3	-9.2	4252 191	,	15.8	- 4 9	2	1.9	67.3	-9.2	. 1	. 6	-1.2
TOP	286.50	61.3	- 7 . 2.	4252 171	(13.5	- 4.0	-	10	Q., Q	Q.Q	Q . Q	Ŷ.Ŷ	Q.Q

TABLE WIND D	7 SHEAR A IRECTION I	90		CONFIGURA	TION C	N DIEGO IN	REFER	ENCE PR	ESSURE	27.0 PSF			ACTOR 1.3	
FLOOR	HEIGHT	FORCE	(KIPS)	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	((F T) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	-KIPS) Z
157	0 .00							•	4.5	1254.7	-229.4	38.5	185.0	-30.1
210	17.00	55.6	~8.5	2034	876	27.4	-9.7	2	10	1199.0	-220.9	34.7	164.2	-29.6
3RD	34.00	50.2	-8.2	2034	876	24.7	-9.4	2	13	1148.8	-212.7	31.0	144.2	-28.9
4TH	54.00	62.3	-8.9	2743	1195	22.7	-7.4	2	15	1086.5	-203.8	26.9	121.9	-28.0
		50.1	-2.5	2303	1038	21.8	-2.4	1	15	1036.4	-201.3	24.9	111.5	-27.2
5TH	63.75	49.4	-3.0	2303	1038	21.4	-2.8	1	17	987.0	-198.3	22.9	101.7	-26.4
6TH	73.50	49.6	-3.9	2303	1038	21.1	-3.7	2	19	938.3	-194.5	21.0	92.3	-25.4
7 T H	83.25	47.9	-4.8	2303	1038	20.8	-4.6	2	21	890.5	-189.7	19.1	83.4	-24.4
8T H	93.00	47.1	-5.7	2303	1038	20.4	~5.5	3	23	843.4	-184.0	17.3	74.9	-23.3
9T H	102.75	46.6	-6.5	2303	1038	20.2	-6.3	3	25	796.8	-177.4	15.6	66.9	-22.1
1 ¢ T H	112.50	45.6	-7.2	2303	1038	20.3	-6.9	4	25		-170.2	13.9	59.4	-20.9
11TH	122.25	46.7	-7.9	2303	1038	20.3	-7.6	4	25	750.1			52.3	-19.7
12TH	132.00	46.8	-8.5	2303	1038	20.3	-8.2	5	26	703.4	-162.3	12.2		-18.5
13TH	141.75	46.9	-9.2	2303	1038	20.4	-8.9	5	26	656.6	-153.8	10.7	45.6	
14TH	151.50	46.3	-10.3	2303	1039	20.1	-10.0	6	27	609.7	-144.6	9.2	39.5	-17.2
15TH	161.25			2303	1038		-11.3	7	28	563.4	-134.3	7.9	33.8	-15.9
16TH	171.00	45.0	-11.8				-11.2	7	28	518.4	-122.5	6.6	28.5	-14.5
17TH	180.75	45.6	-11.6	2303	1038			7	27	472.8	-110.9	5.5	23.6	-13.2
18TH	190.50	46.2	-11.4	2303	1038		-11.0			426.6	-99 4	4.5	19.3	-11.9
1978	200.25	46.8	-11.3	2303	1038		-10.9	6	27	379.8	-88.2	3.6	15.3	-10.5
2011	210.00	47.4	-11.1	2303	1038	20.6	-10.7	6	26	332.5	-77.0	2.8	11.9	-9.2
	219.75	47.0	-11.0	2303	1038	20.4	-10.6	6	26	285.5	-66.1	2.1	8.8	-7.9
215T		46.6	-10.8	2303	1038	20.2	-10.4	6	26	239.0	-55.3	1.5	6.3	-6.7
2 2 N D	229.50	46.2	-10.6	2303	1038	20.0	-10.2	6	26	192.8	-44.7	1.0	4.2	-5.4
2 3 R D	239.25	45.8	-10.5	2303	1038	19.9	-10.1	6	25	147.0	-34.2	. 6	2.5	-4.2
24TH	249.00	45.4	-10.3	2303	1038	19.7	-9.9	6	25	101.6	-23.9	. 3	1.3	-3.0
25TH	258.75	42.3	-9.9	2303	1038	18.4	-9.6	6	27	141.0	63.7	. 0	•••	

TABLE Wind D	7 SHEAR IRECTION	AND MONE 190	NT DIAGR	ANS : Configura	SAN TION C	I DIEGO IN	TERCONT REFEI	ENENTAL Rence pr	HOTEL - Essure	- EAST TO 27.0 PSF	DWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (: X	SQ FT> Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHE AR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	59.3						-		59.3	-14.0	. 1	. 5	-1.8
TOP	286.50	39.3	-14.0	4252	1917	13.9	-7.3	(28	0.0	Q.Q	Q.Q	Q.Q	Q .Q

	7 SHEAR	AND MOMEN	IT DIAGR	ANS : CONFIGUR	SA ATION C	N DIEGO IN	TERCON Refi	TINENTAL Erence pr	HO TEL Essure	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.	32
FLOOR	HEIGHT	FORCE	(K1PS)	AREA X	(SQ FT) Y	P RE SSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	-KIPS) Z
1 S T	0.00				0.24		- 4 4 - 6	4	17	1074.5	-274.9	46 1	158.5	-37.4
2ND	17.00	43.6	-10.2	2034	876		-11.6			1030.9	-264.7	41.5	140.6	-36.6
3RD	34.00	38.9	-9.3	2034	876		-10.7	5	19	992.0	-255.4	37.1	123.4	-35.9
4TH	54.00	51.5	-11.3	2743	1195	18.8	-9.5	5	23	940.5	-244.0	32.1	104.0	-34.6
STH	63.75	45.1	-3.3	2303	1038	19.6	-3.2	2	23	895.3	-240.7	29.7	95.1	-33.6
6TH	73.50	44.4	-3.8	2303	1038	19.3	-3.7	2	26	850.9	-236.8	27.4	86.6	-32.4
		43.7	~4.8	2303	1038	19.0	-4.5	3	28	807.2	-232.1	25.1	78.5	-31.2
7TH	83.25	43.1	-5.7	2303	1038	18.7	-5.5	4	30	764 2	-226.3	22.9	70.8	-29.9
8TH	93.00	42.4	-6.7	2303	1038	18.4	-6.4	5	32	721.8	-219.6	20.7	63.6	-28.5
9T H	102.75	41.8	-7.6	2303	1038	18.1	-7.4	6	34	680.0	-212.0	18.6	56.8	-27.0
1 ¢ T H	112.50	41.3	-8.5	2303	1039	17.9	-8.2	7	34	638.6	-203.4	16.6	50.3	-25.5
11TH	122.25	40.9	-9.5	2303	1038	17.7	-9.1	8	35			14.6	44.3	-24.0
12TH	132.00	40.4	-10.4	2303	1038	17.6	-10.0	9	35	597.8	-194.0		38.7	-22.5
1 3 T H	141.75	40.0	-11.3	2303	1038	17.4	-10.9	10	35	557.3	-183.6	12.8		
14TH	151.50	39.7	-12.4	2303	1038	17.2	-11.9	11	36	517.4	-172.4	11.0	33.4	-21.0
1 5T H	161.25	39.7	-13.3	2303			-12.8	13	38	477.7	-160.0	9.4	28.6	-19.4
16TH	171.00	39.5	-13.4	2303	1038		-12.9	13	37	437.9	-146.7	7.9	24.1	-17.7
17TH	180.75			2303	1038		-13.1	13	36	398.4	-133.3	6.6	20.0	-16.1
18TH	190.50	39.3	-13.6				-13.2	12	36	359.1	-119.8	5.3	16.3	-14.5
19TH	200.25	39.1	-13.7	2303	1038			12	35	320.0	-106.1	4.2	13.0	-12.9
2 O T H	210.00	38.9	-13.8	2303	1038		-13.3			281.1	-92.2	3.3	10.1	-11.4
21ST	219.75	38.8	-13.5	2303	1038		-13.0	12	35	242.3	-78.7	2.4	7.6	-9.9
22ND	229.50	38.8	-13.2	2303	1038		-12.7	12	36	203.5	-65.5	1.7	5.4	-8.3
23RD	239.25	38.8	-12.8	2303	1038	16.8	-12.4	12	36	164.7	-52.7	1.1	3.6	-6.8
	249.00	38.7	-12.5	2303	1038	16.8	-12.0	12	36	126.0	-40.2	. 7	2.2	-5.2
24TH		38.7	-12.2	2303	1038	16.8	-11.7	12	37	87.3	-28.0	. 4	1.1	-3.7
25TH	258.75	37.0	-12.0	2303	1038	16.0	-11.6	12	37					

TABLE Wind D	7 SHEAR IRECTION	AND MOMENT DIAGR	ANS : SAN CONFIGURATION C	DIEGO INT	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TE	OWER OUT	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SØ FT) X Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	She ar X	(KIPS) Y	NDNENT X	(1090-FT- Y	KIPS) Z
MECH	268.50	50.4 -16.0	4252 1917	11.8	- 9 7	12 39	50.4	-16.0	. 1	. 5	- 2 . 2
TOP	286.50	JV.4 "10.V	72J2 1717	11.5	-05	12 37	Q _ Q	Q.Q	Q.Q	\$. \$	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND MOMEN	T DIAGR	ANS : Configura	SA TION C	N DIEGO IN	TERCONT REFE	INENTAL I Rence pri	HOTEL Essure	EAST T 27.0 PSF	OVER OUT	GUST F	ACTOR 1.3	32
FLOOR			(KIPS)	AREA (X	SQ FT>	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NOMENT (X	1000-FT- Y	-KIPS) Z
1 S T	0.00							-		970.2	-252.7	41.7	143.1	-48.2
210	17.00	34.5	-10.8	2034	876		-12.4	6	25	935.7	-241.9	37.5	126.9	-47.2
380	34.00	30.6	-10.6	2034	876	15.1	-12.1	10	29	905.1	-231.3	33.5	111.2	-46.2
		40.5	-12.8	2743	1195	14.8	-10.7	11	35	864.6	-218.5	29.0	93.5	-44.7
4TH	54.00	42.6	-2.2	2303	1038	18.5	-2.1	2	32	822.0	-216.3	26.9	85.3	-43.3
5TH	63.75	42.4	-2.7	2303	1038	18.4	-2.6	2	35	779.6	-213.6	24.8	77.5	-41.8
6T H	73.50	41.7	-3.8	2303	1038	18.1	-3.6	3	38	737.9	-209.9	22.7	70.1	-40.2
7TH	83.25	41.0	-4.8	2303	1038	17.8	-4.7	5	41	696.8	-205.0	20.7	63.1	-38.5
8T H	93.00	40.4	-5.9	2303	1038	17.5	-5.7	6	43	656.5	-199.1	18.7	56.5	-36.7
9T H	102.75	39.8	-6.9	2303	1038	17.3	-6.6	8	45	616.7	-192.2	16.8	50.3	-34.8
1 0 T H	112.50	39.5	-7.6	2303	1038	17.2	-7.3	9	46	577.1	-184.6	15.0	44.5	-32.9
11TH	122.25	39.3	-8.3	2303	1038	17.0	-7.9	10	47		-176.4	13.2	39.0	-31.0
12TH	132.00	39.0	-8.9	2303	1038	16.9	-8.6	11	48	537.9			34.0	-29.0
1 3 T H	141.75	38.7	-9.6	2303	1038	16.8	-9.3	12	49	498.9	-167.5	11.5		
14TH	151.50	38.0	-10.6	2303	1038	16.5	-10.2	14	51	460.2	-157.9	10.0	29.3	-27.0
15TH	161.25	36.3	-12.0	2303	1038	15.8	-11.5	17	53	422.2	-147.2	8.5	25.0	-25.0
16TH	171.00			2303	1030		-11 9	18	52	385.8	-135.3	7.1	21.1	-22.8
17TH	180.75	35.7	-12.4				-12.3	19	52	350.1	-122.9	5.8	17.5	-20.7
18TH	190.50	35.1		2303	1038		-12.7	19	51	314.9	-110.2	4.7	14.2	-18.7
19TH	200.25	34.5		2303	1038				50	280.4	-97.0	3.7	11.3	-16.7
20TH	210.00	34.0		2303	1038		-13.0	20		246 4	-83.5	2.8	8.8	-14.7
21ST	219.75	34.1	-13.1	2303	1038		-12.6	19	51	212.3	-70.4	2.1	6.5	-12.7
22ND	229,50	34.3	-12.6	2303	1038		-12.2	19	51	178.0	-57.8	1.4	4.6	-10.7
2 3 R D	229.30	34.5	-12.2	2303	1038		-11.7	18	51	143.5	-45.6	. 9	3.1	-8.8
	237.23	34.7	-11.7	2303	1038	15.1	-11.3	17	51	108.8	-33.9	. 5	1.8	-6.8
24TH		34.8	-11.3	2303	1038	15.1	-10.9	17	51	74.0	-22.6	. 3	. 9	-4.8
25TH	258.75	32.1	-11.0	2303	1038	13.9	-10.6	18	53					

TABLE Wind D	7 SHEAR IRECTION	AND MOMENT DIAGRI	RMS : SAN Configuration C	DIEGO IN	TERCONT Refei	INENTAL HO Rence pres	STEL -	- EAST TO 27.0 PSF	WER OUT	GUST	FACTOR 1 3	2
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (X	FT) Y	SHEAR X	(KIPS) Y	N DN E NT X	(1000-FT- Y	KIPS) Z
MECH	268.50	41.8 -11.6	4252 1917	9.8	-6.1	18 4	54	41.8	-11.6	. 1	. 4	-2.9
TOP	286.50	41.6 -11.6	4232 1711	7.0	- 6 . 1	10 1	, -	Q,Q	Q.Q	Ç.Ç	Q .Q	Q,Q

TABLE	7 SHEAR IRECTION	AND NOMEN	T DIAGR	ANS : Configura	SI TION C	N DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL	EAST TO 27.0 PSF	DWER OUT	GUST F	ACTOR 1 3	32
FLOOR	HEIGHT		(KIPS)		SQ FT>	PRESSURE	(PSF) Y	ECCEN	I (FT) Y	SHEAP X	(KIPS)	HONENT : X	(1000-FT- Y	-KIPS) Z
15T	0.00	n	•							809.3	-134.5	20.5	121.6	-57.3
	17.00	23.7	-8.6	2034	876	11.6	-9.9	12	34	785.7	-125.9	18.3	108.1	-56.4
2ND		20.4	-8.5	2034	876	10.0	-9.8	15	36	765.3	-117.3	16.2	94.9	-55.5
3RD	34.00	29.0	-11.8	2743	1195	10.6	-9.9	20	49	736.3	-105.5	14.0	79.9	-53.8
4TH	54.00	36.3	4	2303	1038	15.8	4	0	43	700.0	-105.1	13.0	72.9	-52.3
STH	63.75	35.3	7	2303	1038	15.3	6	1	47	664.8	-104.4	11.9	66.2	-50.6
6T H	73.50	35.0	-1.3	2303	1038	15.2	-1.3	2	51	629.8	-103.1	10.9	59.9	-48.8
7T H	83.25	34.7	-2.0	2303	1038	15.0	-1.9	3	55	595.1	-101.1	9.9	53.9	-46.9
8T H	93.00	34.3	-2.7	2303	1038	14.9	-2.6	5	59	560.8	-98.4	9.0	48.3	-44.9
9T H	102.75	34.0	-3.3	2303	1038	14.8	-3.2	6	62	526.7	-95.1	8.0	43.0	-42.7
1 ¢ T H	112.50	33.8	-3.8	2303	1038	14.7	-3.6	7	64	492.9	-91.3	7.1	38.0	-40.5
11TH	122.25	33.5	-4.2	2303	1038	14.6	-4.1	8	66		-87.1	6.2	33.4	-38.3
12TH	132.00	33.3	-4.7	2303	1038	14.4	-4.5	10	69	459.4		5.4	29.1	-36.0
13TH	141.75	33.0	-5.1	2303	1038	14.3	-4.9	11	71	426.1	-82.5		25.1	-33.6
14TH	151.50	32.2	-5.7	2303	1038	14.0	-5.5	i 3	75	393.1	-77.4	4.6		-31.1
15TH	161.25	30.5	-6.3	2303	1038	13.2	-6.1	17	81	360.9	-71.7	3.9	21.4	-28.5
16TH	171.00	30.2	-6.5	2303	1038	13.1	-6.3	18	81	330.4	-65.4	3.2	18.0	
17TH	180.75			2303	1038	13.0	-6.5	18	81	300.2	-58.9	2.6	15.0	-25.9
18TH	190.50	29.9	-6.7	2303	1038	12.8	-6.7	19	81	270.3	-52.2	2.1	12.2	-23.4
1 9 T H	200.25	29.6	-6.9			12.7	-6.8	20	81	240.7	-45.2	1.6	9.7	-20.8
20TH	210.00	29.3	-7.1	2303	1038		-6.4	18	81	211.4	-38.1	1.2	7.5	-18.3
215T	219.75	29.4	-6.7	2303	1038	12.8		17	91	182.0	-31.5	. 9	5.6	-15.8
22ND	229.50	29.6	-6.2	2303	1038	12.8	-6.0			152.4	-25.3	. 6	3.9	-13.3
23RD	239.25	29.7	-5.8	2303	1038	12.9	-5.5	16	91	122.7	-19.5	. 4	2.6	-10.8
24TH	249.00	29.9	-5.3	2303	1038	13.0	-5.1	14	81	92.8	-14.2	. 2	1.5	-8.4
2578		30.1	-4.9	2303	1038	13.0	-4.7	13	81	62.7	-9.3	. 1	. 8	-5.9
2318	239.13	27.8	-5.2	2303	1038	12.1	-5.0	15	83					

TABLE Wind D	7 SHEAR IRECTION	AND NOMES	NT DIAGR	ANS : SAN Configuration C	DIEGO IN	TERCONT Refei	INENTAL HOTEL Rence pressure	EAST T 27.0 PSF	OWER OUT	GUST	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	34.9	-4.2	4252 1917	8.2	- 2 2	12 98	34.9	-4.2	. Ç	. 3	-3.5
TOP	286.50	34.7		4232 1717	0.2	- 2 . 2	12 70	Q.Q	Q.Q	¢,¢	Q .Q	Q.Q

TABLE Wind D	7 SHEAR IRECTION	ANO MONEI 230	NT DIAGR	ANS : Configur	ATION C	N DIEGO IN	TERCONT Refe	INENTAL Rence P	HOTEL Ressure	EAST T 27.0 PSF	OVER OUT	GUST Ff	ACTOR 1.3	32
FLOOR	HEIGHT	FDRCE X	(KIPS) Y	AREA X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCE X	N (FT) Y	SHEAR X	(KIPS) Y	NONENT (X	1000-FT- Y	-KIPS) Z
1 S T	0 .00							7.0	<i></i>	587.0	-122.5	19.2	9¢.6	-51.6
2ND	17.00	9.5	-6.2	2034	876	4.7	-7.1	39	60	577.4	-116.3	17.2	80.7	-50.8
3RD	34.00	6.8	-6.6	2034	876	3.3	-7.5	55	57	570.6	-109.8	15.3	70.9	-50.1
4TH	54.00	14.6	-10.6	2743	1195	5.3	-8.9	51	70	556.0	-99.1	13.2	59.6	-48.5
578	63.75	29.9	. 1	2303	1038	13.0	. 1	-0	49	526.1	-99.2	12.2	54.4	-47.1
6TH	73.50	28.9	4	2303	1038	12.5	3	1	54	497.2	-98.9	11.3	49.4	-45.5
7TH	83.25	28.3	-1.2	2303	1039	12.3	-1.2	3	58	468 9	-97 6	10.3	44.7	-43.8
8T H	93.00	27.7	-2.1	2303	1039	12.0	-2.0	5	63	441 2	-95.5	9.4	40.2	-42.1
9TH	102.75	27.1	-3.0	2303	1038	11.8	-2.9	7	67	414.0	-92.6	8.5	36.1	-40.2
	112.50	26.5	-3.7	2303	1038	11.5	-3.6	10	71	387 5	-88.8	7.6	32.2	-38.3
1018		25.8	-4.2	2303	1038	11.2	-4.0	12	75	361.7	-84.6	6.7	28.5	-36.3
11TH	122.25	25.1	-4.7	2303	1038	10.9	-4.5	15	78	336.6	-80.0	5.9	25.1	-34.3
1278	132.00	24.4	-5.1	2303	1038	10.6	-4.9	17	82	312.2	-74.9	5.2	21.9	-32.2
13TH	141.75	23.7	-5.6	2303	1038	10.3	-5.4	20	86	288.5	-69.3	4.5	17.0	-30.1
14TH	151.50	22.5	-5.6	2303	1038	9.8	-5.4	23	92		-63 8	4.J 3.8	16.3	-27.9
15TH	161.25	20.8	-4.6	2303	1038	9.0	-4.5	23	103	266 0				-25.6
16TH	171.00	20.8	-4.9	2303	1038	9.0	-4.7	24	103	245.2	-59.1	3.2	13.8	
1778	180.75	20.8	-5.2	2303	1038	9.0	-5.0	26	103	224.4	-54.2	2.7	11.5	-23.4
18TH	190.50	20.7	-5.4	2303	1038	9.0	-5.2	27	104	203.6	-49.1	2.2	9.4	-21.1
19TH	200.25	20.7	-5.7	2303	1038	9.0	-5.5	29	104	182.9	-43.6	1.7	7.6	-18.8
20TH	210.00	21.3	-5.6	2303	1039	9.2	-5.4	27	101	162.1	-38.0	1.3	5.9	-16.5
215T	219.75	21.8	-5.5	2303		9.5	-5.3	25	99	140.8	-32.4	1.0	4.4	-14.2
2 2 N D	229.50	22.4	-5.5	2303	1038	9.7	-5.3	23	96	119.Ŷ	-26.8	. 7	3.1	-11.9
23RD	239.25	22.4	-5.4	2303	1038	10.0	-5.2	22	93	96.6	-21.4	. 4	2.1	-9.6
24TH	249.00				1038	10.2	-5.1	20	91	73.7	-16.0	. 3	1.2	-7.3
25TH	258.75	23.5	-5.3	2303					92	50.1	-10.7	. 1	. E	-5.1
		21.6	-5.3	2303	1038	9.4	-5.1	22	72					

TABLE Wind D	7 SHEAR IRECTION	AND MONER	IT DIAGR	AMS : Configur	ATION C	N DIEGO IN	TERCONT Refei	I nent al Rence pr	HOTEL - Essure	- EAST TO 27.0 PSF	OWER OUT	GUST	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA X	(SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
MECH	268.50	28.5	-5.4	4252	1017		- 2 - 0	19		28.5	-5.4	. Q	. 3	-3.0
TOP	286.50	20.J	-3.4	4292	1917	6.7	-2.0	17	101	0.0	0 .0	0 .0	Q.Q	Q .Q

TABLE Wind D	7 SHEAR IRECTION	AND NOME	NT DIAGR	ANS : CONFIGUR	ATION C	AN DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL Ressure	EAST T 27.0 PSF	OVER OUT	GUST FA	CTOR 1.3	32
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCE X	H (FT) Y	SHEAR X	(KIPS) Y	NONENT (X	1000-FT- Y	-KIPS) Z
15 T	0.00							5 4	-95	333.6	-128.5	22.1	54.1	-35.2
2ND	17.00	-4.4	-2.3	2034	876	-2.2	-2.7	50		338.0	-126.1	19.9	48.3	-34.6
3RD	34.00	-7.5	-2.5	2034	876	-3.7	-2.9	16	-49	345.5	-123.6	17.8	42.5	-34.2
4TH	54.00	-2.6	-8.1	2743		-1.0	-6.8	129	-42	348.1	-115.5	15.4	35.6	-33.1
STH	63.75	20.1	~.5	2303		8.7	4	1	50	328.0	-115.1	14.3	32.3	-32.0
6TH	73.50	19.4	8	2303	1038	8.4	8	2	55	308.7	-114.2	13.2	29.2	-31.0
7TH	83.25	19.1	-1.9	2303	1038	8.3	-1.8	6	59	289.5	-112.3	12.1	26.3	-29.8
8TH	93.00	18.9	-3.0	2303	1038	8.2	-2.9	10	63	270.6	-109.3	11.0	23.6	-28.6
9TH	102.75	18.7	-4.1	2303	1038	8.1	-3.9	14	66	251.9	-105.2	9.9	21.0	-27.3
10TH	112.50	18.4	-4.9	2303	1038	8.0	-4.7	18	68	233.5	-100.3	8.9	18.6	-26.0
		17.6	-5.2	2303	1038	7.6	-5.0	21	72	215.9	-95.2	8.0	16.4	-24.6
11TH	122.25	16.9	-5.4	2303	1039	7.3	-5.2	24	76	199.1	-89.8	7.1	14.4	-23.2
12TH	132.00	16 . 1	-5.6	2303	1038	7.0	-5.4	28	79	183.0	-84.2	6.2	12.6	-21.8
13TH	141.75	15.4	-5.8	2303	1038	6.7	-5.6	31	83	167.6	-78.4	5.4	10.9	-20.3
14TH	151.50	13.8	-5.4	2303	1038	6.0	-5.2	37	94			4.7	9.3	-18.8
15TH	161.25	11.7	-4.2	2303	1038	5.1	-4.0	42	116	153.8	-73.0			-17.3
16TH	171.00	11.9	-4.7	2303	1038	5.2	-4.5	44	113	142.1	-68.8	4.0	7.8	
17TH	180.75	12.2	-5.2	2303	1038	5.3	-5.0	47	110	130.2	-64.1	3.4	6.5	-15.7
18TH	190.50	12.4	-5.7	2303	1038	5.4	-5.5	48	106	118.0	-58.9	2.8	5.3	-14.2
19TH	200.25	12.7	-6.1	2303	1038	5.5	-5.9	50	103	105.6	-53.2	2.2	4.2	-12.6
20TH	210.00	12.9	-6.2	2303	1038	5.6	-6.0	48	100	92.9	-47.1	1.7	3.3	-11.0
21ST	219.75			2303		5.7	-6.0	46	97	79.9	-40.9	1.3	2.4	-9.4
22ND	229.50	13.2	-6.3				-6.1	44	94	66.7	-34.6	. 9	1.7	-7.8
23RD	239.25	13.4	-6.3	2303		5.8				53.3	-28.3	. 6	1.1	-6.2
24TH	249.00	13.7	-6.4	2303		5.9	-6.1	43	92	39.6	-21.9	. 4	. 7	-4.7
25TH	258.75	13.9	-6.4	2303		6.0	-6.2	41	89	25.7	-15.5	. 2	. 3	-3.2
		10.5	-6.8	2303	1039	4.6	-6.5	56	38					

TABLE Vind D	7 SHEAR IRECTION	AND MOMEN 240	IT DIAGR	ANS : SAN Configuration C	DIEGO IN	TERCONT REFE	INENTAL HOTEL	- EAST TO 27.0 PSF	DWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHE AR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
NECH	268.50		-8.8	4252 1917	3.6	-4.6	54 94	15.2	- 8 . 8	. 1	. 1	-1.9
TOP	286.50	15.2	-0.0	4232 1717	3.4	- 4.0		Q , Q	0.0	Q .Q	9.0	Q.Q

TABLE Wind D	7 SHEAR	AND MONEN	T DIAGR	ANS : Configura	SAI TION C	N DIEGO I	NTERCONT : Refei	INENTAL Rence P	HO TEL RESSURE	27.0 PSF	OWER OUT	GUST FA	CTOR 1.3	2
FLOOR	HEIGHT	FORCE	(∦IPS) Y	AREA (X	SQ FT) Y	PRESSUR	E (PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT (X	1000-FT- Y	KIPS) Z
1 S T	0 .00						4 5			10.6	-154.1	27.2	6.9	-9.3
2ND	17.00	-16.3	1.3	2034	876	-8.0	1.5	- 1	-11	26.9	-155.4	24.6	6.6	-9.1
3RD	34.00	-17.9	1.2	2034	876	-8.8	1.3	-0	-1	44.8	-156.5	22.0	6.0	-9.1
4TH	54.00	-18.9	-5.1	2743	1195	-6.9	-4.3	6	-23	63.7	-151.4	18.9	4.9	-8.7
5TH	63.75	5.6	-3.4	2303	1038	2.4	-3.3	8	14	58.1	-148.1	17.4	4.3	-8.6
6TH	73.50	5.4	-3.6	2303	1038	2.3	-3.5	13	20	52.7	-144.5	16.0	3.8	-8.4
7TH	83.25	5.2	-4.5	2303	1038	2.3	-4.3	20	24	47.5	-140.0	14.6	3.3	-8.2
8TH	93.00	5.0	-5.4	2303	1038	2.2	-5.2	28	26	42.4	-134.6	13.3	2.8	-7.9
9TH	102.75	4.9	-6.3	2303	1038	2.1	-6.0	34	27	37.6	-128.4	12.0	2.4	-7.6
10TH	112.50	4.6	-6.9	2303	1039	2.0	-6.7	39	26	32.9	-121.5	10.8	2.1	-7.2
1 1 T H	122.25	4.2	-6.9	2303	1039	1.8	-6.7	42	26	28.7	-114.5	9.6	1.8	-6.8
	132.00	3.8	-6.9	2303	1038	1.7	-6.7	46	25	24.8	-107.6	8.5	1.5	-6.3
1278		3.4	-6.9	2303	1038	1.5	-6.7	50	24	21.4	-100.6	7.5	1.3	-5.9
13TH	141.75	3.0	-7.0	2303	1038	1.3	-6.7	53	23	18.4	-93.7	6.6	1.1	-5.5
14TH	151.50	2.1	-6.2	2303	1038	. 9	-5.9	61	21		-87.5	5.7	. 9	-5.1
15TH	161.25	. 8	-4.5	2303	1038	. 3	-4.3	78	14	16.2				-4.7
16TH	171.00	. 9	-5.2	2303	1038	. 4	-5.1	70	13	15.4	-03.1	4.9	. 8	
1778	180.75	1.1	-6.0	2303	1038	. 5	-5.8	64	12	14.5	-77.8	4.1	. 6	-4.3
18TH	190.50	1.3	-6.8	2303	1038	. 5	- 5 5	60	11	13.4	-71.8	3.3	. 5	-3.9
19TH	200.25	1.4	-7.6	2303	1038	. 6	-7.3	56	10	12.1	-65.0	2.7	. 4	-3.5
20TH	210.00	1.7	-7.7	2303	1038	. 7	-7.4	56	12	10.7	-57.4	2.1	. 3	-3.1
21ST	219.75	2.0	-7.8	2303	1039	. 8	-7.5	56	14	9.1	-49.7	1.6	. 2	-2.6
22ND	229.50	2.2	-7.9	2303	1038	1.0	-7.6	55	16	7.1	-41.9	1.1	- 1	-2.1
2 3 R D	239.25				1038	1.1	-7.6	54	17	4.9	-34.1	. 7	. ¢	-1.7
24TH	249.00	2.5	-7.9	2303			-7.7	54	19	2.4	-26.2	. 4	. 0	-1.2
25TH	258.75	2.8	-8.0	2303	1038	1.2				4	-18.1	. 2	0	7
		1	-8.2	2303	1039	0	-7.9	37	- 0					

TABLE Wind D	7 SHEAR IRECTION	AND NOMEN 250	T DIAGR	ANS : SAN Configuration C	DIEGO IN	TERCONT I REFER	NENTAL Ence pri	HOTEL - Essure	- EAST TO 27.0 PSF	WER OUT	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE X	(PSF) Y	ECCEN X		SHE AR X	(KIPS) Y	NONENT X	(1000-FT-) Y	KIPS) Z
MECH	268.50	3	-9.9	4252 1917	1	- 5 3	42	- 1	3	-9.9	. 1	¢	4
TOP	286.50		- 7.7	4232 171:	1	- J. 2	42	-1	0.0	0.0	Q.Q	0.0	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND NONEN	(T DIAGR	ANS : CONFIGURA	TION C	N DIEGO IN	TERCONT	INENTAL Rence Pi	HOTEL Ressure	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS)	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEI	N (FT)	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00									-133.2	-154.3	28.2	-13.1	17.5
210	17.00	-22.5	4.2	2034	876	-11.1	4.8	2	10	-110.7	-158.5	25.6	-11.0	17.3
380	34.00	-23.2	4.3	2034	876	-11.4	4.9	3	15	-87.5	-162.8	22.8	-9.3	16.9
4TH	54.00	-26.7	8	2743	1195	-9.7	7	-0	12	-60.8	-162.0	19.6	-7.8	16.6
	63.75	-2.1	-5.4	2303	1038	9	-5.2	-128	50	-58.7	-156.6	18.0	-7.3	15.8
5TH		-2.0	-5.5	2303	1038	9	-5.3	-127	46	-56.7	-151.1	16.5	-6.7	15.0
6TH	73.50	-1.8	-5.9	2303	1038	9	-5.6	-115	36	-54.8	-145.2	15.1	-6.2	14.3
7TH	83.25	-1.7	-6.3	2303	1039	7	-6.9	-104	28	-53.2	-139.0	13.7	-5.6	13.6
8TH	93.00	-1.5	-6.7	2303	1038	7	-6.4	-94	22	-51.6	-132.3	12.4	-5.1	12.9
9T H	102.75	-1.4	-6.9	2303	1038	6	-6.7	-86	18	-50.2	-125.4	11.1	-4.6	12.3
1 Q T H	112.50	-1.5	-6.9	2303	1038	6	-6.7	-87	18	-48.7	-118.5	10.0	-4.1	11.7
11TH	122.25	-1.5	-6.9	2303	1038	7	-6.6	-87	19	-47.2	-111.6	8.8	-3.7	11.1
12TH	132.00	-1.5	-6.8	2303	1038	7	-6.6	-87	20	-45.7	-104.7	7.8	-3.2	10.4
13TH	141.75	-1.6	-6.8	2303	1038	7	-6.6	-87	20			6.8	-2.8	9.8
14TH	151.50	-2.5	-6.3	2303	1038	-1.1	-6.1	-93	37	-44.1	-97.9		-2.4	9.1
15TH	161.25	-4.5	-5.4	2303	1038	-2.0	-5.2	-89	74	-41.6	-91.6	5.9		8.3
16TH	171.00	-4.1	-6.0	2303	1038	-1.8	-5.8	-90	62	- 37 . 1	-86.2	5.0	-2.0	7.5
17TH	180.75	-3.7	-6.6	2303	1038	-1.6	-6.3	-89	50	-33.0	-80.3	4.2	-1.6	
18TH	190.50	-3.3	-7.1	2303	1038	-1.4	-6.9	-86	40	-29.3	-73.7	3.4	-1.3	6.8
19TH	200.25		-7.7	2303	1038	-1.3	-7.4	-82	31	-26.0	-66.6	2.8	-1.1	6.0
2 Q T H	210.00	-2.9		2303	1038	-1.3	-7.5	-79	30	-23.1	-58.9	2.1	~.8	5.3
215T	219.75	-3.0	-7.8					-76	29	-20.1	-51.1	1.6	6	4.6
22ND	229.50	-3.0	-7.9	2303	1038	-1.3	-7.6			-17.1	-43.1	1.1	4	3.9
23RD	239.25	-3.0	-8.0	2303	1038	-1.3	-7.7	-73	28	-14.¢	-35.1	. 8	3	3.2
2478	249.00	-3.1	-8.1	2303	1038	-1.3	-7.8	-70	27	-11.0	-27.0	. 5	2	2.6
25TH	258.75	-3.1	-8.2	2303	1038	-1.3	-7.9	-68	25	-7.9	-18.8	. 2	1	1.9
EUIII	200.00	-5.6	-8.4	2303	1038	-2.4	- 8.1	-63	42					

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN	T DIAGR	ANS : Configur	ATION C	I DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL - Essure	- EAST TO 27.0 PSF	DWER OUT	GUST I	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y		(SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NONENT	(1000-FT-) Y	KIPS) Z
MECH	268.50	. 5 7	-10.4	4252	1917	5		100	0.7	-2.3	-10.4	. 1	0	1.2
TOP	286.50	÷∠.3	-10.4	4232	1716	3	-3.4	-108	23	0 .0	0.0	Q.Q	\$.0	Q.Q

TABLE VIND D	7 SHEAR IRECTION	AND NOMEN	T DIAGR	AMS : Configura		N DIEGG IN	TERCONT REFE	INENTAL Rence Pr	HOTEL	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS)	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT)	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00						6.1	3	16	-318.7	-152.8	28.3	-39.9	42.3
2ND	17.00	-26.8	5.4	2034	876	-13.2			23	-291.9	-158.2	25.6	-34.7	41.8
3RD	34.00	- 26 . 7	6.4	2034	876	-13.1	7.3	5		-265.2	-164.6	22.9	-30.0	41.2
4TH	54.00	-34.5	2.9	2743	1195	-12.6	2.5	2	28	-230.7	-167.5	19.6	-25.0	40.2
5TH	63.75	-11.2	-7.6	2303	1038	- 4 . 8	-7.3	-64	94	-219.5	-159.9	18.0	-22.8	38.7
6TH	73.50	-10.8	-7.6	2303	1038	-4.7	-7.3	-68	97	-208.7	-152.4	16.5	-20.7	37.1
7TH	83.25	-10.9	-7.1	2303	1038	-4.7	-6.8	-66	102	-197.8	-145.3	15.0	-18.7	35.5
8TH	93.00	-11.1	-6.6	2303	1039	-4.6	-6.4	-63	106	-186.8	-138.7	13.6	-16.9	33.9
9TH	102.75	-11.2	-6.1	2303	1038	-4.9	-5.9	-60	111	-175.5	-132.6	12.3	-15.1	32.3
		-11.2	-5.8	2303	1038	-4.9	-5.6	-59	114	-164.3	-126.8	11.0	-13.4	30.7
1078	112.54	-10.8	-6.0	2303	1038	-4.7	~ 5 . 8	-64	116	-153.5	-120.8	9.8	-11.9	29.1
11TH	122.25	-10.4	-6.2	2303	1038	-4.5	-5.9	-70	118	-143.1	-114.6	8.7	-10.4	27.4
1278	132.00	-9.9	-6.4	2303	1039	-4.3	-6.1	-76	119	-133.2	-108.2	7.6	-9.1	25.8
13TH	141.75	-9.5	-6.5	2303	1038	-4.1	- 6.3	-82	120	-123.7	-101.7	6.6	-7.8	24.1
14TH	151.50	-9.2	-7.2	2303	1038	-4.0	-6.9	-91	117	-114.5	-94.5	5.6	-6.7	22.3
15TH	161.25	-9.5	-8.3	2303	1038	-4.1	-8.0	-97	112	-105.0	-86.2	4.7	-5.6	20.5
16TH	171.00	-9.6	-8.0	2303	1038	-4.2	-7.7	-95	114		-78.2	3.9	-4.6	18.6
17TH	180.75	-9.7	-7.8	2303	1038	-4.2	-7.5	-94	116	-95.4		3.2	-3.8	16.8
18TH	190.50	-9.7	-7.5	2303	1038	-4.2	-7.2	-92	118	-85.7	-79.4		-3.0	14.9
19TH	200.25	-9.8	-7.3	2303	1038	-4.2	-7.0	-90	120	-76.0	-62.9	2.6		
20TH	210.00	-9.7	-7.4	2303	1038	-4.2	-7.2	-90	117	-66.2	~55.6	2.0	-2.3	13.1
21ST	219.75	-9.6	-7.6	2303	1038	-4.2	-7.3	-91	114	- 56 . 5	~48.2	1.5	-1.7	11.3
2 2 N D	229.50	-9.5	-7.8	2303	1038	-4.1	-7.5	-91	111	-47.0	~40.6	1.0	-1.2	9.5
2 3 R D	239.25	-9.4	-7.9	2303	1038	-4.1	-7.7	-91	108	- 37 . 5	-32.8	. 7	- .8	7.7
24TH	249.00			2303	1038	-4.0	-7.8	-92	105	- 28 . 0	-24.9	. 4	4	6.0
25TH	258.75	-9.3	-8.1				-7.6	-80	105	-18.7	~16.7	. 2	2	4.3
		-10.4	-7.9	2303	1038	-4.5	- (.9	-64	103					

TABLE WIND D	7 SHEAR IRECTION	AND HONEN 270	IT DIAGRI	AMS : SAN Configuration C	DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure 2	EAST TO	DWER OUT	GUST F	FACTOR 1.32	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE		ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NONENT X	(1090-FT-1 Y	(IPS) Z
MECH	268.50	-8.3	-8.8	4252 1917	-2.0	-4 5	-152 144	-8.3	- 8 . 8	. 1	1	2.5
TOP	286.50	-0.3	-0.0	4232 1917	-2.0	- 4.8	-152 144	Ģ.Ģ	Ŷ.Ŷ	¢,¢	2.0	¢.¢

TABLE WIND D	7 SHEAR IRECTION	AND NOMEN	T DIAGR	ANS : Configura	SP TION C	IN DIEGO IN	TERCONT REFE	INENTAL Rence P	HOTEL Ressure	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT		(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCE X	N (FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00							-	16	-515.6	-142.1	26.6	-70.8	56.0
210	17.00	-30.5	5.7	2034	876	-15.0	6.5	3		-485.2	-147.8	24.1	-62.3	55.5
380	34,00	-31.5	7.6	2034	876	-15.5	8.7	6	23	-453.7	-155.4	21.5	-54.4	54.7
4TH	54.00	-41.5	6.6	2743	1195	-15.1	5.6	5	33	-412.1	-162.0	18.4	-45.7	53.3
		-17.6	-8.0	2303	1039	-7.6	-7.7	-38	84	-394.6	-154.0	16.8	-41.8	51.5
5TH	63.75	-17.5	-8.3	2303	1039	-7.6	-8.0	-41	96	-377.0	-145.7	15.3	-38.0	49.7
6TH	73.50	-18.0	-7.3	2303	1038	-7.8	-7.1	-37	91	-359.0	-138.4	14.0	-34.4	47.8
7TH	83.25	-18.5	-6.3	2303	1038	-8.0	-6.1	-32	95	-340.5	-132.0	12.6	-31.0	45.8
8T H	93.00	-19.0	-5.3	2303	1038	-8.2	-5.1	-28	99	-321.6	-126.7	11.4	-27.8	43.8
9T H	102.75	- 19.3	-4.7	2303	1039	-8.4	-4.5	-25	102				-24.7	41.7
10TH	112.50	-19.0	-5.1	2303	1039	-8.3	-4.9	-28	104	-302.3	-122.0	10.2		
11TH	122.25	-19.8	-5.4	2303	1038	-8.2	-5.2	-31	107	-283.3	-116.9	9.0	-21.9	39.6
12TH	132.00		-5.8	2303	1038	-8.1	-5.6	-34	110	-264.4	-111.5	7.9	-19.2	37.4
13TH	141.75	-18.6		2303	1038	-8.0	-5.9	-37	112	-245.8	-105.7	6.8	-16.7	35.2
14TH	151.50	-19.4	-6.1				-7.6	-48	109	-227.4	-99.6	5.8	-14.4	32.9
15TH	161.25	-18.1	-7.9	2303	1038	-7.8				-209.3	-91.7	4.9	-12.3	30.5
16TH	171.00	-17.6	-11.1	2303	1039	-7.7	-10.7	-62	98	-191.7	-80.6	4.1	-10.3	28.1
1778	180.75	-17.5	-10.0	2303	1038	-7.6	-9.5	-60	105	-174.2	-70.6	3.3	-8.5	25.7
1878	190.50	-17.4	-8.9	2303	1038	-7.6	-8.5	-57	112	-156.8	-61.8	2.7	-6.9	23.2
		-17.3	-7.7	2303	1038	-7.5	-7.5	-53	119	-139.5	-54.1	2.1	-5.5	20.8
19TH	200.25	-17.2	-6.6	2303	1038	-7.5	-6.4	-49	126	-122.3	-47.4	1.6	-4.2	18.3
20TH	210.00	-17.4	-6.7	2303	1038	-7.5	-6.5	-48	125	-104.9	-40.7	1.2	-3.1	15.8
215T	219.75	-17.6	-6.8	2303	1038	-7.6	-6.6	-48	124	-87.3	-33.8	. 8	-2.2	13.3
22ND	229.50	-17.7	-6.9	2303	1038	-7.7	-6.7	-48	122			. 5	-1.4	10.8
2 3 R D	239.25	-17.9	-7.0	2303	1038	-7.8	-6.8	-48	121	-69.6	-26.9			8.3
24TH	249.00	-18.1	-7.1	2303	1038	-7.8	-6.9	-47	120	-51.7	-19.8	. 3	8	
25TH	258.75	-17.2	-6.8	2303	1038	-7.5	-6.6	-47	118	-33.6	-12.7	. 1	~ .4	5.8
		-16.2	-0.0	2040										

TABLE Wind D	7 SHEAR IRECTION	AND MONEN 260	T DIAGR	ANS : Configurati	ON C	DIEGO IN	TERCONT Refe	INENTAL HOTEL - Rence pressure	- EAST TI 27.0 PSF	OVER OUT	GUST I	ACTOR 1.32	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (SQ X	EFT) Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	(IPS) Z
MECH	268.50	-16.5	-5.9	4252 1	917	-3.9	-7 1	-65 183	-16.5	-5.9	. 1	1	3.4
TOP	286.50	- 18 - 7	- J. 7	4232 1	. 7 . 1	- J. 2	- J . L		Q.Q	Q.Q	Q.Q	Q.Q	¢ .¢

TABLE WIND D	7 SHEAR IRECTION	AND MONEN 290	T DIAGR	AMS : Configura	TION C	AN DIEGG IN	TERCONT Refe	INENTAL Rence Pri	HO T E L E S S UR E	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT>	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MONENT X	(1000-FT- Y	KIPS) Z
1 S T	0,00								14	-719.3	-233.4	41.6	-103.0	55.2
2N D	17.00	-35.2	4.3	2034	876	-17.3	4.9	2		-684.1	-237.7	37.6	-91.1	54.7
3RD	34.00	- 38 . 6	7.2	2034	876	-19.0	8.3	4	20	-645.5	-245.0	33.5	-79.8	53.9
4TH	54.00	-49.0	5.1	2743	1195	-17.9	4.3	3	28	-596.5	-250.1	28.6	-67.3	52.5
578	63.75	-25.6	-10.5	2303	1038	-11.1	-10.2	-25	61	-570.9	-239.6	26.2	-61.6	50.7
6TH	73.50	-25.6	-11.0	2303	1038	-11.1	-10.6	-27	62	-545.3	-228.5	23.9	-56.2	48.8
7TH	83.25	- 25 . 6	-10.4	2303	1038	-11.1	-10.0	-26	65	-519.7	-218.2	21.7	-51.0	46.9
	93.00	- 25 . 7	-9.8	2303	1038	-11.1	-9.4	-26	68	-494.0	-208.4	19.6	-46.1	44.9
8TH		-25.7	-9.1	2303	1038	-11.2	-8.8	-25	71	-468.4	-199.3	17.6	-41.4	42.8
9TH	102.75	-25.8	- 8.8	2303	1038	-11.2	-8.4	-25	73	-442.6	-190.5	15.7	-36.9	40.7
1 0 T H	112.50	-26.0	-9.2	2303	1038	-11.3	-8.8	-26	73	-416.6	-181.4	13.9	-32.7	38.6
11TH	122.25	- 26 . 2	-9.6	2303	1038	-11.4	-9.2	-27	73		-171.8	12.2	-28.8	36.4
1278	132.00	- 26 . 4	-10.0	2303	1038	-11.5	-9.6	-27	72	-390.4			-25.1	34.2
13TH	141.75	-26.6	-10.4	2303	1038	-11.5	-10.0	-28	72	-364.0	-161.8	10.6		
14TH	151.50	-26.6	-12.0	2303	1038	-11.5	-11.6	-32	70	-337.4	-151.4	9.1	-21.7	32.0
15TH	161.25	-25.8	-14.8	2303	1038	-11.2	-14.3	-38	67	-310.9	-139.4	7.6	-18.6	29.8
16TH	171.00	-25.5	-13.9	2303	1038		-13.4	-38	70	-285.1	-124.6	6.3	-15.7	27.5
17TH	180.75	-25.2	-12.9	2303	1038		-12.5	-38	74	-259.6	-110.7	5.2	-13.0	25.2
18TH	190.50		-12.0	2303	1038		-11.6	-37	77	-234.4	-97.8	4.2	-10.6	22.8
19TH	200.25				1038		-10.7	-36	81	-209.4	-85.8	3.3	-8.4	20.4
20TH	210.00	-24.7	-11.1	2303				-35	81	-184.8	-74.7	2.5	-6.5	18.0
215T	219.75	~25.2	-11.1	2303	1038		-10.7			-159.5	-63.6	1.8	-4.8	15.6
22ND	229.50	- 25 . 8	-11.1	2303	1038		-10.7	-34	80	-133.7	-52.5	1.3	-3.4	13.2
23RD	239.25	-26.4	-11.1	2303	1038		-10.7	-33	79	-107.3	-41.4	. 8	-2.2	10.7
24TH	249.00	-27.0	-11.2	2303	1038	-11.7	-10.7	-33	79	-80.3	-30.2	. 5	-1.3	8.2
25TH	258.75	- 27 . 6	-11.2	2303	1038	-12.0	-10.8	-32	78	- 52 . 7	-19.0	. 2	7	5.7
2010	200.00	- 23 . 9	-10.0	2303	1038	-10.4	-9.5	-35	82					

TABLE WIND D	7 SHEAR IRECTION	AND HONEN 290	IT DIAGRI	ANS : Configurat		DIEGO IN		INENTAL HOTEL Rence pressure 2		OWER OUT	GUST I	FACTOR 1.32	2
FLOOR	HEIGHT	F DR C E X	(KIPS) Y	AREA (S X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-) Y	(IPS) Z
MECH	268.50	-28.8	-9.1	4252	1917	-6.8	-4.7	-34 107	- 28 . 8	-9.1	. 1	3	3.4
TOP	286.50	-20.0	-7.1	7232	1717	- 5 . 5	- 4 . 7	-34 197	Q .Q	0.0	Q.Q	Q.Q	Q.Q

TABLE WIND D	7 SHEAR IRECTION	AND NOMEN	NT DIAGR	AMS : Configur	ATION C	N DIEGO IN	TERCONT REFE	INENTAL Rence pr	HOTEL Essure	EAST T 27.0 PSF	OVER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA	(SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHE AR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00			.		64 Å	7 0		9	-903.7	-330.4	58.3	-129.4	48.8
2ND	17.00	- 42 . 8	2.8	2034	876	-21.0	3.2	1		-860 9	-333.2	52.7	-114.4	48.5
3RD	34.00	- 46 . 9	5.3	2034	876	-23.0	6.1	2	14	-814.0	-338.6	47.¢	-100.2	47.8
4TH	54.00	- 59 . 7	2.3	2743		-21.4	2.0	1	20	-755.4	-340.9	40.2	-84.5	46.6
578	63.75	- 35 . 8	-12.2	2303	1039	-15.5	-11.7	-15	44	-719.6	-328.7	36.9	-77.3	44.8
6TH	73.50	-35.6	-12.8	2303	1038	-15.5	-12.4	-16	45	-684.0	-315.9	33.8	-79.4	43.0
	83.25	-34.6	-12.8	2303	1038	-15.0	-12.3	-17	47	-649.3	-303.1	30.8	-63.9	41.2
7TH	93.00	- 33 . 7	-12.8	2303	1038	-14.6	-12.3	-19	49	-615.7	-290.3	27.9	-57.8	39.3
8TH	102.75	-32.7	-12.7	2303	1038	-14.2	-12.3	-20	52	-583.0	-277.6	25.1	-51.9	37.3
9TH		-32.0	-12.8	2303	1038	-13.9	-12.3	-21	53	-550.9	-264.8	22.5	-46.4	35.3
10TH	112.50	- 32 . 2	-13.3	2303	1038	-14.0	-12.8	-22	53	-518.8	-251.5	20.0	-41.2	33.3
11TH	122.25	- 32 . 3	-13.7	2303	1038	-14.0	-13.2	-22	52	-486.4	-237.8	17.6	-36.3	31.3
1278	132.00	- 32 . 5	-14.2	2303	1038	-14.1	-13.6	-22	51	-453.9	-223.7	15.3	-31.7	29.4
13TH	141.75	- 32 . 7	-14.6	2303	1038	-14.2	-14.1	-23	51	-421.2	-209.0	13.2	-27.4	27.4
14TH	151.50	-33.2	-15.6	2303	1038	-14.4	-15.0	-23	49	-388.0	-193.5	11.2	-23.5	25.4
15TH	161.25	-33.6	-17.0	2303	1038	-14.6	-16.4	-24	47	-354.4	-176.4	9.4	-19.9	23.4
16TH	171.00	- 32 . 5	-16.8	2303	1038	-14.1	-16.2	-25	49	-321.9	-159.6	7.8	-16.6	21.4
17TH	180.75	-31.4	-16.5	2303	1038	-13.6	-15.9	-26	50	-290.5	-143.1	6.3	-13.6	19.4
18TH	190.50	-30.4	-16.2	2303	1038	-13.2	-15.6	-28	52	-260.1	-126.9	5.0	-10.9	17.3
19TH	200.25	-29.3	-16.0	2303	1038	-12.7	-15.4	-29	54	-230.8	-110.9	3.9	-8.5	15.3
2 Q T H	210.00	-29.9	-16.0	2303	1038	-13.0	-15.4	-29	53			2.8	-6.4	13.2
215T	219.75	-30.4	-15.9	2303	1038	-13.2	-15.4	-28	53	-200.9	-95.0			11.2
22ND	229.50	-31.0	-15.9	2303	1038	-13.5	-15.3	-27	53	-170.5	-79.0	2.0	-4.6	
2 3 R D	239.25	-31.6	-15 9	2303	1038	-13.7	-15.3	-27	53	-139.5	-63.1	1.3	-3.1	9.1
24TH	249.00	- 32 . 1	-15.9	2303	1038		-15.3	-26	52	-108.0	-47.2	. 8	-1.9	7.0
25TH	258.75	-31.4		2303			-13.8	-24	52	-75.9	-31.2	. 4	-1.0	4.9

TABLE Wind D	7 SHEAR IRECTION	AND MONENT D	DIAGRANS : Configur		DIEGO IN	TERCONT Refei	INENTAL HOTEL Rence pressur	E 27.0 PSF	OWER OUT	GUST F	FACTOR 1.32	2
FLCOR	HEIGHT	FORCE (KI X	Y AREA X	(SQ FT) Y	PRESSURE X	(PSE) Y	ECCEN (FT)	SHEAR X	(KIPS) Y	NOMENT X	€1000-FT-K Y	(IPS) Z
MECH	268.50	-44.5 -1	16.9 4252	1917	-10.5	-8.8	-22 58	-44.5	-16.9	. 2	4	3.0
TOP	286.50	-44.3 -1	10.7 4636		14.5	v . v		0.0	0.0	0.0	ð. Ó	ð. Ó

TABLE Wind D	7 SHEAR I IRECTION	AND MOMEN 310	NT DIAGRA	AMS ; Configura	TION C	DIEGO IN	TERCONT REFE	INENTAL I Rence pri	HO T E L E S S U R E	EAST T 27.0 PSF	OVER OUT	GUST F	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT>	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00		_					•		-1082.3	-292.4	51.1	-157.4	38.4
2ND	17.00	-46.2	1.2	2034	876	-22.7	1.3	0	6	-1036.0	-293.6	46.1	-139.4	38.1
380	34.00	-49.3	3.5	2034	876	-24.2	4.0	1	10	-986.7	-297.1	41.1	-122.2	37.6
411	54.00	-62.6	. 7	2743	1195	-22.8	. 6	٥	14	-924.1	-297.7	35.2	-103.1	36.7
578	63.75	-43.1	-10.9	2303	1038	-18.7	-10.5	- 8	30	-881.0	-286.9	32.3	-94.3	35.4
		- 42 . 9	-11.4	2303	1038	-18.6	-11.0	- 8	31	-838.1	-275.4	29.6	-85.9	34.0
6TH 	73.50	-42.0	-11.4	2303	1038	-18.3	-11.0	- 9	32	-796.1	-264.0	26.9	-78.0	32.5
7TH	83.25	-41.2	-11.3	2303	1038	-17.9	-10.9	- 9	34	-754.9	-252.7	24.4	-70.4	31.0
8T H	93.00	-40.4	-11.3	2303	1038	-17.5	-10.9	-10	36	-714.5	-241.5	22.0	-63.2	29.4
9T H	102.75	-39.8	-11.3	2303	1038	-17.3	-10.9	-11	37	-674.7	-230.1	19.7	-56.5	27.8
1 ¢ T H	112.50	- 39 . 8	-11.7	2303	1038	-17.3	-11.2	-11	37	-634.9	-218.5	17.5	-50.1	26.2
11TH	122.25	- 39.9	-12.0	2303	1039	-17.3	-11.6	-11	36	-595.0	-206.5	15.5	-44.1	24.6
12TH	132.00	- 39 . 9	-12.4	2303	1038	-17.3	-11.9	- i i	36	-555.1	-194.1	13.5	-38.5	23.1
13TH	141.75	-40.0	-12.7	2303	1039	-17.3	-12.3	-11	36			11.7	-33.3	21.5
14TH	151.50	-40.8	-13.4	2303	1038	-17.7	-12.9	-11	35	-515.1	-181.4		-28.4	19.9
1 5 T H	161.25	- 42.0		2303	1038	-18.2	-13.7	-11	33	-474.3	-168.0	10.0		18.4
16TH	171.00	-40.5		2303	1038	-17.6	-13.5	-12	35	-432.3	-153.8	8.4	-24.0	
17TH	180.75	- 39.1		2303	1038		-13.3	-13	36	-391.8	-139.7	7.0	-20.0	16.8
18TH	190.50		-13.7	2303	1038		-13.2	-13	37	-352.7	-125.9	5.7	-16.4	15.2
19TH	200.25			2303	1039	-15.7	-13.0	-14	39	-315.0	-112.2	4.5	-13.1	13.6
2 Q T H	210.00		-13.5		1038	-16.0	-13.2	-14	39	-278.7	-98.7	3.5	-10.2	12.0
21ST	219.75	- 36 . 7		2303				-14	39	-242.0	-85.0	2.6	-7.7	10.4
2 2 N D	229.50	- 37 . 2	-13.8	2303	1039		-13.3			-204.8	-71.2	1.8	-5.5	8.8
2 3 R D	239.25	-37.7		2303	1038	-16.4	-13.4	-14	39	-167.1	-57.3	1.2	-3.7	7.1
24TH	249.00	- 38 . 2	-14.1	2303	1038	-16.6	-13.5	-14	39	-128.9	-43.2	. 7	-2.2	5.5
25TH	258.75	- 38 . 6	-14.2	2303	1038	-16.8	-13.7	-14	39	-90.3	-29.0	. 4	-1.2	3.8
2018		- 37 . 7	-12.6	2303	1038	-16.4	-12.2	-12	37					

TABLE Wind D	7 SHEAR IRECTION	AND MOMENT DIAGRA	NS : SAN Configuration C	DIEGO IN	REFE	INENTAL HOTEL Rence pressure 2	EAST TO	DWER OUT	GUST F	ACTOR 1.32	
FLOOR	HEIGHT	FORCE (KIPS) X Y	AREA (SQ FT) X Y	PRESSURE X	(PSF) Y	ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-K Y	IPS) Z
MECH	268.50	-52 5 -16 4	4252 1917	-12.4	-8.5	-12 39	-52.5	-16.4	. 1	5	2.2
TOP	286.50	-52.5 -16.4	7232 1717	- 16.7	.	12 37	Q.Q	Q.Q	¢.¢	\$.0	Q.Q

TABLE Wind D	7 SHEAR IRECTION	AND NOMEN	T DIAGRA	NS : Configura	SAN Tion C	DIEGO IN	ITERCONT REFE	INENTAL Rence Pr	HOTEL Essure	EAST T 27.0 PSF	OVER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00		F	2034	876	-22.4	6	- 0	5	-1271.0	-224.2	39.9	-192.3	28.7
2ND	17.00	- 45.5	5				2.3	ò	9	-1225.5	-223.7	36.1	-171.0	28.5
3RD	34.00	-48.1	2.0	2034	876	-23.7				-1177.4	-225.8	32.3	-150.6	28.1
4TH	54.00	-65.1	1.1	2743	1195	-23.8	. 9	0 _	11	-1112.2	-226.9	27.8	-127.7	27.4
5TH	63.75	-49.0	-7.0	2303	1038	-21.3	-6.7	- 3	19	-1063.2	-219.9	25.6	-117.1	26.4
		-48.5	-7.3	2303	1038	-21.0	-7.1	- 3	19	-1014.7	-212.5	23.5	-107.0	25.5
6TH	73.50	- 47 . 3	-7.5	2303	1038	-20.5	-7.2	- 3	20	-967.5	-205.0	21.5	-97.3	24.5
7TH	83.25	-46.1	-7.7	2303	1038	-20.0	-7.4	- 4	22	-921.4	-197.4	19.5	-88.1	23.5
8T H	93.00	-44.8	-7.8	2303	1038	-19.5	-7.5	- 4	23	-876.6	-189.6	17.6	-79.4	22.4
9T H	102.75	-44.1	-8.0	2303	1038	-19.2	-7.7	- 4	24	-832.4	-181.5	15.8	-71.0	21.3
1 O T H	112.50	-44.9	-8.5	2303	1038	-19.5	-8.2	- 5	24		-173.0	14.1	-63.1	20.2
11TH	122.25	-45.6	-8.9	2303	1038	-19.8	-8.6	- 5	24	-787.6			-55.7	19.0
12TH	132.00	-46.3	-9.4	2303	1038	-20.1	-9.1	- 5	24	-742.0	-164.1	12.4		17.8
13TH	141.75	-47.0	-9.9	2303	1038	-20.4	-9.5	- 5	25	-695.7	-154.7	10.9	-48.7	
14TH	151.50		-10.4	2303	1038	-21.1	-10.1	- 5	24	-648.6	-144.8	9.4	-42.1	16.6
15TH	161.25	- 48 . 6				-22.0	-10.6	- 5	23	-600.0	-134.4	8.1	-36.0	15.4
16TH	171.00	-50.7	-11.0	2303	1038			_	23	-549.3	-123.4	6.8	-30.4	14.2
17TH	180.75	-50.0	-11.0	2303	1038	-21.7	-10.6	-5		-499.2	-112.4	5.7	-25.3	13.0
1878	190.50	- 49 . 3	-11.0	2303	1038	-21.4	-10.6	- 5	24	-449.9	-101.4	4.6	-20.7	11.7
19TH	200.25	-48.6	-11.1	2303	1038	-21.1	-10.7	- 6	24	-401.2	-90.3	3.7	-16.5	10.5
		- 47 . 9	-11.1	2303	1038	-20.8	-10.7	- 6	25	-353.3	-79.2	2.9	-12.9	9.2
20TH	210.00	- 47.9	-11.0	2303	1038	-20.8	-10.6	- 6	25	-305.4	-68.2	2.1	-9.6	8.0
2157	219.75	-47.9	-11.0	2303	1038	-20.8	-10.6	- 6	25	-257.4	-57.2	1.5	-6.9	6.7
22ND	229.50	- 47.9	-10.9	2303	1039	-20.8	-10.5	- 6	25		-46.3	1.0	-4.6	5.5
2 3 R D	239.25	-47.9	-10.8	2303	1038	-20.8	-10.4	- 6	25	-209.5			-2.8	4.2
24TH	249.00	-47.9	-10.8	2303	1038	-20.8	-10.4	- 6	25	-161.6	-35.5	. 6		
2 5 T H	258.75	-47.4		2303	1038	-20.6	-9.8	- 5	24	-113.6	-24.7	. 3	-1.5	3.0
		- 41.4	1.4.1											

TABLE Wind D	7 SHEAR IRECTION	AND NOME 320	NT DIAGR	AMS : Configur:		I DIEGO IN	TERCONT Refe	INENTAL Rence pr	HOTEL - Essure	- EAST T 27.0 PSF	OWER OUT	GUST	FACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NONENT X	(1000-FT- Y	KIPS) Z
MECH	268.50		-66.2 -14.6	4252	1917	-15.6	-7.6	- 6	25	-66.2	-14.6	. 1	6	1.8
TOP	286.50	-68.2		4232	1717	-13.6	- (. 6	- 6	23	0.0	0.0	0.0	0 .0	0 .0

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN 330	T DIAGR	AMS : Configurf	SA TION C	N DIEGG IN	TERCONT Refe	INENTAL Rence Pr	HOTEL Essure	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00	- 42 . 7	5	2034	876	-21.0	- 6	- 0	6	-1320.0	-113.4	21.4	-203.1	16.2
2 N D	17.00	-43.8	1.9	2034	876	-21.5	2.1	0	9	-1277.2	-112.8	19.5	-181.0	16.0
3 R D	34.00	-60.4	2.1	2743	1195	-22.0	1.7	٥	9	-1233.4	-114.7	17.6	-159.7	15.6
4 T H	54.00		-2.6	2303	1038	-22.3	-2.5	- 1	10	-1173.0	-116.8	15.3	-135.6	15.0
5TH	63.75	-51.3					-2.8	- 1	11	-1121.7	-114.2	14.1	-124.4	14.5
6TH	73.50	-50.8	-2.9	2303	1038	-22.1			12	-1070.9	-111.2	13.0	-113.7	13.9
7 T H	83.25	- 49 . 4	-3.1	2303	1038	-21.4	-3.0	-1		-1021.6	-108.1	12.0	-103.5	13.3
8T H	93.00	- 47.9	-3.2	2303	1038	-20.8	-3.1	- 1	12	-973.6	-105.0	10.9	-93.8	12.7
9T H	102.75	-46.5	-3.3	2303	1038	-20.2	-3.2	- 1	13	-927.2	-101.6	9.9	-84.5	12.1
1¢TH	112.50	-45.6	-3.5	2303	1038	-19.8	-3.4	- 1	13	-881.5	-98.1	9.0	-75.7	11.5
11TH	122.25	-46.5	-3.9	2303	1038	-20.2	-3.7	- 1	13	-835 1	-94.3	8 ¢	-67.3	10.9
1278	132.00	-47.3	-4.2	2303	1039	-20.5	-4.1	- 1	13	-787.7	-90.1	7.1	-59.4	10.2
1378	141.75	- 48 . 2	-4.6	2303	1038	-20.9	-4.4	- 1	13	-739.6	-85.5	6.3	-52.0	9.6
14TH	151.50	-49.0	-4.9	2303	1038	-21.3	-4.8	- 1	13	-690.6	-80.5	5.5	-45.0	8.9
		- 50 . 8	-5.3	2303	1038	-22.1	-5.1	- 1	13	-639.8	-75.3	4.7	-38.5	8.3
1578	161.25	- 53.4	-5.4	2303	1038	-23.2	-5.2	- 1	12	-586.4	-69.8	4.0	-32.6	7.7
16TH	171.00	- 52 . 8	-5.6	2303	1038	-22.9	-5.4	- 1	12	-533.6		3.3	-27.1	7.0
17TH	180.75	- 52 . 2	-5.7	2303	1038	-22.7	-5.5	- 1	12		-64.3		-22.1	6.4
18TH	190.50	-51.6	-5.9	2303	1038	-22.4	-5.7	- 1	12	-481.4	-58.5	2.7		5.7
19TH	200.25	- 51.1	-6.0	2303	1038	-22.2	-5.8	- 1	13	-429.7	-52.6	2.2	-17.7	
2 0 T H	210.00	-51.2	-6.1	2303	1038	-22.2	-5.9	- 2	13	-378.7	-46.6	1.7	-13.8	5.1
21ST	219.75	-51.4	-6.2	2303	1038	-22.3	-6.0	- 2	13	-327.4	-40.5	1.3	-10.3	4.4
2 2 N D	229.50	-51.5	-6.3	2303	1038	-22.4	-6.0	- 2	13	-276.1	-34.3	. 9	-7.4	3.7
2 3 R D	239.25			2303	1038	-22.4	-6.1	- 2	13	-224.6	-28.0	. 6	-4.9	3.0
24TH	249.00	-51 6	-6.4			-22.5	-5.2	- 2	14	-173.0	-21.6	. 4	-3.0	2.3
25TH	258.75	-51.8	-6.4	2303	1038					-121.2	-15.2	. 2	-1.6	1.6
		-50.7	-6.2	2303	1038	-22.0	-6.0	- 2	i 3					

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN	T DIAGR	ANS : Configurat	SAN San	DIEGO IN	TERCONT REFE	INENTAL HOTEL Rence pressure	27.0 PSF	OVER OUT	GUST F	ACTOR 1.32	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA (S X	Q FT) Y	PRESSURE	(PSF) Y	ECCEN (FT)	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-K Y	(IPS) Z
MECH	268.50	- 70 5		4252	1917	-16.6	-4.7	-2 14	-70.5	-9.0	. 1	6	1.0
TOP	286.50	-70.5 -9.0	4232	1717	-10.0	- 4.1		Q.Q	0.0	Q,Q	Q.Q	Q.Q	

TABLE Wind D	7 SHEAR IRECTION	AND MOMEN 340	T DIAGR	AMS : Configura	SAI TION C	N DIEGO IN	TERCONT Refe	INENTAL Rence pr	HOTEL Essure	EAST T 27.0 PSF	OWER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (X	SQ FT) Y	PRESSURE	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	KIPS) Z
1 S T	0.00			0.47.4	0.74			~		-1382.9	-28.9	5.5	-215.7	1.2
2 N D	17.00	-43.4	-2.4	2034	876	-21.3	-2.8	-0	4	-1339.5	-26 5	5.0	-192.5	1.0
3R D	34.00	-43.8	-1.1	2034	876	-21.6	-1.3	-0	4	-1295.7	-25.4	4.6	-170.1	. 8
4 T H	54.00	-59.5	3	2743	1195	-21.7	3	-0	2	-1236.2	-25.0	4.1	-144.8	. 7
STH	63.75	- 52 . 7	. 6	2303	1038	-22.9	. 6	- 0	- 1	-1183.5	-25.6	3.8	-133.0	. 7
6TH	73.50	- 52 . 3	. 6	2303	1038	-22.7	. 6	- 0	- 1	-1131.2	-26.2	3.6	-121.7	. 8
718	83.25	-50.4	. 4	2303	1039	-21.9	. 3	- 0	- 0	-1080.8	-26.6	3.3	-111.0	. 8
8TH	93.00	-48.6	. 1	2303	1038	-21.1	. 1	- 0	- 0	-1032.2	-26.7	3.1	-100.7	. 8
9TH	102.75	-46.7	2	2303	1038	-20.3	2	- 0	0	-985.5	-26.5	2.8	-90.8	. 8
1078	112.50	- 45 . 8	5	2303	1038	-19.9	4	- 0	ð	-939.7	-26.0	2.5	-81.4	. 8
		- 47.4	7	2303	1038	-20.6	6	- 0	0	-892.3	-25.4	2.3	-72.5	. 7
11TH	122.25	-49.9	8	2303	1038	-21.2	8	- 0	1	-843.4	-24.5	2.1	-64.0	.7
1278	132.00	-50.5	-1.0	2303	1038	-21.9	-1.0	- 0	1					. 7
13TH	141.75	- 52 . 1	-1.2	2303	1038	-22.6	-1.2	- 0	1	-792.8	-23.5	1.8	-56.1	
14TH	151.50	-53.8	-1.1	2303	1038	-23.4	- i . i	- 0	0	-740.8	-22.2	1.6	-49.6	. 6
15TH	161.25	-55.0	6	2303	1038	-23.9	6	0	- 0	-687.0	-21.1	1.4	-41.6	. 6
16TH	171.00	-55.2	-1.0	2303	1038	-24.0	-1.0	- 0	0	-631.9	-20.5	1.2	-35.2	. 6
17TH	180.75	- 55 . 4	-1.4	2303	1038	-24.1	-1.4	- 0	0	-576.7	-19.5	1.0	-29.3	. 6
18TH	190.50	- 55 . 6	-1.8	2303	1038	-24.1	-1.8	-0	1	-521.3	-18.0	. 8	-24.0	. 6
1 9 T H	200.25	-55.8	-2.2	2303	1039	-24.2	-2.2	-0	1	-465.7	-16.2	. 6	-19.1	. 6
2 ¢ T H	210.00				1038		-2.1	- 0	1	-410.0	-14.0	. 5	-14.9	. 5
21ST	219.75	-55.8	-2.1	2303		-24.2				-354.2	-11.8	. 4	-11.2	. 4
22ND	229.50	-55.8	-2.0	2303	1038	-24.2	-2.0	- 0	1	~298.4	-9.8	. 3	-8.0	. 4
2 3 R D	239.25	-55.8	-1.9	2303	1038	-24.2	-1.9	- 0	1	-242.8	-7.8	. 2	-5.3	. 3
24TH	249.00	~55.8	-1.8	2303	1038	-24.2	-1.8	- 0	1	-186.8	-6.0	. 1	-3.2	. 2
25TH	258.75	~55.8	-1.7	2303	1038	-24.2	-1.7	- 0	1	-131.0	-4.3	. 1	-1.7	. 2
E W (R	200.00	-55.0	-1.6	2303	1038	-23.9	-1.5	- 0	i					

TABLE Vind D	7 SHEAR IRECTION	AND MOMEN 340	IT DIAGR	AMS : Configue	RATION C	N DIEGO IN	TERCONT Refe	INENTAL I Rence pri	IOTEL SSURE	EAST TO 27.0 PSF	DVER OUT	GUST F	ACTOR 1.3	2
FLOOR	HEIGHT	FORCE X	(KIPS) Y	AREA X	(SQ FT) Y	PRESSURE X	(PSF) Y	ECCEN X	(FT) Y	SHEAR X	(KIPS) Y	N DNENT X	(1000-FT-) Y	KIPS) Z
HECH	268.50	.76 4	-76.0 -2.7	4252	2 1917	-17.9	.14	- 0	1	-76.0	-2.7	. ٥	7	. 1
TOP	286.50	- 7 6 . V		4236		. (. 7	L . T	v	•	0.0	0.0	Ģ. Ģ	9.0	0. 0

TABLE WIND D	7 SHEAR IRECTION	AND HONEN	IT DIAGRI	AMS : Configura	TION C	AN DIEGO IN	TERCONT Refe	INENTAL Rence p	HOTEL Ressure	EAST T(27.0 PSF	IVER OUT	GUST F	ACTOR 1.3	32
FLCOR	HEIGHT		(FIPS)	APEA (X	SQ FT) Y	PRESSURE X	(PSF) Y	ECCE	N (FT) Y	SHEAR X	(KIPS) Y	MOMENT X	(1000-FT- Y	-KIPS) Z
1 S T	0.00				876	-22.7	-4.8	- 0	2	-1396.3	63.5	-11.2	-216.3	-12.2
210	17.00	-46.2	-4.2	2034						-1350.1	67.7	-10.1	-192.9	-12.3
380	34.00	-46.0	-2.7	2034	876	-22.6	-3.1	-0	2	-1304.1	79.4	-8.9	-170.4	-12.3
4TH	54,00	-62.7	-1.1	2743	1195	-22.8	9	¢	- 2	-1241.5	71.5	-7.5	-144.9	-12.2
	63.75	- 54 . 2	3.9	2303	1039	-23.5	3.8	- 1	- ġ	-1187.3	67.6	-6.8	-133.1	-11.7
578		- 53.4	4.2	2303	1038	-23.2	4.1	- 1	-10	-1134.0	63.4	-6.2	-121.8	-11.2
6T H	73.50	- 51.3	3.9	2303	1038	-22.3	3.8	- 1	-10	-1082.7	59.5	-5.6	-111.0	-10.7
7TH	83.25	-49.2	3.7	2303	1038	-21.4	3.5	- 1	-10	-1033.5	55.8	-5.0	-100.6	-10.1
STH	93.00	- 47 . 1	3.4	2303	1038	-20.5	3.3	- 1	-11	-986.4	52.4	-4.5	~90.8	-9.6
9T H	102.75	- 46 . 0	3.2	2303	1038	-20.0	3.0	- 1	-11		49.3	-4.0	-81.4	-9.1
1 0 T H	112.50	- 47 . 6	3.1	2303	1039	-20.7	2.9	- 1	-11	-940.4				-8.6
11TH	122.25	-49.2	3.0	2303	1038	-21.4	2.9	- 1	-11	-892.7	46.2	-3.5	-72.5	
12TH	132.00	-50.9	2.9	2303	1038	-22.1	2.8	- 1	-11	-843.5	43.3	-3.1	-64.0	-8.1
13TH	141.75				1038	-22.8	2.7	- 1	-11	-792.8	40.4	-2.7	-56.0	-7.5
14TH	151.50	- 52 . 5	2.8	2303				- 1	-11	-740.2	37.6	~2 . 3	-49.5	-7.¢
15TH	161.25	~54.0	3.1	2303	1038	-23.5	3.0			-686.1	34.5	-2 0	-41.6	-6.4
16TH	171.00	-54.6	3.9	2303	1039	-23.7	3.8	-1	-11	-631.5	30.6	-1.7	-35.2	-5.8
1778	180.75	-54.9	3.5	2303	1039	-23.8	3.4	-1	-10	-576.6	27.1	-1.4	-29.3	-5.2
	190.50	- 55 . 2	3.1	2303	1038	-24.0	30	- 1	-10	~521.4	24.0	-1.1	~23.9	-4.7
1878		~ 55 . 4	2.7	2303	1038	-24.1	2.6	- 0	- 9	-466.0	21.2	9	-19.1	-4.2
19TH	200.25	- 55 . 7	2.3	2303	1038	-24.2	2.2	- 0	- 9	-410.3	18.9	7	-14.8	-3.7
2 0 T H	210.00	-55.9	2.4	2303	1038	-24.2	2.3	- 0	- 9	-354.4	16.5	5	-11.1	-3.2
21ST	219 75	-56.0	2.4	2303	1038	-24.3	2.3	- 0	- 9		14.1	- 4	-7.9	-2.7
2 Z M D	229.50	- 56.1	2.5	2303	1038	-24.4	2.4	- 0	- 9	-298.4				-2.2
2 3 R D	239.25	- 56.3	2.6	2303	1038	-24.4	2.5	~ 0	- 8	-242 3	11.6	3	-5.3	
24TH	249.00	-56.4	2.6	2303	1038	-24.5	2.5	- 0	- 8	~186.0	9.0	2	-3.2	-1.7
25TH	258.75				1038	-23.7	2.5	- 0	- 9	-129.6	64	1	-1.7	-1.2
		- 54 . 6	26	2303	10.30	-23.1	č. J	Ŷ	-					

TABLE Vind D	7 SHEAR IRECTION	AND MOMEN	T DIAGRA	AMS : SA Configuration C	N DIEGO IN	TERCONT Refe	INENTAL HOTEL Rence pressure 2	EAST TI	OVER OUT	GUST I	FACTOR 1.32	2
FLOOR	HEIGHT	FORCE	(KIPS) Y	AREA (SQ FT) X Y	PRESSURE X		ECCEN (FT) X Y	SHEAR X	(KIPS) Y	NOMENT X	(1000-FT-K Y	(IPS) Z
MECH	268.50	78 4	n 1	4252 1917	-17.6	2 0	-1 -10	-75.0	3.8	~ . ¢	7	8
TOP	286.50	-75.0 3.8	7232 1918		- . *		Q.Q	¢.¢	Q.Q	Ŷ.Ŷ	¢.¢	

TABLE 7. SAN DIEGO PROJECT 7750 SCALE = 300 GUST FACTOR = 1.32 NUMBER OF SIDES = 4	INTERCONTINENTAL HOTEL EAST TOWER IN CONFIGURATION A REF PRESSURE = 27.0 Standard Floor Height = 9.75 NO OF FLOORS = 26
SIDE ANGLE	Z-AXIS
i 0.0 2 90.0 3 180.0 4 270 0	4.725 2.130 4.725 2.130
FLOOR # LABEL	HEIGHT-FT
1 1 1 1 1 1 1 1 1 1 1 1 1 1	17.00 20.00 9.775 9.

TABLE 7. SAN DIEGO PROJECT 7750 SCALE = 300 CUST FACTOR = 1.32 NUMBER OF SIDES = 4	INTERCONTINENTAL HOTEL EAST TOWER OUT CONFIGURATION C REF PRESSURE = 27.0 STANDARD FLOOR HEIGHT = 9.75 NO OF FLOORS = 26
SIDE ANGLE	Z-AXIS
1 0.0 2 90.0 3 180.0 4 270.0	4.725 2.130 4.725 2.130
FLOOR # LABEL	HEIGHT-FT
1 1 STD 23 RD 4 5 5 5 5 7 8 9 4 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7 7	$ \begin{array}{c} 17 \\ 00 \\ 17 \\ 00 \\ 9 \\ 75 \\ 9 $

APPENDIX A

PRESSURE DATA

Note: Pressure coefficients are defined in Section 4.3. Pressure tap designation is explained in Figure 3.

W D	TAP	CPMEAN CPRMS	CPNAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPREAN	CPRMS	CPMAX	CPMIN
p \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	P 123456789012345678901234567890123456789012345678901234567890	CP ME A N CP R MS - 191 115 - 004 1288 1000 1388 1000 1389 1290 1441 1899 1408 - 0799 1233 - 0799 1233 - 1672 1144 - 1987 1244 - 1987 1244 - 1987 157 4670 157 2803 1479 - 1567 283 149 - 3533 157 4670 1567 2803 1473 - 1244 1148 - 1157 1148 - 1157 1158 - 1458 1149 - 1154 1158 - 1165 1167 - 1464 1667 - 1157 11667 - 1165 1167 - 1167 1167 - 11	X 92441404919202046295800199924465555592540420417129 H 247465581011920204629582014558840199924665555592540420417120 11.02209111219 11.02209111219 11.02209111219	C	¥ \$	P 123456789012345678901234567890123456789012345678901234123456 A 5555555555666666666666677777778888888888	CP 06644 - 0662295 - 06644 - 0662295 - 06644 - 0662295 - 0662295 - 0662295 - 062295 - 06220	CP	x 1446503711689916899460816227866361833866285031088807617 n 6340125742958232740958491313475956518176539439285155 1111 111 111 1111 1111 1111	U	# 000000000000000000000000000000000000	- 222222222222222222222222222222222222	6 7.5 4.6 5.2 2.4 5.5 4.6 5.2 2.2	132054234283777745892753262158745033339776449189661929 11111111111111111111111111111111	3039872191560487334175520046675481522048818975600172 111589047821126481120876013277882701644531256818975600172 1111111220876013277882701644531121111112211683575601172	

P	Ĥ	c.	F	4	2
r -	-	u	L		<u> </u>

WD TAP	CPNEAN CPRMS	CPNAX	CPNIN	WD	TAP	CPMEAN CPRI	IS CPMAX	CPMIN	ыD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
789701217945978970123459789789789789789789789789789789799999999	$\begin{array}{c} -234 & 118 \\ -265 & 114 \\ -240 & 112 \\ -237 & 109 \\ -237 & 116 \\ -2037 & 116 \\ -2037 & 110 \\ -209 & 109 \\ -211 & 109 \\ -211 & 110 \\ -2265 & 124 \\ -265 & 124 \\ -265 & 108 \\ -2261 & 077 \\ -2261 & 077 \\ -2261 & 077 \\ -2261 & 077 \\ -2261 & 077 \\ -2261 & 077 \\ -2261 & 077 \\ -2262 & 116 \\ -2234 & 108 \\ -2234 & 108 \\ -2256 & 112 \\ -256 & 102 \\ -2256 $	31421502676582604982376864093186087235027523866184 12992832938213506821731197222517085904453270021397110 11112001011111200000111111111111111		00000000000000000000000000000000000000	33333333333333344444444444444444444444	- 251 11 - 25454 11 - 22454 11 - 22459 11 - 22429 11 - 22429 11 - 22429 11 - 22429 11 - 22429 11 - 22429 11 - 22455 11 - 224459 11 - 22455 11 - 22459 11 - 22559 11 - 2555 00 -	587968377653691872406061919312657063333882122657968377963691872406061191931265706333388212683521813565444453384419927589974442002	48517551743598375750966173440014580500593214071108	00000000000000000000000000000000000000	7424567891234567895678901289012345612312345678901 74234567891234567895678901289012345612312345678901	- - - - - - - - - - - - - - - - - - -	10013384931915012579665560813981557933531587606136 11111121210131141211110222343511225474174674 111111111111111111111111111111	3325800002200649533305006492066 2222220649533305006492066 1009866 1009866	

APPENDIX A -- PRESSURE DATA) CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN PAGE A 3

ыD	TAP	CPMEAN CPRMS	CPMAX	CPMIN	ШD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	80	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
	23456781234567890123456789012345678901234567890123	$\begin{array}{c} 1315\\ 1417\\ 2362\\ 1447\\ 1417\\ 23645\\ 1447\\ 1472\\ 1447$	9595555496 027218855840219856325575510144965360190988894 1211104682756321912148761152886325575512121087 111104682756321214876115288404950017022575312109568949 11111	60377065914167240254028354569270440506733685820889 690180675323501027337241854214692237532685820821001468 11111111111111111111111111111111111		1111111111111111111111111111111111111	$\begin{array}{c} - & 2321\\ - & 23570955115082\\ - & 125092111508231144098722631464\\ - & 2039211554209216511285542051285960933735\\ - & 20392115542092257585960933735\\ - & 205275285960933735\\ - & 11633643009237585960933735\\ - & 11633649766112885960933735\\ - & 20527588596093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275885960093375\\ - & 205275865960093375\\ - & 20527586596009375\\ - & 20527586596009375\\ - & 20527586596009375\\ - & 20527586596009375\\ - & 20527586596009375\\ - & 20527586596009375\\ - & 20527586596009375\\ - & 20527586596009375\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 20527566666\\ - & 2052756666\\ - & 20527566666\\ - & 20527566666\\ - & 205275666666\\ - & 20527566666\\ - & 205275666666\\ - & 205275666666\\ - & 205275666666\\ - & 205275666666\\ - & 20527566666666\\ - & 2052756666666\\ - & 20527566666666\\ - & 2052756666666666666666666666666666666666$	7012333444323435020166739585906011138490625370728655 22080967414689976432034876551802577469762367676520	594 792444418429437636574367592160180156421367785555	- 756916048868948899990436334091043338883902885646633915537 - 0007990436034097128885646633915537 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		1222222222222222222222222222222222222		5107 0293427197556391077402325094283030183070892818 044454565333233333344433122833542222232343434343232	21111197790303043208695798614016549016967 212111977903035129901486614016549016967	

APPENDIX A -- PRESSURE DATA (CONFIGURATION A) SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN PAGE A 4

ЧD	TAP	CPMEAN CPRMS	CPMAX	CPMIN	MD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	90	TAP	CPMEAN	CPRMS	срмах	CPMIN
	01234567890123456789012345678901234567890123456789 5555555555555555566666666666677777777788888888	26 1385 12368 13857 12372 113857 12383 12211 12383 12211 12383 12211 12383 12211 12383 12211 12242 12244 12383 12244 12242 12244 11531 12244 123258 133258 1111 12244 12252 1123358 1123258 123258 1123258 123258 1123258 123258 123258 123258 123258 123258 123258 1123258 1123258 1123258 1123258 1123258 1123258 1123258 1123258 1123258 1123258 1123258 1123258 1133258 113258 1133258 113258 1133258 113258 1133258 113258 1133258 113258 1133258 11433358	784775245787355590085123111735577383691128375365496283 11223223231477089417171716125659738369112218375365496283 11223223231011122132110011111112112112112112110110110110110	13967258229435807741250013334426015254092063454243 9447798421412197590121889472675964032957727385555644 -1111		012345478901234547890121234547494042878123454789 0000000000011111111111220000000001111111		12869485034649092511529761284476078601515248624088	50977949i26102052194476919899541434719654254728499 779091510112425001921029676716339347341611318989899 11011111122212019210296767163393473416113189898999			55555555556666666666777777777777777777	11527714271345756579644884448727541037262316087293 92168695185645742410679345940888072614798684103215 92268695185645742410679345940888072614798684103215	508834578280235538315915394058716326105141463172407 12433320161356124354223212331371132162263651213159	1459944335621130261136 203112391562130261136 112303151626136 2031123026136 2031123026 20466 204666 200	

W D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	срмах	CPMIN	ыD	TAP	CPMEAN	CPRMS	CP MA X	CPMIN
00000000000000000000000000000000000000	567255959595955551111111111111111111111111	69866028314137679749976291626190416181132565663929	30847155396894504130251112862517089214093500151579 1222121111111111111111111111111111111	1097277415169901142152300345476355116885610780894658 19101431237321468665222120641011168512225411218 19101431237321468665222120645547687611218 1111		00000000000000000000000000000000000000	11111111111111111111111111111111111111	264179755656583011535770066557883596744293152203290 97343664940642952228633495649907922491184313463117716 1111111111111111111111111111111	22402573039311226247108872822741269823005468153854 78766412277766641676665522112656564308014655537553225	02700799668495967799426505774181451167502322087352 9261750440202812068989922841464207898077592855404559522 97117431120111651111680099428505774181451167502322087352		00000000000000000000000000000000000000	11111111122222222222222222222222222222	1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 -	25328635695998212261642442735074696691641513429379 2546310033337478767724333444577552112234556422142454	99536794755993775858477566349608073786 630946295906343883797999337668812446520 222110112222232111102111102123849608073786	++++++++++++++++++++++++++++++++++++++

ыD	TAP	CPMEAN CPRMS	CPMAX	CPHIN	¥D.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	80	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	34567890120345678901234567890120345678901203456789012 4444445555555555555556666666666777777777	1 272 181 1 1609 1167 1 1809 1123 1 1633 1123 1 1633 1231 1 1633 1231 1 1633 1231 1 1633 1231 1 1633 1235 1 1632 1134 1 12356 1134 1 1452 1134 1 1528 1452 1 1533 1102 22566 1795 1226 1 1533 1102 225464 1978 1102 226464 11098 1102 1 1533 1102 2224433 1102 2218 1 1122 1233 1 1122 1233 1 1122 1233 1 1122 1233 1 1122 1233 1 1122 1233 1 11	35775146724170578173207408904242706995513859889887745 222222112222222222140974089042427069955188598898845 2222221122222222222122223111122111122111122211122212121212111111		00000000000000000000000000000000000000	3456789012345678901234567890121234567890121234567812 99989990000000000111111111222000000000011111111	- 258390032424242004082002594711666401359917857523115289412612 - 117792242333204082002594711666401359917857523115289412612 - 1222333320408202594711666401359917857523115289412612 - 1222322221112222222111222220557523152894122612 - 1222322221112222222112222222112222205575231522894122612 - 122232222211222222211222222221122222222	\$662237823925622147615428330688374902005015410126013 361111001121111011222122110012112112142242224029011111900013 11111111111111111111111111	814324719417266513659246281252838662809112765242292 112222111111021111212111121212111112123114467565142492	98289048443903128182947066320910784201826056845481	00000000000000000000000000000000000000	55555555555555556666666667777777777777	- - - - - - - - - - - - - - - - - - -	29465066048509695266349227158404127955814403391841 11111111111112099222341134451134111110140111425127265 111111111111111111111111111111111111	207 313 310 299	

ыD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ШD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	W D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
 	123123456789012345678123456789012345678901234567890123456789	1 1 <td>47995624490986970089742256751939927192986728038255 110111222211211212121111111111111111</td> <td>1038451777789899949477734587146995197206353415974668 767147987544786741861773445871469951631971184994775972 0220132022112300423505766352152279720635300111691175</td> <td>04171929535821923666347283421400614911119376622903</td> <td></td> <td>012345678901234567890123456789012345678901234567890123456789</td> <td>- -</td> <td>46016355671184039768081804548179534303207034303903 3233207876445333327855664298075443221778553307113343</td> <td>11890358587011790881284980418416672429397934543176 118903587820027911886510279112414023473180422835200 1118865102791128420121891074100128775</td> <td></td> <td></td> <td>0123456789012341234567890123222</td> <td>87476599469955444408370998454994610435845691271540 30766658812272408210236095940100036928581211147555740 133202352232102236095940100036928581211147555740</td> <td>460806442126827538722442285954131839246746135968289 3662233555524331094435589013362334546680931223344467.982203 1111111111110111111202422859541311111122334467.982203</td> <td>120443199722443866266483432973070 - 222097224435666483432973070 - 2227090 - 2227090 - 2227090 - 112227090 - 112227000 - 11227000 - 112270000 - 112270000 - 112270000000000000000000000000000000000</td> <td>1 1</td>	47995624490986970089742256751939927192986728038255 110111222211211212121111111111111111	1038451777789899949477734587146995197206353415974668 767147987544786741861773445871469951631971184994775972 0220132022112300423505766352152279720635300111691175	04171929535821923666347283421400614911119376622903		012345678901234567890123456789012345678901234567890123456789	- -	46016355671184039768081804548179534303207034303903 3233207876445333327855664298075443221778553307113343	11890358587011790881284980418416672429397934543176 118903587820027911886510279112414023473180422835200 1118865102791128420121891074100128775			0123456789012341234567890123222	87476599469955444408370998454994610435845691271540 30766658812272408210236095940100036928581211147555740 133202352232102236095940100036928581211147555740	460806442126827538722442285954131839246746135968289 3662233555524331094435589013362334546680931223344467.982203 1111111111110111111202422859541311111122334467.982203	120443199722443866266483432973070 - 222097224435666483432973070 - 2227090 - 2227090 - 2227090 - 112227090 - 112227000 - 11227000 - 112270000 - 112270000 - 112270000000000000000000000000000000000	1 1

ыD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ыD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	\$7800123456780012345678001234567800123456780012345678001234567800123456780012345678001234567800123456780012345	65758916119860952075754077944708440185399565333702 09235258916119860952075754077944708448132056492003203211 21200220055451192202341112220235571111220203555441120202211 212002200554541122202341112220235571111220203555555555555555555555555555555	05559171628442171255647550586332303566612746307318 1233556102522346711221244790832111344127411343355620	07905928194478074817484661581727 12111112222231112332119860261758887 1221111122222311123321198602617758887	56821027884390443076666491486068607188333499554072517		\$789012345\$789012345\$789012345\$789012345\$789012345\$7890123 8888999999999999900000000011111111112(NOO000000011111 222202222222222222355555555555555555555	79160466157256798190656594262868708180838315503215 12222367842446133356647721424425738813424261115545503215 2022222678424461333566447221424457738134242426111554554258 202222222222222222222222222222222222	71996371562299778433878712588801903686571700166477	024691251619242744626795384510 2222221112211222122122111221112			44444555555555555555555555555555555555	+ + + + + + + + + + + + + + + + + + +	29659612221584782221093140008177977989537542293130 1109990112145241813433190232651233662233220002300163	31225201169716844125727435930155444654938375795588 492285480905961439946150798547562238919701798923108 11798923108 11798923108	

W D	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
B 000000000000000000000000000000000000	+ 777777788889999999999999999999999911111111	H 665777678706028904219556777192532674292684707581240	5 11950285910555005970841098907616084224173309086394 1111111111111112222121122121111111111	787015259970874935301 21222232201030229982 		- 444444444444444444444444444444444444	. 34567890123456789012345678901234567890123456789012 2222222222335555555555555555555555555	- 1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1-1	37865048782199174386599111825991230542387337317345 13221111111222199977533311998765403869785431049786450	084	$\begin{array}{c} -1 \\ 62505729 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -205057297 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -$	- 444444444444444444444444444444444444	11111111111111111111111111222222222222		40604676183580790916863466926486368213680894687294 710454327533976656565320143343996970213345446453322323 2311111111111111111111111111111	065320819620842336518594540352691114104 999220842336518594540352691114104	60514637788992636254867716637753103997901888066324503 4551246776894006347961898156628224245929186950213 4551246776894006347961898156628224245929186950213 411111111111111111111111111111111111

WD	TAP	CPMEAN CPRM	S CPHAX	CPHIN	99	TAP	CPMEAN	CPRMS	CPHAX	CPMIN	ЯD	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
++++++++++++++++++++++++++++++++++++++	90127456789012745678901274567 890127555555555555555555555555555555555555	5777340324142330079024443590574413590867961117193414435900 9890352667841727796369574413590867961117193411411331114 48094669999926442005709657441350867961117193411411331114 2255688811112225796369574413508679611171934124645990 22556888111122255888121722965724413508679611171934114111331114 11111111111111111111111	51315749969882657524952111323997828850348771430669 51315749966988265752495211122241513122522111121011212 12236162112222345426237522111222211313122522111121011212 122361621122223454262575249522111222211313122522111121011212 122361621122223454262575249522111222211313122522111121011212 122361625752495698826575524952111222	04787408873621412406997035810539116390526076237 784017399343970576053997198099406361678866795713 11222116666795343970576053997198099406361678866795713	000000000000000000000000000000000000000	90127473789012347870789012347890127474747678901212747890 78888888888888888888888888888888888	4458759636784858309268442173323246616157028330045334 2333411222233454555576036260070176058796732213590249334 345875962858796732209335776036260070176058796732213590249343 4345875963628907	4764804616824778948006723858492222034541875555562677352112467889006911245451011244540000011264265444	18688345761658088958989828584571519250848762702 748888345761658080989848080816816011111115550868440 74888834576165808805898285808168110111111115550848762	98503656932576171597788800472478194502461402542391	000000000000000000000000000000000000000	78901234567812345678901234567890123456789123456789567 00011111111100000000011111111000000000	58055547877515546807785597841405888704012015297838 432223555240355080657170548514205287897401201100101 432223555240355080657170548514205240120110011001001 432223555478775154680778552855485140588870401201528888 43222355547877515546807788558541405888704012015288888 43222355547877515546807788558578414058887040120015288888 43222355547877515546807788558578414058887040120015288888 4322235554788775155468077885585784140588870401200152888888 4322235554788775514035508887040120011000110001100011000110001100011	30450437844066255785800129272095513865472052125500341552212 1111111111111111111111111111111	049918776539242023795339532769494 1766752255562422787534790422157984 1766752255562422787534790422157984 1	03741685165113115306929432200483034079308164882377

											CPMIN	ыD	TAP	CPMEAN	CPRNS	CPMAX	CPNIN
WD	TAP	CPMEAN I	CPRMS	CPMAX	CPMIN	WD	TAP		CPRMS	CPMAX			166	.424	. 161	. 959	223
40 40	718	054 118	111	.311	437 561	50 50	116 117	- 133 - 291	.148	331	- 534 - 704	50 50	167	373	. 161	975	- 061
40	720	046	121	.347	- 468	50 50	118	- 334 - 382	.120	- 021	841 836	50 50	$168 \\ 169$	- 114	. 157	. 367	804
4 ¢ 4 ¢	721 722	052 075	. 115	277	591	50	120	311	121	.097	- 722	50 50	170	- 363	. 139 . 126	012	852 844
40 40	728 729	284 318	233	.355	-1.653	50 50	121 122	180	. 116	. 180	582	50 50	172	- 263	095	.018	580 376
40	730	- 195	.151	.335	-1.216	50 50	123	275 .445	. 141 . 213	.202 1.070	850 317	50	174	- 168	. 106	. 115	- 596
4 Ç	732	- 150	120	248	- 758	50 50	125	525	.175	1.251	118 004	50 50	175 176	- 165	110	.212	284
4 0 4 0	733 734 735	122	. 121	312	579	50 50	127	184	182	.800	368 668	50 50	177	.052	.170	.714	525 683
4 0 4 0	736	- 116 - 095	.137	.305	833	50	129	363	145	192	858	50 50	179	- 310 - 390	.141	.131	800 887
40	801 802	140 096	.106	.197 .285 .362	- 520 - 514	50 50	$130 \\ 131$	434	. 128	069	801	50 50	181	- 522	. 134	022	- 994 - 857
4 0 4 0	803 901	- 049 - 399	116	- 362	458 934	50 50	132	229 190	. 127	.147	731 599	50	183	219	. 699	. 111	- 584
40	902 903	- 456	219	220	-1.399	50	134	157	.110	.181 1.290	584 301	50 50	184 185	.249 .350	. 164	.930	113
40 40	904	287	. 219	. 415	-1.389	50 50	136	550	.166	1.093	101 078	50 50	186 187	339	.142	918	089 339
4 Ç 4 Q	905 906	826 207	.190	- 392	-1.592	50	138	. 174	163	658 486	- 372	50 50	189	- 108	. 154	. 400	- 595
40 40	907 908	343 805	.195	.269	-1.387	50 50	$139 \\ 140$	161 407	. 154	. 0 97	938	50 50	190	- 467	. 134	- 057	951 756
40	909 910	-1.002	235	- 271	-1.852	50 50	141 142	- 495 - 342	.131	112	934 754	50	192	- 254	110	. 132	677
40	911	- 179	188	.374	-1.085	50 50	142 143 144	192	.113	.228	555 659	50 50	$193 \\ 194$	- 132 - 129	102	. 222	552
40 40		- 389	. 225	- 390	-2.059	50 50	145	- 160	114	257	591 224	50 50	201 202	- 243	.144	213	833 842
40 40	914 915	- 082	. 168	430	- 858 -1 393	50	147	. 026	. 159	564	- 450	50	203	- 226 - 238	132	. 228	703 755
40	916 917	- 032 - 078	.147	.513	849 946	50 50	148 149	- 196 - 414	.151	. 1 0 6	-1.139	50	205	- 351	185	167	-1.184
4 0	918 101	- 192	125	178	- 944	50 50	150	- 437 - 521	.133	- 178 - 125 139	916 -1.053	50 50	206 297	- 418	. 142	.055	-1.192
5¢ 5¢	102	. 098	. 170	.667	- 478	50 50	152	- 286	. 145	.139	805 673	50 50	208	- 393 - 396	.132	021	-,900 -,956
50 50	$103 \\ 104$	013 - 130	167	. 389	528	50	154	495	187	1.250	- 189 - 138	50 50	210 211	- 462	. 254	.219	-1.641 -2.078
50 50	105	- 235 - 271	.118	.204	- 671 - 781	50 50	155 156	. 46 9	. 191	1.112	- 025	50 50	212 213	- 241	. 140	. 131	783 781
50	107	- 343	.154	.118	-1.199 -1.568	50 50	157 158	.148 - 167	. 181	705	- 424 - 791	50	214	- 242	. 133	. 199	- 701
50	109	- 298	149	105	-1.111	50 50	159 160	344 445	.134	.034 085	891 887	50 50	215 216	- 255 - 335	.156	. 239	-1.112
50 50	110 111	221	. 129	. 187	700	50 50	161	- 328	126	067	- 688 - 614	50 50	217 218	- 405 - 464	. 148	164	- 925 - 964
50 50	112 113	.491 .459	178	1.044	099	50	163	- 151	106	247	- 493 - 596	50 50	219 220	- 441 - 410	. 143	006	939 892
50	114 115	269	173	.859 .614	218 467	50 50	$164 \\ 165$	- 210	.173	940	350	50	221	- 234	269	. 338	-1.677
50 50	114 115	.269 .975						392		940			221	234	. 269	. 338	-1.677

W D	TAP	CPMEAN CPRMS	CPMAX	CPHIN	ыD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ЯD	TAP	CPMEAN	CPRMS	CPMAX	CPNIN
৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽৽	23456789012345678901234567890123456789012345678901 22222222222335555555555555555555555555	66005333044637742522534295072235442950728568505288797724644214 355407333000321225283344467552287972464429533944295539544295539544295528669807252879772464421112222222222222325222222222222222222	575554126667744974574666755744784969954575944774554126916555242132000577223244097055248016556426595043447745541269142621126211269142691409	$\begin{array}{c} -1 & . & . & . \\ 7.3521 & . & . & . \\ -1 & . & . & . \\ 7.741 & . & . & . \\ 8.0 & . & . & . \\ 9.2 & . & . & . \\ 9.2 & . & . & . \\ 9.2 & . & . & . \\ 1. & . & . & . \\ 9.2 & . & . & . \\ 1. & . & . & . \\ 9.2 & . & . \\ 7.799 & . & . \\ 9.0 & . \\ 7.799 & . \\ 9.0 & . \\ 7.799 & . \\ 9.0 & . \\ 7.799 & . \\ 9.0 & . \\ 7.799 & . \\ 9.0 & . \\ 7.799 & $	00000000000000000000000000000000000000	23456789012345678901234567890123456789012345678901 7777777888888888889999999999000000001111111111		79498980159029779804648784103036131934474833746993 4445412345450321224474093090122247750212244650111232028 11111111111111111111111111111111111	5639474236087559323 67559474236087559323 69755932549770551 1001422111010551		00000000000000000000000000000000000000	212345678901234567812345678901234567890123456712345678912345 2000000000000000000000000000000000000	13493721200059795239865608155843540824899863984980 25335223535222252001111223501100024510011222252001122100 253552232522520011122155201112222520011222100	08096836210636242458431574626426891519962549196864 63453765401010901110911123312131431000222115622101353	077 392 169	

									CPMAX	CPMIN	ыD	TAP	CPMEAN	CPPMS	CPMAX	CPMIN
ЫD	TAP	CPMEAN CPRM		CPMIN	ШD	TAP	CPMEAN					159	499	. 146	020	-1.065
50 50	706 707	202 .11		- 639 - 602	60 60	109	218 169	. 147	235	847 847	60 60	160	- 400	143	. 123	- 875
50	708	045 . 12	4 .643	513	60	111	165	137	378	775 385	60 60	161 162	- 217	.126	. 198	662 551
50 50	709	045 .11		523 621	60 60	113	. 386	. 224	1.065	343	60	163	- 163	. 114	. 186	617
50	716	066 .12	2 .297	- 545	60 60	114 115	.117	.185	.748	383 795	60 60	164 165	- 195	. 111	202	725 637
50 50	717	051 .10	5 .332	421	60	116	319	. 142	.179	915	6.0	166	. 382	. 207	1.024	378
50	719	- 185 .10		525 392	60 60	117 118	419 345	137	012	- 862 - 737	60 60	167 168	275	. 173	. 525	271 632
50 50	720 721	080 .10	9.324	558	60	119	359	. 134	.053	780	60	169	353 489	. 160	. 226	965 982
50 50	722 728	- 140 .11		561 -1.060	60 60	120	262	. 142	282	766 677	60 60	171	- 371	. 130	.081	780
50	729	262 .19	4 .234	-1.572	60	122	- 170	124	. 247 . 264	606 780	60 60	172 173	- 230	.090	. 020 028	- 511 - 446
50 50	730 731	192 .10		696	60 60	124	. 513	240	1.200	598	60	174	- 168	. 105	. 279	458
50	732	222 . 12	1.155	- 635 - 615	60 60	125 126	441	212	1.143	460 235	60 60	175	165	.118	223	613 428
5¢ 5¢	733 734	194 .10	6 .264	-1.141	60	127	023	. 159	. 487	468	60	177	- 166	177	. 401	-1.062
50 50	735 736	215 .13		866 784	60 60	128	- 310 - 430	.149	.183	908	60 60	178 179	383	. 125	021	761
50	801	- 168 .11	7 .187	597	60	130	- 395	. 125	081	802 657	60 60	180 181	- 431 - 506	. 118	077	788 -1.178
50 50	802 803	- 164 .09		485 389	60 60	131 132	- 272	. 126	323	886	60	182	- 238	. 134	.177	- 837
50	901	297 .11	4 .086	892	60	133	165 166	133	290	730 695	60 60	183 184	- 215	.121	.153	- 696 - 325
50 50	902 903	370 .17	9 .231 5097	-1.244	60 60	135	. 45 9	242	1.262	625	60	185	. 326	. 159	1.011	- 081
50	904	167	6 .348	-1.260	60 60	136	466	211	1.178	824 289	60 60	186 187	238	. 168	.787	- 388 - 572
50 50	905 906	878 .19	¢ .488	655	60	138	035	. 186	. 722	664	60	188	312	. 147	200	- 882 - 912
50	907 908	230 .16		969 -1.567	60 60	139	387 531	. 168	. 101 - 091	-1.139	60 60	189 190	417 518	.131	071	-1.047
50 50	909	-1.257 .24	5 495	-2.205	60	141	451	. 160	013	- 926	60	191 192	- 342	. 133	.039	- 857 - 613
50 50	910 911	015 .12		425 690	60 60	142 143	228 158	.136	176	722 548	60 60	193	- 127	. 110	. 255	- 524
50	912	- 133 10	5 .182	789	60	144	- 165	124	.277	588 737	60 60	194 201	- 137	.115	.328	506 716
50 50	913 914	-1.049 .31	0 .445 5 .440	-2.063	60 60	145 146	- 183	. 130	964	637	60	202	- 192	. 135	178	- 686
5¢	915	- 608 .25	7.102	-1.675	60 60	147	- 188 - 417	185	427	-1.012	60 60	203	- 214	.132	180	- 730
50 50	916 917	014 .10		402 592	60	149	555	. 156	058	-1.063	60	205	515	. 216	. 181	-1.521
50	918 101	- 272 13	9 .046	834 578	60 60	150 151	454 344	.138	- 058	-1.006	60 60	206 207	- 496 - 396	. 198	110	- 855
60 60	102	054 . 18	6 .555	724	60	152	- 166	. 121	. 273	- 557	60	208	- 339	126	. 063 . 276	- 791 - 787
60 60	103 104	- 112 .16		709 574	60 60	153 154	- 167	. 126	218 1.084	629	60	210	243	. 167	298	937
60	105	264 .11	0 .172	- 719	60	155	. 448 . 350	200	1.093	183 215	60 60	211 212	- 226	. 240	632	-1.165
60 60	106	323 .11		855	60 60	156 157	- 063	187	635	707	60	213	228	. 145	279	-1.017
é ó	108	- 357 16		-1.128	60	158	379	. 181	. 288	-1.035	60	214	259	. 148	. 219	- 836

W D	TAP	CPMEAN CPRMS	CPNAX	CPHIN	ыD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	9 D	TAP	CPMEAN	CPRMS	CPMAX	CPNIN
ୠ୶ୠୠ୶ୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠୠ	5678901N745678901N745678901N745678901N745678901N745578901N74 11111N0N0N0N0N0N5555566666 NN0N0N0N0N0N0NNNNNNNNNN	$\begin{array}{c} 334 & 1722 \\ 1726 \\ 3457 & 19505 \\ 19505 & 19505 \\ 19505 & 19505 \\ 19505 & 11555 \\ 19505 & 11555 \\ 19505 & 11555 \\ 19505 & 11555 \\ 19505 & 11555 \\ 11555 & 11555 \\ 11144 \\ 2956 & 11555 \\ 11144 \\ 2956 & 11555 \\ 11144 \\ 2956 & 11577 \\ 11220 \\ 11220 \\ 11220 \\ 11220 \\ 11$	487851547714988520950415305511528092509197548225095142505 4878515579175505891815165295511385892559197554825095591 1 0 0 0 0 0 0 0 0 0 10 0 0 0 0 0 0 0 0	11111	\$	56789012345678901234567890123456789012345678901234 666666777777777788888888888999999999999	24149620655072617233551030338558151532080679650096 2227716803722772436979546589898989141228898154355679 232355803722772436979546589898989141228898151532080679650096	432125852095159540554122917912030895368866952218779	05412632004203133283509874365676706039161575297321 222110003791100002721111000148811211002451220023521	$\begin{array}{c} -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -\\ -& -& -& -& -\\ -& -& -& -& -\\ -& -& -& -& -\\ -& -& -& -& -\\ -& -& -& -& -& -\\ -& -& -& -& -& -\\ -& -& -& -& -& -\\ -& -& -& -& -& -\\ -& -& -& -& -& -& -\\ -& -& -& -& -& -& -\\ -& -& -& -& -& -& -& -& -& -\\ -& -& -& -& -& -& -& -& -& -& -& -& -& $		56789012123456789012345678123456789012345671234567 11111122200000000111111111111100000000111111	32422611385032343655235939726562279827680561989845 1122221002233513351123000292828208620301597706744171011 1122221002223513351123000292828208620301597706744171011	99049558825407322841656023864337970127349689107786 111111221146274531012189111001112321013455510903311453 11111111111111111111111111111111	224692400230131262015588113783152727400070890790035964 224692407221294551458811378315272174743400070890790035964 1 4235552211147434501556768224	

ыD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	НD	TAP	CPMEAN	CPRMS	срмах	CPMIN	ыD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	910 911 912	901426049643096835955112218162303614966608928766571 11222100220777788688359551122181623036149666608928766571	12321376915007898464511232816156979180604716978515 11111111101111111111111111111111111	122112735126803880042840683777415 		77777777777777777777777777777777777777	11111111111111111111111111111111111111	$\begin{array}{c} 7 \\ 0 \\ 1 \\ 3 \\ 3 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 3 \\ 2 \\ 4 \\ 5 \\ 3 \\ 3 \\ 2 \\ 4 \\ 5 \\ 3 \\ 3 \\ 2 \\ 4 \\ 3 \\ 3 \\ 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 4 \\ 3 \\ 3 \\ 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 4 \\ 3 \\ 3 \\ 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 4 \\ 3 \\ 3 \\ 2 \\ 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 4 \\ 3 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 4 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 2 \\ 4 \\ 3 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	111106387686565289180715739416471222719615905506682 77213531112364321412113704443112279275431022076442	810520998841046474884917581102280693919540931470052 188867844147874201017286972883217259562953297549714151 1 1 1 1 1 1 1	$\begin{array}{c} -& 8\\ -& -& 7\\ -& -& 7\\ -& -& -& -& -& -& -& -& -& -& -& -& -& $	77777777777777777777777777777777777777	11111111111111111111111111111111111111	26153863868419927542721893830293751180798106304663 65965624665404867959976425345258123313339129929649 1111025421122120244211113443422581223313339129929649	03970514465963593563453540374287585598841993311155 1114800853241100238743287017632241125055988419933111155 2105111111153211111000111111111210101111111111	522465498135942215868171895435094139638890423 9726212221096300100124100012288720001232321 1	

																	CPMIN
W D	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	9 D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ЯD	TAP	CPMEAN		CPMAX	
00000000000000000000000000000000000000	89012345678901234567890123456789012345678901234567 0011111111111110000000000000000000000	1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1 <td>433855085800005037699675781874205310772671333651538 11111111111111122111111111112211111221122212280796589</td> <td>19434223 94434223 968523224 1005342249 11022329</td> <td>44801719385787368105980477722213733967648852459168 776668690912225411681643274345058735721100651560946 776668690912225411681643274345058735721100651560946 777668690912225411681059804777222213755233027351901</td> <td>77777777777777777777777777777777777777</td> <td>890193456789019345678901934567890193456789019345678901934567 5536666666666677777777777888888888899999999</td> <td>90586759887354994231221274536261122850745086770684 4377730309260689811178444101112745362611122850745086770684 10111127344200111111221001121 100111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 10011111111</td> <td>711067282115835651307204584388003605877361573583827 809580044666688041743778648212457547940091228290012 121122112211112111221121111111111</td> <td>89393666048385427868841903204300219067398872886201201 2110488110983102256021720610471579784483808864551188 111111111111111111121188</td> <td>$\begin{array}{c} -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1$</td> <td>77777777777777777777777777777777777777</td> <td>33333333333333444444444444444444444555555</td> <td>39311885491422912907476144709844146897128031694586 43051452350377220573348447102352392514582443995225 222001111122210023523948447102352392532274382643995225</td> <td>768689929553628050131442978606577823966536733822626 111139012121111111111111111111110011129002223966536733822626 111111111111111111111111111100111119002223966536733822626</td> <td>111 243 020 663 175</td> <td></td>	433855085800005037699675781874205310772671333651538 11111111111111122111111111112211111221122212280796589	19434223 94434223 968523224 1005342249 11022329	44801719385787368105980477722213733967648852459168 776668690912225411681643274345058735721100651560946 776668690912225411681643274345058735721100651560946 777668690912225411681059804777222213755233027351901	77777777777777777777777777777777777777	890193456789019345678901934567890193456789019345678901934567 5536666666666677777777777888888888899999999	90586759887354994231221274536261122850745086770684 4377730309260689811178444101112745362611122850745086770684 10111127344200111111221001121 100111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 1001111111221001121 10011111111	711067282115835651307204584388003605877361573583827 809580044666688041743778648212457547940091228290012 121122112211112111221121111111111	89393666048385427868841903204300219067398872886201201 2110488110983102256021720610471579784483808864551188 111111111111111111121188	$\begin{array}{c} -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 $	77777777777777777777777777777777777777	33333333333333444444444444444444444555555	39311885491422912907476144709844146897128031694586 43051452350377220573348447102352392514582443995225 222001111122210023523948447102352392532274382643995225	768689929553628050131442978606577823966536733822626 111139012121111111111111111111110011129002223966536733822626 111111111111111111111111111100111119002223966536733822626	111 243 020 663 175	

WD	TAP	CPMEAN CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	66666666677777777777777777777777777777	$\begin{array}{c} 240 & 116\\ 149 & 115\\ 2061 & 116\\ 389 & 141\\ 1589 & 141\\ 1589 & 129\\ 1611 & 129\\ 1649 & 1129\\ 1649 & 129\\ 1202 & 1222\\ 1222 & 1226\\ 1206 & 110\\ 1206 & 110\\ 1207 & 12222 & 1225\\ 1207 & 12222 & 1225\\ 1207 & 12222 & 1225\\ 1207 & 12222 & 1225\\ 1207 & 12222 & 1225\\ 1207 & 12222 & 1225\\ 1207 & 1225 & 1225\\ 1207 & 1225 & 1225\\ 1207 & 1225 & 1225\\ 1207 & 1225 & 1225\\ 1207 & 1225 & 1225\\ 1207 & 1207 & 1225\\ 1207 & 1207 & 1225\\ 1207 & 1207 & 1225\\ 1207 & 1207 & 1225\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 1207\\ 1207 & 1207 & 120$	23910000783353614651577843405548581240069271893888397 23991019046738137192365608171537665909070228488165 23909101904673813419232432405548512111121212403128488165 23222324324025131111212124006927189388397 2321042131131111212121232321044881657			54567812345678501234567850123456785012345678501234 1111110000000001111111111111111111111	$\begin{array}{c} -1 \\ +5 \\ +2 \\ +2 \\ +2 \\ +2 \\ +2 \\ +2 \\ +2$	43009942820051228295655818997654397659245015362652 31224248421521110003422211100098894423010117804421001 111111111111222111110001342221111100098894423010111112221111111111111111111111111	- 349 - 312 266 106 - 136			11111111111111111111111111111111111111		177455305284822947401379475290883540250222421470836 11745511012094420001969743318800663433411846343441000 1111333111412000111032111110011111111111	13098224597812484827417526435612219 243975001312225863279351920016755 1312221994101112220016755	

ЧD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ЯD	TAP	CPMEAN	CPRMS	срмах	CPMIN	<b>WD</b>	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
A 888888888888888888888888888888888888	+ 123456789011234567890120345678901234567890123345678901234567890	N 1 1 1 1 2 3 4 3 3 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1	5 38803258773443067458876049854790919741255140407175 4 1111121111211111111121111111111111111	8421420520723567100706116635009865147785514801230 95964065765419670483906238663572996629235514801230 112222222225551459522242114120522215225514801230	51457031745939750480467451488399443457186533055810 686644408755518902987810079611129111885058191954044231998 68664408755518902987810079611129111885058191954044231998		. 12345678901234567890123456789012345678901234567890 555555555555555555555555555555555555		82890546444944835841959730884133422565424619273968 75933589606768332667780098835668646233334773581090922 2011	10964261382226024683717501577472904959474557637529 15723482027576794720116780115164911893173403374074 1111 111 11	-111111		12345678901234567890121234567890123456781234567890 00000000011111111112020000000011111111	503153471093313160442882637747538 <b>964741</b> 35872267527 262011115116524100577038838720245938 <b>65</b> 78237703022045511 20011112220011111210577038838720245938 <b>65</b> 78237703022045511 20001111222001111220011333033430112200022101122200000	952843828506292688550999999212011600570769509802222 2066601112211360019001235147155520023189210901112129000 1112112210001111212121121111111111	154 088 627 185	

ыD	TAP	CPMEAN CPRMS	CPMAX	CPHIN	AD	TAP	CPHEAN	CPRMS	CPMAX	CPMIN	ЯD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$	12345671234567891234567895678901289012345612312345 11111100000000000000111111222223333300000000	$\begin{array}{c} 1393 \\ 4985 \\ 1711 \\ 4985 \\ 1671 \\ 4985 \\ 1711 \\ 4985 \\ 1711 \\ 1227 \\ 024 \\ 1175 \\ 1020 \\ 1195 \\ 1020 \\ 1110 \\ 1020 \\ 1110 \\ 1110 \\ 1120 \\ 1110 \\ 1120 \\ 1110 \\ 1120 \\ 1120 \\ 1110 \\ 1120 \\ 1120 \\ 1110 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 1120 \\ 112$	<b>1</b> 282097633599303410776242034796901113599016024486623350 <b>1</b> 21227516499804955870049917969011102116728146662337798 <b>1</b> 111		00000000000000000000000000000000000000	6789012345678123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890		2009888868644793116338688736751603011427448216390218 3123110231126428311230900066521121100000095731010091098 111311011011122111111111111111221114110000009573101111110091091098	468910213445292120410761672591463 542232210110113222220410761672591463 	$\begin{array}{c} - & - & - \\ - & - & - & - \\ - & - & - &$	\$\$\$\$\$\$ <b>\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$</b>	11111111111111111111111111111111111111	75136136373817996808317032737927960004589282606453 42897799996070876730968967772237164988756908395475508 4210000004423200000014322320000002311000001022	28315215215212995635046827018546158894212339316155775 11110000434190096173210009951632097790420210908352 111101209083152	434 3168 09788 2269 2281 2324 1474	

មេទ	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	нo	TAP	CPMEAN	CPRHS	CPMAX	CPMIN	ыD	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	901234123456789012345678901234567890123456789012345678501 8999990000000000111111111111200000000000		33923461908329268010791224364532839923005494965215 2200099312469966679232357766889822344717019212566177 1111100111111111111111111111111111	46378864431644334730795368 6788231765364334730795368 92222333403128880444 1111	10934154154095094585213367328926534452463757018348	98999898999999999999999999999999999999	456789019345678901934567890193456789019345678901934567890193 44444955555555555666666666666777777788888688888899999	56429164888344629070710818712924580300766134500087 521429464888344629070710818712924580300766134500087 1 1 1 1 1 1 1 1 1 1 1 1 1 1 2 3 4 3 3 5 9 2 2 0 7 8 8 2 1 7 6 7 9 9 2 2 1 1 1 1 4 6 9 9 9 9 0 4 2 1 2 1 1 1 1 2 3 4 3 3 5 9 2 2 0 7 8 8 2 1 7 6 7 9 9 2 2 1 1 1 1 1 2 3 2 0 7 8 8 2 1 7 6 7 9 9 9 2 2 1 1 1 1 1 2 3 2 0 7 8 8 2 1 1 1 1 1 2 3 2 1 1 1 1 1 2 3 2 0 7 8 8 2 1 1 1 1 1 2 3 2 1 1 1 1 1 2 3 2 0 7 8 8 2 1 1 1 1 1 2 3 2 1 1 1 1 1 2 3 2 0 7 8 8 2 1 1 1 1 1 2 3 2 1 1 1 1 1 2 3 2 1 1 1 1	24711230412396461262356003746977762365791002682276 29258870582216671670810234679188015668452123346637 2111112121111111211211211111111111111	56057623274779809867718553101598 8489576232135924222222210509420635524 1112215205524	95293437975781296507647864310085335213519251471926	\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$\$	456789012345678901234567890121234567890123456789012345678123 9998998000000000001111111112120000000000	28155239429088738811510142370225829298834375992345 2111112962564111512204522115823222882244360120092777 3111111229625641115122045221158232228822443601200011110000	103348852194954135861469725144124342477821420456148 21100013222330912324500000111145457245529912089110099 21111111111111111111111111111111		$\begin{array}{c} -1 & -1 & -1 & -1 & -1 & -1 & -1 & -1 $

ШD	TAP	CPMEAN CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ЯD	TAP	CPMEAN	CPRMS	ср ма Х	CPMIN
ŎŎĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊĊ	45678901234567123456789123456789567890128901234561	$\begin{array}{c} - 101 & 1013 \\ - 1026 & 1126 \\ - 1026 & 1126 \\ - 1026 & 1126 \\ - 00132 & 1092 \\ - 00132 & 1092 \\ - 00262 & 1332 \\ - 1092 & 1092 \\ - 00262 & 1332 \\ - 1092 & 1092 \\ - 10$	875685344247654259499786647033727098868328241463092 03026853442476522656565215518381542453215248760731 222233534801184155447342155183815418675298866328241463092 11			2312345678901234567812345678901211111111111111111111111111111111111		697357505874258883073900849388511615255476772182029 11392523322361108003278875452100222214342110111122143421 11101112211122143421	91406700775249585784086195246586196112 9833968071809531025830559246324658196112 90511320051758331025924632465921005111	22763975812662956346659337958912392316561583624084	10000000000000000000000000000000000000	11111111111111111111111111111111111111		37313960276406564437128100887093047436183402512562 1111274534111111464101006574201000987633300879034321 11112221111111111111111111222111111000987633300879034321	732428908936138739354438318344 9612323222023223231222222445 9123232220232232312222222445 1222222222222223223122222222444	49953662353965819060543470972817031532179016914930

ыD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	шD	TAP	CPMEAN	CPRHS	CPMSX	CPHIN	ЯD	195	CPMEAN	CPRMS	СРМнХ	CPMIN
00000000000000000000000000000000000000	123456789012341234587890123456789012345678901234567890123412111111111111111111111111111111111	1 + + + + + + + + + + + + + + + + + + +	10001461627470958680097373748778459683145910176241 100234180300111754656877611227544556613485459101724145 10175111111111111111111111111111111111	3188154851875269 31541511565533110 321273232222323554	32730591959640783640788715481801104755850382894715		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	7514539879791023100504185321667762847601338333892978 4575060574540897977665330869655445955642465487789653 11124539879791023100504185328655445955642465487789653 11124539879791023100504185321637662847601338333892978	001699786887844574595807075468098771056017656540987 074586566110755864457111485074020144100517305456400 1011111050014311111111111111111111111111	6005108100501101111111111111111111111111	513215522223371272062246453019200109128636938693869386938645	00000000000000000000000000000000000000	7.8901234597.8901234567.8901234567.8901234567.890121234567.8901234 888959999999999990000000011111111112120200000000	82951320515419350991419558348746964798582040405257910 11111111111111111111111111111111111	67770048790455219565765455017877557790857400401988 11176668905000012232100001225000909112346868234845905000 11111111110101111111111111111111	126 053 497 046	+10005104000076317040300007051856774776664335049550

ШD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRHS	CPMAX	CPMIN	ЯD	TAP	CPMEAN	CPRMS	CPMAX CPMIN
11111111111111111111111111111111111111	56781234567890123456712345678912345678956789012890 1111100000000111111114000000000000000	- 1134266025300 1120496025300 1120496025300 11204960208800 11204960188153773214434318496010096555996226009 11200008932211015722070696555996226009 1111200029322110157220000115559996226009	06669341055591903569644788112855556487000714988970811 1111111111111111111111111111111110111111	111469368877943494464167695198759793050242237698014 7611205404416655445417845785257935465743845529328529 11125407438452852579354674312337325231	63602529187713277416534644199669708027739747620899		1234561231234567890123456781234567890123456789012345678901232 335535500000000000111111111000000000011111111		1543456930219630590644957318373866677087648585858187 11111111111111211211211212146197786421433551664582858187 132	617669768165710784799171085777785833821355788865 6175487940997108003196831250678548814801135578886 1377487940997108003174201232373782011355788865		1100 111100 11100 11100 11100 11100 111000 111000 11000 11000000	4567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123		37783139435686925611789583055315561232588916730237 32111111111321111111111111111111112148854210730237	$\begin{array}{c} -1 & 9 \ 37 \ 0 \ 0 \ -1 \ 1 \ 97 \ 95 \ 95 \ 95 \ 95 \ 95 \ 95 \ 95$

₩D	TAP	CPMEAN CPR	IS CPMAX	CPHIN	W D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ЯD	TAP	CPMEAN (CPRNS	срнах	CPMIN
11100000000000000000000000000000000000	45678901234567890123412345678901234567890123456789 77777788888888889999900000000111111112002020020	1 1	19849-2419-362-667-8629-1514-167-8582-863-9151-5652-56660-57-851 9496-5549-486-85-96-85-04-9-86-4-94-866-7-9-1 2391-24-24-24-24-24-24-24-24-24-24-24-24-24-	23900088871215072309043008578170185190400553308739 402857219644922665571463355629783829412430584848195 11111111111111111111111111111111111		©1007403/080010990000000000000000000000000000000	1330103788906731329408551912791185488846772397540226 335327886593304157600020127558935476934471122036378889 111111111111111111111111111111111111	294 3080-775 260 30 2516 24 67 686610307 92691844 0531406540 2 78315544544672453 4 3446674535354404034232736433 11223341111111212051111111112120545545355440403423245332736433	1493917700235794227258270 2748237473221731212229497 111 11	7997886504246747443413889985133178602096350157283295		01234567890123456789012345678901234567890123456789012123456789000000000000000000000000000000000000	64994028032472890726833745734528087387995276745243 2221111111222001111112222111112222111111	8082103975328350884142158473738505218188887558483 2231211111111111111111111111111111111	244 234 260 147	

₩D	TAP	CPNEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ШD	TAP	CPMEAN	CPRMS	CPMAX	CPNIN
00000000000000000000000000000000000000	4444444444445555555555555555555566666666	58599237343437688678860432008953100147946000239048521673 20125999237343437688678604320089531001479460002390485216226 1111100000091125776998853100144794600023904852116226	18912276127195779204450982946087453304417423469513 199901118000931125555100002244501009231132944377862332231	166881805381575511837022556391682112910672428210956 8453856732757504519758734232420554955955543561819 174452655455555197587342324426955455554356121722223554356554555955435655455595565545555455	154836113833482671872273850597248444796465566457;4	11000000000000000000000000000000000000	90108901084561281284567890128456781284567890128456789012845678901284567812845678901211111111111111111111111111111111111	5199275590079615141999970804128743877626051814473767 2235823978615141999970804128743877626051814473767 23000100010000402484770014003001183937180000098822140 300140000000000000000000000000000000	50474733399521660056658073555520286962024159717807416 7335544854534321292320536333564435649766440133249552 11121111111111111111111111111111111	46325591984610677335648743656415397146237625 749542175372821289127688555096114857474775538 21273422222443434344715732445553821323232323222	$\begin{array}{c} -1 & -1 & -1 & -1 & -1 & -1 & -1 & -1 $	12200000000000000000000000000000000000	789012345678901234567890123456789012345678901234567890123456 11112222222222233333333333444444445555555555	826074043848048777774403010002210842240658089749041 7776687804352469887988907845999991129369988998831309887988564 0000013522469867988707774403011111129369988998831309887988564 100000013522410000011111111000000987988564	141925918552113441488698353968736742302941917776665 1111232896422142348196311113457642111235216422033441 111111111111111111111111111111111	6135923567276139223262877675579958347450 41405927001296934860210423752724857090263 43222433577343222484333424237527248857090263	

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A ; SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN

1	P	G	G	F	A	2	6.

 	CPMEAN		CPHAX	CPHIN	¥D.	IAP	CPMEAN	CPRMS	CPMAX	CPHIN	шD	TAP	UPHEAN	CFRMS	CPMAX	CPMIN
P 789012345678901234567890123412345678901234567890123 A 66677777777888888888999990000000001111111111	H 890020098668756000570113088715487591450664343319527	5 3553221284901430447424997401119257527112279251102998 87743198149432301488174100245880077783951458800010929 6	596782256565648936495689289975549 473472411277777248971249518977589 473472411277777248971249518977549	51639819351796572718946398849471639468797590851508	+ 2000000000000000000000000000000000000	. 34547880+234567880+1234567890+234567890+234567890+23 : 24342433335555335354+4444444455555555555	0907929745112291185853010171755747004773638886063942 1163089412231042428940500846039365110893138343997750834 1100012122104242894050084603282222110031213834397750834 11222222211000121222222110001212222 1100012122250834	16791440016597899606868888860855145077558889195097246 345558089809544466767662465885504445657455344333335550 44456545534435335355504	0170971573039237943113426655411966345392 123749855571133574322489354312733546345392 11	14650055313942873100628738241765550843404644853978 8600570024932150749171582333487688809164880574419751 99677700078198667891882857939905885998807088554419751	00000000000000000000000000000000000000	34567890123456789012345678901234567890123456789012 777777888888888800999999999000000000000	99660558840058840589500055807090086084156735961366 198688838212255456212187545527310255144219465841360 2112900112220000001222110000000122100000122 1011111111	040015150500445000549090701111064004074070943619 8745560555541224765547411124601155558762004071111111111111111111111111111111111	55554111233795772126 5598686548705837999	20707037919781151202520473096584607064229334006642

ЫD	TAP	CPNEAN C	PRMS C	PMAX	CPHIN	B D	TAP	CPMEAN	CPRMS	сриах	CPMIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
11111111111111111111111111111111111111	12345678901234567812345678901234567123456789123456 00000000000111111111000000000011111111	- 19611157944 - 117777944 - 003962200428139175974 - 0088204281391103974779810 008820428139110397479810 	. 138 1 . 110 . 095 . 103 . 104 . 096 . 123 . 127 . 127 . 127 . 127 . 128 . 127 . 139 . 139 . 139 . 176	33741212334212334422334422334 4214511651195019621		11111111111111111111111111111111111111	7895678901289012345612345678909999999999991111111111 0000111111222225555550000000000	111366637454999148191136913697910422287100844065817695313 11200553745499914819113024600646422287100242214995313 11200646065817695314499531491000646200085344226000884065817695313	74405753977054298712694394240708973766760858957331 62320105127535429871269439424070897376676085895202211	6243342212224436551870164237313154124 62433422122244366243782987313154124		00000000000000000000000000000000000000	012345676901234567890123456789012345678901234567890123456789		41284193059739571448186411115272133158634488871788206 11218341930597395714481864111152764211111224114 1111111111111111111111111	75698630499882518590677422009127851416765 6576409746484033272002677535733647182803348 72234233222233344332220267753573364718280348	777784385769871445598786131280578292158186789535446 7777844385769871985765452748643008107997458145699

ыD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	ТнР	CPMEAN	CPRMS	CPMAX	CPMIN	ыb	TAP	CPHEAN	CPRMS	срмах	CPMIN
	012345678801234567880123456789012341234567880123456788012345678801234567880123456788012345678801234511111111111111111111111111111111111	21978378892677587178254548180041021356872702603986 99988367542107677587178254548180041021356872702603986 000011154210767758717825454818000410011356872702603986 0111111111111111111111111111111111111	82703758438130969969823451970041577037264696991797 011122443210077113010911145740210144455791499013358 0111111111111111111111111111111111111	23438647453674538717844374445735788714568846778287888 3906886884745387111544877448744457888458978881118864778888097 3236688686474538111174488787874444578884588946738142886473814468 30068868846474538111111	139629162103057304542723964675686925338440504847934 486192648481749968865940395098826431730003969751067 44567769844423652455346279755445120777002998751067	00000000000000000000000000000000000000	&7&\$^\$+\$MMANANANANANANANANANANANANANANANANANANA	14404324474641942446010400896028018120255118344467 	59099844419622999999999226098971097606914266997246448 2780429164948494828705444724376683599107679453709556682 21222524294641111223999999705444724376683599107679453709556682	855 991 8930 8920 892 892 892	76037612940769870964944049163225062678941661046977 56777779758776999887764997864944049163225062678941661046977	00000000000000000000000000000000000000	67890123456678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890	81207356601882731223546515249510939464399?153211293 74477224468282232125217039291500071454899?153211293 	089726082799880762034423846393304872178121499269207 224893183647987535222489433462113785313247765232222	2384249562275928193315840012394175289933220086+2992 662294544826538890342814577078208955588831113788440100 73566851113966686743553545883553454555588831113788440100	

U D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	6789012123456789012345678123456789012345678 33333334444444444444444555555555555555	9080848404857160449436747700137914447013525002619 900000000000000000110022037400135250026000	42240873440621140604398318353824750535261159604934 44763211463233129090009999003310024511902321190001000 11111111111111110101111111111	90156858982197955206575177912778457427076575149837 77498767823050464727789414466298492629315559525950530 567635278234534534535555555206575177912778457427076575149837		11111111111111111111111111111111111111	91234567895678901239012345612312345678901234567812 0000000001111112222033333500000000000000	59036605960760745698823410395105569742377921284559 0152747434106153501095290710551443501523331222136854473 0101000000001100000000000000000000000	55124552453293719769805211162787813354321929825178 122125661209014111721122066320022024384064698599337109 121111111211112111111111111111111111	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		11111111111111111111111111111111111111	3456789012 345678 9012 3456789 012 34567890123456789012 34567890123456789012		1848992789 874784975584809968422579087827451608153 3 1111111111111111111111111111111111	286 237 245 363	+5269301138106282275906753880159527701378135684510

W D	TAP	CPNEAN CP	PRMS	CPMAX	CPMIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
14400000000000000000000000000000000000	34567890123456789012345678901234567890123412345678 5555555555666666666777777778888888888			43128203201617040276201487691102795480904729705701 2222521212121211322222102211211221142993052705334724870969 22225212121212122121132222210222121122112211422211222222233589000 11		140 140 140 140 140 140 140 140 140 140	901234567890123	- 009347993350081522001521221221212121213569652756 - 12230850815826552266527107113580000122171125820000074435000112217125820000075237335696522756 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	20297225443140269384716609291842163101021131900857 20923571334397922459481686123407773675695505323348 20111112222111111112222118407773675695505323348	547984255425966467632 11115566675966467632 11115566675966467632		00000000000000000000000000000000000000	90123456788901234567890123456789012	3222829986330399977229650686325567663013538340536006 320962316630850737621929292350259154953354777077091970 1 1 1 1 1 1 1 1 2 1 0 1 3 2 2 2 0 0 0 0 0 0 0 1 2 3 5 4 7 7 7 0 7 7 0 9 1 9 7 0 1 2 3 5 0 0 1 0 1 1 2 3 5 0 0 1 0 1 1 2 3 5 0 0 1 0 1 1 2 3 5 0 0 1 0 1 1 2 3 5 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 1 0 1 1 2 3 5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	8652174845915438000710752877828839900364694223835335 221144221338220161434591844010349742541001157844602238 11111112211435915438000710752877828839900364694223835335	$\begin{array}{c}1\\1\\5\\5\\5\\6\\6\\2\\2\\2\\6\\6\\3\\5\\6\\6\\6\\3\\5\\7\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6\\6$	

WD	TAP	CPHEAN	CPRMS	CPNAX	CPMIN	U D	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	MD	ΤP	CPMEAN	CPRMS	CP MA X	CPNIN
D 000000000000000000000000000000000000	T 333333333333444444444444444444555555555	CPMEAN 20378 110685333227033794 237801102853332210094994 232120094994 10020011094522336878665734 10000005522336878665734 1005997566644457 10059975666644557 10059975666644557 10059975666644557 10059975666644557 10059975666644557 10059975666644557 10059975666644557 10059975666644557 1005997566664557 1005997566664557 1005975566664557 1005975566664557 1005975566664557 100597556666555 10059755666555 10059755666555 100597556665555 100597556665555 100597555 100597555 100597555 100597555 100597555 100597555 10055555 10055555 100555555 10055555 100555555 100555555 100555555 100555555 10055555 100555555 10055555 100555555 10055555 1005555555 10055555 100555555 100555555 100555555 100555555 10055555 100555555 10055555 100555555 100555555 1005555555 100555555 100555555 100555555 1005555555 1005555555 1005555555 1005555555 10055555555	CPR 168887112991201111100000000000000000000000000	X 4996248001484775240456358053081320906159001950254 A 0098431871051594108587451066389298398613200477968896 P 8856446679976597446858745106638081320906159001950254 C	C	U 000000000000000000000000000000000000	P 23456789123456789567896128961234561231234567896112 F 6656666677777777777777777777777777788699999999	HH H H H H H H H H H H H H	CPR 11995062488905450489478455350894349860052410134754507	031704939147797692989103316862463865212241107546 223633266645578444345043631476401076560934867934 2236332666455784443450436916862463865212241107546	C P P 443355745739524862812501332426200028430558838682801	W 4666666666666666666666666666666666666	P 45578123456789012345678901234567890123456789012345678901234	N 2712712710774559349800923081538933834604208029007022 P 23334222222221232900890923081538933834604208029007022 1112121222112222211122222111122222211112222	C PR 201684560244 213354560244 213354560244 213354560244 21333676556024 2133367265653300186344 2121011111111111111111111111111111111	280 455 418 291 206 190 221 228	N 17206975558924947743332979884466253352717277940857

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN PAGE A 32

W D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ND	TAP	CPMEAN	CPRHS	CPMAX	CPHIN	₩Đ	TAP	CPMEAN	CPRHS	CPHAX	CPMIN
11111111111111111111111111111111111111	67890123456789012345678901234567890123456789012341 444455555555555555555555555555555555	9062773195724775840663897504046127418203567691559469 22221976478010758406638975040461277418203567691559469 11111111111111111111111111111111111	31582716026485741729054464916520772183001742617643 111101101104857417290544649165207721830011742617643	890186580716586178555832734442159969386667272613203 035865720716586178555832734442159969386667272613203		00000000000000000000000000000000000000	234567890123456789012345678901234567890123456789012345678901 000000000011111111111111200000000000		97392416619973465680854682574397544456263581030371 432455856531445886874212222566972323243588662134477777	010598125891258917514542536710577299033983749509852 12362244708598535779887146347343228853342693712988695 11111 1111 1111 1111 1111 1111		00000000000000000000000000000000000000	23456789012345678901234567890123456789012345678901 3555555556666666666666677777778888888888	97333147104640187975228281194017603701687232229241 90089416742647573821223862461000603620744067518194 	17997288811109693592114534379132960973036118386293 111235786111021693592114534379132960973036118386293 111247516023333774443322313753254118386293	3768763649029666434496666548076127119156020563355574 7412662112835378481172551440280502857156810867444555799 11 11 11 11	

$\begin{array}{c ccccccccccccccccccccccccccccccccccc$

WD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	80	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	80	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
	90123456789001234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890001234567890012345678900123456789000000000000000000000000000000000000		1012081115192089249939549453113645751523339877501410585 1111111111111111111111111111111111	9359676270441586793021781578112101210121111221111112 02878483746461586793022178157811210121012111122111112 04694271312111111111111111111111111111111111		00000000000000000000000000000000000000	90;1234123456789012345678901234567890123456789012345678901234 8999990000000011111111111220002020202333333344444		46168372563590890803036244878806864792469934698455 00211124453554454242346768852222355667764221124565852522 11111111111111111111111111111111	85472427247626656936786818704000888831152772124447626656936786818704000888831124668335332 1121212355775542211780020743113489635882736688335332 111111111111111111111111111111111		000000000000000000000000000000000000000	5678901234567890123456789012345678901234567890123456789099 \$4\$\$\$\$5555555555566666666677777778888888888	79082282787291204456197583051536521366927343985006 2135553393922575314976001072035028620009448238823885006 11102455533101102444203502862000944823823885006	083223333133062972878621529140540889435825788969019 246978842234576552111123355441702433456532112233425229019 111111111111111111111111111111111	$\begin{array}{c} 3 \\ 6 \\ 6 \\ 8 \\ 9 \\ 0 \\ 5 \\ 2 \\ 2 \\ 0 \\ 5 \\ 2 \\ 2 \\ 0 \\ 5 \\ 2 \\ 2 \\ 0 \\ 5 \\ 2 \\ 2 \\ 0 \\ 5 \\ 2 \\ 2 \\ 0 \\ 5 \\ 1 \\ 2 \\ 2 \\ 0 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 5 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2$	

WD	TAP	CPHEAN	CPRMS	CPMAX	CPHIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
160	295	. 136	. 125	. 549	247	160	505	- 194	111	.107	- 583	160	803	193	. 106	. 547	144
160	296	109	117	503	- 220	160	506	- 185	. 105	. 146	531	160	901	- 350	. 138	. 066	827 -1.063
160	297	160	115	654	172	160	507	- 184	108	170	538	160	902	- 332 - 326	. 177	237	955
160	298	. 265	. 128	.678	- 180	160	508	. 080	. 199	. 973	652	160	903 904	- 379	. 195	244	-1.274
160	299	. 364	. 126	.852	094	160	509	. 032	. 141	. 512	599 408	160 160	905	- 321	167	217	-1.136
160	300	389	. 128	.847	057	160	510 511	. 038 . 062	. 104	. 429 . 432 . 372	- 295	160	906	- 384	193	196	-1.136 -1.198
160	301	. 348	133	.820	- 057 - 076	160 160	512	- 044	116	372	- 471	160	907	- 353	. 169	. 306	-1.182
160	302	. 286	.128	.699 .891	- 144	160	513	- 144	108	181	- 523	160	908	- 327	. 165	. 143	952
160 160	303 304	. 291 . 278	165	.910	- 198	160	514	- 051	125	. 478	486	169	909	369	. 168	. 147	-1.270
160	305	218	120	657	- 182	160	515	. 184	125	. 690	267	160	910	391	. 220	. 306	-1.846
160	306	321	. 123	.732	162	160	516	256	. 108	.706	019	160	911	- 308	. 163	105	-1.212
160	307	. 370	. 133	812	.006	160	517	. 158	.105	. 544	236	160	912 913	319	. 182	225	-1.526
160	308	398	. 141	. 933	068	160	601	028	.107	. 345	398 653	160 160	914	- 304	153	230	-1.005
160	309	. 359	. 133	. 8 9 3	- 039	160	602 603	- 194	. 103	331	- 469	160	915	- 329	167	192	-1.181
160	310	. 303	. 1 39	.845	150 189	160 160	604	- 056	103	243	- 465	160	916	301	. 147	. 157	855
160	311 312	279	. 119	.802	- 178	160	605	256	. 121	686	- 166	160	917	296	. 143	224	936
160 160	313	190	136	578	- 209	160	606	- 058	110	253	4 4 4	160	918	- 302	. 122	. 053	769
160	314	144	118	.535	250	160	607	- 337	. 238	253	-1.545	170	101	203	. 122	. 274	616 764
160	315	248	. 124	.722 .953	143	160	608	238	. 140	. 217	825	170	102	- 220	. 120	. 184	692
160	316	248	130	. 953	068	160	609	. 151	129 121	577	4 4 6	170	103	- 217	125	176	730
160	317	. 403	. 1.47	. 928	- 018	160	701	. 039	109	. 410	- 108	170	105	- 218	129	265	- 646
160	318	457	137	.947	.020 029	160 160	702 703	219	105	590 525 686	- 182	170	106	- 237	124	. 096	818
160	319	. 411	144	.883 .980	049	160	704	254	127	686	- 265	170	107	- 234	. 121	240	- 910
160 160	320 321	365	. 140	804	- 078	160	705	207	127	. 7 6 3	- 265	170	108	- 224	120	. 204	661
160	322	291	136	851	167	160	796	207	. 117	. 682	- 151	170	109	- 229	. 115	. 179	- 608 - 708
160	401	291	191	1.122	311	160	707	. 179	105	. 584	- 252	170	110	- 218	. 113	. 209	663
160	402	253	149	1.122	215	160	708	. 230	106	634	136	170	111	- 216	. 116	198	596
160	403	. 041	. 124	. 526	412	160	709	228	. 113 . 099	. 549	- 131 - 135	170	113	- 191	1114	172	- 582
160	404	. 091	. 1 0 9	. 541	- 279	160 160	715	. 191	.115	. 604	- 172	170	1:4	- 191 - 213	128	. 220	972
160	405	289	129	.837	- 155	160	717	179	102	589	- 203	170	1:5	- 199	111	. 133	615
160 160	406 407	. 258 . 208	115	.618	- 181	160	718	285	. 120	. 897	055	170	116	198	. 115	. 162	632
160	408	338	137	923	- 071	160	719	. 356	. 139	. 891	033	170	117	- 215	. 115	. 116	622
160	409	- 013	105	. 369	381	160	720	. 21 2	. 100	. 594	- 130	170	1:8		. 112	. 284	622 583
160	410	015	. 1 0 4	329	413	160	721	. 144	. 094	. 459	171	170	119	201	. 106	.130	580
160	411	033	. 1 1 1	286	- 478	160	722	. 289	. 119	. 727	068 117	170	1 11	- 193	108	151	- 652
160	412	052	.110	. 328	420	160	728 729	. 208 . 192	.097	. 540	184	170	1 2	- 199	105	. 158	- 545
160	413	. 229	.141	.659 .542	- 209	160 160	730	190	104	597	- 186	170	i : 3	- 254	120	. 232	763
160	414	. 233	.094	.629	- 230	160	731	192	108	595	- 251	170	1.14	190	. 106	. 173	528
160 160	415 416	089	116	285	547	160	732	138	099	595	179	170	1 - 5	193	. 108	169	576
160	417	088	114	281	510	160	733	060	. 137	. 338	605	170	16	184	. 113	. 213	560
160	418	- 068	. 113	324	- 393	160	734	. 128	. 101	. 460	249	170	1.7	213	. 113	. 183 . 197	627 610
160	501	. 259	. 199	1.054	432	160	735	.010	. 119	. 445	453	170	1:18	209 211	. 117	. 177	- 668
160	502	207	. 1 1 8	. 241	- 680	160	736	. 118	. 114	469	- 295 - 238	170	1.30	- 199	115	207	547
160	503	197	.112	.162	- 664	160 160	801 802	.140	.118	. 565	- 379	170	171	- 202	. 110	. 129	- 530
160	504	189	. 1 02	.147	504	104	0 Y Z	. 1 4 1	0			• • •	• • •				

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	UD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	90	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
111111111111111111111111111111111111111	23456789012345678901234567890123456789012345678901	111 1111 111 111	39927148321427796903033798454381526574083606909456 000000000000000000000000000000000000	83366147919595339825586236069180708294171419514824 662966147919595339822558623606918070829417116001111211 11211211222121221122112208533636941701419514824		11111111111111111111111111111111111111	234567890123412345678901234567890123456789012345678901234567 886868899999900000001111111111222222222222222	- 1297150578290229373131392338894580138886033492478623335 - 12972971505778290229337313923388945801388860334924125679 - 120729202293373139233889458013888603349224786233535	523882367347941218920515932721913698744186667345750 120001010212121334439443323126577776422222147777752221125 11111111111111111111111111	11111111111111111111111111111111111111		17770000000000000000000000000000000000	22222222222222222222222222222222222222	498460595459208064081265257294728432287920206388588 543545243740516066152171325330365418889031933350159 1122245542011013554112221013443101123433221101122	44286062879444869806927599505663677346286453944992 111111111111111111111111111111111	$\begin{array}{c} 35881558815548069287355280145528225632890593841770666729070\\ 119963454806928735280146512257651229632890841808177066729070\\ 11111111111111111111111111111111111$	

P	A	G	Ε	A	37	
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W D	TRP	CPMEAN	CPRMS	CPHAX	CPHIN	ыD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
111111111111111111111111111111111111	r 8899123456789012345678901234567890121212345678901212345 1111111112220000000001111111111112111111	372 3579 191 2191 2191 2191 2191 2191 2191 2191 2192 2191 2191 2191 2191 2191 2191 2191 2191 2191 2191 2286 22716 3341 3202 2106 3342 22306 2213391 3442 2237 2213391 4412 22352 2015 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255 2255	5 27304159222933219328739626911245998884551850012991811211212459988845518500129918112112112112459988845518500199181129112111211121112111121111111111	21031610902434712445046584680988077838481968897031 88956436679888866987997.6656565764998867173448681183223562 1 3 4 5 4 5 6 7 8 7 8	28173866272383645114776776776696304123372474096659083	17700000000000000000000000000000000000	4445555555555555555555566666666666677777777	- 1447 - 15200234 - 152002234 - 152002234 - 15200237 - 221734 - 22174 -	100787705111006883469066831109066831109066834690668346906683469066834690068834690068834690011110009100011100099032968033539	335057589517665415520263484500508973963903210770747 71346270077485914985894012432946587609213656082925 71346270077485914985894012432946587609213656082925 7134627007747		17700000000000000000000000000000000000	23456123123456789999999999999111111111111111111111111	36140224005659007632592607766172984667194441382742 1012284232152222597178666122222222179912100029830 1012284232152222597178666122222222221799122100029832 122222222222222222222222222222222222	996442277449064336828777335741938759903453243111111111111111111111111111111111	21638 16678 12697 1697 1694 1241 1694 1241 1631 1467 2197 12731	964743197092081601090528483907550804046305118833132

WD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	WD	TAP	CPMEAN	CPRNS	CPHAX	CPNIN	WD	TAP	CPHEAN	CPRMS	CPMAX	CPHIN
	56789012345678901234567890123456789012345666666777777 2222223333333334444444445555555555556666666666		452282033484699510111694319695803265206735435613029 1112111101111098319595803265206735435613029 11111011110989	27955249694396118209207649242878680134848280010035 66743617140398049219299511746583872447948198613 121212224481980492192995517465838724479481448198613 1212122447948198613	<pre>(</pre>		11111111111111111111111112222222222222	- 1974 - 12768 - 116768 - 12254 - 12267 - 1267 -	02739720864006174634931109565826730930680804458011 11111111111102344333354233842387667523121111111111111111111111111111111111	403062155866798765541446555421112402198532101471985 729862155866798765541446555421112402198532101471985 71112111112112211221221446555421112402198532101471985 1111			12345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890		81583688812183644209556829851634666103018129085342 11122334778644220878655568298516346666103018129085342 111111111111111111111111111111111111	$\begin{array}{c} 4 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\$	1 1

APPENDIX A -- PRESSURE DATA / CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN

PAGE A 39

180 281 180 132 .654 254 180 409 061 .103 .245 496 180 720 .273 .106 180 282 .108 .124 .535 289 180 410 102 .108 .271 550 180 .721 .248 .113 180 283 .121 .126 .507 324 180 411 152 .114 .207 527 180 .722 .307 .110 180 284 .068 .134 .576 332 180 412 .137 .120 .315 616 180 .728 .246 .105 180 .284 .068 .134 .576 332 180 413 .028 .127 .649 358 180 .729 .218 .107 180 .284 .066 .134 .576 .332 180 413 .028 .127 .649 .358 180 .729 .218 .107 <th>609 - 110 573 - 119 689 - 105</th>	609 - 110 573 - 119 689 - 105
180 285 183 180 749 .235 180 749 .235 180 729 .216 107 180 286 .216 123 180 .113 .028 .235 180 729 .216 107 180 286 .216 .123 .111 180 .115 .007 .214 .450 .474 180 .733 .216 .007 180 286 .216 .124 .450 .474 .287 .216 .124 .450 .474 .275 .006 .216 .017 .244 .019 .019 .275 .216 .017 .016 .019 .019 .019 .019 .019 .019 .019 .019 .019 .019 .019 .019 .019 .019 .010 .	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN PAGE A 40

P			40

WD T	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	WD.	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	WD	TAP	CPMEAN	CPRNS	CP MA X	CPMIN
	- 111111111111111111111111111111111111			x 372323027427238145101766885593751708955361390787182 222156110224892678056685593751708955361390787182 1122211021122678056685593751708955361390787182			1111111111111111111111111111111111000000		663918585225948825577420835698304265741275588957053 111110701100002261010001258353454433545366886534334	22216239511844135563355033334916438811884459 0011141221202211211212135777663312		11111111111111111111111111111111111111	456789014345678901434567890143456789014345678901434567890143	- 242331076555730311987884505020947614412515669943236	2484164202758084150815443257062226492846666686459265 111111111111111111111111111111111111	$\begin{array}{c} 22254572841748485457792616410926442481133450097714713\\ 111259803259599422984587398410926442481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599422481133450097714713\\ 111259803259599442481133450097714713\\ 11125980325959942481133450097714713\\ 11125980325959442481133450097714713\\ 11125980325959442481133450097714713\\ 111259803259594424811334500997714713\\ 111259803259594424811334500997714713\\ 1112598000000000000000000000000000000000000$	18853502587608089893542113446291941444566152254899425

WD	TAP	CPMEAN CPRMS	CPNAX	CPMIN	80	TAP	CPMEAN	CPRMS	CPMAX	CPNIN	ШD	TAP	CPHEAN	CPRMS	CPNAX	CPMIN
111111111111111111111111111111111111111	45678901234567890123456789012345678901234567890121 777777888888888899999999999990000000000	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 12268495\\ 12368495\\ 998646700\\ 138616700\\ 138616700\\ 138616700\\ 138616700\\ 1986465922397462378780\\ 198646592239746237780\\ 19864659223974663327780\\ 19977601440\\ 19977668\\ 19977601440\\ 19977668\\ 19977668\\ 19977668\\ 19977668\\ 19977668\\ 19977668\\ 19977668\\ 19977668\\ 1097668\\ 1097668\\ 1097668\\ 1097668\\ 1097668\\ 1$		11111111111111111111111111111111111111	23456789012345678123456789012345671234567891234567 0000000011111111110000000001111111100000	1242778824070555626518887604337802750916577229501144777487 	6831830365044260159505031936983399148973308555360162 1111112300000142283295050319369833991489733085570091162 1111111112300222444118973308555360162	17867252812451125101019715982923054620715950379624 94678982111132311121163211210322121533245656666 1	1096889706532112991971555480606290638931808635962	11111111111111111111111111111111111111	777777777777777778889999999999999999999	56152238927653219336185787106657126446373768654105 222233222235222211101223910920610216586744598890133456	74428745901105691578065038502534078812227337193804991 11109092111110002268502534078812227337193804991 1111111111111111111111111111111111	25142 1142 1484 11730 4030 40743 12095 14065 140555 140555 140555 140555 1405555 1405555 1405555555 14	$\begin{array}{c}$

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A ; SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN PAGE A 42

UD TAP CPMEAN CPRMS CPMAX CPMIN UD TAP CPMEAN CPRMS CPMAX CPMIN	ND TE	P CPMEAN CP	PRNS CPMAX CPMIN	
WD TAP CPHEAN CPHIN WD TAP CPHEAN CPHIN CPHEAN CPHEAN CPHIN 200 111 243 .131 307 723 200 161 197 121 .239 648 200 113 184 .133 .307 662 200 161 197 121 .239 648 200 114 184 .133 .307 601 200 163 196 .126 .126 206 206		789012345678901234567890123456789012345678901234566789012345664969	RMSCPMAXCPMIN152 804 -130 189 -141 534 -135 083 -144 267 -145 436 -145 436 -145 436 -145 436 -1921 212 1921 212 1921 212 193-1731237-1731237-1731237-1731237-1731237-1731237-1731237-1841033175-1841046-077152952-243158466-158466-158466-532130216216-237138137236141191123138136-1372361372361384-12313841241531372361384-23911641627201384-141191152-15	

W D	TAP	CPMEAN	CPRMS	CPHAX	CPHIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	₩Đ	ΤΩΡ	CPMEAN	CPRMS	CPNAX	CPMIN
 NANANANANANANANANANANANANANANANANANANA	- 78901234567890123455678901234556789012345567890123455678901234556789012345		88650244755471563610909421135540682250623595234879725 111111111111111111111111111111111111	9437544811344109644199022664927572150301817062025346 000762012909766547878876564389887755466897866557788		00000000000000000000000000000000000000	78901212345678901234567812345678901234567890123456789 1112222000000011111111111000000000111111	43681115468049365590756694448883277611973378841643061035 1111661680493655907566944488832776110222222222222222222222222222222222	62840961059294549170839368256360865917072722462827 11111111151125022945491708393682563608659170727224462827	301 469 246 200 190 175 614 206		00000000000000000000000000000000000000	777777777777777777777777778889999999999	83017295317981895395396197233598401363419796290409697656212 227886179816468107233598401363419796290409697656212	882678547726682749831044523424119991389631159315062 11100078547726682749831044523424119991389631159315062	.138 .314 .145 .285 .255 .157 .197 .198	

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- E ST TOWER IN

PAGE A 44	P	60	E	Ĥ	44
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U D	TAP	CPMEAN C	PRHS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD.	ΤP	CPMEAN	CPRMS	CPMAX	CPMIN
	4567890123456789012345678901234567890123444444444444444444444444444444444444		1111212221111111111221111111111122211111	71759232794942697919516476933700424799434394741 322100222222221310112368371958940349887064505078956	499443284114064115216033036118507485979288838297679		11111111111111111111111111111111111111	- 14633182500239393333933334483073600021417998233334833493351004172539	0282889335328699331288827053138337761055800906493764 22121444821021110135558138337761055800906493764 111111111111111111111111111111111111	1112222111110011131211222112221013666517730 96641655567733226437591378481006051779068711 100111312122211222112220136665434079344773		22222222222222222222222222222222222222	01234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789		567996844697801515537149553988697679543946179681745 8819664444558015155371499533988697679543946179681745 11111111111111111111111111111111111	228 941 967 1 9921 839 518 437 189 142 103 143	

WD	TAP	CPHEAN CPR	IS CPMAX	CPMIN	M O	TAP	CPMEAN	CPRMS	CPMAX	CPNIN	N D	ThP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	01234567890123456789012345678901234567890123456789 6666666666667777777777888888888899999999	$\begin{array}{c} 087 & 1 \\ - 238 & 1 \\ - 291 & 1 \\ - 2967 & 1 \\ - 2466 & 1 \\ - 2455 & 1 \\ - 4552 & 1 \\ - 4552 & 1 \\ - 4552 & 1 \\ - 4568 & 1 \\ - 0489 & 0 \\ - 1994 & 0 \\ - 2264 & 1 \\ - 2264 & 1 \\ - 2264 & 1 \\ - 2264 & 1 \\ - 2264 & 1 \\ - 2264 & 1 \\ - 3855 & 1 \\ - 3$	347 29741403703779035001103997121 297414037097722387790735001103997121 207742119965220238799372500119997512100751665144611446119 2077221996522022199937756654460596651555080802 207722199937234663342055555665446654446655555080802 20772219937234663342055555665446654446655555080802 1 887234665174665446654446654666565555080802 1 887234665174665446654446654666565555080802 1 887234665174665446654446654666565555080802 1 8872346651746654465465446654666565555080802 1 88723466544665466544665466546654666565555080802 1 887234665314665446654665466546654666566565555080802 1 88723466546654465545665446654666566566566656		22222222222222222222222222222222222222	01234567890121234567890123456789012345678901234567890123456789012121411111111111111111111111111111111	121 1384 344070126815939736097440939693847303540223675213 111214000768115959736097440939693847303540223675213 1112222223675213 11122222223675213	6992627840393032320623265555240568599851819297870184 1111334221111012326122200002011210965200284522798111 111111111111111111111111111111111	55588888766665566878212253422183232114141112248832 55588888766665566596878212253422183232114141112248832 56782498535227596878212253422183232114141112248832		2100 2210 2210 2210 2222 2222 2222 2222	34567891234567895678901289012345612312345678901234 6000000 600000 600000 600000 60000 60000 60000 60000 60000 80012345612312345678901234 50000 8000000		97132180817935664164264237324005378808235983717648 10111218210001110121111111111111111111	1716279360038906636266330605794838866225166167 336666666866978688665566579954594496523783 6666686686697868886655665579954594496523783	

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- E-ST TOWER IN PAGE A 46

ШD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD.	T P	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	56781034567890123456789012345678901234567890123456 11112000000001111111111111111111111111		19834107414433705506728274900924261077355765242733 217655456724215833335550982721333347902933332233457402331 2111111211221122112211221333347902933332233457402331	12691771355573560794450535336002062355380437921079 110773774947845775147464156466235589280437921679 1211221141211011223121120001112220013589280437921679		00000000000000000000000000000000000000	789012345678901234567890123456789012345678901234567890123456789000		09467744072981113949500089160988112075981282445889 11123122123483033110111337333011123613200111139473338 11111111233613200011111394733380 111111123613200011111123889	1393056723424165017948881144655507920133902718870 12201212121211011168968874111932450399726451438230 1111011110121212110121211012211212000000	28832228741505545504912021664339883661603302405918	00000000000000000000000000000000000000	34567890123456789012345678901234567890123456789012 20222022222222222222222222222222222	596609??*40404592??82232??07838?3?39626980218819802 00123444402431014433332354202343355302343553023435131022	92564524578921828807901736970330404042714008493793 74334709842976555677470997435577399766555669657444	$\begin{array}{c} 1567\\ 2024\\ 1007\\$	

						TAP	CONCAN	****	COHAY	COMIN	ដក	тр	CPHEAN	CPRMS	CPNeX	CPMIN
D 000000000000000000000000000000000000	C	P 1211111111221111111111111111111111111	C PM 08936557334601134722272174150116334214445098001134996 705886936577610216415011655747227787788542778055557809800111 1 09655547222663342144405057405532996 1 09775546098001134996 1 097755555555555555555555555555555555555	C	D 000000000000000000000000000000000000	P 34567890123456789012123456789012345678123456789012 A 000000011111111112220000000000111111111	C P M 11459668874839977667588456888240111521445866158320576900 114496733333352475548456888240111222322221285730921211112223222212857333144409438861583205769000 1	S 72805650696160990379613394403574339826991272164235 P 1123210101344609903796133394403574339826991272164235 P 11232111111111111111111111111111111111	201 175 160 158 723 255 657		D 000000000000000000000000000000000000	T 55555666666666667777777777777777777777	C C	C C C C C C C C C C C C C C C C C C C	8340038206975904538154793795142613544453883813064 212593211732226657885655788666666675454555667144313064	E []] [] [] []] [] [] [] []] [] [] []]
		1 1	$\begin{array}{c} - & 0.0 \\ 0$	- 312 137 108 - 606 1391 1018 - 506 1721 1156 - 522 1931 1085 - 337 173 686 0951 150 643 - 284 140 156 - 3422 159 115 - 284 140 156 - 3422 159 115 - 284 140 156 - 2951 209 6033 2744 1999 974 469 469 1911 1066 486 486 17511 410 522 2921 152 921 157 $- 2941 140 0722 -22941 1260 0722 -22941 140 0621 22991 140 0621 22991 1357 5261$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} -312 \\ -312 \\ -668 \\ 217 \\ -729 \\ -925 \\ 220 \\ -300 \\ 139 \\ 1013 \\ -289 \\ 220 \\ -300 \\ 139 \\ 1013 \\ -289 \\ 220 \\ -377 \\ 173 \\ 1085 \\ -037 \\ 220 \\ -377 \\ 173 \\ 1085 \\ -037 \\ 220 \\ -377 \\ 173 \\ 1085 \\ -170 \\ 220 \\ -377 \\ 173 \\ 1085 \\ -170 \\ 220 \\ -377 \\ 142 \\ 067 \\ -769 \\ 220 \\ -337 \\ 142 \\ 067 \\ -769 \\ 220 \\ -337 \\ 142 \\ 067 \\ -775 \\ 220 \\ -337 \\ 142 \\ 067 \\ -775 \\ 220 \\ -337 \\ 142 \\ 067 \\ -775 \\ 220 \\ -337 \\ 142 \\ 067 \\ -775 \\ 220 \\ -337 \\ 142 \\ 067 \\ -775 \\ 220 \\ -337 \\ 142 \\ 067 \\ -733 \\ 220 \\ -733 \\ 220 \\ -295 \\ 137 \\ 142 \\ 067 \\ -775 \\ 220 \\ -733 \\ 220 \\ -295 \\ 137 \\ 142 \\ 067 \\ -733 \\ 220 \\ -733 \\ 220 \\ -295 \\ 129 \\ 153 \\ 146 \\ 613 \\ -455 \\ 220 \\ -139 \\ 120 \\ -157 \\ -318 \\ 220 \\ -139 \\ 120 \\ -157 \\ -318 \\ 220 \\ -220 \\ -236 \\ 045 \\ -317 \\ -218 \\ 220 \\ -220 \\ -220 \\ -139 \\ 120 \\ -157 \\ -318 \\ 220 \\ -317 \\ 129 \\ -220 \\ -313 \\ 220 \\ -317 \\ 129 \\ -220 \\ -314 \\ -279 \\ -220 \\ -314 \\ -220 \\ -314 \\ -220 \\ -314 \\ -313 \\ 220 \\ -358 \\ 220 \\ -355 \\ -355 \\ -220 \\ -355 \\ -355 \\ -220 \\ -355 \\ -355 \\ -355 \\ -220 \\ -355 \\ -355 \\ -220 \\ -355 \\ -355 \\ -220 \\ -355 \\ -355 \\ -220 \\ -355 \\ -355 \\ -355 \\ -355 \\ -220 \\ -355 \\$	$\begin{array}{c} -312 \\ -312 \\ -008 \\ -777 \\ -200 \\ -2$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} -312 & 137 & 108 & -777 & 220 & 303 & 112 & 127 & 575 \\ -008 & 217 & 729 & -925 & 220 & 304 & 145 & 122 & 594 \\ 300 & 199 & 108 & -289 & 220 & 305 & 349 & 138 & 910 \\ 508 & 172 & 1156 & -023 & 220 & 305 & 345 & 138 & 910 \\ 508 & 172 & 1156 & -037 & 220 & 307 & 277 & 115 & 629 \\ 337 & 173 & 886 & -170 & 220 & 307 & 276 & 115 & 629 \\ 095 & 150 & 649 & -430 & 220 & 309 & 156 & 105 & 566 \\ 044 & 136 & 433 & -462 & 220 & 310 & 116 & 110 & 545 \\ -284 & 140 & 156 & -769 & 220 & 311 & 138 & 106 & 545 \\ -342 & 159 & 115 & -1062 & 220 & 311 & 138 & 106 & 545 \\ -337 & 142 & 067 & -775 & 220 & 312 & 207 & 116 & 935 \\ -337 & 142 & 067 & -775 & 220 & 314 & 338 & 146 & 1964 \\ -284 & 140 & 156 & -241 & 220 & 317 & 327 & 129 & 785 \\ 031 & 209 & 603 & -7333 & 220 & 316 & 393 & 146 & 1 & 064 \\ 274 & 199 & 974 & -286 & 220 & 318 & 247 & 119 & 822 \\ 329 & 152 & 921 & -205 & 220 & 318 & 247 & 119 & 822 \\ 469 & 191 & 1 & 066 & -241 & 220 & 317 & 327 & 129 & 785 \\ 005 & 141 & 564 & -420 & 220 & 320 & 157 & 113 & 533 \\ 005 & 141 & 564 & -420 & 220 & 321 & 145 & 107 & 447 \\ -294 & 152 & -7559 & 220 & 401 & 044 & 106 & 143 \\ -294 & 152 & -7559 & 220 & 401 & 044 & 106 & 443 \\ -294 & 152 & -778 & 188 & 220 & 403 & 066 & 133 & 536 \\ 445 & 166 & 1062 & -081 & 220 & 405 & 288 & 119 & 667 \\ 286 & 154 & 1021 & -087 & 220 & 405 & 288 & 119 & 667 \\ 286 & 154 & 1022 & -031 & 220 & 405 & 288 & 119 & 667 \\ 286 & 154 & 1022 & -087 & 220 & 406 & 133 & 136 & 683 \\ 1079 & 141 & 525 & -4322 & 220 & 407 & 352 & 124 & 832 \\ 157 & 137 & 721 & -082 & 220 & 411 & -141 & 107 & 216 \\ 2297 & 153 & 654 & -2798 & 220 & 407 & 352 & 124 & 832 \\ 159 & 139 & 721 & -062 & 220 & 415 & -1385 & 118 & 228 \\ 103 & 145 & -724 & -082 & 220 & 415 & -185 & 118 & 228 \\ 103 & 145 & -724 & -082 & 220 & 415 & -185 & 118 & 228 \\ 103 & 145 & -724 & -082 & 220 & 415 & -185 & 116 & 276 \\ 137 & 725 & -766 & 220 & 505 & -232 & 117 & 113 & 364 \\ -155 & 134 & 238 & -6366 & 2200 & 505 & -2352 & 169 & 214 \\ -1044 & 136 & 493 & -003 & 220 & 505 & -235 & 169 & 214 \\ -108 & 443 & -248 & $	$\begin{array}{c} -312 & 137 & 729 & -925 & 220 & 304 & 145 & 122 & 575 & -340 \\ 300 & 199 & 1 & 016 & -289 & 220 & 304 & 145 & 122 & 574 & -316 \\ 300 & 199 & 1 & 016 & -0289 & 220 & 304 & 145 & 122 & 574 & -316 \\ 300 & 199 & 1 & 016 & -0289 & 220 & 305 & 334 & 138 & 910 & -097 \\ 522 & 193 & 1 & 085 & -023 & 220 & 306 & 336 & 120 & 6637 & -029 \\ 532 & 193 & 1 & 085 & -027 & 220 & 306 & 230 & 126 & 647 & -151 \\ 337 & 153 & 649 & -170 & 220 & 308 & 230 & 126 & 647 & -151 \\ 044 & 136 & 433 & -462 & 220 & 310 & 116 & 110 & 464 & -232 \\ -342 & 149 & 156 & -769 & 220 & 311 & 138 & 106 & 545 & -238 \\ -342 & 149 & 156 & -775 & 220 & 312 & 207 & 119 & 649 & -245 \\ -337 & 122 & 057 & -633 & 220 & 314 & 338 & 141 & 965 & -102 \\ 031 & 209 & 603 & -733 & 220 & 316 & 359 & 130 & 975 & -094 \\ 469 & 191 & 974 & -280 & 220 & 316 & 359 & 130 & 975 & -094 \\ 469 & 191 & 410 & -004 & 220 & 318 & 247 & 119 & 822 & -158 \\ 153 & 146 & 613 & -455 & 220 & 312 & 157 & 113 & 533 & -184 \\ 045 & 153 & 146 & 613 & -455 & 220 & 320 & 157 & 113 & 533 & -184 \\ 105 & 141 & 0-72 & -726 & 220 & 321 & 145 & 107 & 447 & -199 \\ -139 & 120 & 157 & -503 & 220 & 322 & 158 & 119 & 627 & -202 \\ 153 & 146 & 613 & -455 & 220 & 320 & 157 & 113 & 533 & -184 \\ 106 & 045 & -042 & -051 & 220 & 322 & -158 \\ 2291 & 156 & 1062 & -031 & 220 & 404 & 228 & 173 & 1 120 & -282 \\ 145 & 166 & 1062 & -031 & 220 & 404 & 228 & 173 & 1 120 & -282 \\ 145 & 166 & 1062 & -031 & 220 & 406 & 334 & 130 & 863 & -114 \\ 103 & 146 & 741 & -358 & 220 & 406 & -141 & 105 & 217 & -487 \\ 239 & 153 & 761 & -242 & 220 & 410 & -141 & 105 & 217 & -487 \\ 239 & 153 & 761 & -242 & 220 & 410 & -141 & 105 & 217 & -887 \\ 397 & 171 & 1 & 033 & -109 & 220 & 416 & -185 & 118 & 228 & -683 \\ 109 & 143 & 584 & -313 & 220 & 416 & -185 & 118 & 228 & -683 \\ 109 & 143 & 584 & -313 & 220 & 416 & -144 & 107 & 216 & -353 \\ 397 & 171 & 1 & 033 & -109 & 220 & 416 & -185 & 118 & 228 & -683 \\ 109 & 143 & 584 & -313 & 220 & 504 & -273 & 114 & 933 & -661 \\ 109 & 143 & 584 & -3550 & 220 & 506 & -273 & 114 & 963 & -353 \\ 397 & 171 &$	$ \begin{array}{c} r & r & r & r & r & r & r & r & r & r $	LPMAN LPMAN <th< td=""><td>Dynking Cyrking <thcyrking< th=""> Cyrking <thcyrking< th=""></thcyrking<></thcyrking<></td><td>CPPNEAR CPPNEAR <t< td=""><td>112 1137 1108 - 775 220 304 220 314 - 177 116 220 - 0000 1237 1108 - 2000 304 1121 127 3140 2200 314 - 177 116 2200 - 0000 1237 11085 - 0037 2200 3044 1115 6434 - 0175 1142 1213 1217 11015 1217 1142 1213 1220 334 - 1029 2200 35 6 1144 14444 1444 1444</td></t<></td></th<>	Dynking Cyrking Cyrking <thcyrking< th=""> Cyrking <thcyrking< th=""></thcyrking<></thcyrking<>	CPPNEAR CPPNEAR <t< td=""><td>112 1137 1108 - 775 220 304 220 314 - 177 116 220 - 0000 1237 1108 - 2000 304 1121 127 3140 2200 314 - 177 116 2200 - 0000 1237 11085 - 0037 2200 3044 1115 6434 - 0175 1142 1213 1217 11015 1217 1142 1213 1220 334 - 1029 2200 35 6 1144 14444 1444 1444</td></t<>	112 1137 1108 - 775 220 304 220 314 - 177 116 220 - 0000 1237 1108 - 2000 304 1121 127 3140 2200 314 - 177 116 2200 - 0000 1237 11085 - 0037 2200 3044 1115 6434 - 0175 1142 1213 1217 11015 1217 1142 1213 1220 334 - 1029 2200 35 6 1144 14444 1444 1444

N D	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
NUNNANNANNANNANNANNANNANNANNANNANNANNANN	99999999999991111111111111111111111111	C	E 282838117693085500644036783425478681383571664762046 222228381111111111221123112367834403332444454114115411411111111111111111111	5775481624197335997469319559914621733223 	N 613992215443892036122949003650460092076877609490039	> >	11111111111111111111111111111111111111		5 5929007121139276222190960290721111148754100095 1113333112345611212121359444907221501441071111148754100095 1111111115561100095	11706186838365829648793709961111860835108918236 145235231782369633337407982611118608359108918216 112112110121211311002111118695959108918296		**************************************	012341234567890123456789012345678901234567890123456789012345	380346073537215641485780688662972827142754591324973 37078214884822541092260844997200215194217526438623174 100110012233333234201133223045310223322035410223322	$\begin{array}{c} 1 \\ 1 \\ 1 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\$	$\begin{array}{c} 1285\\ 05444339\\ 14839539\\ 025792222537\\ 113825792428271\\ 113974349910077248871\\ 1139743499110657248871\\ 11382208579\\ 11585\\ 1158$	

ЧD	TAP	CPMEAN	CPRMS	CPNAX	CPNIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	¥D.	ΤP	CPMEAN	CPRMS	CPMAX	CPNIN
00000000000000000000000000000000000000	67890123456789012345678901234567890123456789012345 444455555555555566666666666677777777588888888	342919702354311996883197167646331185388389224467734	9712296666690710676670475259041413030886492749986406 1111112121258755331322965432761253432011153532232033223 1111111111111111111111111111	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	13000053207141833501723515497345850068417083225089	00000000000000000000000000000000000000	67890123456789012345678901212345678901212345678901234567890123455555	335402229813563495949172837321116583654840152849377309869 111227494937322173465839054840152849377309869	4637467405537388884435279045892312200720338323652492 11111002332111200234433211110111248232410111183211137412 11111111111111111111111111111111111	603192809246482004876329034258259063779108668632618 7985544568877554668999976545557497978111221112322011 798554456809246482004887632903425825906377938773087006		00000000000000000000000000000000000000	55555555555566666666677777777777777777	69040950430885545842904702116537433714848054353681 2222416879189855458429047021166537433714848054353681 20054168791897789655584290470211653776291110798896889082 22224168791898855435842904702116537762911120798896889082 22222222222222222222223332211220102223	689144559064207526255747684609565788236251716803469 112214155906642075262557476884609565788236251716803469 1011111111111111111111111111111111111	225	

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN

W D	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	M D	TAP	CPMEAN	CPRHS	CPMAX	CPMIN	MD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	123456789012234567812345678901234567890123456789012 20000000001111111111111111111111111	413304089165104967101600072787409811282307823828279 141317944891655931677860072787409811282345823078238400 11111111111111111111111111111111111	02134317198045119418562292399772721429514306421811 1122122211229872987438674333229171418324342124743332238218 112212234295143306421811121122111222111112474333111111121122	- 093 128 022 231 188 258 280 153	34397523218953659140115345198790468088171462072953	00000000000000000000000000000000000000	34567890123456789012345678901234567890123456789012 33533344444444555555555566666666667777777777	$\begin{array}{c} -378711\\ -11571138769316\\ -115711387693678977220508052933360791884938163319088362\\ -1112245357765745220508052933360791884938163319088362\\ -11122350657889772205080552933360791884938163319088362\\ -111223377663319088362\\ -111223377663319088362\\ -111223377663319088362\\ -111223377663319088362\\ -111223377663319088362\\ -111223377663319088362\\ -111223377663319\\ -111223360279188493881\\ -111223360279188493881\\ -11122336287\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -1112233628\\ -111223377663319\\ -1112233628\\ -1112233628\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -111223377663319\\ -1112233628\\ -1112233628\\ -111223377663319\\ -1112233628\\ -1112236628\\ -111223668\\ -1112263668\\ -1112263668\\ -11122668\\ -11122668\\ -11122668\\ -11122668\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -11122688\\ -1112688\\ -1112688\\ -11122688\\ -1112$	14350771879189897920006344151048054043891581013470 3311111113334751011124714421411113578021400022982510113470	074030629211348090728524052660935771430103885655 5452222000354312200053731512323172264580033042045448530 5452222003543122000522222216045621212201339111001		00000000000000000000000000000000000000	34567890123412345678901234567890123456789012345678 8:58088999999000000000000000000000000000	17573676903490927550989231920473356540803880409382 54876945968773496905842223226886184618326473986192 11112325611100112222224551011222212354201226473986192	85184037743440509806128054010319088753720047729663 2111001233166774311457551855343245234655544323454065 2111112222111111111111111111111111111	159934 11999 121514 159934 116779 1167792 11677924 11677924 11677224 116777224 1167777224 1167777224 1167777224 1167777224 1167777224 1167777224 1177777224 117777777777777777777	- 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1

PAGE A 50

WD	TAP	CPMEAN	CPRMS	CPHAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	4D	TAP	CPNEAN	CPRHS	CPMAX	CPMIN
9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	- 901234567890123456789012345678901234567890123456789012345678	$\begin{array}{c} \bullet \bullet$	4787077883493099633060333211586260635175147514751475147514751475147514751475	32639762237249790191226418224873436822578480442233514 113230743858496562119858035156219948326437473068736885930 111111111111111111111111111111111111	9386695707765858504814544457440626510965825901294293	00000000000000000000000000000000000000	90123456789012345678901223456789012123456789012123456789012345678	96063643170268344008154405863043075560003449728747 967867456593008747941544058630430755560003449728747 	67596310397270871660560368626949289790131586192550 111333334532111011222221111133434110011114573423111101922 111111111111111111111111111111	3266660489612215737060517987938720688881000238158157 965700488676586359318642259167609234272634197023673 11222112	933395511550779649615951478668748229018511031829889	00000000000000000000000000000000000000	445555555555555555556666666677777777777	48440770635488589588650547877321248586052411532395 103233211222011111030111113522222222222432232221211	89573960309007013326058599648144872259548201855286 1109431101132121111111111111110921259548201855286		

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN

P	AG	F	A	52

W D	TAP	CPMEAN	CPRMS	CPHAX	CPHIN	90	TAP	CPMEAN	CPRHS	CPMAX	CPMIN	ND	TAP	CPNEAN	CPRMS	CPMAX	CPNIN
	3456123123456789 7777888899999999999	$\begin{array}{c} 270\\ 270\\ 2008\\ 1281\\ 1281\\ 1091\\ -100\\ 100\\ 100\\ 100\\ 100\\ 100\\ 100\\ 1$	111228341026128045336850468531464503461188484807788442582211 112283441122124364536850468531464503461147411121121121121121121121121112111211	50793994196343878134364838189726193379175869242041 64745671531412353184230113332211244843321022367833 6879379175869242041		00000000000000000000000000000000000000	67890123456789012345678901234567890123456789012345 2222353333535444444445555555556666666666		34484060733398452827670022576072292222669858526002585 11114577133211014522210111125833331100246009858526002585 111111111111112333111111258333311100246009858526002585	63225783134545320677051127469110990602860532 27803443200289922210027333121028092213210127 1 1 1 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2		00000000000000000000000000000000000000	67890123456789012341234567890123456789012345678901 77778888888888890 77778888888888890 77778888888888	7320749192094309747061564283097156666086277380559178 111123320605297334930980054511850218832411155410122 11122353605297334930980054511122111445021188322411155410122	578151464758328687041677916368600599692855880934706 111111232229655880934706 111111232229655880934706 11112322229655880934706	2252 1852 233802 1442 1084 3157 7488 77488 77488 77488 75575 1804 75575 1804 76487 1807 1807 1807 1807 1807 1807 1807 18	

ND	TAP	CPMEAN	CPRMS	сриах	CPMIN	ЯD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	90	T ::P	CPMEAN	CPRMS	CPMAX	CPMIN
	23456789012345678901234567890123456789012345678901 3333533334444444445555555555556666666666	$\begin{array}{c} - 143 \\ - 143 \\ - 095 \\ 5052 \\ - 1695 \\ - 22543 \\ - 1695 \\ - 22543 \\ - 12253 \\ - 12253 \\ - 13295 \\ - 13295 \\ - 112552 \\ - 112552 \\ - 112552 \\ - 112552 \\ - 11255 \\ - 11255 \\ - 11255 \\ - 1125 \\ - $	$\begin{array}{c} 1131\\ 1139\\ 1139\\ 1139\\ 1139\\ 1133\\$	40727709760998401744090341125238650907924008239912 407277097609984017440903411252236650907924008239914 1111 111 111 111		00000000000000000000000000000000000000	2345678901234567890123456789012345678901234567890123456789 8888888899999999999000000001111111111	- 3551777380566572358556105333981287840023771413655109149 	96563860931654724208755421207573378147948932854489 03643860931654724208755421207573378147948932854489 11111111111111111111111111111111111	60255052607974285817690336776405367442544181393565 3739932144105778821526105788309755841804509504503518 44988755445427767545466756445468897555465467189681		00000000000000000000000000000000000000	012345678123456789012345671234567891234567877777777777777777777777777777777777	63952045414815069092753748112761065133810329373282 1261802454148150690927537481127610937753166022078055 1022201198880772345139837753166022078055 222333250	1137600978152494301664211473252914169049466370928555 1100000078152494301642114732010308812049466370928555 1110111473201030881211000000002285555	225777739307558699555997016764494581037694811981236 222222233452112252621121494221624127665556565697567	1 1

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- E'ST TOWER IN PAGE A 54

UD.	TAP	CPMEAN	CPRMS	CPHAX	CPMIN	MD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	MD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚๚	12890123456123123456789012345678123456789012345678 222233333333300000000000111111000000000111111	902280391341030154073925037623863692390474360749973 223666857134103015686007931111669233233270474360749973 10110001204000001204 101110001204000001204	74432712007040134112023227939476811496356726705595	424496942148916026960275457955043000452252341601071 1812857708828287226960275457955043000452252341601071 2000000000000000000000000000000000		๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛๛	90123456789012345678901234567890123456789012345678 12222222222222222333333333344444444455555555	$\begin{array}{c} - & 0.51\\ 3.4657419753263768137955939356488770599515602704666150\\ - & - & - & - & - & - & - & - & - & - $	$1854426994639031848503720223408623846833333719381405\\1111222110011111478322100623846833333719381405\\11111111111111111111111111111111111$	69797417610782960332937854892075545894440336117801 11 11 11 11 11 11		00000000000000000000000000000000000000	901234567890123456789012341234567890123456789012345678901234 - Ser Street Ser Street S	710339551258039704804614148271588710866631265596816	42817531849530278547050829772619821847675480732739 1111122109003609100002369179752124432259633322233116 111111111111111111111111111	162462283079202098393945836835380649794848180807207322332113789275425322321137889275425322321137889275422322323211378832213223232321137883221322323232113788322132323232321137883221323232323232113783222332321137832223323211378322233232113783222332321137832223323211378322233232113783222332321137832223323211378322233232113783222332321137832223323211378322233232113783222332321137832223323211378322233232113783222332323232323232323232323232323232	<pre>(</pre>

WD	TAP	CPNEAN	CPRMS	CPMAX	CPHIN	MD.	TAP	CPMEAN	CPRMS	CPHAX	CPMIN	WÐ	ΤP	CPMEAN	CPRMS	CPNAX	CPNIN
NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN	- 56789012345678901234567890123456789012345678901234 2222223333333333344444444445555555555	3192	782570286788172749190832937790660416006461150534	1 83928799084881173100047655059995335461298796689230361 0839287990848881173100047655059995335461298796689230361 1 95532305649972655 1 955332355550599533554612987966892303651 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		- 000000000000000000000000000000000000	56789012345678901234567890123456789012345678901212 777778888888888889999999999900000000011111111	- 1593 - 1593 - 1644 - 002483 - 0024836 - 2048240933657 - 2048240933657 - 1122882 - 2048240933657 - 1122882 - 2048240933657 - 1122882 - 2048240 - 1122883 - 2048240 - 1122883 - 20482 - 1122883 - 20482 - 1122883 - 20482 - 1122883 - 20482 - 20483 - 20482 - 20482 - 20482 - 20482 - 20483 - 20482 - 20483 - 20482 - 20483 - 20482 - 20483 - 20482 - 20483 - 20482 - 20483 - 20482 - 20482 - 20483 - 20482 - 20483 - 20482 - 20483 - 20482 - 20482 - 20483 - 20482 -	06222877259438093444894574943214051951169556739524 1111112174324223233221000001232111200321112001110212 1111111111	58894121616991530733841249754720121553391924760420 478034022016587386774264505055644445565554545455756 254444575478873485754754720121553391924760420		00000000000000000000000000000000000000	***************************************	20986870362851926953030061957638433143586667327826 590929107184561196275655396979835781237113223191499	494514824847424422534044789729268963393506667931256 1122112000073111117435370099729268963393506667931200000 1111111111111111111111111111111		1 1

₩D	TAP	CPMEAN C	PRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD.	ΤP	CPHEAN	CPRMS	CPMAX	CPMIN
NNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNNN	77777777777777777777888999999999999999	$\begin{array}{c} 043\\ -14225\\ -0912\\ -0912\\ -0992\\ -2274\\ -14133\\ -0980\\ -2274\\ -14133\\ -0980\\ -14133\\ -0758\\ -1881\\ -0758\\ -1881\\ -00730\\ -0665\\ -1111\\ -006555\\ -1111\\ -006555\\ -1111\\ -0065\\ -0665\\ -1111\\ -0065\\ -0665\\ -1111\\ -0065\\ -0065\\ -0065\\ -0065\\ -0065\\ -006\\ $	786377806248499052352055575593113678982383906967783	5121 5151 51551 51555 515555555 51555		222222222222222222222222222222222222222	23456789012345678901234567890123456789012345678901		7164016253003504666440644327551532321006885728119249	468072131571244700396489546310844431052954990666961 1111 111 111 111		00000000000000000000000000000000000000	234567890123456789012345678901234123412845678901234567		97758353086172496502276403486732887789466685075541 1718210012332469999155560010014468559291542090672101	35579 2227 2220 3357 3354 3564 5	1

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- E ST TOWER IN

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	•	u.	-	•	

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	ΤP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	890123456789012345666666666666666		775354871992497819366650951676611635699878397603985	1121955831173126903552071904207173149993318 652122333376422223345397180561474464512228 733337642222333331111323367551423333378	$\begin{array}{c} -& -& -& -& -& -& -& -& -& -& -& -& -& $	00000000000000000000000000000000000000	22222222222222222222222222222222222222		65757673819727483895078341529604042329752716384524 20999658032000011121101111111111111111111111111	74218399440717559513643325611354646324872535240004 3223112224422444464333344553450433382301488255644555534		22222227777777777777777777777777777777	333334444444444444444455555555555555555	896511009994920392541051749491307077632120210734509	59568580510413076870710996697828187003946819537569 900000011131110010200001113319900238187003946819537569	$\begin{array}{c} 2423207652218197776090348873233446881024273099133583\\ 1 & 6615249830469847660688798879881024225332448155781\\ 2 & 122295322448155781\\ 3 & 522498304698676666688798879881024273099133583\\ 2 & 122295322448155781\\ 3 & 52248155781\\ 3 & 522481557832266668876887666688768666\\ 4 & 5222953224481557863\\ 4 & 522295322448155783\\ 2 & 522285324481557883\\ 2 & 522285324481557863\\ 2 & 522285324481557883\\ 2 & 522285324481557863\\ 2 & 52228532448155783\\ 2 & 522285324481557883\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 52228532448155783\\ 2 & 522285324488155783\\ 2 & 522285324488155783\\ 2 & 522285324488155783\\ 2 & 522285324488155783\\ 2 & 522285324488155783\\ 2 & 522285324488155783\\ 2 & 522285324488156\\ 2 & 522285324488156\\ 2 & 522285324488156\\ 2 & 522285324488156\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 52228532448815\\ 2 & 522285666666666666666666666666666666666$	<pre></pre>

WD	TAP	CPMEAN CPR	MS CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	ТнР	CPMEAN	CPRMS	CPMRX	CPMIN
00000000000000000000000000000000000000	23456789567890128901234561231234567890123456789299999991111	242 1 1781 1 0221 1 1888 1 1888 1 17781 1 1888 1 17781 1 1888 1 17791 1 17795 1 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1223 0 1248 1 0483 1 1332 1 1333 1 1233 1 12499 1 1333 1 1252 1 13365 1	09070442855676889819151809244149550321421020002910009480099115882002285391447769783235343434343434343434343434343434343434			56789012345678901234567890123456789012345678901234 0000011111111111111111111111111111111	- 11026485154632271002375210519456544612122157286586 	66001847483824792984067435962966721354577358637896 11112457001110214587900111124669001011135788001111334660	76223601002917930950049852862001878308445258894885 74757442136400488414058991145532523310145472936989488915 1111111111111111111111111111111111		00000000000000000000000000000000000000	11111111111111111111111111111111111111	8590518880131969865380886935241200683955243216112493 662711207343542472633930693416112224143952230228591134 5538000010135543000001013952230228591134 600011013952230228591134 6000013955243216112493	010090550866663944086291046840324652678124991857116 111122575981000223259901244560324652678124991857116	126 117 157 322	

APPENDIX A -- PRESSURE DATA ; CONFIGURATION A : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER IN PAGE A 59

WD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPHEAN	CPRMS	CPMAX	CPNIN
 ■ 222222222222222222222222222222222222	+ 2222223232322222222222222222222222222	H 209368122267950626702365801699475394502266802369650	S 082966713322797536167391088573221663859462704405168 1231531220009996852221009111988734221663859462704405168 PP	. 429	L 16752148460775222244893427019446936729197901004459		- 123456789012345678901234567890123456789012345678901234567890 - 222222222222222222222222222222222222		5 81286829638821398028994695786311719436359346411986 010987520096590311110001028771001310118511011111111111111111111111111	63569242794039202718523418429868152 23831606031951078788881106760568195 238316060519510787888811067605681952	L	 	. 1234567890121234567890123456789012345678123456789012234567123 . 333333333333344444444444444444444444	29654990000112312428971000260354892929203243424206557761000 1229654990000000000000000000000000000000000	83304010589974218566029119425493866515760344166115996 11240001447185660291194254938665157603441661151899	1 11177045334046244652985074185854250696864975885265581 1 876023244284552985074185854250696864975885265581 1 876023243247114250695854552611135099710 1 23244324711425069585455265581	

WD	TAP	CPMEAN CPRM	S CPHAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
 	45678912345678956789012890123456123123456789012345	- 0302870 + 11001 + 11002 + 10000 +	9824542466424708497177863582627824357848142248461		- 000000000000000000000000000000000000	678123456789012345678901234567890123456789012345678901234567	- 00718066734635961957348914854035346569820160127456195 0071886220396538524694553358520001100245552000477092198554 001121002122100134542533368707669820160127456195	34217368685440443250131649638575242301295452108633 320567621145664342133557678343323667792252345798743	081296313965858726070241410023282200068383001483584 497364081965858726070241410023282200068383001483584 1111 111 111 111 111	98487799261188145715028011152767173149718501814054	00000000000000000000000000000000000000	890123456789012345678901234567890123456789012345678901234 11111111111111111111111111111111111	70080527109679698079344252561222037693089819258834 6408593111460892603202407539240725246122796754455291 10235500011102464200001102453201001343000000244315291 1011 111 111 111 111 111 111 111 111 1	011141028670494070189181571968188751429504438892251 1144578223334457772111413223582211233561011112446673229 11111111111111111111111111111111111	109	

W D	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
- - - - - - - - - - - - - -	555566666666677777777777777777777777777		471587809588707692422195955503399931206655368381102 112119901034923208111452400090122050020020127181377	237288712606901543090649394520179952108958454435535 1 3204323746643454655478964445558882577344404556259301 2 320432374664345544399064939452017995210895845445556259301		000000000000000000000000000000000000	99999999991111111111111111111111111111		974919869205687654841130742377518909078866038163863 729672586365521112455645312447677518909078866038163863	1000 3595 5554 3368 42368 2704 2707		00000000000000000000000000000000000000	12345678901234567890123456789012345678901234567890	92137231846132234270016248173466116961691513840384	13757147698737155618305729727419610509866420096990 1166643444367513434656863323224444267122233471122122 111111111111111111111111111111	$\begin{array}{c} 91969774781\\ 9998702274781\\ 408774781\\ 5322103774738249234\\ 11103221535777382290453796679999999999\\ 1233229041379667766799699991788229249234\\ 111103221535777382290413796679306609991788222249067\\ 12333229041379667796679999999999999999999999999999$	

N D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	ND	TAP	CPNEAN	CPRMS	CPMAX	CPMIN
D 000000000000000000000000000000000000	r 11111222422222222222222222222222222222	C	C 1144336584207074441858678157555490905270314412803 C 11448336584207074441858678157555490905270314455424912803	1.014 .888 .951 .711 .050 .101 .112 .243 .336	N 0908616066046284310044373915028107530916945064777361	B 000000000000000000000000000000000000	<pre>P 78901234567890123456789012345678901234567890123456 P 789012345658666666666666667777777788888888888899999999</pre>	R 01918914372815465091295193729649491701390145194743	5 40694885096136568548078642408759865722171035375313 H 4322917164320121287642109801146322111287552121212196 H 1112112112164330961365685480786424087598657221111287552121212196	1237014572899657731087046619237755121807643150848803 8122233331122111444222211122111113111122220124744371812060	n 71377913274495894542721693274630650591338050643828	************************************	- 22233333333333333333333333334444444444		s o 48840238699495811088837298066798715144704193459205534845 11226694958111468837298066798715144704199990889990091354845 1111111111111111111111111111111111		- 1

WD	TAP	CPMEAN CPRMS	CPMAX	CPMIN	WD.	TAP	CPMEAN	CPRNS	CPMAX	CPMIN	ЯD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	78901234567123456789123456789567890128901234561231 55555555555556666666666677?777777777777	$\begin{array}{c} - 061 & 112 \\ - 025 & 105 \\ - 0309 & 1065 \\ - 126 & 1340 \\ - 0942 & 1099 \\ - 0942 & 1099 \\ - 0942 & 1099 \\ - 0942 & 1099 \\ - 00421 & 0999 \\ - 00421 & 0999 \\ - 00421 & 1099 \\ - 00421 & 1099 \\ - 00133 & 1099 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00138 & 1222 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00229 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00136 \\ - 00137 \\ - 0000 \\$	85512805483567832367786246836414407614326191789453 244423322363333283567186246836414407614326191789453 2444233223677868996 2444233223677868996 24442332236778689 244432583236778689 24442332236778689 244432583236778689 24468356783236778689 24668356783236778689 24668356783236778689 24668356783236778689 24668356783236778689 24668356783236778689 24668356783236778689 24668356783236778689 24668356783236778689 246783286783236778689 246783286783236778689 24688368788 246783286788 246783286788 24678888 246788888 2467888888 24678888888 2467888888888888888888888888888888888888	374153680314847975569812623714549379619499666989399	35335353535353535353535353535353535353	99999999999999999999911111111111111111		958230906844283673362561800777771005091854189868615 11122112267206681662333221113244322212354656441302345564 1112211221122111211111111111111111111	39 112 394 022 098 192 480 177 394	9571931135857081720899925515661269044706590353060543	33333333333333333333333333333333333333	456789012345678901234567890123456789012345678901234567890123	15567097332556780610218976115675915398472648187014 0228848283117153238805713888416102821650354288835687 022884828311715323880610218976115675915398472648187014	21114050273394375375824002541359635910721985109072 11123344675423355666571224455566333002222444230023333436	20063755272610986641376999201448207157514350970234 11248862717450206244974133669552864451502756986858 1111111111111111111111111111111111	47776310103485420010670280568194200781763946439314 68212010348542001067764106660517633946439314 03112010348542001067764106660517633946439314 031201067764101023753100014 031201067764101023753100014 031300014 031400781559284173600025

WD	TAP	CPMEAN	CPRMS	CPHAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD.	TAP	CPMEAN	CPRNS	CPMAX	CPMIN
33353353535353555555555555555555555555	45678901234123456789012345678901234567890123456789 11111111122222222222222223333333333333	$\begin{array}{c} 1 \\ 1 \\ 1 \\ 2 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3 \\ 3$	7358999968105273212005174835988166307528820777575266 111112235342273212005174835988166307528820777575266 1111121112222235266307528820777575266	862880026498130836753074904703175010879397430142988 109763056224231391553475010879738974301226122878	334695087977963499328136820289017041957526477745194	33130000000000000000000000000000000000	01234567890123456789012345678901234567890123456789 4444444445555555555555666666666777777778888888888		012887743361052209295546777531518466899791910709406 1122887743361052209295546777531518466899791910709406 111121111211110210021518466897911910709406 11123111211121111111111111111111111111	08556 0956 0956 0956 0956 0956 0956 0956 0		31000000000000000000000000000000000000	012345678901234567890123456789012123456789012	95526116920006048164952835655390838591347260045347 22222333612297522245335222222453352222222222222222222	77643675097875359824511871773322144438187715257872	.076 .108 .071 .107 .121 .108 .210 .106 .109 .205	1224696987611075016869811286114945162313236110009627190

N D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD.	TAP	CPMEAN	CPRHS	CPMAX	CPNIN	AD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
33333333333333333333333333333333333333	45555555555555555555555555555555555555		52850661504913269583087356457028299747041933358305 91354310991563100389095101054439205529102521551532	33806 33826 54617 9924318 9924318 9924318 2004 12388 3911 23084 225610 123084 2204 23091 23084 2404 2204 2204 2204 2204 2204 2204 2		00000000000000000000000000000000000000	4561231234567890123456781234567890111111111111111111111111111111111111	$\begin{array}{c} -24934\\ -1009274388994\\ +40993484847059894\\ +448905986885527222338896043037424121412214196747\\ -100223782323388960430374241221412214196747\\ -10022378232338896043037422110833742212221\\ -100237823100837422122221233889604303742222222222222222388960430374222222222222222222222222222222222$	27792421271720730450958953833952732550195461034588	090 1330 1666 - 2001 2004 2005 2005 2005 2005 2005 2005 2005	01052936865528765632276791281398850315633966991087	00000000000000000000000000000000000000	11111111111111111111111111111111111111		81322048452009450095965294579624860078037611468902 356787423237667655155567775213456566312224446720222	$\begin{array}{c} 6800\\ 1\\ 1\\ 1\\ 1\\ 2\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\ 3\\$	

U D	TAP	CPMEAN	CPRMS	CPHAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPHAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
	78901234567890123412345678901234567890123456789012 77788888888889999990000000001111111112222222222	82466949773961562918476066337782865095120499948824313 	735026074431379401421527955868892671214729146123666	$\begin{array}{c} 122899416009481660984702486625566247884694011010222785269\\ 111111111111111222211101102110011001100$		00000000000000000000000000000000000000	345678901234567890123456789012345678901234567890123456789012 22222222222222222222222222222222222		42597064136629513827434651944083933818809499688284 1111111111111111111111111111111111	329679272713175247375546325510204759868254343388864 122123783363209974689057195390443497405682546325876732		00000000000000000000000000000000000000	34567890123456789012345678901123456789012121234567890 8888888899999999999999990000000011111111		868761535465074711178734737693606044172706003719922 111224650747111133111222236060444172270603719922	07055763763711360113586344033115465576637663766376631155863440155586344015559176639	

W D	TAP	CPMEAN CPRMS	CPNAX	CPHIN	90	TAP	CPMEAN	CPRHS	CPMAX	CPMIN	90	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	444444445555555555555555555555666666666	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	50795500220365528894047132239211160005644172997482454 333324324380185528894047132239211160005644172992482454 11	1	00000000000000000000000000000000000000	28901234561231234567890123456781234567890123456789 2223335535000000000000111111111111111111	- 16431 224531256583257128996229904693580025578328666568462455201 112246583333333288665568462455201 1138879932888580045578328666568462455201 11000122007551	58150337891618404345978251434921370596108836668871 11111111111111111111111111111111	4185514 4185514 4185512 24185514 2418551 222831357286 2228313517 2228313517 228313517 29961190380253 201490380253 201490380253	532690242943772643795481809154263341336577733703335 68726902429437726437954818091542633413365777331000		11111111111111111111111111111111111111	999410902242389083167080346769210534220533345499712 8815870384782316912830702134666649952422686475572320272	71694009506778698746952430510455570138320979663496	97792476851808104837259199594852845700024599582252916 1111 8524766851226604999594852845700024599582252916 1111 111 1111 1111	

					CONTN	но	TAP	C P M F A N	CPRHS	CPNAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
0 0	T 111777777788801234567890123412345678901234567890122345 A 77777777788888888999999900000001111111122222222	CPM 481328 481328 10150130027 481328 10150130027 481328 10150130027 481328 1001304698 481328 1001304698 481328 1001304698 1001304698 10013046988 1001304898 100130480 100110 100100 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 100000 1000000 1000000 1000000 100000 1000000 1000000 100000000	CPR 166766682975279086726346144973149155288 CPR 16627666829752790867263461445614456144456260096672669297527908672663426009660044099349155288667669642600966000460934915552886676696426009669660000000000000000000000000	C 111755909047909047907374072629967688857244167379111122525474116737909054479073742110010100000011112252547441673	CPM 072237359216517303608523855795075947628696730809767 001424960023655511630914416577521489218267315923564667 002237555211001445577778877887765566666666666666666666 001444600236675471001445577777887788776286967308097667	D 000000000000000000000000000000000000	p. 67890123456789012345678901234567890123456789012345 A 222233333333334444444445555555555555	C	CPR 109694 11213700749087114 11220749087114 1120719087114 110663335881117454 110100060611499230 11110109722919231 1109722919230 11109722919230 111090720919230 111090720919230	X 2269291327616275897502955644304042192644822742188737	C	0 0	P 678901234567890123456789012345678901234567890121234567890123	N N N N N N N N N N N N N N N N N N N	C .110112243828383707090543686014972162395	X 48392093055366621635262579306057674560601926784032 A 815534410455536662162579306057674560601926784032 C 000100002240874702859729922941055042601926784032	C [

W D	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	нD	TAP	CPMEAN	CPRHS	CPMAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
	444444444444444555555555555555555555555	74389147408632243668134592719018818806442252033337374	498177955885562304275058004012857154009998627113702 7003010109091809999045642099001340128571540099986271112110001111111000000000000000000000	81233175794043617700781626129912159293769 2643576087811570628092034447296085233611166 26435750087811570628092034447296085233611166	++25412620008356314202940581634496619315873066461960 67614122342423335442435556745443222029857366820303322	00000000000000000000000000000000000000	56789012890123456123123456789012345678123456789012 1111122222353535300000000001111111111111	1155245720995152000223730024921068215804719565499946185 22121122452985452000223730024921068215804719565499946185 22122122122123333334433482427138024719565499946185	13675273554704080091177402768984859152236655813625 13344303246426425610223355843665476576231213144533221 111111111111111111111111111111111		2864437112019765552238566020315883980873188910176655060606	00000000000000000000000000000000000000	34567890123456789012345678901234567890123456789012 11111112111111111111111111111111111	447315426977412422266008250343468538056923724051068	04454206646235284276494949397624639105167539662532 257878864212246779653121458786421677888853123689763 111111111111111111111111111111111111	$\begin{array}{c} 1383114\\ 125546859293220475671977675339287095373613717402222\\ 111125312047567197767533928802553512578045504\\ 1112532880255328402553512578045504\\ 111125328802553512578045504\\ 1111125328802553512578045504\\ 1111125328802553512578045504\\ 111112532880255351257804\\ 11111253280455352804\\ 1111125586665535535286655355552286\\ 111112558666555555555552\\ 1111125566755555555555555555555555555555$	

WD TAF	CPMEAN (CPRMS C	PMAX	CPHIN	UD.	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ыD	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
WD 1664 MD 1677 MD 16	- 12160631578321257832122243157832122241419688822003067428888220233 - 2160665315783212578321257763066742888822023 - 1377832412558122241419658 - 2241419688822003228888822028288888 - 2288828888882200330667428888882200 	1174 1174 11318 11318 1158 1 11723 1007 1007 1007 1007 1007 1007 1007 100	P 3322370006221670119141247110743210221011129206387 H 332225700062221670119141247110743210729804170129206387	C	U 444444444444444444444444444444444444	T 000000000000000000000000000000000000	C	$ \begin{array}{c} \text{CPR} & 111933353446222132069505792565519448874243405003486881\\ & 1110111221132069505792565519448874243405003486881\\ & 1110111201111011120111011101110034866811\\ & 1110111011100334866811\\ & 11101110111011101110111011101110034866811\\ & 1110111011101110111011101110034866811\\ & 11101110111011101110111011101110034866811\\ & 11101110111011101110111011101110034866811\\ & 11101110111011101110111011101110034866811\\ & 11101110111011101110111011101110034866881\\ & 1110111011101110111011101110034866881\\ & 1110111011101110111011101110034866881\\ & 11101110111011101110111011101110034866881\\ & 111011101110111011101110111011101110034866881\\ & 1110111011101110111011101110034866881\\ & 11101110111011101110111011101110034866881\\ & 11101110111011101110111011101110034866881\\ & 11101110111011101110111011101110034866881\\ & 111011101110111011101110034866881\\ & 111011101110111011101110034866881\\ & 111011101110111011101110034866881\\ & 111011101110034866881\\ & 11101110034866881\\ & 11101110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 1110034866881\\ & 110034866886881\\ & 110034866881\\ & 1100366886881\\ & 110036686881\\ & 1100366$	CPM 069965473062449596393420307199397517335122605784440 1105206244959653934203071594403851223992240545454545454545454545454545454545454	C	D 000000000000000000000000000000000000	T 222222222222222222222222222222222222	N N 46498652972024008337885457317454491414282728096665	CPRMS . 107348845999645999645100 . 10888459996459996 . 10996459996459996 . 100996459996645999664599966459996645999664599966459996645999664599966459996645955664595556661497555566149751110000000000000000000000000000000000	CPMAX 19996985867286688308299708379126935901336964882008115 	C 1 1 1 1 1 1 1 1 1 1

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W D	TAP	CPMEAN C	PRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN
00000000000000000000000000000000000000	9012123456789012345678123456789012345678912 1222000000001111111110000000000011111111	1333527724 2973527724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 22887724 2288728 22887278 2288728 2288728 2288728 <td>5144906805678381848484480413259322682411390065995188</td> <td>49319799936882446361229565320191949196810961287800 1100101600176636646411259083193301909047644708489138 11</td> <td></td> <td>00000000000000000000000000000000000000</td> <td>777777777777777777777777777888899999999</td> <td></td> <td>45988657013989125256078155206431921099372093855371 1111111111111111111111111111111111</td> <td>445582230640927627915970566947526267708657 4455582231421231222412356870412786507130 1221377988890203978213095669475266267708657</td> <td>75822852410768163022389365654123504924166211134528</td> <td>00000000000000000000000000000000000000</td> <td>6789012345678901234567890123456789012345 0000111111111111111111111111111111111</td> <td>396968134518583207864438687832423240175060043 1111112455421012201355419126116485423240175060043 1111112455421012201355419126116485423240175060043</td> <td>45265250760899686747792326473598688494983962815307</td> <td>544929060615203841786668818158885173228886581897304078 11.208592459245923984999773228885818997304078 11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1</td> <td></td>	5144906805678381848484480413259322682411390065995188	49319799936882446361229565320191949196810961287800 1100101600176636646411259083193301909047644708489138 11		00000000000000000000000000000000000000	777777777777777777777777777888899999999		45988657013989125256078155206431921099372093855371 1111111111111111111111111111111111	445582230640927627915970566947526267708657 4455582231421231222412356870412786507130 1221377988890203978213095669475266267708657	75822852410768163022389365654123504924166211134528	00000000000000000000000000000000000000	6789012345678901234567890123456789012345 0000111111111111111111111111111111111	396968134518583207864438687832423240175060043 1111112455421012201355419126116485423240175060043 1111112455421012201355419126116485423240175060043	45265250760899686747792326473598688494983962815307	544929060615203841786668818158885173228886581897304078 11.208592459245923984999773228885818997304078 11.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1.1	

ND	TAP	CPHEAN	CPRMS	CPHAX	CPMIN	ND.	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
 В 000000000000000000000000	r 67890123456789012345678901234567890123412345678901	$ \begin{array}{c} 1 & 3 \\ 1 & 4 \\ 0 & 7 \\ 1 & 3 \\ 1 & 4 \\ 0 & 7 \\ 1 & 3 \\ 1 & 4 \\ 0 & 7 \\ 1 & 3 \\ 1 & 4 \\ 0 & 7 \\ 1 & 1 \\ 1 & 4 \\ 0 & 1 \\ 1 & 3 \\ 1 & 4 \\ 0 & 1 \\ 1 & 3 \\ 1 & 4 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 1 & 1 \\ 1 & 2 \\ 2 & 2 $	110 1	$\begin{array}{c} & & & & & & & & & & & & & & & & & & &$		 377787787878787878787878787878787878787	. 23456789012345678901234567890123456789012345678901 . 11111111202222222222222222222222222222	478291110222222222222222222222222222222222	.1067377900098372403456271085483341771445944155759966254 .1111100111101110057599962254	5984578665952893390896676078665037405132592883986078011121125928839844960111111202111112021111202111120211112021111202111120211112021111120211111202111111			23456789012345678901234567890123456789012345678901123456789011	982522578511971329188303474128906079344347463888201 223122222222222222222222222222222222	10994548923180295968231652567049205478431565754535 1100976010760111091111000000000000000000	41759965530453834453274419697199585054338272457781 1001100011001000000000000000000001110012899901111111111	

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WD TAP	CPMEAN CPRMS	CPNAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WÐ	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
3331456789012121234567890 355000000440067890 3555000000440067890 400078904411178 411178 411178	$\begin{array}{c} -254 & .116 \\ -240 & .109 \\ -258 & .109 \\ -237 & .108 \\ -237 & .108 \\ -239 & .110 \\ -249 & .105 \\ -249 & .105 \\ -256 & .112 \\ -2556 & .112 \\ -2556 & .112 \\ -2556 & .112 \\ -253 & .143 \\ 017 & .205 \\ -268 & .116 \\ -267 & .120 \\ -268 & .116 \\ -268 & $	078 1254 1281 1280 0939 1367 1367 1378 1778 2172 1266	C PH 4866929949693589594357299971362	U 000000000000000000000000000000000000	T 55555555555566666666667777777777777777	C P ME AN 414 - 034 - 0307 - 33968 - 12561 - 12561 - 15561 - 15561 - 16559 - 16559 - 16559 - 16559 - 116454	CPRHS 158511005747 11005747 11109622936 11134607622936 111349937 111349937 111221069 111349937 111221069 111221069 111229 111229	CPN 99409 9940 99409 99409 9940 99409 9940 99409 9940 9940 9940 9940 9955 9940 9940	CPM 1268914491733401724091487787	D 35500000000000000000000000000000000000	P 901289012345612312345678999999999999999999999999999999999999	C PH E 83294 - 11484 - 12509494 - 22509494 - 22509494 - 22509494 - 225094 - 225584 - 225	CPRMS 29837729859702239866211332555596612 11228859702239866211332555596612 112286239866211332555596612 11228447332555596612 1125724447332555596612 1125724447332555596612	2740 3149 33449 12892969 115492 20330 110639699 115492 20330 110639699 11558 10639699 11750 116339699 11750	PM 198216682981479911

ND T	TAP CPHERI	CPRMS	CPNAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPREAN	CPRMS	CPMAX	CPNIN
00000000000000000000000000000000000000	111	s s s s s s s s s s s s s s s s s s s	K 5?171512414?41381416981375510582748881684232242424342 821926525124414?413894165549990115827488969684232242242 1112213024277189416554999011775150011122130198552202 11122112211221122112211221120111221301112213011122130 11122112211221122112211221122112211221	43088329066625264360802566679279686869283295423066628564 	- 888888888888888888 - 22222222222222222	533454614313553345461431353345461431353345461431353 79667330011111222779991111122279667330011279667330011279	324712926322374447111165319860385964328316476171069 1147203214552243722115582216942711432978316476171069	11889339350628510897891865533380580546491273603326826 11022375262375311059897891865533380580546491273603326826 1122221522011133882380580546491273603326826 112222152201110	674653738989372888369658897660212661950943676 1221123122211239771064428358035112661950943676 			34546143135334546143135334546143135334546143135334 66733001112796673300111279667330011227966733001127966	04431638608396993859742756105362329237823703374586 77711438221279711339332279811420221266611329222256 7804431638608396993859742756105362329237823703374586	17860154950184848660184502252340709170778236559856 89735353222111187521111444111238123412420011444112211100222 11222211111333112221111444112221114441122221111444111212111444	70852088830638512005428551311104153221069256916	

ND	TAP CP	MEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMERN	CPRHS	CPMAX	CPHIN	MD	TAP	CPNEAN	CPRHS	CPMAX	CPMIN
+++++++++++++++++++++++++5555555555555		61113292222456123202223351232028901223512988218621102 862528961790116809449109059624444441502246735443536	30559280324483142722707489426601959518181431019601 3111121114441111211113441111311113441111122111133 31111211114441111211113441111344055585043008205565181431019601	6788512106881493348729311392118883262874193088502 22120111156422120211170872221128672221234023198 22120111156422120211170872221128672221234023198 1	419766369394317807123049234401715755248893919789116 11763741595461816943949234401715755248893919789116	222222224444444444444486666666666666688888888	9111112227799999111112227799999111112227799999 1127938733454614693125334546146931353345461469	$\begin{array}{c} - 262936 \\ - 22936 \\ - 22936 \\ - 1225714 \\ - 11224936 \\ - 2254631 \\ - 2254631 \\ - 2254634 \\ - 11224931 \\ - 22548899 \\ - 12254678 \\ - 2254634 \\ - 2254634 \\ - 12254 \\ - 223398 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 22339 \\ - 2233 \\ - 23$	60076222236571104642463891318010005408776530083789 9745434143000486444322044017883743228124096096412153 31111123311111233111123311112331111283111023321111233	301324737597311388943496223417 5013251111177622812951154438820 	-1-1-1	***************************************	11111222779999911111222779999911111222779999911111222779966733000011279667330000112796673	$\begin{array}{c} - & - & - & - & - & - & - & - & - & - $	143670011628499663640013300835361700221577888718889744164 1123316528499663640013300835361700221577888718889744164 11223111122221111228221111222211112222111122221111222211112222	$\begin{array}{c} 1 & 1528\\ 1 & 2402789\\ 2 & 1021789\\ 2 & 1021789\\ 3 & 184027589\\ 4 & 318467122027588860\\ 8 & 122027588860\\ 8 & 122027588860\\ 1 & 22027588860\\ 1 & 22027588860\\ 1 & 22027588860\\ 1 & 22027588860\\ 1 & 22027588860\\ 1 & 202758860\\ 1 & 20275860\\ $	2304383331158062279490191860136082988137125078966759 264960522649580975457880077878254274462282977426675952 36662208097545788007787825427446228839231642988458 36662209754875552 36662209754857552 36662520980975552 3666257552 3666257552 3766666029774266759 3766666029774266759 37666662989881377125078966759

ND	TRP	CPMEAN C	PRMS	CPNAX	CPNIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND	TAP	CPNEAN	CPRMS	CPMAX	CPMIN
666666888888888888888888800000000000000	91127966733000091127933000091127966733045461469311279966733454614693112793000011127933454614693112796673300		$\begin{array}{c} 1424\\ 1106881277516556900414498985200347663539362142149231121221121808765100411498985200347663539362112180876550041141132211218087655004114111411211211211211211211211211211211$	- 2173421104221 217342110969906 110995906 110995906 1109633115386996 1102231215386996 110222415386996 1112289096 1112289096 1112260 112260 11260 11260 11260	70454834954967071970301142702026594664910606438259	777777777777777777777777777777778888888	11111222779991111122277999111112227799	$\begin{array}{c} 454\\ +93\\ -2271\\ -1498\\ -22711\\ -1465\\ -11886\\ $	8382712782878865130432022241940210309395355337972035 111130120878865130432022241940210309395355337972035 111188	24630082197766795494839060473388222611117883 - 11222266085118315047338822291932241117883 - 112222647338822291932241117883 - 11223285118906047338823202113328843	$\begin{array}{c} -& -& -& -& -& -& -& -& -& -& -& -& -& $	222224444444444444444444444444444444444	277999111112227799911111222779991111122277999111112227 73300112796673300112796673300112796673300112796673	42990272533957487808822009904306091367674109560996949 42200823111077478211231310888200990430609113101047479211220232846 411007111155441100011111554110009111155411009111115541100911111554110091111155411009111115541100091111155411000911111554110009111115541100091111155411000911111554110009110000910000000000	1746244939134295717086758077492647208199981410876590 110009011077736086758077492647208199981410876590 111018765790 111018765790	3522306226695022709607977815455551112 10092669502270960797781554555551112 110092532944460797788155455555112242242424 1111 1111 1111 111	

WD	TAP	CPNEAN CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	80	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
\$	6143135334546143135	$\begin{array}{c} - 199 & 1777 \\ - 00196 & 2857 \\ - 0196 & 2857 \\ - 11376 & 1103 \\ - 11376 & 1037 \\ - 11376 & 1037 \\ - 11376 & 1037 \\ - 11376 & 1103 \\ - 1125 & 2016 \\ - 125378 & 1889 \\ - 12031 & 1179 \\ - 12032 & 1147 \\ - 1202 & 1147 \\ - 1202 & 1147 \\ - 1202 & 1147 \\ - 11310 & 1022 \\ - 11310 & 1022 \\ - 11370 & 1047 \\ - 1202 & 1047 \\ - 1137 & 1167 \\ - 1202 & 1047 \\ - 1137 & 1167 \\ - 1202 & 1047 \\ - 1137 & 1167 \\ - 1137 & 1167 \\ - 1237 & 1162 \\ - 102349 & 1217 \\ - 11234 & 2194 \\ - 12347 & 1168 \\ - 102349 & 13699 \\ - 2051 & 1068 \\ - 1088 & 2228 \\ - 1202 & 1068 \\ - 1088 & 2228 \\ - 1088 & 2228 \\ - 1088 & 2228 \\ - 1088 & 2228 \\ - 1088 & 2228 \\ - 1088 & 2228 \\ - 1088 & 2228 \\ - 1088 & 1068 \\ - 2051 & 1108 \\ - 1108 & 2051 \\ - 108 & 2051 \\ - 108 & 2051 \\ - 108 $	50643670797 56 93245450788315598643755454535898830535 024437394672955553486089371559864537545454545454545454545454545 1111 - 1111 - 1111 - 1111 - 1111 - 1111 - 1111	11	99900000000000000000000000000000000000	43135334546143135334546146931353345461469313533454 011127966733001112796673300001112796673300001112796673 9911112227799911112227799999111112227799999111112227		80097334933791289060017893969297379089713194622821 12110902104500376031122180581175821113192892034632121 1221201222111211221805811758221113192892034632121 12212012221221221805811758221113192892034632121	1111 1111 1111 1111 1111 1111 1111 1111 1111	279109117400488175885566936727150138578358177074160	44444446666666666666668888888888888888	61469313 5334546146 931 353345461469 3135334 5461469 313 3000011127 96673300000112796673300000112796673300000112	49.68.68.61379302.6802.625457.66754856688130622863.665622 035833467669751640325588308740629933446001888961164787 035833467669751640325588308740629933446001888961164787 04.00000000000000000000000000000000000	76809697351398255411053680410307846308703214511339 11022122222056927688812220459203442323214511339 202222222225692768881222204592034423232345113224639497 2022222222222222222222222222222222222	1651501514395382527804882101138712967205565466 2284602779335912732780488221011387129672055721765565466 1 2220000001154391200000015460701387129672055721765565466	

9 D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	MD.	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	MD.	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	9911112227799999112533454614693135 9911112227799999112796673300001127 9911112227799999112122277999991127	$\begin{array}{c}$	27411641369336917407169968944757615216152740109209 33311111122022218530088411122125428395431111214530911952221321		2277581339616773229618889534499197789127191485342569 22775831586400717783395953293189735525964260277449 2221111122221777833959532931897355259644405677449	88880000000000000000000000000000000000	46931353345461469313533454614313533454614313533454614313533454673 9999111112227799999111122277999111122277996673366112796673	$\begin{array}{c} -1 \\ -1 \\ -2 \\ -2 \\ -2 \\ -2 \\ -2 \\ -1 \\ -1$	<b>57060445036927398496110342485958108441547654028414 2232210122167029922342485958108441547654028414 11121259306231111111212593062311111111111111111111111111111111111</b>	5881967304596797028010902288884999984177053 41373211792499027430657965565646590144112 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		66668888888888888888888888888888888888	79991111222779991111222779991111122277999111112227799911111222779 300112796673300112796673300112279667330011279667330 30011227966733001122796673300112279667330011279667330	44873221875219233182302144226676641540328564096381 57931476982220001415577222200140111222222233311122222223 6131776982222001415577222200140111222222233311122222223 6131776982222001415577222200140111222222223 6131776982222001415577522200140111222222223 6131776982222001415577522200140111222222223 613177698222200141557752220014011122222222223 6131776982222001415577521823 61317769822220014155775222001140111222222222223 6131776982222000141557752220001401112222222222223 6131776982222000141557772222001140111222222222223 6131776982222000141557772222000140111222222222222222222222222	861400023133776629511305270842463556171224750222182 122133333111112133321121204224635561712247502222182 11111273322112112042246355617712247502222182 11111273	2975997457987476411548942417099482166 975997457987476411134113222215535796 11385777748155357966 11385777748155357966	

WD	TAP	CPHEAN CPRHS	CPNAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN (	CPRNS	CPMAX	CPMIN
224444444444446666666668888888888888888	43135334546143135334546143135334454614 991127966733001122796673300112796673300	$\begin{array}{c} -376 & 151 \\ -341 & 160 \\ -1126 & 1126 \\ -1126 & 1126 \\ -1126 & 1126 \\ -1126 & 1122 \\ -1267 & 1122 \\ -1267 & 1122 \\ -1267 & 1122 \\ -1222 & 269 \\ -1122 & 299 \\ -1222 & 269 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -1222 & 299 \\ -122$	0324148374432317626371388928612050288886735 03241101430112124371788928612050288886735 1101430112124371788928612050288886735 11110567852111 033001121243711389286120502888865 00132221111056735		80000000000000000000000000000000000000	3135334546143135334546143135334546143 11112227799911112227799911112277999 11112227799911112227799911112277999	- 334 - 117703055 - 117703055 - 11770305 - 117705 - 117	11110000288924699927241543288667769715 11210000288924699927241543288667769715 112100001102203646999227241543288667769715	6790348909724663550609211575045774 224120603859182963874714778355981 12112000220111211575045774		66666666668888888888888888888888888888	111122277999111122277999111122277999 127966733001127966733001127966733001 127966733001127966733001127966733001		11811152366385868408260237763038383006 11811152355868408260237763038383006 11111111111111111111111111111111111	18655969046013227880382366986 12528904601322780382366986 115075075075075075075075075075075075075075	

WD	TAP	CPNEAN CPRMS	CPNAX	CPNIN	WD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN	ND.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	123456789012345678901234567890123456789012234567890 000000011111111111111111111111111111	$\begin{array}{c} - & 2896 \\ - & 1350 \\ 0351 \\ 11368 \\ 1128 \\ - & 01234 \\ - & 01234 \\ - & 227765 \\ 11228 \\ 11228 \\ - & 227765 \\ 11364 \\ 12765 \\ 11364 \\ 12765 \\ 11364 \\ 12765 \\ 11364 \\ 12765 \\ 11364 \\ 12765 \\ 11364 \\ 12765 \\ 11364 \\ 12765 \\ 11364 \\ 12765 \\ 11364 \\ 1275 \\ 11351 \\ 12252 \\ 11252 \\ 12351 \\ 12252 \\ 11252 \\ 12351 \\ 12252 \\ 12351 \\ 12252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 \\ 1252 $	42255512524091944632637660759866655621284452055122447 654276885944363263766075988665562128446220684112212247 11111111111111111111111111111		000000000000000000000000000000000000000	123456789012345678901234567890123456789012341211111222222	7.65283500156093042612458041042841385935356511320305 	81031212181069809420238988691216372193433738170567 64213167774420113485654100364564312244564520095112222	$\begin{array}{c} 32100074509222278163413000727173298633811947988098323827324389731809513511947188182097518414899513511947468980920\\ 111111111111111111111111111111111111$		000000000000000000000000000000000000000	7890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678		111785033955400315229227299412430983837049652975824 11171101101101101111111111110000000000	614463094026600395598949303216085852912347775028814 1122682149167278495032160858529123477750288145 1111111110000112118726898529123477750288145 1111111111111111111111111111111111	

WD.	TAP	CPHEAN CPRHS	CPNAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD.	TAP	CPHEAN	CPRHS	CPNAX	CPNIN
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ND TAP C	CPMEAN CPRHS	CPHAX CPHI	N ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	₩Ð	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       1       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412516837974556078138884110244792694689921556515291220 C PR 41251683797455607813884110244792694689921556515291220 C PR 41251683797455607813884110244792694689921556515291220 C PR 41251683797455607813884110244792694689921556515291220 C PR 412516837974556078138841100100000000000000000000000000000	$\begin{array}{c} 1 \\ 228\\ 889\\ 611\\ 5379\\ 898\\ 3229\\ 111729649\\ 8322544011347649402504696029387436945\\ 229480071953257422003696029387436945\\ 2276594987436949\\ 22248007149594987436949\\ 22248007149594987436949\\ 22248007149594987436949\\ 22248007149594987436949\\ 22248007149594987436949\\ 22248007149594987436949\\ 22248007149594987436949\\ 2224800071495949\\ 2224800071495949\\ 2224800071495949\\ 2224800071495949\\ 2224800071495949\\ 2224800071495949\\ 2224800071495949\\ 22248000714959\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007149\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 222480007122\\ 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N D	TAP	CPHEAN CPRHS	CPNAX	CPNIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
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2012 - 2012 - 2014 - 2012 - 2	63960826127304695669311161890004227537 11116651890004227537 11111111111111111111111111111111111	$\begin{array}{c} 125\\ 125\\ 6926\\ 9368\\ 4259\\ 8860\\ 1259\\ 8860\\ 1259\\ 8860\\ 1259\\ 1259\\ 734\\ 4509\\ 7374\\ 43509\\ 7374\\ 43509\\ 7374\\ 43509\\ 7374\\ 1295\\ 8387\\ 2138\\ 1220\\ 740\\ 1295\\ 2217\\ 1205\\ 1205\\ 740\\ 1205\\ 740\\ 1205\\ 740\\ 1205\\ 740\\ 1205\\ 740\\ 1205\\ 740\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 720\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ 1205\\ $	$\begin{array}{c} - 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& 6588\\ - & 65787\\ - & 113757618\\ - & 77918\\ - & 77918\\ - & 5543527\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - & 1335750\\ - 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30	117	011 .134	. 521	- 415	30	167	. 365	. 173	1.054	051	30	223	526	. 264	043 166 143 170 158 247 236 222 206 080	-1.740

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W D	TAP	CPHEAN I	CPRMS	CPHAX	CPHIN	90	TAP	CPMEAN	CPRNS	CPHAX	CPHIN	<b>M</b> Đ	TSP	CPMEAN	CPRMS	CPNAX	CPHIN
40	233	802	. 271	047	-1.550	40	283	- 285	. 132	. 142	- 830	40	412	.251	. 121	. 723	122 412
40	234	819	. 253	018	-1.889	40	284	136	. 113	. 278	651 504	40 40	414	- 006	095	295	326
40	235	185	.102	.246	547	40	285 286	118	.099	. 223	428	40	415	- 051	106	279	461
40	236 237	- 183	.105	.175	512	40 40	287	- 169	106	229	- 507	40	416	1114	099	407	- 249
40	238	- 196	115	300	- 551	40	268	- 222	108	142	- 602	40	417	.135	. 102	. 522	212
40	239	- 208	130	.175	- 788	40	289	218	110	. 152	- 669	40	418	.123	. 096	. 478	244
40	240	213	. 134	. 157	874	40	290	251	. 131	. 199	8 5 9	40	501	099	. 090	. 241	398 533
40	241	264	. 149	297	861	40	291	269	. 142	. 203	791 782	40 40	502 533	- 174	. 109	. 149	- 734
49	242	- 376	. 188	.265	-1.315	40 40	292 293	- 295 - 305	133	.073	- 767	40	564	- 168	1119	188	- 624
40	243 244	648 855	.282	.135 081	-1.826	40	294	- 430	153	002	- 996	40	5.5	068	120	. 596	- 309
40 40	245	866	296	- 030	-2.213	40	295	- 114	. 099	211	- 430	40	56	227	. 139	. 834	166
40	246	189	108	.267	- 580	40	296	- 100	. 106	. 247	454	40	5.7	.171	. 125	. 666	210
40	247	- 196	112	.301	- 643	40	297	128	. 104	174	4 48	40	5-8	164	. 160	. 354	989
40	248	195	. 124	. 244	694	40	298	171	. 099	. 153	525	40	59	- 315 - 282	. 132	.161	-1.020 712
40	249	209	. 137	.243	- 760	40	299	214	. 108	. 194	607 754	40 40	5.0 51	- 297	126	204	- 750
40	250	223	.148	. 232	-1.008	40	300 301	- 235	. 127	.121	- 738	40	5 2	- 273	121	110	- 757
40	251 252	282 391	.157	.226	-1.105	40	302	- 276	130	132	- 729	40	5 3	- 227	113	172	- 599
40 40	252	640	273	037	-1.988	40	303	- 283	122	078	- 744	40	54	143	. 098	. 226	500
40	254	- 175	107	189	- 535	40	304	- 294	131	. 1 0 1	- 753	40	5 5	135	. 109	. 188	547
40	255	157	095	148	596	40	305	133	100	. 191	457	40	5 6	- 173	. 107	. 162	527
40	256	170	. 1 04	.145	521	40	306	175	. 109	. 147	592	40	517	149	. 102	. 195	496
40	257	197	. 115	.214	592	40	307	206	. 114	. 211	602	40	6:1	.109	. 100	.515	222
40	258	210	. 122	. 166	664	40	308	223	. 126	.246	816 661	40	6.2	.250	131	.796	- 202
40	259	207	. 130	.162	709	40	309	238 263	. 124	077	722	40	64	192	.119	645	- 151
40	260	260 364	.153	.292	942	40 40	$310 \\ 311$	- 272	129	126	- 901	40	6 5	461	141	910	091
40 40	261 262	579	270	079	-1.849	4č	312	- 309	135	079	- 779	40	6:6	- 001	. 099	. 332	339
40	263	- 794	350	- 005	-1.979	40	314	- 117	091	159	- 419	40	6 ^ 7	038	. 145	. 619	508
40	264	- 852	385	001	-2.493	40	315	141	. 101	. 204	457	40	6 8	081	. 111	. 411	536
40	265	- 153	106	271	497	40	316	172	. 111	. 159	5 3 3	40	619	153	. 114	. 253	598 428
40	266	137	. 096	.185	- 426	40	317	206	. 103	.079	581 593	40 40	7 1 7 1 2	.094	. 153	. 726 . 857	- 477
40	267	143	. 101	.170	594 551	40 40	318 319	204 213	.111	211	- 590	40	7 3	007	217	. 925	- 705
40	268 269	- 174	106	.110	- 551	40	320	- 225	120	254	- 608	40	2.4	- 074	160	. 514	- 545
40	270	- 215	126	196	- 602	40	321	- 253	. 124	107	- 692	40	7.5	127	. 115	258	531
4ŏ	27 I	- 264	143	254	- 894	40	<u>322</u>	- 276	. 115	049	677	40	7.6	.014	. 113	. 573	326
40	272	- 289	167	. 191	-1.090	40	401	275	. 123	. 129	749	40	7.7	.022	.150	. 630	482
40	273	410	. 223	208	-1.399	40	402	249	. 113	. 151	827	40	78	- 137	. 133	. 305	655 641
40	274	- 508	. 265	.127	-1.727	40	403	244	121	098	-1.135	40	7975	106	.114	268	475
40	275	638	.354	.071	-2.405	40	404	202 265	. 101	.156	- 792	40	76	- 092	113	. 284	- 521
40	276 277	134 194	100	.205	- 468 - 648	40 40	406	- 239	122	294	- 714	40	7.7	- 094	108	251	- 465
40	278	- 220	121	239	- 635	40	407	- 251	104	091	- 605	40	7 8	- 125	. 114	. 230	516
	279	- 230	117	244	- 797	40	408	- 202	108	. 135	- 597	40	7:9	215	. 123	. 169	864
	280	- 242		167	- 858	40	409	205	. 689	. 520	052	40	7 0	104			
40	281	257	136	. 244	777	40	410	. 263				40	7:1				
40	282	274	. 134	. 1 4 9	752	40	411	. 273	. 115	. 682	117	40	(_2	484	. 199	. 297	
	280 281	- 242	. 127	.167	- 858	40	409	205				40		- 104 - 058 - 084	102 108 109	. 265 . 313 . 247	477 409 421

W D	TAP	CPMEAN CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	MÐ	T SP	CPHEAN	CPRMS	CP MA X	CPNIN
8 4444444444444444444444444444444444444	r 777777777788899999999999999999999911111111	$\begin{array}{c} -343 & 227 \\ -343 & 227 \\ -351 & 172 \\ -351 & 203 \\ -147 & 117 \\ -128 & 117 \\ -128 & 117 \\ -1295 & 181 \\ -0982 & 111 \\ -1199 & 121 \\ -1129 & 121 \\ -387 & 221 \\ -387 & 221 \\ -387 & 221 \\ -387 & 221 \\ -387 & 221 \\ -388 & 207 \\ -2728 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 \\ -390 & 168 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	67895 77777777777777777777778889999999999	32563544752709724606136659002283324565217182397041223397	111120109000000000000000000000000000000	404916212970421021749430699840508152636211814818 580937739558198279993924939261812141423470355144 13223122231322322221103132234221413217642144		77000000000000000000000000000000000000	11111111111111111111111111111111111111	- 13221 - 133948 - 133948 - 133948 - 133948 - 133948 - 133948 - 1155070464380 - 1155070464 - 11540708 - 11540708 - 11540708 - 11540708 - 115408 - 1	25290824329715142996478127607033019885574395191795 20027522111211100206322211121110098754330198885574395191795	$\begin{array}{c} 2109553221\\ 129753211\\ 2217287221\\ 12975390553221\\ 12975390555900748975582288\\ 221728741955022884886691\\ 22172875758222884886691\\ 10055628164886691\\ 10055628164886691\\ 100556018861493361\\ 2150188613666691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686691\\ 10085686690\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 1008666900\\ 100866000\\ 100866000\\ 1008660000\\ 1008600000\\ 100860000000\\ 10086000000000\\ 100860000000000000000000000000000000000$		~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	901234567890123456789012345678901234123412345678901234	256610076286382548034549248211230622349586745669698 431645486748748785474803454924821123098295222262441463332 1111333203321111113332211230623495222262441463332 11113332203321111113332211123062349586745669698	2611187041073196340754700300923492302783727320301975 1111111111111111111111109990002301975	049 155 355 539	<pre></pre>

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ND TA	P CPMEAN	CPRMS	CPNAX	CPMIN	ND.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD.	T A P	CPHEAN	CPRMS	CP MA X	CPMIN
TA         1111111222222222222222222222222222222	56789012345678901234567890123456789012345678901234567890121111274860901 12332212913333427340221211178388008217111332001112748696 1111123421121117838800821171133286090011274696 111112746961	CPRMS 112048921128921128269000 112048921128921128289000 110201128921289000 110201128921289000 110201128921289000 11020112892000 1102011289000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 110201128000 1102011280000 1102011280000 1102011280000 1102011280000 1102011280000 1102011280000 1102011280000000000	$\begin{array}{c} 152339345556388477682455563884776824662397\\ - 002660437824662397\\ - 002660437824662397\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 002874662987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 00287466987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 0028766987\\ - 00286987\\ - 00286987\\ - 00286987\\ - 00286987\\ - 002869888\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 0028698\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 0028698\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286988\\ - 00286888\\ - 0028688\\ - 0028688\\ - 00286888\\ - 0028688\\ $	C	¥D 777777777777777777777777777777777777	P         56789012345678901234567890123456789012345678909999999900000000000011111           P         5666666777777777788888888888899999999999	C	S 9377157087732334531437884950183231837385534679552 P 01090023561732201121233090901111325400001315110111124319 P 010900020000000000000000000000000000000	244 2681 1251 038 2057 658	C	¥ 777777777777777777777777777777777777	r 3333333444444444444444444445575555555555	A 4 4 5 0 4 6 8 7 2 2 5 4 1 2 6 5 5 1 1 4 2 5 0 5 3 3 3 6 3 0 7 4 3 6 3 8 2 9 5 9 1 0 6 2 4 2 5 1 2 1 1 2 2 1 9 1 2 0 0 0 1 1 3 3 8 0 3 2 0 2 6 0 3 3 8 2 9 5 9 1 0 6 2 4 2 5 1 2 1 1 2 2 1 9 1 2 0 0 0 1 1 3 3 8 0 3 2 0 2 6 0 3 3 8 2 9 5 9 1 0 6 2 4 2 5 1 2 1 1 1 2 2 1 9 1 2 0 0 0 1 1 3 3 3 3 6 3 0 7 4 3 6 3 8 2 9 5 9 1 0 6 2 4 2 5 1 2 1 1 1 1 2 4 9 6 5 5 1 2 1 1 1 1 0 1 1 3 2 0 0 0 1 1 2 2 0 0 0 1 2 2 2 2 2 1 1 1 1	S 61974231061114027500976141685209500465443683418982 P 1111011111111111111111111111111111111	C 1155203231363066687485580879654130324047419910240 11658204139875885580879654130324047419910240 1222001230066558485580879654130324047419910240 1222001230066558 11001220012230066558 110012200122308558 11001220012230 12222256886858 11001220012230 12222256886858 11001220012230 122222256886858 11001220012230 122222256886858 11001220012230 122222256886858 11001220012230 122222256886858 11001220012230 122222256886858 11001220012240 12222222256886858 11001220012230 122222222222222222222222	C

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W D	TAP	CPNEAN CPRMS	CPNAX	CPHIN	ND	TAP	CPHEAN	CPRHS	CPMAX	CPNIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN
98888888888888888888888888888888888888	9011714567890117456789011754567890112345678901175456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789	$\begin{array}{c} - 040 & 1457 \\ 0757 & 1570 \\ 1953 & 12051 \\ 1953 & 1254 \\ 11213 \\ - 1624 & 1213 \\ 1254 \\ - 23774 & 11254 \\ - 233774 & 11254 \\ - 1224 & 12558 \\ - 12588 & 1657 \\ - 10558 & 1467 \\ - 10558 & 1467 \\ - 10558 & 1467 \\ - 11559 & 11658 \\ - 11559 & 11658 \\ - 11559 & 11658 \\ - 11559 & 11658 \\ - 11559 & 11658 \\ - 11559 & 11658 \\ - 11559 & 11658 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 11559 & 1168 \\ - 115557 & 1239 \\ - 115557 & 1239 \\ - 115557 & 1239 \\ - 115557 & 1238 \\ - 11557 & 1368 \\ - 1151 & 1268 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1159 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1150 & 1368 \\ - 1100 & 100$	78081293378437642645808269321689280096460047247897 261221001212118724813022395689280096460047247897 1111 - 1111 - 111 - 11	1		9012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123	- 436146597768779789544298671954211820024774989111824700 	04830660059921153486070201243228559896569122250808431 11111111111111111111111111111111111	413500768074100226599267028632583377458250691883734 01125100127100127799111011223722210245463842121786633337	<pre>60931846505137190331484891604393006158977077905271</pre>		90124567890121234567890123456781234567890123456712 0112121112222000000000111111111200000000		397861015550822931903367230220581258601108653372645 1134780001100645100521118111000311190000001111110000900911	0637077199773360144218558652077302112800171008436490 24444231112467412242113675338455222302775454475423 2455222302775454475423	<pre></pre>

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VD TAP	CPNEAN CPRNS	CPMAX	CPHIN	WD .	TAP	CPNEAN	CPRMS	сриах	CPHIN	WD	TAP	CPHEAN	CPRMS	CPMAX	CPNIN
WD       TAP         6034       6045         880       6066         880       6067         7703       77067         7716       77167         880       880         77057       7717         880       880         880       880         77033       77167         880       77057         7717       77333         880       880         880       880         880       880         880       880         77057       7167         880       7007         7717       77333         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880         880       880	$\begin{array}{c} \mbox{CPRMS} \\ 159 & 120 \\ 123 & 114 \\ 506 & 139 \\ 062 & 098 \\ -035 & 125 \\ 074 & 112 \\ -056 & 102 \\ -074 & 112 \\ -056 & 102 \\ -074 & 112 \\ -056 & 102 \\ -075 & 101 \\ 069 & 121 \\ 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372756851092288028666059979085003000255725225066381	CPR 13365224653326894603000997819823292567141226061869 1131100224653326894603000997819823292567141260011000011000009978119823292567141100001100001100000997811982329256714110000110000000000000000000000000000	$\begin{array}{c} - & 0.31 \\ - & 0.35 \\ 171 \\ - & 254 \\ - & 196 \\ - & 2120 \\ - & 371 \\ - & 0.931 \\ - & 2355 \\ - & 2264 \\ - & 2062 \\ - & 2062 \\ - & 2325 \\ - & 2062 \\ - & 2062 \\ - & 2325 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 \\ - & 2062 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W D	TAP	CPMEAN CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN C	PRNS	CFMAX	CPMIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPNIN
<ul> <li>         GOUDOOOOOOOOOOOOOOOOOOOOOOOOOOOO</li></ul>	- 345678901111111111120000000000000000000000000	$\begin{array}{c} -284 & 137\\ -359 & 1620\\ -2433 & 1084\\ -1972 & 1360\\ -2433 & 1084\\ -1972 & 1360\\ -2433 & 1666\\ -1169 & 1131\\ -2853 & 1166\\ -1875 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1200\\ -33269 & 1126\\ -2853 & 1266\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 100\\ -1266 & 1$			- 999999999999999999999999999999999999	. 345678901 <b>03</b> 4567890103456789010345678901034567890103 55555555666666666667777777788888888889999999999		1001112225791145164874820009305121958186623013582195 111222576645164874820009305121958186623013582195	660782289801940187064525059065916017616245428055521 842246458806886356049230687718307312055976154315344559 1111 111 111	<pre></pre>	- <b>99999999999999999</b> 9999999999999999999	34567890124567890121234567890123456781234567890123 00000000111111111222000000000111111111000000	49908479284794470677527705410649896178544834319782	40942465278198680007510140935874264313903326365594 10911111245819910156941111210711000031110900110000900 1011111124581991000111111111111111111111111111111001111	82588947915517427704947320643609635671941658572127 9077683884235482292316525699536391168854431509223872	

WD	TAP	CPNEAN CPRNS	CPHAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPNIN	WD	TAP	CPMEAN	CPRMS	CPNAX	CPMIN
D 000000000000000000000000000000000000	4567123456789123456789556789012890123456123	CP NEAN CPRMS 057 098 079 092 089 105 089 105 089 105 089 105 089 105 089 105 089 105 089 105 089 105 089 109 061 112 077 102 055 100 045 1131 055 110 0068 109 007 105 108 025 111 0068 109 007 105 106 040 1132 008 109 051 097 044 102 026 130 051 097 044 102 026 130 051 097 049 091 051 107 089 122 117 118 080 1103 059 103 059 103 059 103 059 103 059 103 059 103 059 103 059 103 059 103 042 099 047 098	3133516232719990709884070988407098840709884070988407191999090712 335122316232712 1.33244025918344077910064460931777730093225604053311 1.332440259183440779100644609317777300533283 2.325604053311		900 900 900 900 900 900 900 900 900 900	99999999991111111111111111111111111111		173168144508161659624575795309459417631557 9242216445508161659624575795309459417631557	04230011650494300865282774386111339123630826 343157111650494300866659806277438611133912010010191316 			1444444455755555555556666666667777777777	$\begin{array}{c} -1133223715745164048107005347568588974329430\\ -114322423715745164048107005347568582974329430\\ -1143224232423220877333221111773355324420000015315332\\ -1143224232423220877333221111773355324420000000000000000000000000000000$	568318023549781961565077184549213156513489 00033251336650771845492131565513489 1112009998819611110003319320001111100043513489	$\begin{array}{c} 2626\\ 229765395409945\\ 229765395409945\\ 229765395409945\\ 229765395409945\\ 229765395409945\\ 229765395409945\\ 22976539564122453317419806645\\ 22976529564122453317419806645\\ 22976529564122453317419806645\\ 22976529564122453317419806645\\ 22976529564122453317419806645\\ 229765295641224553177412985\\ 229765295641224553177412985\\ 229765295641224553177412985\\ 229765295641224553177412985\\ 229765295641224553177412985\\ 229765295641224553177412985\\ 229765295641224552956412245529564122455295641224552985\\ 22976529641224552956412245529849249249849249985\\ 22976529641224552956412245529849249985\\ 229765296412245529849249249985222222222222222222222$	
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$\begin{array}{cccccccccccccccccccccccccccccccccccc$	111111111111111111111111111111111111111	123412345678901234567890123456789012345678901234567890123		200467762572113377344568513388679991352562574688099022500336	13313048696872593903652603911181365521076211498 2223121111135678212001459280971118136552821276211498 11 11 11 11 11 125948281972000145928009711181365521002880 11 11 11 11 11 11 11 11 11 11 11 11 11	62078542004293595016003442573586196219956827917	1000 1000 1000 1000 1000 1000 1000 100	78901234567890123456789012345678901234567890123	- 33920137673758001764194750011539680026115702625079485 	7939411993950683405727391743438307111447848425501 1111111111111111111111111111111111	9123567116183867224401455871244052272639475418118 805601121002381982211224790911123478321112456778 11			789012345678901245678901212345678901212345678901234567812345	873544534583681202104959798253511482455116933988 57794010696125322276046959798253511482455116933988 1110022221111101322100000000000000012124 1110013221000000000000000000012124	549340532311692924797584835857230190625930665556 11002033301321133490001211447521111118010000210000 11111111100111000000111110001000	719351649834894031898769790740194167952886592824 2191424871233456722222478973200953865344446333322224	C (())) ()) ()) ()) ()) ()) ()) ()) ())

WD	TAP	CPNEAN	CPRMS	CPNAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND	TAP	CPNEAN	CPRMS	CPNAX CPNI	( N
100	508	. 036	. 096	. 363	302	100	903	131	. 111	. 272	597	110	135	- 603	. 30 5	.069 -1.76	52
100	509	- 004	105	. 331	445	100	904	042	. 135	. 440	588	110	136	597	. 284	.052 -1.89	5
100	510	067	. 093	.240	381	100	905	282	175	. 153	959	110	137	- 586	. 285	.130 -1.80	17
100	511	095	1 02	. 246	454	100	306	- 088	. 133	390	680	110	138 139	- 392 - 260	. 223	240 -1.24 265 - 87 135 - 72	
100	512	098	. 112	. 369	- 415	100	907	106	. 154	. 362	930	110 110	140	- 211	132	.13572	
100	513	053	. 098	. 287	- 365	100	908 909	- 238 - 877	221	- 078	-1.674	110	i4i	- 169	122	212 - 55	
100	514	017 073	. 105	.319 .271	373 452	100	910	- 104	129	329	- 794	110	142	- 173	115	199 - 56	
100	515 516	062	. 101	.259	- 396	100	911	- 229	156	251	8 4 4	110	143	- 166	118	. 183 61	2
100	517	- 069	098	.249	- 397	100	912	- 620	. 185	- 053	-1.286	110	144	147	. 115	. 197 54	14
100	601	- 021	102	343	- 423	100	912 913	- 865	. 210	- 261	-1.855	110	145	141	. 106	. 227 49	1
100	602	023	. 1 02	.360	360	100	914	- 182	155	. 318	-1.014	110	146	- 499	. 236	122 -1.40	9
100	603	. 015	. 097	. 3 9 8	287	100	915	684	. 153	215	-1.324	110	147	331 245	173	198 -1 30 258 -1.12	24
100	604	. 038	. 1 0 3	.340	380	100	916	- 277 - 396	. 186 . 176	260	-1.449	110	148 149	- 223	. 142	.28068	
100	605	. 647	.119	1.072	.158	100	917 918	- 396 - 514	. 176	086	-1.276	110	150	- 187	121	.24659	
100	606	.033 145	.103	430	- 312	110	101	- 719	259	- 024	-1.954	110	151	- 172	109	.24659	
100	607 608	- 021	102	328	- 456	110	102	697	225	004	-1.608	iiò	152	- 151	106	. 298 - 61	1
100	609	. 074	102	.427	- 256	110	103	- 559	225	147	-1.524	110	153	- 130	. 096	.29861 .24143	59
ioč	701	010	130	429	- 475	110	104	390	. 208	285	-1.176	110	154	- 648	283	053 -1.80	8
iòò	702	004	104	364	- 322	110	105	297	. 200	. 225	-1.075	110	155	673	. 312	.053 -1.80	59
100	703	002	. 1 1 0	419	379	110	106	227	. 178	. 234	-1.243	110	156	592	. 27 0	. 095 -1.49	6
100	704	. 087	. 105	511	298	110	107	- 185	. 145	. 251	- 833	110	157	380	.214	.206 -1.25	
100	705	. 031	. 1 07	396	288	110	108	181	.145	233	-1.407	110	$158 \\ 159$	261	134	214 - 84	
100	706	. 095	. 1 1 1	. 346	337	110	109	- 170	.118	260	724	110	160	- 185	121	208 - 63	
100	707	. 100	.117	. 582	- 277 - 315	110	111	- 183	119	277	- 589	110	161	- 156	102	187 - 53	fi –
100	708 709	. 025	. 104	.443	- 286	110	112	- 647	263	152	-1.619	110	162	- 137	. 111	. 190 54	10
100	715	- 042	103	.333	- 394	110	112	- 661	263	205 233 152 062	-1.797	110	163	130	. 099	. 241 - 46	
iòò	716	- 056	089	247	- 399	110	114	506	. 215	. 0.94	-1.366	110	164	- 138	. 105	280 - 56	9
ióó	717	- 077	101	247	- 473	110	115	362	. 180	176	-1.128	110	165	821	. 315	107 -2.19 027 -1.76	16
100	718	032	. 103	. 378	380	110	116	271	. 168	257	987	110	166	761	. 284	. 027 -1.76	56
100	719	. 107	. 130	. 591	457	110	117	- 223	153	. 224	977	110	167 168	536 370	. 226	. 293 -1.52 .176 -1.13	
100	720	027	. 1 0 3	. 3 3 9	- 360	110	118	- 182	. 144	185	- 806 - 839	110	169	- 370	171	. 186 - 1.20	31
100	721	043	. 097	278	- 437	110	119	- 178	125	238	- 628	110	170	- 204	140	.18683	27
100	722	002	.113	.341	485	110	121	- 165	. 114	216	- 539	110	171	- 196	117	177 - 61	2
100	728	092 073	.116	293	- 596	110	122	169	105	149	- 491	110	172	- 146	108	. 183 - 56	2
100	729 730	- 070	115	.268	- 472	iiò	i 2 3	154	. 112	221	- 584	110	173	- 130	. 100	.18356	
100	731	- 059	094	. 306	403	110	124	591	272	125 022 139	-1.580	110	174	128	. 113	.25650	
ĪÓÒ	732	- 053	. 099	719	353	110	125	617	. 272	. 022	-1.614	110	175	126	. 109	. 234 48	
100	733	- 039	. 129	. 363	- 617	110	126	- 583	256	. 139	-1.564	110	176	- 364	. 159	147 -1.05	22
100	734	047	. 101	243	452	110	127	- 380	. 196	229	-1.294	110	177	295	. 138	.16588 .14893	
100	735	042	.109	.318	- 657	110	128	- 290	175	201	-1.026	110	179	- 231	145	. 256 74	
100	736	040	.100	. 3 2 5	- 492	110	129	- 223	170	. 181	867	110	180	- 168	112	.24167	6
100	801	027 003	.093	363 248 325 275 275	- 335 - 355	110	131	- 199	130	234	- 671	110	181	- 145	108	. 235 53	88
100	802 803	041	.087	.243	391	110	132	- 176	112	196	- 603	iiò	182	- 127	. 101	.28660	2
100	901	- 014	121	369	- 556	iiò	132	- 178	110	. 183	593	110	183	143	. 109	.23056	
iŏŏ	902	039	100	309	- 458	iiò	134	- 179	112	291	- 649	110	184	368	. 216	244 -1.45	57
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WD	TAP	CPMEAN	CPRMS	CPHAX	CPHIN	WD.	TAP	CPMEAN	CPRHS	CPMAX	CPHIN	WD	TAP	CPNEAN	CPRMS	CPMAX	CPMIN
11111111111111111111111111111111111111	56789012341234567890123456789012345678901234567890 8888899999000000001111111111222222222222	44936255663985348634295638488230810629175213618348	185614733827796846392326833656146847480007985584474 0843219110446420124462332233467701212122556779113344	81159285167320059361151060585995087597515023012025 58919285167320059361111035895998211014767224198560 10015569111123556811111035895982110147691072210015 111111111035891101101469107221012025	3312448148647616068067101574085539388743404732666326	1100 1110 1110 1110 1110 1110 1110 111	12345678901234567890123456789012345678901234567890 4444444455555555555666666666677777778888888888	783537225243228516798471231773842402257645929185275 	68724850073144167126415678562045681854100864407965 111111111111111111111111111111111111	787831206048840735222480555800712293564735190072033502 11102355890111102368999122123799067203519007203502 11102368999122123799067203519007203502 111023689999122123799067203509 111123799067203502		1100 1110 1110 1110 1110 1110 1110 111	12345678901234567890114567890121234567890123456781	171923211110012221110012221112913220186681030000051143232       1719233333000100000011110012233300000051143232       17192333300000000111100112233330000000011110011132232	111198639229878169101391061627003366177094906005835 11111111111111111111111111111111111	18416018538078051424480615913475002674556786385657 689922212356782234776723234569784436334237335883234	

W D	TAP	CPNEAN	CPRMS	CPHAX	CPHIN	90	TAP	CPMEAN	CPRHS	CPMAX	CPNIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
D	T 55555555555555555666666666667777777777	P       147330615114947722390112006607530075688918511536733698229         P       1	CPR 1177771473204488008856246881477405099511099885624688009950109985624688009951100999510092266187776411120000099511093776641142450095	35651686302894376567343845887575228839253302584 64760618181090378426971095622652829953875480643 76064381810903784384588757528829953875480643 760643	C	WD 1000000000000000000000000000000000000	P. 61231234567890123456789991111111111111111111111111111111111	C P N 002556652992091166500310 002255665299209116650052109031120001120000000000000000000000000	C 68137229037306204895197008152700955212515402968927 P 00110546535710897096286757008152700955212515402968927 C 1111112211122112211122211122221533245521121111112168927	9363262562517??166459557146185299296457387445298 383711946194033948666459557146185299296457387445298 	C	D 2000000000000000000000000000000000000	T 111111111111111111111111111111111111	C	CP 113212792855851316427582387137368868861174545751358 PP 1132127928558513164275823871373688688688117454575151558	$\begin{array}{c} 27\\ 34\\ 45\\ 06\\ 55\\ 34\\ 67\\ 12\\ 05\\ 53\\ 46\\ 71\\ 20\\ 78\\ 02\\ 47\\ 80\\ 24\\ 06\\ 96\\ 96\\ 96\\ 95\\ 95\\ 33\\ 75\\ 11\\ 20\\ 79\\ 94\\ 33\\ 44\\ 12\\ 22\\ 13\\ 21\\ 13\\ 23\\ 88\\ 84\\ 11\\ 20\\ 79\\ 94\\ 33\\ 44\\ 9\\ 12\\ 22\\ 13\\ 21\\ 12\\ 23\\ 88\\ 84\\ 11\\ 20\\ 79\\ 95\\ 94\\ 49\\ 12\\ 22\\ 13\\ 21\\ 12\\ 22\\ 13\\ 21\\ 12\\ 23\\ 88\\ 84\\ 11\\ 20\\ 79\\ 95\\ 94\\ 49\\ 12\\ 22\\ 13\\ 21\\ 12\\ 22\\ 13\\ 21\\ 12\\ 23\\ 12\\ 12\\ 22\\ 12\\ 12\\ 22\\ 12\\ 12\\ 22\\ 12\\ 1$	C

PAGE A 10	ь.
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S D	TAP	CPMEAN CP	RHS C	PMAX	CPHIN	. ND	TAP	CPMEAN	CFRMS	CPMAX	CPMIN	MD	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
11111111111111111111111111111111111111	90123456789012341234567890123456789012345678901234 78888888899999000000000111111111202222222333333		171 156 162 112 1009 1234 159	251 388 2441 1531 2551 2551 2551 2551 2551 2551 255		11111111111111111111111111111111111111	56789012345678901234567890123456789012345678901234 3373374444444455555555555555666666666677777777	$\begin{array}{c} 2074\\ -& 3131\\ -& 16575\\ -& 31677\\ -& 316775\\ -& 205324\\ -& 165755\\ -& 21601788\\ -& 2302681\\ -& 2302681\\ -& 2302681\\ -& 122066832\\ -& 1220732031677\\ -& 203732031677\\ -& 1224455616339\\ -& 1220326823\\ -& 1220732031677\\ -& 203720323\\ -& 12206683\\ -& 1220732031677\\ -& 20372032\\ -& 12207320316\\ -& 203720683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12202683\\ -& 12$	945316110461675278511138420163672752563571496622723 945316110461675278511138420163672752563571496622723	028279652517071764329805939257310600927893083115343 112283590905022489999111135779096116169954886658853145743 1		11111111111111111111111111111111111111	22222222222222222223333333333333333333		6142735701995563772688013924809328338065922206926532 112133480900111213220011112349093283380659922006926532 11111111111111111111111111111111100090011 11111111	07092969403303073434779173429036673916559441944681 09536846044098625840641945685844443921470288484870603 0212345677832123556772345667812235678895336444313237	

WD	TAP	CPMEAN CP	RMS CP	MAX	CPMIN	MD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD.	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
11111111111111111111111111111111111111	444445555555555555555555555555555555555	1234         123499         123499         123499         1221212         11811         12221212         1182574         002194         002194         002194         002194         002194         002194         002194         002194         002194         002194         002194         002194         00442         004467         004467         004467         004467         004467         004467         004467         004467         004467         004467         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457         004457	116       .         1147       1         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .         1100       .	602223111114543334334334933456545567443323933343 265577064085522557264371531926129588662107172311206 14671500134978956174365037723743861558140895130061		00000000000000000000000000000000000000	01234561231234567890111111111111111111111111111111111111		63172296119812006638707037689915485228363342579727 1101109911046852666638707037689915485228363342579727 1111122221112111112222111111122227	389 2137 2633 26337 26337 26337 26337 26337 26337 26337 26376 26376 2611 26374 26376 26376 26376 26376 26376 26376 26376 26376 26376 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 26377 263777 263777 263777 263777 263777 2637777 2637777777777		11111111111111111111111111111111111111	11111111111111111111111111111111111111	570003597096326708219105511106074250823137015450206 24776908632195577176029088106209788819912188055875028 2422223222222222232229088106209788819912188055875028 233333333333221	488226874707050149025777266244523815073465498010953 111111111223221111110033421445238815073465498010953 111111111111111111111111111111111111	1155 0750 1168 11115 12977 120617 120617 1118 0907 120617 1118 0907 1118 00017 1118 00017 1118 00017 1118 00017 1118 00017 1108 110977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 1008 100977 100977 100977 100977 100977 100977 100977 100977 100977 100977 100977 100977 100977 100977 100977 1009777 100977 100977 100977 100977 100977 1009777 1009777 1009777 1009777 10097777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 1009777 10097777 1009777 10097777 10097777 10097777777777	

U D	TAP	CPMEAN	CODME	CPHAX	CPHIN	MD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPNIN
11111111111111111111111111111111111111	3456789012345678901234123456789011234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345	1978         1977         11799         12249         12219         12219         12219         12219         12219         12219         12219         12219         12222         12322         12322         12322         12322         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12323         12333         12333         12333         12333         12334         12333 </td <td>05171525185084711564234213526583009706342667389025 111267532112226542111122332221124384421122557664310124 1111111111111111111111111111111111</td> <td>.183</td> <td>45189502587925642268124404250450579707088037517588</td> <td>11111111111111111111111111111111111111</td> <td>901234567890123456789012345678901234567890123456789012345678 28333533333344444444555555555566666666667777777777</td> <td>241334948608185591203930520628139334945757664121555299 </td> <td>42384410295166571894821568159664635460158239015633 468643111124456543234444758601596646655460158239015633</td> <td>1222848296222523398533301405196670812799005775606695065196657465111456898655235 18884899577556008712800065196657465111456898655265 11111111111111111111156898655265</td> <td></td> <td>00000000000000000000000000000000000000</td> <td>90123456789012345678901234567890123456789012121234567 788888888889999999999999000000011111111122200000000</td> <td>56062163582738401631951736992324699469950980243670 12222211100122221000001222200001222220000133324100211 100122221000001222200001222220000133324100211</td> <td>913441521116138660328069823056431223934989227498930619 1134429001111231229109101232500111244490000134343475111220 11111111111111111111111111111111</td> <td>15990004237244027485471180544248137859314153684918 579762222456788323355776772246688891234679881853755 1853759</td> <td></td>	05171525185084711564234213526583009706342667389025 111267532112226542111122332221124384421122557664310124 1111111111111111111111111111111111	.183	45189502587925642268124404250450579707088037517588	11111111111111111111111111111111111111	901234567890123456789012345678901234567890123456789012345678 28333533333344444444555555555566666666667777777777	241334948608185591203930520628139334945757664121555299 	42384410295166571894821568159664635460158239015633 468643111124456543234444758601596646655460158239015633	1222848296222523398533301405196670812799005775606695065196657465111456898655235 18884899577556008712800065196657465111456898655265 11111111111111111111156898655265		00000000000000000000000000000000000000	90123456789012345678901234567890123456789012121234567 788888888889999999999999000000011111111122200000000	56062163582738401631951736992324699469950980243670 12222211100122221000001222200001222220000133324100211 100122221000001222200001222220000133324100211	913441521116138660328069823056431223934989227498930619 1134429001111231229109101232500111244490000134343475111220 11111111111111111111111111111111	15990004237244027485471180544248137859314153684918 579762222456788323355776772246688891234679881853755 1853759	

APPENDIX A -- PRESSURE DATA (

8D

CONFIGURATION C : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT

TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	
408	. 084	. 111	. 568	364	1 30	719	. 259	. 144	. 989	158	140	117	300	. 121	. 124	847	
409	- 041	080	.174	- 367	130	720	. 024	. 099	. 359	- 303	140	118	281	. 124	. 129	666	
	- 046	. 093	265	- 364	130	72i	017	101	374	- 363	140	119	- 273	. 118	. 129	706	
410				441	130	722	- 074	. 158	426	- 636	140	120	- 258	. 119	. 175	752	
411	059	. 1 00	.280			728	014	107	352	- 436	140	121	235	120	242	- 720	
412	063	. 103	.260	432	130						140	122	- 241	115	138	- 629	
413	. 137	. 155	. 6 0 9	348	1 30	729	. 057	. 121	. 486	375		123	- 248	123	150	- 690	
414	. 218	. 1 08	. 5 5 3	147	130	730	032	. 113	. 333	508	140						
415	. 315	.150	. 900	094	130	731	. 012	. 105	. 362	363	140	124	- 271	. 116	. 083	- 662	
416	142	. 124	. 265	595	130	732	. 044	. 099	. 433	285	140	125	- 270	. 113	. 096	667	
417	031	. 099	. 296	- 376	130	733	012	. 114	. 379	494	140	126	- 260	. 109	. 108	692	
418	- 027	105	325	- 399	130	734	. 021	. 095	. 341	284	140	127	- 281	. 112	. 148	726	
501	- 089	124	. 500	- 460	130	735	025	. 108	. 329	510	140	128	- 291	. 112	. 083	674	
502	- 208	111	200	717	130	736	012	107	364	- 372	140	129	- 296	. 116	. 044	703	
302			125	- 875	130	801	024	097	372	- 323	140	130	- 295	. 118	. 122	723	
503	207	. 1 1 1		- 711	130	802	. 076	116	424	- 494	140	iši	- 269	113	125	- 639	
504	231	. 121	.147			ê ô ŝ	. 011	100	341	- 329	140	i 32	- 255	121	146	- 715	
505	261	. 118	.141	729	130			153	173	- 890	140	133	- 235	115	176	- 645	
506	320	. 154	.160	-1.189	1 30	901	304				140		- 253	121	159	- 708	
507	067	. 133	. 464	536	130	902	324	. 157	. 185	987		134			091	- 701	
508	. 114	. 140	. 678	303	130	903	360	. 164		-1.164	140	135	- 256	. 112			
509	. 027	. 121	. 432	384	130	904	259	. 160	. 344	841	140	136	- 250	. 118	. 098	634	
510	. 004	. 116	. 375	467	130	905	433	. 190		-1.113	140	137	- 264	. 106	. 071	- 644	
511	- 004	. 1 1 9	.453	442	130	906	273	. 168	. 353	958	140	138	280	. 113	. 061	910	
Ši2	002	129	458	- 549	130	907	336	. 156	. 165	957	140	139	- 295	. 115	. 114	659	
513	076	112	515	- 271	130	908	- 419	. 156		-1.077	140	140	290	. 108	. 186	656	
514	. 089	103	. 4 4 6	- 257	i 30	909	- 508	213		-1.405	140	141	- 280	. 115	. 097	806	
				- 354	130	910	- 365	229	241	-1.525	140	142	- 260	. 114	. 046	737	
515	. 070	. 1 02	.416		130	911	- 395	191	230	-1.207	140	143	- 233	116	172	- 619	
516	. 071	.104	.416	260			- 436	157	076	-1.066	140	144	- 225	109	136	- 590	
517	. 044	.100	.354	319	130	912	- 436	107		-1 246	110	123	- 229	115	234	- 656	

130	408 .084	. 1 1 1	.568364	130 130	719 2 <b>59</b> 720 024	.144	.989158 .359303	140	117 - 300 118 - 281	. 121	.124847 .129666
130	409 - 041 410 - 046	.080 .093	.174367 .265 - 364	130	721 .017	101	374 - 363	140	119 - 273	118	129 - 706
130	411 - 059	100	280 - 441	130	722 - 074	. 158	.426636	140	120 - 258	. 119	.175752
130	412063	. 103	.260 - 432	130	728 .014	. 107	.352436	140	121 - 235 122 - 241	.120	.242720 .138629
130	413 .137	. 155	.609348	130	729 .057 730032	. 121	.486375 .333508	140	122 - 241 123 - 248	. 123	150690
130	414 .218 415 .315	.108	.553147 .900094	130 130	731 .012	.105	.362363	140	124 - 271	. 116	.083 - 662
130	415 .315 416142	124	.265595	130	732 .044	099	433 - 285	140	125 - 270	. 113	. 096 667
130	417 - 031	099	296 - 376	130	733 - 012	. 114	.379494	140	126 - 260	. 109	.108692
130	418 - 027	. 1 0 5	.325399	130	734 .021	. 095	.341284	140	127 - 281 128 - 291	.112	.148726 .083674
130	501089	.124	.500 - 460	130	735025 736 .012	. 108	.329510 .364372	140	128 - 291 129 - 296	.116	.044703
130	502208 503207	. 111	.200717 .125875	130 130	801 .024	097	372 - 323	140	130 - 295	118	122 - 723
130	504 - 231	121	.147711	i 30	802 .076	116	.424494	140	131 - 269	. 113	.125639
130	505 - 261	118	.141729	130	803 .011	. 100	.341329	140	132 - 255	. 121	.146715
130	506 320	. 154	.160 -1.189	130	901 - 304	.153	.173 - 890 .185 - 987	140 140	133 - 235 134 - 253	. 115	.176645 .159708
130	507067	. 1 3 3	.464 - 536 .678 - 303	130 130	902 - 324 903 - 360	.157	277 -1.164	140	135 - 256	112	091 - 701
130	508 .114 509 .027	.140	.678 - 303 .432 - 384	130	904 - 259	160	344 - 841	140	136 - 250	118	.098634
130	510 .004	116	375 - 467	130	905433	190	227 -1.113	140	137 - 264	. 106	.071644
130	511004	. 119	.453442	130	906 - 273	. 168	353 - 958	140	138 - 280	. 113	.061910 .114659
130	512 .002	. 129	.458 - 549	130	907 - 336	. 156	.165957 .030 -1.077	140	139 - 295 140 - 290	.115	.114659 .186656
130	513 .076	112	.515271 .446257	130	908 - 419 909 - 508	.156	055 -1.405	140	141 - 280	1115	.097806
130 130	514 .089 515 .070	.103	.416354	130	910 - 365	229	241 -1.525	140	142 - 260	. 114	.046737
išŏ	516 .071	104	416 - 260	130	911 - 395	. 191	230 -1.207	140	143 - 233	. 116	.172619
130	517 .044	. 100	354 - 319	130	912 - 436	. 157	.076 -1.066	140	144 - 225	. 102	136590 .234656
130	601030	. 099	.279369	130	913 - 519	. 187	017 -1.246	140	145 - 229 146 - 268	. 115	.112 -1.052
130	602 - 062 603 - 087	. 1 03	.340 - 464 .236 - 447	130	914 - 399 915 - 478	. 195	034 -1.167	140	147 - 286	114	080 - 706
130	603087 604 .023	.103	359 - 365	130	916 - 414	168	. 141 - 1.232	140	148 - 325	118	. 195 814
130	605 603	138	.990 .096	130	917417	. 150	.012950	140	149 - 308	. 110	.077781
130	606 .035	. 1 0 2	.416 - 347	130	918 - 425	. 163	.135980	140	150 - 283 151 - 236	.117	.145718 .127581
130	607199	. 190	.402938 .318580	140 140	101 - 346 102 - 324	. 124	072 - 863 076 - 833	140 140	151 - 236 152 - 248	112	.069693
130	608 - 086 609 . 100	.122	.318 - 580 .574 - 330	140	103 - 318	129	.119890	140	153 - 236	113	. 195 653
130	701 108	148	.589462	140	104 - 336	. 133	.072990	140	154 - 250	. 125	.120 -1.235
išó	702 .120	. 109	543 - 250	140	105364	. 152	.148 -1.306	140	155 - 254	. 108	.079625 .050 -1.097
130	703 .019	. 114	.466356	140	106345	.145	.101 -1.112 .183965	140	156 - 272 157 - 284	. 118	.050 -1.097 .085930
130	704 .105 705 .075	.126	.692 - 296 .499 - 324	140 140	107 - 322 108 - 291	.131	.190701	140	158 - 313	113	019 - 728
130	706 222	123	680 - 154	140	109 - 285	141	176 - 885	140	159 - 301	. 117	.097 - 689
130	707 .218	129	775 - 202	140	110 - 247	. 125	203 - 624	140	160 - 258	.115	.090635
130	708 .051	. 1 1 1	.437359	140	111238	. 132	.175801	140	161 - 237	.113	.177618 .120601
130	709 .060	. 098	.407299	140	112 - 281 113 - 278	. 115	.196697 .166678	140 140	162 - 218 163 - 213	113	.187578
130	715 .023 716001	108	.393 - 331 .365 - 336	140	113278	.111	.097713	140	164 - 209	116	169 - 608
130	717034	105	.310435	140	115 - 280	115	113 - 734	140	165 - 251	140	133 - 853
130	718 .034	104	450 - 332	140	116 - 310	121	. 455 799	140	166 - 254	. 120	.138670

**PAGE A 109** 

$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	CPNEAN CPRNS CPNA)	CPHEAN CPRNS CPNAX	CPMIN
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C

WD	TAP	CPMEAN	CPRMS	CPNAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	¥D.	TAP	CPMEAN	CPRMS	CPMAX	CPNIN
140	402	. 248	. 154	. 788	341	140	708	. 106	. 101	. 434	306	150	111	251	. 116	. 188	692
140	403	. 093	. 122	. 639	389	140	709	. 104	. 097	. 461	224	150	112	- 250	.107	. 098	609 646
140	404	. 041	. 115	. 563	360	140	715	. 052	. 100	. 413	366	150	113	- 245 - 257	. 105	. 108	- 634
149	405	. 287	. 1 27	.738	171	140	716	. 043	. 106	.404	318 317	150 150	115	- 266	108	103	639
140	406	. 235	. 125	.707	168	140	717 718	.018 .057	. 107 . 101	427	252	150	116	- 289	113	. 134	- 729
140	407	. 181	. 116	.758	269	140 140	719	. 253	137	867	- 136	150	117	- 277	1117	149	- 704
140 140	408 409	.129 062	. 112	.152	- 354	140	720	. 472	100	. 489	311	150	118	265	112	. 156	702
140	410	068	091	283	- 379	140	721	065	095	413	297	150	119	272	. 122	. 112	668
140	411	- 090	liói	282	- 467	140	722	. 028	. 142	. 467	5 5 3	150	120	256	. 118	. 188	763
140	412	- 092	. 100	. 225	- 458	140	728	. 073	. 105	407	302	150	121	254	. 111	.151	- 677
140	413	. 161	. 169	.716	351	140	729	. 111	. 103	. 476	- 245	150	122 123	25¢ 245	.109	102	- 646
140	414	. 244	. 1 16	.735	145	140	730	.052 .061	.111	580	355 326	150	124	- 272	112	212	- 743
140	415	. 337	. 155	1.043	130 590	140	731 732	. 078	100	408	247	150	125	- 248	110	120	- 661
140	416 417	141 039	.118	240	- 390	140	733	- 012	121	365	- 608	150	126	263	. 102	. 071	627
140	418	038	100	337	- 358	140	734	063	. 099	393	286	150	127	267	. 111	. 100	673
140	501	- 009	163	. 6 9 5	434	140	735	027	. 113	. 311	563	150	128	- 278	. 102	. 087	670
i 4 ò	502	- 233	114	. 1 37	- 704	140	736	. 045	. 097	. 368	331	150	129	278	. 108	. 115	629
140	503	233	. 115	.079	- 720	140	801	. 057	. 097	. 368	- 269	150	130 131	266 254	.108	.115	- 588
140	504	243	. 1 1 8	.153	- 636	140	802	. 074	. 111	. 460	- 393 - 323	150 150	132	- 251	112	120	- 636
149	505	263	. 1 0 9	.131	665	140	803 901	. 045 327	104	388 .143	-1.019	150	133	- 244	1111	112	- 712
140	506	314	. 125	.088	861 680	140	902	- 317	.144	. 122	-1.123	150	134	- 252	. 114	115	686
140	507 508	158	.152	.267	- 320	140	903	- 313 - 335	146	160	-1.032	150	135	253	. 112	. 114	647
140	509	034	121	537	- 446	140	904	- 313	162	332	-1.095	150	136	243	. 106	. 197	660
140	510	- 014	122	537	- 451	140	905	- 313 - 371	. 160	. 158	-1.046	150	137	- 268	. 116	. 094	631
140	511	- 003	. 121	. 431	521 733	140	906	328	. 176		-1.193	150	138	276	. 109	.105	645 703
140	512	003	. 135	. 485	733	140	907	338	. 152		-1.046	150 150	139 140	- 290 - 285	.101	107	694
140	513	. 109	. 121	. 597	473	140	908 909	363 394	. 148		-1.034	150	141	- 263	113	159	- 640
140	514	. 116	. 107	.714	372	140 140	910	- 411	219		-1.684	150	142	- 270	113	. 132	- 678
140	515 516	.086 .082	.103	440	- 270	140	911	- 383	173		-1.196	150	143	219	. 109	. 188	647
140 140	517	. 071	101	382	- 258	140	912	- 393	146	200	980	150	144	241	. 106	. 123	624
140	601	- 026	096	277	- 372	140	913	449	. 173		-1.305	150	145	233	. 114	. 194	636
140	602	098	105	. 238	484	140	914	421	. 185		-1.408	150	146	245	.105	.135	639 597
140	603	117	. 1 04	. 246	~ .485	140	915	391	. 162		-1.244	150 150	147	267	110	090	- 672
140	604	. 019	. 1 0 3	.351	377	140	916 917	404 387	.160		-1.156	150	149	- 252	107	103	- 727
140	605	538	. 131	.960	.012 308	140 140	918	362	137	026	848	150	150	- 238	104	143	594
140 140	606 607	.033 - 205	.099 .204	.454	-1.105	150	101	308	131	090	- 844	150	151	- 230	. 108	. 133	674
140	608	118	130	.313	628	150	102	- 289	. 119	212	735	150	152	240	. 111	. 074	674
140	609	. 092	120	.467	- 366	150	103	293	. 116	. 046	806	150	153	222	. 109	. 096	- 585
140	701	. 088	135	. 580	377	150	104	304	. 125	. 085	740	150	154	225	. 107	. 189	- 642 - 618
140	702	. 133	. 109	. 576	262	150	105	300	. 133	122	782	150	155 156	- 247	.114	.117	607
140	703	. 059	. 1 1 1	. 5 3 3	305	150	106	315	. 134	.186	944	150 150	130	- 271	101	. 029	- 639
140	704	. 119	. 1 1 1	.623	260	150 150	107	280 285	.131		-1.000	150	158	- 281	110	071	- 626
140	705	. 097	. 1 0 3	.511 .618	301 181	150	109	- 266	132	173	- 667	150	159	- 255	115	072	- 631
140 140	706 707	. 204 . 203	.118	.867	- 298	150	110	- 251	121	137	- 639	150	160	- 255	110	. 214	641
144						• • •	•										

W D	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
000000000000000000000000000000000000000	12345678901234567890123456789012341234567890123456 6666666666777777777888888888889999990000000001111111111	573122055643397140067049843920998982195709344020799 222122223556433971400670498439222222223559 11554412924722545222222223559 1155440020799344020799 1155441292472254529998989 1159709344020799 1159709344020799 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924400207999 12970924000000000000000000000000000000000	4536438966863871969946223110640019931449022414308444 1111111111111111111111111111111111	89244754450209715762007970125739924618469080166979 25242322760783894486449643249363432817136357446479 2121212121210112111211121121121100324575422104579		11111111111111111111111111111111111111	78901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345666666666666666666666666666666666666	3701 41360 10137782 10137782 100137782 100137782 1002824467352 1002824467352 1002824467355 1002824519 100282451 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 1002826555 100286555 100286555 100286555 100286555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 1002865555 10028655555 10028655555 100286555555555 10028655555555 10028655555555555555555555555555555555555	68556230519420151900785451299933583110333527083773 11151222101246663200785451299933583110333527083773	5894162339648966730055225350776557301896262537964896673005522535077655730189626253796537196 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		90000000000000000000000000000000000000	222222222222222222222222222222222222222		44974254940155096599592075713904429801343697926440	486850777484453870972896858685502379029733915394776 27257897531465777782443568777653278361136689681254 1557922783611366896812579	

W D	TAP	CPMEAN	CPRMS	CPNAX	CPHIN	₩D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
D 000000000000000000000000000000000000	T 33333444444444444444444445555555555555	C	CP 112334700455294372194372194325570994618619123344 CP 112334050425813529437219437219430934525570994618619123344 1112023344 1112023244 111202344	98073562227793223711110176443445333221394 10772877776611122277932237111101764434453333221394 112227793223711111017644344533333221394 139665	C	D 000000000000000000000000000000000000	P 23456789567890128901234561231234567890123456781234	GP ME 41 1454 13722 1456 13722 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 11583 1	C 11111099010056320254564993297690067207245266565	600119446319680251837580039136079126352033607 8922113888133804758894550960325224878741704770 111010101	L	U 000000000000000000000000000000000000	r 56789012345678901234567890123456789012345678901234	H 06292974867308428603379119386897718194635868851415 F 222222222222222222222222222222222222	Cr 1332533348824418504884245282373892634784709725624981	$\begin{array}{c} & & & & \\ & & & & \\ & & & & \\ & & & & $	

160 155 - 246 105 084 - 670 160 211 - 212 111 173 - 693 160 211 235 160 156 - 253 103 097 - 641 160 212 - 240 114 088 - 649 160 212 010 160 157 - 249 102 084 - 589 160 213 - 248 118 156 - 722 160 253 - 140 160 158 - 277 118 128 - 713 160 214 094 146 559 - 317 160 234 - 217	. 128	.784 - 208 .444 - 361
160       128       -       777       118       128       -       717       160       214       004       148       558       -       2272       160       245       -       0102         160       128       -       713       160       214       0047       148       558       -       2272       160       245       -       0102       160       245       -       0102       160       245       -       0102       160       245       160       245       -       0102       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245       160       245	945324407139944818234572636179682123158652886376 11233429944818234572636179682123158652886376	$\begin{array}{c} 2405\\ 5933\\ 2205\\ -& 44318\\ 8798\\ -& 00045\\ 8798\\ -& 00045\\ 8798\\ -& 00045\\ 8798\\ -& 00045\\ 8798\\ -& 00045\\ 8798\\ -& 00045\\ 8798\\ -& 00045\\ 8798\\ -& 00045\\ 88798\\ -& 00045\\ 88798\\ -& 00045\\ 88798\\ -& 00045\\ 88798\\ -& 00045\\ 88798\\ -& 00045\\ 88798\\ -& 00045\\ 88798\\ -& 00045\\ 88798\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 00045\\ -& 0004$

N D	TAP	CPMEAN	CPRMS	CPHAX	CPHIN	WD	TAP	CPHEAN	CPRMS	CPHAX	CPNIN	WD	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
111111111111111111111111111111111111111	12456789012123456789012345678123456789	293473227150181093256871150014259224224234057 	15919363841337537871661861094904023639 11011111211215622871651861094904023639	<b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b> <b>1</b>		16600000000000000000000000000000000000	66666777777777777777777777777777777777	- 4552 + 454489 - 2236909 - 2236909 - 2236909 - 2236909 - 223898709 - 22389709 - 2239709 - 2239700 - 22397000 - 2239700 - 2239700 - 2239700 - 2239700 - 2239700 - 2239700 - 2	1309445612345916529299517292023733025487 111111111111111111111111111111111111	338116527010307402406906324415882296437 30151867225555445678555545454848441112		1600 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 17700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 177700 1777000 1777000 1777000 177700000000	99111111111111111111111111111111111111	17315341449347428250269852996541422777 3356567788666773345667553344436687544443 222222222222222222222222222222222	3867949659637523333882604414699925313701 111211111111111111111111111111111111	00446973780018881751083790786662206 11810193180088881751083790786662206 1197780011111111111111111111111111111111	
160	508	230	. 183	.708	517	160	903	309	. 148	183 222 1823 1003 155 110 142 081 089 134	-1.023	170	135	247	. 110	. 160	616

WD	TAP	CPNEAN	CPRMS	CPNAX	CPHIN	WD	TAP	CPMEAN	CPRHS	CPHAX	CPHIN	ND	TAP	CPHEAN	CPRHS	CPNAX	CPMIN
111111111111111111111111111111111111	r 455555555555666666666666777777777788888888	98589501466981403213785319677053763736647662546935	1284570620024467774439999213427966226752024467583879	11026070654906812698197863358804521645383878969743409 11022119112001165851269812083511137838387969743409	18050035942621064141414032850140851076811007032379	- 7700000000000000000000000000000000000	56789012345678901234567890123456789012345678901234 0000001111111111111112222222223333333444444444	096 096 00634 00634 00634 00634 00634 00634 0072050 0122820 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 0122800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 00000 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 012800 0128000 000000000000000000000000000000000	99059667471103720713500932456123939010570383139689 11222966674711191456443320000455556416123959010570383139689	$\begin{array}{c} 56674413128966683384486927963597606359169356680278911033272719169230916953891693127000974331103332722719169232002589916933237233272332323232$		111111111111111111111111111111111111	56789012345678901234567890123456789012345678901234 5555566666666667777777788888888889999999999	- 0091871399914417251801141594216188962402904853824335 599187139991445893203558807722265173876801786509757427 	61765615621949274297144197508237469384039979917587 113146465615621949274297144197508237469384039979917587 1111111111111111111111111111111111	21960075879763531610395153438448308952249423724368 358144123477998853116772739478448436855526567777676 11	

W D	TAP	CPHEAN	CPRMS	CPHAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
111111111111111111111111111111111111111	56789012456789012123456789012345678123456789012345 56789012456789012123456789012345678123456789012345	2333332222182864502516366839533525247960022986243358	13907716843492166299127116315608765797829124324454 222222102023322311653333260111624211610000001249466880	264721931934085029356016640897628884138346383692229 009369775333478591072521935896701112810011076535474 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		17700000000000000000000000000000000000	6712345678912345678956789012890128901284561234567890 1100000000000000000111111222234561231234567890	0120599 - 22561 - 22562 - 2	80652462385910885463674406349881338583894829180247 02111102145501211101111111110020403202054445744457	1445666455564689656555655554455111010011 14456664471699201865974918722982528418947		11111111111111111111111111111111111111	99999999111111111111111111111111111111		11111111111111111111111111111111111111	098 131 300 209 166 191 251 190	

¥D.	TAP	CPNEAN	CPRMS	CPHAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPHEAN	CPRHS	CPMAX	CPNIN
180	143	242	. 112	. 081	- 603	180	193	265	. 120	. 144	781	180	249	.438	. 161	1.046	. 017
180	144	234	111	.090	- 601	180	194	- 262	.135	. 193	869 804	180	250 251	.296	.147	.766 .567	178 351
180 180	145 146	240	.105	.177	- 559	180	202	074	. 130	372	521	180	252	- 080	. 118	. 402	416
180	147	218	. 111	. 169	386	180	203	. 048	. 127	. 517	- 349 - 433	180 180	253 254	- 142	.109	. 250 . 294	- 581 - 475
180 180	148 149	240 252	.105	.099	607 683	180 180	204	.112	. 123	.559	- 255	180	255	038	125	. 457	378
180	150	- 258	117	.140	643	180	206	. 080	. 126	522	348	180	256	. 190	. 137	. 675	220
180	151	292	. 106	.092	647	180	207	.003	. 114	328	495 565	180 180	257	.412	.144	.977 1.033	128
180 180	152 153	- 256	.107	.147	618 717	180 180	208 209	- 209	. 116	. 187	- 681	180	259	388	. 140	. 879	. 0 1 0
180	154	203	. 1 08	. 2 0 4	597	180	210	239	. 122	122	801	180	260	.223	.140	. 660	190
180	155	222	. 111	.164	572	180 180	211 212	- 253	.123	. 154	648 562	180 180	261 262	- 175	. 125	. 579 . 268	469 539
180 180	156 157	239 232	. 106	.107	596 635	180	213	- 090	124	. 331	498	180	263	221	. 105	. 145	567
180	158	226	. 1 0 2	. 128	608	180	214	. 289	. 164	. 976	290	180	264	231	. 120	. 191	650
180	159	260	. 115	.140	618 706	180 180	215 216	.411	. 167 . 153	1.084	020 086	180 180	265 266	102 .029	. 122	. 286 . 536	557 367
180 180	160 161	288 271	121	.161	624	180	217	. 425 . 372	. 155	. 862	163	180	267	.177	. 134	. 831	251
180	162	253	. 112	.081	624	180	218	. 251	. 136	. 715	151	180	268 269	.383 .437	. 149	.891 1.036	031 .030
180	163	250 210	.105	.046	701 601	180 180	219	.060 062	.130	.575	378 480	180 180	270	. 4 3 7	.150	.891	- 104
180 180	164 165	191	112	172	- 582	180	221	170	. 106	. 181	- 583	180	271	. 238	. 140	. 795	271
180	166	196	. 110	. 128	541	180	222	215	. 113	.215	641	180	272 273	- 110	. 122	. 427 . 263	337 488
180	167 168	192 194	. 102	.128	554 552	180 180	223	- 240	.106	.079	606 635	180 180	274	- 188	. 105	.150	- 606
180 180	169	209	. 1 1 0	196	564	180	225	045	. 125	. 473	335	180	275	188	. 095	. 101	536
180	170	224	. 110	.112	585	180	226	. 201	. 151	.746	234	180	276	.254 .352	132	.740 .834	244 173
180 180	171	256 277	.105	.068 .190	- 634	180 180	227 228	.416 .483	. 160	948	- 108 - 018	180	277 278	.363	129	. 889	- 175
180	173	- 278	115	112	671	180	229	. 375	. 158	. 875	041	180	279	.348	. 124	. 875	032
180	174	236	. 112	. 1 0 2	- 661	180	229	. 228	. 158	. 811	334	180	280 281	.301	.133	.973 .610	108 213
180 180	175 176	236 199	. 111	.126 .235	- 658 - 629	180 180	231 232	. 022 179	.134	.467	428 585	180 180	282	135	109	455	- 222
180	177	214	103	.117	- 552	180	233	226	. 117	. 133	619	180	283	.124	. 118	. 535	310
180	178	203	. 1 0 5	.154	565	180	234	- 229	. 111	139	700 645	180 180	284 285	.069	. 124	.532 .589	327 340
180 180	179 180	218 223	.102	105	609 777	180 180	235	- 220	. 119	. 178	365	180	286	.189	108	. 561	158
180	181	279	. 117	. 068	655	180	237	. 215	. 139	768	252	180	287	.305	. 125	. 785	- 044
180	182	277	. 1 2 1	.079	746	180	238	. 447	.155	1.036	023	180 180	288 289	.348 .339	.130	.781 .801	032 044
180 180	183 184	267 225	126	.137	719 748	180 180	239 240	.509	. 155	.940	- 001	180	290	251	1118	. 615	091
180	185	- 187	. 1 0 2	. 143	544	180	241	. 245	. 157	. 792	288	180	291	.171	. 106	504	226
180	186	208	.107	.120	561	180	242 243	- 172	. 133	. 472	387 562	180 180	292 293	.188	. 110	. 376	156 415
180 180	187 188	213	.105	.146	572 542	180 180	243	215	106	091	- 535	180	294	110	. 113	576 508 328	525
180	189	218	. 699	. 1 98	587	180	245	228	109	. 141	612	180	295	219	. 138	. 736	245
180	190	216	.101	.182	575	180 180	246 247	. 338 . 458	.148	1.134	034 041	180 180	296 297	235	. 124	.631 .699	132 151
180 180	191 192	271 230	.112	.089	630 715	180	248	. 438	.155	1.204	.022	180	298	314	125	.740	- 027
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180 315 280 127 832 - 173 180 608 - 359 151 062 - 918 190 102 - 226 142 227 - 714 180 316 344 144 987 - 017 180 609 - 006 153 457 - 591 190 103 - 240 137 172 - 661 180 317 417 149 1 010 - 091 180 701 054 106 422 - 303 190 104 - 263 136 187 - 840 180 718 411 133 932 - 003 180 702 107 184 458 - 218 190 105 - 272 133 265 - 7840	4
180 316 344 144 987 - 017 180 609 - 006 153 457 - 591 190 103 - 240 137 172 - 661 180 317 417 149 1 010 - 091 180 701 054 106 422 - 303 190 104 - 263 136 187 - 840 180 718 411 133 932 - 003 180 702 107 184 458 - 218 190 105 - 272 133 265 - 7840	1
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180 319 352 137 940 - 051 180 703 129 108 584 - 223 190 106 - 274 143 278 -1.179 180 320 271 123 730 - 162 180 704 186 105 584 - 148 190 107 - 291 138 079 - 923	ź
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186 322 222 119 568 - 175 186 766 119 099 462 - 198 190 109 - 256 121 174 - 719	<u>9</u>
100 401 160 156 700 - 269 180 707 115 098 449 - 178 190 110 - 280 125 127 - 819	9
180 402 268 155 827 - 231 180 708 171 104 550 - 180 190 111 - 278 126 208 - 891	1
- 180	1
180 404 009 138 511 - 522 180 715 197 107 583 - 253 190 113 - 216 122 162 - 631	1
180 405 265 132 733 - 190 180 716 164 096 462 - 145 190 114 - 219 119 167 - 682 180 406 346 131 819 - 042 180 717 221 117 621 - 172 190 115 - 232 115 208 - 617	4
180 406 346 131 819 - 042 180 717 221 117 621 - 172 190 115 - 232 115 208 - 617 180 407 276 128 720 - 153 180 718 317 137 914 - 087 190 116 - 233 118 196 - 643	
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180 408 220 119 610 - 123 180 719 196 119 671 - 225 190 117 - 264 123 150 - 645 180 409 - 174 068 087 - 376 180 720 182 102 512 - 160 190 118 - 261 115 118 - 726	ē
180 410 - 180 108 217 - 535 180 721 249 107 587 - 126 190 119 - 257 115 146 - 719	9
180 410 - 180 108 217 - 535 180 721 249 107 587 - 126 190 119 - 257 115 146 - 719 180 411 - 215 105 113 - 535 180 722 194 099 541 - 129 190 120 - 235 122 145 - 652	2
- 180 - 412 - 221 - 118 - 094 - 671 - 180 - 728 - 159 - 110 - 601 - 196 - 190 - 121 - 245 - 114 - 131 - 624	4
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180 417 - 214 121 257 - 651 180 733 - 038 133 319 - 570 190 126 - 224 123 146 - 682 180 418 - 203 110 184 - 602 180 734 154 112 537 - 327 190 127 - 226 118 173 - 606	
180 418 - 203 110 184 - 602 180 734 154 112 537 - 327 190 127 - 226 118 173 - 606 180 561 329 173 987 - 300 180 735 - 072 118 336 - 544 190 128 - 267 116 141 - 737	
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180 503 - 249 113 103 - 657 180 801 183 097 509 - 162 190 130 - 274 129 139 - 767 180 504 - 215 097 141 - 530 180 802 096 104 405 - 321 190 131 - 245 121 066 - 771	i
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180 506 - 218 104 135 - 573 180 901 - 310 141 115 - 989 190 133 - 231 107 158 - 579	9
180 507 - 236 113 154 - 728 180 902 - 302 138 167 - 873 190 134 - 224 116 198 - 635	
180 508 .027 .221 .661665 180 903308 .157 .168 -1.128 190 135223 .115 .239596	
180 509 - 179 210 552 - 848 180 904 - 310 144 081 - 958 190 136 - 215 .108 .151 - 647	1

4D	TAP	CPMEAN CPRM	S CPMAX	CPHIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD	TAP	CPHEAN	CPRMS	CPHAX	CPMIN
D 000000000000000000000000000000000000	T 111111111111111111111111111111111111	CPRM 111 231 111 2331 111 2331 111 2331 111 2335 111 2335 111 2335 111 2335 111 122 2365 111 122 2365 111 122 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2352 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 2357 235	11545719493740558599223579304898586754757356474631 12545719493740558599223579304898586754757356474631 12545719493740558599223579304898586754757356474631 11545719493740588598585847860754757356474631	C	W 9000000000000000000000000000000000000	P 78901234123456789012345678901234567890123456789012	C	S 3940604555889599052244175887774110621916747738830524 P 11002234455588959905224411758877741106219111111111111111111111111111111111	X 729714258404491401858525857881022078331215677029312 N 11061355594104499406585258578810220783312152949269912 N 11212266666530221241916755810220783312155942699912 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	U	# \$??\$?\$???????????????????????????????	<pre>+ 222222222222222222222222222222222222</pre>	H 47574106596529438758587963610300117813955149456912 C 222444310210134420124011344210113332200012225476212 C 22244431021013442012220134421011333220001222352111 C 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	75300313949186240826961264842562933505244841640589 11116774545430234564310102344443101034353521112333344201	726317761712378574463627999934474081529253962548007 1117913388311377597520925399985321188277655557677868555 111111111111111111111111111111111	

WD	TAP	CPNEAN	CPRMS	CPNAX	CPHIN	ND	TAP	CPMEAN	CPRNS	CPMAX	CPHIN	ND	TAP	CPHEAN	CPRNS	CPMAX	CPMIN
190	293	010	. 126	. 381	473	190	504	222	. 131	. 333	670	190	802	.080	. 105	. 400	387
190	294	- 134	. 126	.250	612	190	505	229	. 097	. 077	569	190	803	.203	.110	.613	184
190	295	. 299	135	.735	135	190	506	217	. 103	. 129	- 548 - 550	190 190	901 902	- 332	146		-1.098
190	296	. 274 . 315	.141	.798	- 106	190	507 508	234 056	. 108	. 132	907	190	903	- 289	151	223	- 944
190	297 298	.315	. 134	.842 .747	108 014	190	509	- 237	228	545	-1.003	190	904	357	. 179	. 086	-1.175
190 190	299	. 344	135	765	- 114	190	510	- 266	. 204	. 597	- 994	190	905	272	. 155	. 287	973
190	300	274	132	747	093	190	511	301	. 152	295	929	190	906	345	. 168		-1.584
190	301	. 215	. 129	. 6 3 9	191	190	512	- 358	. 155	. 270	965	190	907 908	- 319	.141	. 064	899 938
190	302	. 159	. 127	.702	255	190	513 514	280 237	. 181 . 222	. 381	907 947	190 190	909	- 285	170	. 143	-1.362
190	303 304	. 152	. 126	. 601 . 581	225 246	190 190	515	- 061	142	. 473	- 732	190	910	356	. 164	. 121	-1.428
190 190	305	. 133 . 327	141	927	- 063	190	516	- 008	. 113	. 425	- 405	190	911	322	. 143	. 152	- 986
190	306	355	. 134	.825	062	190	517	- 094	. 119	256	603	190	912	- 347	. 181	263	-1.509 -1.393
190	307	. 361	. 137	. 843	067	190	601	206	. 123	. 155	- 628 - 663	190 190	913 914	344	. 205	.084	-1.373
190	308	. 309	. 147	. 7 92	122	190 190	602 603	- 240	122	.211	678	190	915	- 336	170	273	-1.224
190	309 310	. 233	.134	.758	- 199 - 256	190	604	110	121	210	- 577	190	916	- 292	. 143	. 139	943
190	311	172	115	593	- 226	190	605	. 435	. 121	1.008	068	190	917	309	. 133	126	751
190	312	174	. 121	593	201	190	606	110	. 115	. 261	501	190	918	320	. 144	. 149	970 817
190	314	. 278	. 149	.764	199	190	607	263	.265		-1.678	200 200	101	228	. 138	190	765
190	315	. 355	. 147	1.067	089 061	190	608 609	- 391	. 164	.534	719	200	103	- 230	138	207	759
190 190	316 317	. 382	129	1.055	- 068	190	701	. 067	. 113	426	- 324	200	104	250	. 132	. 162	- 690
190	318	.354	140	831	- 113	190	702	. 076	. 107	. 411	282	200	105	258	. 140		-1.269
190	319	. 278	. 131	.799	149	190	703	. 130	. 112	. 550	390	200	106	285	. 154	. 222 . 320	-1.224
190	320	. 215	.131	.631	150	190	704	. 182	. 110	.569 .708	268 263	200 200	107	281 290	.143	169	911
190	321	. 191	. 113	. 629	- 164	190 190	705	.175	.136	. 419	- 291	200	109	- 303	148	200	-1.101
190 190	322 401	. 195	.109	.557	- 364	190	707	689	107	471	- 237	200	110	331	. 142	. 137	956
190	402	262	158	ÓÈÈ	- 276	190	708	. 192	. 104	. 661	- 155	200	111	334	. 142		-1.144
190	403	. 117	.170	.805	520	190	709	. 179	. 112	579	188	200	112	237	. 133	. 192	696 696
190	404	. 016	. 158	604	537	190	715	. 204	. 113	. 616	241	200 200	113	- 242	. 125	167	747
190	405	. 257	. 1 3 9	.777	- 172	190	716	. 211	. 110	.586 .718	143	200	115	- 263	129	128	701
190 190	406 407	257 377 312 241	154	.960 .834	076	190	718	326	130	. 859	087	200	116	- 280	. 136	. 195	785
190	408	241	130	722	- 174	190	719	. 171	. 110	528	- 217	200	117	292	. 133	. 127	942
190	409	196	. 087	.063	457	190	720	. 189	. 107	557	189	200	118 119	- 274	129	.146	736 805
190	410	207	.114	305	558	190	721	294	113	. 693	063 184	200 200	120	- 286	128	. 099	- 954
190	411	231	.118	.203	593 771	190 190	722 728	155	108	528	- 284	200	121	- 270	128	. 151	-1.035
190 190	412 413	235	156	.895	- 337	190	729	183	. 121	. 573	214	200	122	272	. 130		-1.044
iśŏ	414	275	126	.787	- 148	190	730	. 093	. 105	437	248	200	123	- 263	. 122	. 207	-1.021
190	415	. 278	. 180	1.103	287	190	731	. 198	.118	710	212	200	124	225 205	. 121	125	553
190	416	360	154	.184	- 917	190	732 733	- 041	. 104	478	- 192	200	125	- 210	114	141	- 669
190	417	222 215	. 129 . 120	.319 .221	728 663	190	734	100	124	484	- 416	200	127	232	. 121	. 142	610
190	418 501	215	. 195	1.235	- 747	190	735	- 102	. 132	. 350	675	200	128	267	. 123	. 190	905
190	502	- 130	. 115	. 267	569	190	736	044	. 129	. 388	618	200	129	288	. 120	. 085	808 710
190	503	- 249	121	119	- 798	190	801	. 184	. 111	. 559	175	200	130	286	. 133	. 174	(14

WD	TAP	CPMEAN CPR	MS CPHAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	MD	TAP	CPHEAN C	PRMS	CPMAX	CPMIN
NNANANANANANANANANANANANANANANANANANAN	1234567890123456789012345678901234566666667777777777890	$\begin{array}{c} 1 & 2907 & 11 \\ - & 2580 & 11 \\ - & 2238 & 11 \\ - & 2230 & 11 \\ - & 22231 & 11 \\ - & 22231 & 11 \\ - & 22231 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22580 & 11 \\ - & 22680 & 11 \\ - & 22680 & 11 \\ - & 22680 & 11 \\ - 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ND	TAP	CPHEAN	CPRMS	CPMAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	ND	TAP	CPMEAN	CPRMS	CPMAX	CPHIN
200	287	. 342	. 131	.837	091	200	416	315	. 143	. 227	911	200	732	.118	.113	. 504 . 336	324 605
200	288	. 272	. 125	. 664	080	200	417	189	. 119	. 211	703	200	733 734	- 037	. 154	. 555	649
200	289	. 164	. 128	. 523	217	200	418	173	.110	. 162	536	200 200	735	- 125	. 125	.240	594
200	290	. 079	. 113	.477	270	200	501 502	. 111 120	. 244	. 874	-1.043	200	736	- 113	144	319	- 734
200	291	. 069	.104	.426	286 432	200 200	503	259	. 125	130	672	200	801	165	125	577	- 270
200	292	. 073	.114	.463 .384	- 419	200	504	- 224	108	. 098	- 609	200	802	.098	113	550	- 306
200	293 294	026 136	.114	251	- 571	200	505	222	109	150	- 620	200	803	. 208	. 102	. 539	128
200	295	. 312	129	.811	- 126	200	506	- 209	101	192	518	200	901	340	. 154	. 283	890
200	296	. 322	121	. 8 0 8	- 026	Žėč	507	217	. 111	. 246	663	200	902	305	. 152	. 150	865
200	297	. 327	. 121	.734	091	200	508	153	. 243		-1.031	200	903	277	.150	. 248	952 -1.303
200	298	. 326	. 124	.731	126	200	509	296	. 218	. 661	-1.016	200	904 905	412	. 186	. 295	~.888
200	299	. 286	. 1 2 2	.776	122	200	510	- 332	. 177	. 403	944	200 200	905	- 442	. 194	021	-1.430
200	300	. 189	. 1 07	. 626	164	200	511	- 323 - 360	.160		-1.422	200	907	- 389	163		-1.077
200	301	. 123	. 108	.462	246 230	200 200	512 513	359	. 163	.356	-1.008	200	908	- 309	153	255	- 924
200	302	. 108	.102	.406	- 372	200	514	- 335	. 244		-1.415	200	909	- 257	158	. 193	879
200	303 304	.094 .089	106	.503	- 248	200	515	- 219	161	248	- 744	200	910	457	. 216	. 102	-1.797
200	305	. 309	125	688	- 175	200	516	013	. 117	. 463	418	200	911	- 393	. 175		-1.093
200	306	. 320	. 1 2 3	.722	- 070	200	517	167	. 126	. 230	689	200	912	371	. 191		-1.162
200	307	272	124	. 6 8 9	- 203	200	601	170	. 115	. 159	618	200	913	353	. 222		-1.840
200	308	. 219	. 1 08	.706	243	200	602	213	. 121	. 196	6 4 7	200	914	393	. 164	. 192 . 288	-1.149 -1.395
200	309	. 121	. 123	. 6 4 2	291	200	603	203	. 124	. 204	6 95	200	915 916	365	. 207		-1.024
200	310	. 095	. 1 1 0	.438	263	200	604	103	. 117	. 280 . 877	544 013	200	917	- 370	162		-1.016
200	311	. 122	. 1 08	. 5 4 3	263	200	605	.409	108	. 209	548	200	918	- 348	170		-1.325
200	312	. 145	. 1 0 5	. 525	214	200	606 607	- 161	. 216	.441	-1.258	210	íòĭ	- 254	140	176	764
200	314	. 322	.116	778	- 062	200	608	- 365	159		-1.067	210	102	- 250	148	246	751
200	315 316	.367 .356	125	.775	- 027	200	609	- 017	168	489	- 612	210	103	232	. 138	. 209	~.706
200	317	. 312	125	755	- 116	200	701	067	113	. 454	356	210	104	251	. 156	. 32 9	-1.396
200	318	239	130	701	- 131	200	702	. 055	. 116	. 4 3 0	375	210	105	291	. 182	. 286	-1.518
200	3i9	. 150	119	.576	243	200	703	. 484	. 117	. 442	337	210	106	310	. 208		-1.844
200	320	. 133	. 096	.550	225	200	704	. 173	. 119	. 551	288	210	107	- 357 - 385	. 232		-1.411
200	321	. 130	. 1 0 8	. 579	291	200	705	. 127	. 121	. 695	389 229	210	108	- 500	222	136	-1.716
200	322	. 137	. 107	.501	215	200	706	.090 .079	.108	. 504	273	210	110	- 552	217	. 072	-1.513
200	401	. 046	- 142	.785	397 169	200	707 708	158	116	508	- 266	210	iii	- 604	259	072	-2.019
200	402	.256	.152	.809 .666	- 519	200	709	. 157	123	. 568	- 255	210	112	- 238	121	. 137	715
200	403 404	042	157	. 6 9 3	- 434	200	215	205	112	622	- 259	210	113	233	. 120	. 128	~.692
200	405	207	. 132	693	- 193	200	716	225	105	662	123	210	114	237	. 130	. 146	664
200	406	363	143	892	~ 193	200	717	. 225	. 141	. 865	188	210	115	237	. 139	. 192	726
200	407	302	134	.768	096	200	718	. 292	. 134	. 897	111	210	116	271	. 154	. 279	940 952
200	408	. 238	. 137	.867	246	200	719	. 125	. 109	. 575	296	210	117	- 289	. 169	.199	-1.079
200	409	171	. 085	.081	441	200	720	. 188	. 114	. 533	165	210 210	118	292	. 182	. 179	-1.133
200	410	180	. 1 07	163	587	200	721	. 283	. 116	.704	140	210	120	- 379	. 198		-1.295
200	411	182	. 113	.190	634	200	722 728	.174	.114	. 507	196 209	210	121	- 401	211		-1.613
200	412	~.198	. 119	.184	612 403	200	729	.156	. 113	.582	224	210	122	- 447	232		-1.499
200	413	. 240	.157	.727 .638	- 153	200	730	074	. 113	. 4 45	324	210	123	- 439	. 229	. 042	-1.432
200	414 415	214	.180	927	- 601	200	731	. 133	128	. 570	- 307	210	124	- 226	. 120	. 192	~.763
200	713			. 7 6 (		- • •											

W D	TAP	CPHERN C	PRMS	CPHAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	<b>H</b> D	TAP	CPNEAN	CPRMS	CP NA X	CPNIN
22222222222222222222222222222222222222	56789012345678901234567890123456789012345678901234 222223333333334444444444455555556666666666		$\begin{array}{c} 1 & 1 & 1 & 2 & 2 & 2 & 1 & 1 & 1 & 2 & 2$	12751275195309145294224505004431995108336019 727302751275135309145294224505000431995108336019 87512730275195309145294505000431995108336019	19036746377539437422146752235199172478209239205450		56789012345678901234123456789012345678901234567890 7777788888888889999999000000001111111112222222222	-       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +       +	54351461373092611092154803902861351545128371211315 2101112470321011136002275548039028613515451283712113328371211315 21111111111111111111111111111111	16823042993181 688504299311 1222181222460083225288 1122221222122288 122322212228 122322228 12232228 12232228 1223222944		22222222222222222222222222222222222222	123456?890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123	2846464600352607570096394875355569528583570034332920 3340711656456887024441777759436010053832201989995971 11111111111111111111111111111111	301583126881126987865254538227317240473107630085755 11137664881126987865254538227317240473107630085755 11111111143223	$\begin{array}{c} 0 \\ 9 \\ 9 \\ 9 \\ 9 \\ 9 \\ 1 \\ 1 \\ 9 \\ 0 \\ 1 \\ 1 \\ 9 \\ 0 \\ 1 \\ 1 \\ 9 \\ 0 \\ 1 \\ 1 \\ 1 \\ 9 \\ 0 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	

APPENDIX A -- PRESSURE DATA )

ND

CONFIGURATION C : SAN DIEGO INTERCONTINENTAL HOTEL -- EAST TOWER OUT

TAP	CPHEAN	CPRMS	CPNAX	CPMIN	ND.	TAP	CPMEAN	CPRMS	CPHAX	CPHIN	MD	TAP	CPHEAN	CPRMS	CPNAX	CPNIN
P 123456789012345678901234567890124567890121212345678 1 222222222222222222222222222222222222	CP HE AN 	CPRMS 742487703874985889665563549853309274796777402586	X 0768300199005484011694660350562110688376854420382 PP 33478977443442888764344976554555987764445348666888 PP 334789774434428888764344976554555987764445348666888	N 39?0764578744679420356681210512653489395760146798		P 0123456781234567890123456712345678912345678912345678956789 1 444444444445555555555555555555666666666	C P ME AN - 1450 - 1582 223494 - 1582 223494 - 1231366 - 203194 - 1231366 - 23144 - 231366 - 23144 - 23156 - 2314 - 23156 - 23144 - 23156 - 23144 - 23156 - 23166 - 23166 - 23167 - 236 - 2334 - 2355 - 236 - 236 - 2356 - 2356 - 2356 - 2356 - 2356 - 2356 - 2366 - 2356 - 2366 - 2356 - 2366 - 200 - 200	CPRMS 410495857750364285772946899781176229446897811179521140998577703642857729446897811119928448978111199298457294	21286902745222962726 869959316922962726 12869316953362726	C	<b>HD</b> 21000000000000000000000000000000000000	P 1289012345812312345678901234567812345678901234567 A 222223333333333330000000001111111111111	CPM 9475426693519271866053864970721193422229278350128210 100526693519274322745276589933222210577300911182110 1110232239552663649707211268993322210577300911182110 1111111111111111111111111111111	CPRMS 711147636541428662159858865194586538849883598622112245886251945865388498835986027115938	6772754368664426529644736874735456529745436866447353559745965297077776443355974596523530331949927777764448148661522011205118846015220112051	N9766831527373889930506478116958312299278275765399968

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₩Đ	TAP	CPNEAN CPRNS	CPNAX	CPNIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	WD.	TAP	CPHEAN	CPRHS	CPMAX	CPHIN
NUNNANANANANANANANANANANANANANANANANANA	· 90123456789012345678901234567890123456789012345678 · 112222222222333333333334444444445555555555	$\begin{array}{c} -334 & 173 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -753 & 294 \\ -754 & 294 \\ -754 & 294 \\ -754 & 294 \\ -754 & 294 \\ -754 & 312 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 \\ -754 & 316 $	91191191919191919191919191919191919191		- 2000000000000000000000000000000000000	90123456789012345678901234123456789012345678901234	9143399381056109424207691430870862650878083388760001 2263399381056109424207691430870862261233331834201239628760001 22633333183388760001 226333331810561094242076914308708622651 226233331810561094242076914308708622651	27074409451362495144435049104391748226892783400019 1115959880111124612111001239548643012466528892783400019	23499682805955800332883100727523473333227 	797515732276204198385167738821117512262737533819339	- 000000000000000000000000000000000000	567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789	420888962254111319321894889856080959722208201959566	945585730777311698575936937957075998743333466881912836 111212220886423111218434232288643431110086342312886	9743344 9743344 974344 97754 190444 190444 197754 11554 94622 94622 94622 10006674 0006674 0006674 10006674 000674 00099998 198558	1013588757620035878663418414046122904633514418002793958688959

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W D	TAP	CPHEAN	CPRHS	CPMAX	CPMIN	¥D.	TAP	CPMEAN	CPRHS	CPMAX	CPHIN	¥D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	56789012345678901234567890123456789012124 777778888888888889999999999990000000111111111	-       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -	56897909438847079643613063475248127379749769585472 04211231934354130931113422120631133322000124222210901164 1111110111111011111111111111111111	31205887404947165231420248129598479032200116663725 197753233308975432432988654334677643345877565333497		00000000000000000000000000000000000000	45478901234547812345678901234567123456789123456789 0000001111111110000000000111111111000000	10435699966005591257863238662755129158888960806593465584471 1200043022211112057863223222223333667378020112672040204200000000000000000000000000000	31964196381213881352684850761488685047619357050469 111118890052637057831200644550761488685047619357050469 111111111111111111111111111111111111	304 143 146 193 166 5311 398 2789 2832 2832		00000000000000000000000000000000000000	77777777777777777888999999999999999999	11369400526662297466002015993940762103586598687111355	192435555556706735642019022743566147700763739313541 1123200111110093023432016240520762799992613222211158244991 111111111111111111111111111111111	3401 - 12231 - 23394 - 312293357 - 12293357 - 122935 - 12295 - 1205 -	

W D	TRP	CPMEAN CPRMS	CPHAX	CPMIN	WD.	TAP	CPMEAN	CPRMS	CPMAX	CPNIN	WD.	TAP	CPHEAN	CPRMS	CPMAX	CPMIN
00000000000000000000000000000000000000	345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567	$\begin{array}{c} 193 \\ 109 \\ 111 \\ 190 \\ 111 \\ 196 \\ 111 \\ 196 \\ 111 \\ 196 \\ 111 \\ 196 \\ 111 \\ 196 \\ 111 \\ 196 \\ 111 \\ 127 \\ 100 \\ 110 \\ 100 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 110 \\ 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<b>5</b> <b>5</b> <b>5</b> <b>5</b>		22222222222233330000000000000000000000	11111111111111111111111111111111111111		47757603132571095451627567108318189865017664241245 3411000113422160101125210000123736752101375320754241245	7.4883851784001782478321101524137999795078784 	$\begin{array}{c} 122 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 $	00000000000000000000000000000000000000	901234567 <b>890</b> 123 <b>45678901234567890123456789012345678</b> 90123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345678901234567890123456789012345666666666666666666666666666666666666	1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1     1 <td>53380236651003822583833823464592929489387531717262 2111222257733220301384433382346459292929489387531717262</td> <td>- 00197777996364449181806088537708488804675703488817422442442442442442442442442442442442442</td> <td></td>	53380236651003822583833823464592929489387531717262 2111222257733220301384433382346459292929489387531717262	- 00197777996364449181806088537708488804675703488817422442442442442442442442442442442442442	

N D	TAP	CPMEAN C	PRMS	CPHAX	CPHIN	MD.	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	W.D	TAP	CPMEAN	CPRMS	CPNAX	CPMIN
00000000000000000000000000000000000000	9012345678901234567890123456789012345678901123456789012345678901211111111111111111111111111111111111		27100144615648288978377457647920463594233412294046	2750973340636006319284970356016537568605987770636485857264606859810666133249703560165375686059877520124181		00000000000000000000000000000000000000	010103456789010345678103456785010345678501234567850103456789123 2220000000000111111111000000000001111111		160857281935403756251700395022159096825464720660623 11111733142377000524220990444437773313000020643200 11111111111111111111111111111111111	14721 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115222 115225 115225 115225 11525 11525 11525 11525 11525 11525 11525 11525 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 11555 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1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1         1       1 <tr< td=""><td>797647761631214537781924251309538815225935803¢689¢ 02090011113410000502534301119182272342657544982¢689¢</td><td>32350711 36235071 3683797 3124797 3124797 31240073249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 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31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 31123249 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 3112400 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N D	TRP	CPHEAN CPRMS	CPMAX	CPMIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	90	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
44444444444444444444444444444444444444	1009011234567890 1111211111111111111111111111111111111	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	02539 11155 22195 22195 2200 216055 2200 216055 2005 552	-1.1060 -1.226 -1.2266 -1.25546 	44444444444444444444444444444444444444	78901234567890 111111111111111111111111111111111111	- 166 - 269 - 2498 - 2298 - 444 - 2296 - 168 - 1895 - 1895 - 1895 - 1956	111133966 229968 111229968 1110777 11277	. 639		44444 <b>4460</b> 0000 44444 <b>44600000000000000000000000000</b>	34567 <b>8</b> 90123456 222222222222222222222222222222222222	410294439994 - 13119994 - 13337781866664 4486664 400	15321 15321 12016 12068 12088 1114 12088 1114 119837	991474309 - 10059 - 10059 100595 100595 100595 100595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 110595 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 11055 110555 110555 110555 110555 110555 110555 110555 1105555 1100	

W D	TAP	CPNEAN	CPRMS	CPNAX	CPMIN	WD	TAP	CPMEAN	CPRHS	CPMAX	CPHIN	WD	TAP	CPHEAN	CPRMS	CPMAX	CPHIN
¥ •	r 3454343545903454343545903454343435459034 r 34543435459034543435459034543435459034 r 345434354543545903454343545903454343454543435459034	Image: Construction of the state of the	r 73218369741133287232731467822021097322266103969171	$\begin{array}{c} 3 \\ 3 \\ 5 \\ 7 \\ 7 \\ 2 \\ 2 \\ 2 \\ 2 \\ 1 \\ 1 \\ 5 \\ 5 \\ 5 \\ 7 \\ 3 \\ 3 \\ 5 \\ 2 \\ 2 \\ 2 \\ 2 \\ 1 \\ 1 \\ 5 \\ 5 \\ 5 \\ 1 \\ 1 \\ 1 \\ 2 \\ 6 \\ 2 \\ 9 \\ 4 \\ 8 \\ 1 \\ 1 \\ 1 \\ 5 \\ 5 \\ 2 \\ 1 \\ 1 \\ 1 \\ 2 \\ 6 \\ 2 \\ 1 \\ 1 \\ 1 \\ 2 \\ 6 \\ 1 \\ 1 \\ 1 \\ 2 \\ 6 \\ 1 \\ 1 \\ 1 \\ 2 \\ 6 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1$	<pre>t 88989798645262595361261466467077301290945402017016</pre>	B 888888888888888888888888888888888888	- 11111122791111111227911111111227911111112279111111122791114 - 5434354590345436677671144456677671144456677671144455		252707176140138205765989700370257002025815872368866 111211010344013820576598970037025740020258158723686866	4654485005220095331101122511293338841093988052224			- 11112279111111112279111111111227911111111		11012270638996393594649354111 11022122222354111 11022112322222354111 11002212222354111 11002212222354111 11002212222354111 11002212222354111 11002212222354111 11002212222354111 11002212222354111 11002212222354111 111022212222354111 111022212222354111 111022212222354111 111022212222354111 111022212222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 111022222354111 1110222222354111 1110222222354111 1110222222354111 111022222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 1110222222354111 11102222222354111 11102222222354111 11102222222354111 11102222222354111 11102222222354111 11102222222354111 11102222222222222222222222222222222	$\begin{array}{c} 06760\\ 06760\\ 117493\\ 112640\\ 00174632\\ 0095343\\ 1023712\\ 1023712\\ 1126432\\ 0095343\\ 11223712\\ 1126330\\ 1122355\\ 0354797\\ 1179923\\ 1126330\\ 1122355\\ 0354797\\ 1179923\\ 1126330\\ 1122355\\ 0354797\\ 1179923\\ 1126330\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112235\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112255\\ 112$	

42 173227 42 17516 42 26479 42 27579	.106 .150	6525	50 50	264	844									
$\begin{array}{c} 19 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ -1 \\ 910 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ $	315       25         1240       144         147       166         1408       191         1408       191         1408       191         1408       191         1408       191         1408       191         14090       141         14090       141         14090       142         14090       144         1000       144         1000       144         1000       144         1000       144         1000       144         1000       144         1000       144         1100       144         1100       144         1100       144         0090       110         0090       110         0000       100         1100       100         1100       100         1100       100         1100       100         1100       100         1100       100         1100       100         1100       100         1100       100	1446915285851648192533607123213100678192	00222222222222222222222222222222222222	27911111111227911111111227911111111227911111111		86700357173942035791513210925027523356186461	21484173488999951265966655624348244533556 0918666753555646807775914682556443414463 1 1 1 1 1 1 1 1 1 1 1 4 4 2 3 1 1 1 1 2 4 4 6 3 1 1 1 1 2 4 4 6 3 1 1 1 1 2 4 4 6 3 1 1 1 1 1 1 4 4 6 3 1 1 1 1 1 1 4 4 6 3 1 1 1 1 1 1 1 4 4 6 3 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	211371265737672331095336946850029721089345282	55%66%6666668999999999999999999999999999	79111111111227911111111227911111111227791111111222791111111 903454343545903454566776711444566776711444566	61777866937935414434103407530015805401064143	1200021111184125607013273203518014401980931 1200021111184120001090097113000609009710990021 1111233101111300013109002351	$\begin{array}{c} 17774787654294402228400010488462689800552006\\ - 32012024623384000104884626898005520424200000000000000000000000000000$	932800565454560599995946643414153689989195335578

WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	MD	TAP	CPMEAN	CPRMS	CPMAX	CPNIN	WD	TAP	CPNEAN	CPRHS	CPMAX	CPMIN
999999999999999999999999999999999999999	34543545903454343545903454343545903454590345435459034	- 13882 - 1142293058403415800494333612511742371266788231903417 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1	213019237068880985568277531446636417131430779822542 000909001209906856827753144663664171314307798822542	35905907296109197228810638916322164569161913951182 11132121095022232339952818860920182586861913925227411 11321210950222332399528188609201825868619332227411 113221210950222332399528188009163221220950211645691000000000000000000000000000000000000		44444444446666666666688888888888888888	5434354590345434354590345434354590345434343545903454 456677671144445667767114445667767114445667767114445	- 17933016588603565405430203094488194602502988875498723 - 112208086035654054302030944888194602502988875498723 - 111111111111111111111111111111111111		91231130565335660730387411981142613 42337679001176093343211297358300988 222298522221112197622220222289820988	1       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -	00000000000000000000000000000000000000	11112279111111112279111111111227911111111	72148290052991182735403371629804454152160576122566 22322213222243222102222222222233211222222233210233323988211300 2232222432222233221022222222223321122222222233221023332239	625853102797188117243796417027505033019173457309999 11144221021110324510083221505033019173457309999		$1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\$

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W D	TAP	CPMEAN	CPRMS	CPHAX	CPMIN	RD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPHIN
88888800000011111111111111111111111111	1122791111111112279111111111227911111111	04931953080174752510172033489870229077939148836456 3321023332442202333244244421024555245552202558258 3321023332454220233324424421024555245552202555258 55255255255555555555555555	215628031792023233632716792148328885449644687576395 79211288891362821098889144272108456281422108835719231 11111111111222212323	2793245857809913129202124712895553334936507066558 111451111222111142100111111186600383870925620218545	-1	66568888888888888888888888888888888888	22791111111112279111111111227911111111227911111111		10534075567811286066720401096959426949374546570481 12087121266662720401096959426949374546570481 1122331332656211286066720401096959426949374546570481	00115595555554813663344889284342167132591559668 00122255512790331444889284342167132591559668 001101559		++6666656666666888888888888888888888888	79111111112279111111112279111111111227911111111		523938126893012702045855685046086667740846336137498 11222212322211106089190401110409804364009481014434311104 123221232221110608919040110409804364009481014434311104	98453833610995499070778622786894600072993479956 	-1111-1-212

W D	TAP	CPMEAN	CPRMS	CPMAX	CPMIN	80	TAP	CPMEAN	CPRMS	CPMAX	CPNIN	WD	TAP	CPMEAN	CPRMS	CPMAX	CPMIN
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